



Europäisches Patentamt
European Patent Office
Office européen des brevets

(19)

(11) Publication number:

0 082 702
A1

(12)

EUROPEAN PATENT APPLICATION

(21) Application number: 82306781.4

(51) Int. Cl.³: **C 07 C 15/04**
C 07 C 15/06, C 07 C 15/08
C 07 C 1/20

(22) Date of filing: 20.12.82

(30) Priority: 23.12.81 US 333845

(43) Date of publication of application:
29.06.83 Bulletin 83/26

(84) Designated Contracting States:
BE DE FR GB IT NL

(71) Applicant: MOBIL OIL CORPORATION
150 East 42nd Street
New York New York 10017(US)

(72) Inventor: Chu, Yung-Feng
121 Randle Drive
Cherry Hill New Jersey 08034(US)

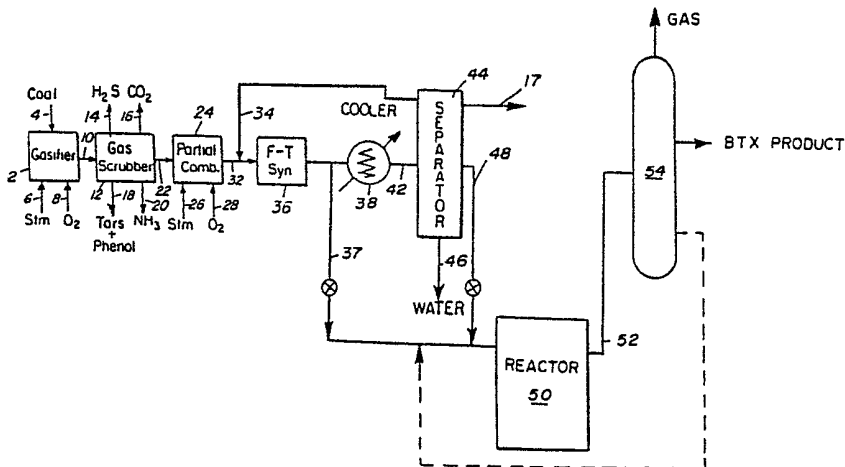
(72) Inventor: Chester, Arthur Warren
517 Country Club Drive
Cherry Hill New Jersey 08003(US)

(74) Representative: West, Alan Harry èt al,
Mobil Court 3 Clements Inn
London WC2A 2EB(GB)

(54) Conversion of Fischer-Tropsch synthesis products to benzene, xylene and toluene.

(57) In a process for producing a mixture of hydrocarbons rich in benzene, toluene and xylene, a fossil fuel is converted to a Fischer-Tropsch synthesis gas containing oxygenated hydrocarbons and the resultant synthesis gas is then converted by Fischer-Tropsch reaction to a product containing oxygenates and hydrocarbons. The Fischer-Tropsch product

is then contacted with a catalyst comprising a metal-promoted porous crystalline zeolite having a constraint index within the range of 1 to 12 and a silica to alumina ratio of at least 12 to produce an effluent stream rich in benzene, toluene and xylene. The benzene, toluene and xylene are subsequently removed from said effluent stream.



EP 0 082 702 A1

CONVERSION OF FISCHER-TROPSCH SYNTHESIS
PRODUCTS TO BENZENE, XYLENE AND TOLUENE

This invention relates to a process for converting oxygenated products derived from Fischer-Tropsch synthesis products to benzene, toluene, and xylene for petrochemical feedstocks.

Processes for the conversion of coal and other hydrocarbons such as natural gas to a gaseous mixture consisting essentially of hydrogen and carbon monoxide, or of hydrogen and carbon dioxide, or of hydrogen and carbon monoxide and carbon dioxide, are well known. Although various processes may be employed for the gasification, those of major importance depend either on the partial combustion of the fuel with an oxygen-containing gas or on a combination of these two reactions. A summary of the art of gas manufacture, including synthesis gas, from solid and liquid fuels, is given in Encyclopedia of Chemical Technology, Edited by Kirk-Othmer, Second Edition, Volume 10, pages 353-433, (1966), Interscience Publishers, New York, N.Y., the contents of which are herein incorporated by reference. Volume 4, pp. 446-488, Interscience Publishers, New York, N.Y.

It is desirable to convert synthesis gas, obtained from coal, natural gas or any other available source to highly valued hydrocarbons such as gasoline with relatively high octane number, petrochemical feedstocks, liquefiable petroleum fuel gas, and aromatic hydrocarbons. It is well known that synthesis gas will undergo conversion to form reduction products of carbon monoxide, such as oxygenates and hydrocarbons, at temperatures in the range of from 300°F to 850°F (149°C to 454°C) under pressures of from about one to one thousand atmospheres pressure, over a fairly wide selection of catalyst compositions. The Fischer-Tropsch process, for example, which has been most extensively studied, produces a range of products including oxygenates, heavy waxy oils, and liquid hydrocarbons which have been used as low octane gasoline. The types of catalyst that have been studied for this process include those based on metals or oxides of iron, cobalt, nickel, ruthenium, thorium, rhodium and osmium.

The present invention resides in a process for producing a mixture of hydrocarbons rich in benzene, toluene and xylene which comprises:

- (a) converting a fossil fuel to a Fischer-Tropsch synthesis gas containing oxygenated hydrocarbons;
- (b) converting the synthesis gas by Fischer-Tropsch reaction to a product containing oxygenates and hydrocarbons;
- (c) contacting said Fischer-Tropsch product with a catalyst comprising a metal-promoted porous crystalline zeolite having a constraint index within the range of 1 to 12 and a silica to alumina ratio of at least 12 to produce an effluent stream rich in benzene, toluene and xylene; and
- (d) removing benzene, toluene and xylene from said effluent stream.

Preferably, the metal used in the catalyst of (c) is selected from the group consisting of Group VIII transition metals, and metals from Group IIB and IIIB. Group VIII metals include iron, cobalt, nickel, ruthenium, rhodium, palladium, osmium, iridium and platinum. The Group IIB metals include zinc, cadmium and mercury. The Group IIIB metals include aluminum, gallium, indium and thallium

The preferred metals for the catalyst of (c) are gallium, platinum and zinc, with the most preferred metal being gallium.

As noted above, the present invention is a process for producing aromatic hydrocarbons particularly benzene, toluene and xylene and mixtures thereof by contacting a Fischer-Tropsch product stream containing oxygenates and hydrocarbon products with a ZSM-5 type zeolite catalyst impregnated with one or more metals selected from the group consisting of Group IIB, IIIB and VIII metals.

The metal promoter in the catalyst composition of step (c) may be present as the metal oxide and/or as metal ions if cations in the ZSM-5 type zeolite have been exchanged with the metal ions therein. In the case where the cations in the zeolite have been exchanged for metal ions, the metal ions are suitably provided as an aqueous solution of metal salts, such as, for instance, the soluble nitrate, chloride or



sulfate salts of platinum, zinc or gallium. Such catalysts may be produced by conventional ion exchange techniques and the catalysts so produced subsequently dried. For example, an aqueous solution of the metal compound such as tetramine platinum chloride, zinc chloride, or gallium nitrate may be placed in contact with zeolite at ambient or elevated temperature, e.g. by refluxing. The exchanged zeolite is then separated by decantation followed by filtration, washed several times with deionized water and finally dried. Before addition to the aqueous solution of the metal compound, the zeolite may be acid treated.

The process of the present invention may also be carried out using catalysts in which, for example, the platinum, zinc, or gallium is only impregnated on the surface of the zeolite or is incorporated in the intra-crystalline zeolite cavities as a metal compound which gives rise to a metal oxide during activation of the catalyst prior to contact with the hydrocarbon feedstock.

Where the catalyst composition is prepared by using a metal compound which ionizes in aqueous solution, for example, gallium nitrate, it is inevitable that some of the metal ions will be exchanged with the cations in the zeolite even if the preparation was directed to impregnation of the zeolite.

Whichever method of catalyst preparation is used, the amount of metal present in the catalyst compositions (metal plus zeolite) may suitably vary between 0.01 and 5 percent, preferably between 0.05 and 2 percent by weight. Obviously, a mixture of two or more metals can be incorporated into the zeolite by the methods discussed above. If zinc is present in the catalyst, it is preferred also to include palladium and/or gallium.

The ZSM-5 type crystalline zeolites utilized herein are members of a class of zeolitic materials which exhibit unusual properties. Although these zeolites have unusually low alumina contents, i.e. high silica to alumina mole ratios, they are very active even when the silica to alumina mole ratio exceeds 30. The activity is surprising since catalytic activity is generally attributed to



framework aluminum atoms and/or cations associated with these aluminum atoms. These zeolites retain their crystallinity for long periods in spite of the presence of steam at high temperature which induces irreversible collapse of the framework of other zeolites, e.g. of the X and A type. Furthermore, carbonaceous deposits, when formed, may be removed by burning at higher than usual temperatures to restore activity. These zeolites, used as catalysts, generally have low coke-forming activity and therefore are conducive to long times on stream between regenerations by burning carbonaceous deposits with oxygen-containing gas such as air.

An important characteristic of the crystal structure of this class of zeolites is that it provides a selective constrained access to and egress from the intracrystalline free space by virtue of having an effective pore size intermediate between the small pore Linde A and the large pore Linde X, i.e. the pore windows of the structure are of about a size such as would be provided by 10-membered rings of silicon atoms interconnected by oxygen atoms. It is to be understood, of course, that these rings are those formed by the regular disposition of the tetrahedra making up the anionic framework of the crystalline zeolite, the oxygen atoms themselves being bonded to the silicon (or aluminum, etc.) atoms at the centers of the tetrahedra.

The silica to alumina mole ratio referred to may be determined by conventional analysis. This ratio is meant to represent, as closely as possible, the ratio in the rigid anionic framework of the zeolite crystal and to exclude aluminum in the binder or in cationic or other form within the channels. Although zeolites with silica to alumina mole ratios of at least 12 are useful, it is preferred in some instances to use zeolites having substantially higher silica/alumina ratios, e.g. 1600 and above. In addition, zeolites as otherwise characterized herein but which are substantially free of aluminum, that is zeolites having silica to alumina mole ratios of up to infinity, are found to be useful and even preferable in some instances. Such "high silica" or "highly siliceous" zeolites are intended to be included within this description. Also included within this definition are



substantially pure silica analogs of the useful zeolites described herein, that is to say those zeolites having no measurable amount of aluminum (silica to alumina mole ratio of infinity) but which otherwise embody the characteristics disclosed.

These zeolites, after activation, acquire an intracrystalline sorption capacity for normal hexane which is greater than that for water, i.e. they exhibit "hydrophobic" properties. This hydrophobic character can be used to advantage in some applications.

The class of zeolites useful herein have an effective pore size such as to freely sorb normal hexane. In addition, the structure must provide constrained access to larger molecules. It is sometimes possible to judge from a known crystal structure whether such constrained access exists. For example, if the only pore windows in a crystal are formed by 8-membered rings of silicon and aluminum atoms, then access by molecules of larger cross-section than normal hexane is excluded and the zeolite is not of the desired type. Windows of 10-membered rings are preferred, although in some instances excessive puckering of the rings or pore blockage may render these zeolites ineffective.

Although 12-membered rings in theory would not offer sufficient constraint to produce advantageous conversions, it is noted that the puckered 12-ring structure of TMA offretite does show some constrained access. Other 12-ring structures may exist which may be operative for other reasons and, therefore, it is not the present intention to entirely judge the usefulness of a particular zeolite solely from theoretical structural considerations.

Rather than attempt to judge from crystal structure whether or not a zeolite possesses the necessary constrained access to molecules of larger cross-section than normal paraffins, a simple determination of the "Constraint Index" may be used. The meaning of Constraint Index and its method of determination are fully described in, for example, U.S. Patent No. 3,905,915

Preferably the zeolite used herein is selected from ZSM-5, ZSM-11, ZSM-12, ZSM-23, ZSM-35, ZSM-38, ZSM-48, and other similar materials, with ZSM-5 being especially preferred.



ZSM-5 is described in greater detail in U.S. Patents No. 3,702,886 and Re 29,948. ZSM-11 is described in U.S. Patent No. 3,709,979. ZSM-12 is described in U.S. Patent No. 3,832,449. ZSM-23 is described in U.S. Patent No. 4,076,842. ZSM-35 is described in U.S. Patent No. 4,016,245. ZSM-38 is described in U.S. Patent No. 4,046,859. ZSM-48 is described in published European Patent Application No. 15132.

The specific zeolites described, when prepared in the presence of organic cations, are substantially catalytically inactive, possibly because the intra-crystalline free space is occupied by organic cations from the forming solution. They may be activated by heating in an inert atmosphere at 540°C for one hour, for example, followed by base exchange with ammonium salts followed by calcination at 540°C in air. The presence of organic cations in the forming solution may not be absolutely essential to the formation of this type zeolite; however, the presence of these cations does appear to favor the formation of this class of zeolite. More generally, it is desirable to activate this type catalyst by base exchange with ammonium salts followed by calcination in air at about 540°C for from about 15 minutes to about 24 hours.

Natural zeolites may sometimes be converted to zeolite structures of the class herein identified by various activation procedures and other treatments such as base exchange, steaming, alumina extraction and calcination, alone or in combinations. Natural minerals which may be so treated include ferrierite, brewsterite, stilbite, dachiardite, epistilbite, heulandite, and clinoptilolite.

In a preferred aspect of this invention, the zeolites hereof are selected as those providing among other things a crystal framework density, in the dry hydrogen form, of not less than 1.6 grams per cubic centimeter. The dry density for known structures may be calculated from the number of silicon plus aluminum atoms per 1000 cubic Angstroms, as given, e.g., on Page 19 of the article ZEOLITE STRUCTURE by W. M. Meier in PROCEEDINGS OF THE CONFERENCE ON MOLECULAR SIEVES, (London, April 1967) published by the Society of Chemical Industry, London, 1968.



When the crystal structure is unknown, the crystal framework density may be determined by classical pycnometer techniques. For example, it may be determined by immersing the dry hydrogen form of the zeolite in an organic solvent which is not sorbed by the crystal. Or, the crystal density may be determined by mercury porosimetry, since mercury will fill the interstices between crystals but will not penetrate the intracrystalline free space.

When synthesized in the alkali metal form, the zeolite is conveniently converted to the hydrogen form, generally by intermediate formation of the ammonium form as a result of ammonium ion exchange and calcination of the ammonium form to yield the hydrogen form. In addition to the hydrogen form, other forms of the zeolite wherein the original alkali metal has been reduced to less than about 1.5 percent by weight may be used. Thus, the original alkali metal of the zeolite may be replaced by ion exchange with other suitable metal cations of Groups I through VIII of the Periodic Table, including, by way of example, nickel, copper, zinc, palladium, calcium or rare earth metals.

In practicing a particularly desired chemical conversion process, it may be useful to incorporate the above-described crystalline zeolite with a matrix comprising another material resistant to the temperature and other conditions employed in the process. Such matrix material is useful as a binder and imparts greater resistance to the catalyst for the severe temperature, pressure and reactant feed stream velocity conditions encountered in many cracking processes.

Useful matrix materials include both synthetic and naturally occurring substances, as well as inorganic materials such as clay, silica and/or metal oxides. The latter may be either naturally occurring or in the form of gelatinous precipitates or gels including mixtures of silica and metal oxides. Naturally occurring clays which can be composited with the zeolite include those of the montmorillonite and kaolin families, which families include the sub-bentonites and the kaolins commonly known as Dixie, McNamee-Georgia and Florida clays or others in which the main mineral constituent is halloysite, kaolinite, dickite, nacrite or anauxite. Such clays can be used in the raw state



as originally mined or initially subjected to calcination, acid treatment or chemical modification.

In addition to the foregoing materials, the zeolites employed herein may be composited with a porous matrix material, such as alumina, silica-alumina, silica-magnesia, silica-zirconia, silica-thoria, silica-beryllia, and silica-titania, as well as ternary compositions, such as silica-alumina-thoria, silica-alumina-zirconia, silica-alumina-magnesia and silica-magnesia-zirconia. The matrix may be in the form of a cogel. The relative proportions of zeolite component and inorganic oxide gel matrix, on an anhydrous basis, may vary widely with the zeolite content ranging from between about 1 to about 99 percent by weight and more usually in the range of about 5 to about 80 percent by weight of the dry composite.

A Fischer-Tropsch Synthesis gas conversion process is relied upon to convert syngas obtained from coal to form particularly hydrocarbons, oxygenates and chemical forming components. The process is complex, expensive to operate and may be conveniently divided into (1) a complex for preparing synthesis gas from coal, (2) a Fischer-Tropsch type of synthesis gas conversion using a fixed catalyst bed operation, a fluid catalyst bed operation, or a slurry bed operation, (3) a product recovery operation, and (4) an auxiliary plant and utility operations required in such a complex.

The extremely diverse nature of the products obtained in such a combination operation amplifies the complexity of the overall process arrangement and its operating economics. The synthesis operation is known to produce a wide spectrum of products including fuel gas, light olefins, LPG, gasoline, light and heavy fuel oils, waxy oils and oxygenates identified as alcohol, acetones, ketones, and acids, particularly acetic and propionic acid. The C_2 and lower boiling components may be reformed to carbon monoxide and hydrogen or the C_2 formed hydrocarbons and methane may be combined and blended for use in a fuel gas pipeline system.

In the operation, the water soluble oxygenates or chemicals are separated and recovered as individual components with the formed



organic acids remaining in the water phase separately processed. Disposal of the oxygenates and formed acids is a very expensive operation. Propylene and butylene formed in the process are converted to gasoline boiling components by polymerization in the presence of a solid phosphoric acid catalyst. Propane and butane on the other hand are used for LPG.

The present invention is concerned with converting the oxygenate and hydrocarbon product of a Fischer-Tropsch synthesis gas conversion operation to premium chemical feedstocks, i.e. benzene, toluene and xylene.

The accompanying drawing is a condensed schematic block flow arrangement of a process directed to the conversion of coal to synthesis gas comprising carbon monoxide and hydrogen, the reduction of carbon monoxide by the Fischer-Tropsch process to form a product mixture comprising hydrocarbons and oxygenates and the recovery of these products for further use.

Referring to the drawing, a coal gasifier section 2 is supplied with pulverized coal by way of a conduit 4 with steam by way of a conduit 6 and with oxygen by way of a conduit 8. The products of gasifier section 2 are then fed through conduit 10 to a gas scrubber section 12. In scrubber section 12, carbon monoxide and hydrogen are separated from hydrogen sulfide which is removed through conduit 14, from carbon dioxide which is removed through conduit 16, from tars and phenols which are removed through conduit 18 and from ammonia which is removed through conduit 20. The carbon monoxide-hydrogen rich gas is passed from section 12 by conduit 22 to a partial combustion zone 24 supplied with steam by conduit 26 and oxygen by conduit 28. The partial combustion operation of section 24 produces a carbon monoxide-hydrogen synthesis gas of desired ratio which is then passed by conduit 32 to a Fischer-Tropsch reaction section 36 which is provided with for example an iron synthesis catalyst and which also receives a C_2 recycle gas introduced by conduit 34. Generally, the



synthesis gas feed is introduced into the section 36 at a temperature of about 160°C and at an elevated pressure of about 365 psig. However, the temperature of the synthesis gas admixed with catalyst in the fluid operation rapidly rises because of the heat liberated so that the Fischer-Tropsch and water gas shift reactions are conveyed by line 40 to a cooler, 38, and the cooled products are then conveyed via line 42 to a separator 44. In practice the cooler 38, line 42 and separator 44 may be one integral unit. Water is removed from separator 44 via line 46, C₂ recycled by conduit 34, other gases via line 17, and liquid hydrocarbon products via line 48. The liquid product is conveyed via line 48 to reactor 50 where it is contacted with the metal impregnated crystalline zeolite.

The flow stream from either Fischer-Tropsch reaction section 36 through line 37 or from separator 44 through line 18 is contacted with the ZSM-5 type zeolite in the reactor 50, preferably in the form of a fixed bed. In a typical, and preferred embodiment of the process of this invention, the feedstream of oxygenates and hydrocarbons is introduced into the reactor 50 at a temperature within the range of 250°C about 650°C, a pressure within the range of 1×10^5 to 30×10^5 pascal (0 to 400 psig), and a WHSV of 0.1 to 10. Preferred temperatures in the reaction zone 33 fall within the range of 400°C to 650°C and preferred pressures fall within the range of 1×10^5 to 15×10^5 pascal (0 to 200 psig). A preferred WHSV is between 0.2 and 3.

Effluent from the reactor 50 is conveyed through line 52 optionally to a cooler and separator (not shown) and the liquid portion thereof is fractionated in a distillation tower 54 into fractions consisting of benzene, toluene and xylene. Any fraction containing hydrocarbons in excess of 9 carbon atoms can be recycled through reactor 50 via line 56 for conversion to benzene, toluene and xylene.

EXAMPLE 1

Acid or hydrogen-form ZSM-5 zeolite catalyst was impregnated with 0.5% by weight gallium. The catalyst was prepared in the form of

extrudate in which the ratio of silica to alumina in the ZSM-5 was 70 to 1. Tests were run using the acid form of zeolite and the acid form containing 0.5% by weight of gallium metal. A Fischer-Tropsch product having the compositions shown in Table I was then passed over each catalyst under the conditions shown in Table I. The results obtained show a substantial increase in the production of aromatics, namely benzenes, toluene and xylene when the gallium impregnated catalyst was used.

In Table II is shown the results obtained with a similar feedstock and catalysts at the same conditions of temperature and pressure as in Table I. In Tables I and II the composition of the feed stock is entered in the column headed "Feed."

F-1382

-12-

TABLE I
BTX From F-T Products (0 psig)

Catalysts:		Ga/HZSM-5	HZSM-5	Ga/HZSM-5	HZSM-5
Temp., °F		----- 1000 -----		----- 1050 -----	
WHSV		----- 0.5 -----			
Yield (g/100g feed) <u>Feed</u>					
BTX		40	30	41	38
C ₉ + Aromatics		15	6	18	8
Aromatics Total	1%	55	39	59	46

TABLE II
dTX From Fischer-Tropsch Products

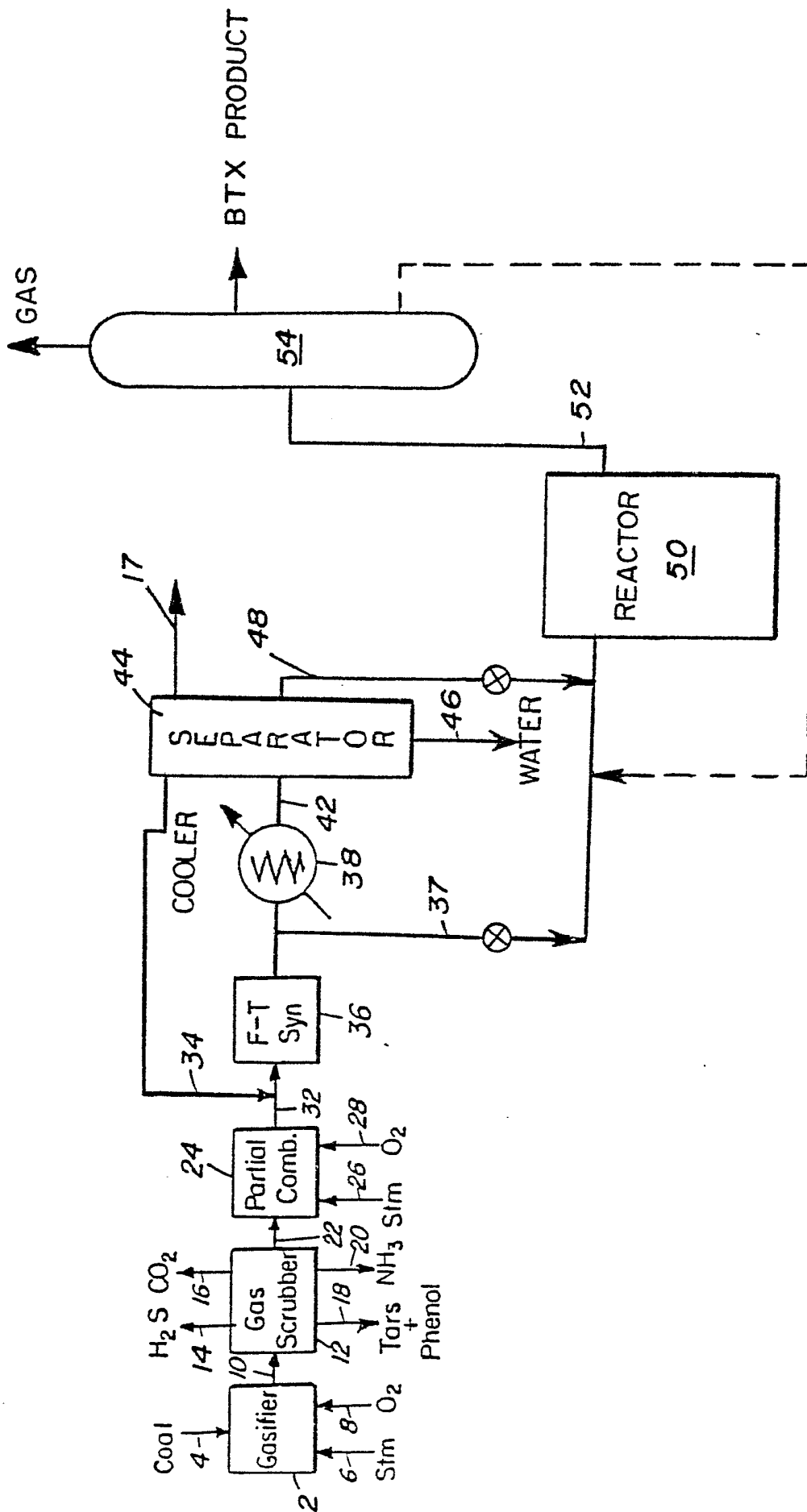
CATALYSTS	0.5% Co/HZSM-5 (70/1 SiO ₂ /Al ₂ O ₃)	1050	1000	1050	1000	HZSM-5 (70/1 SiO ₂ /Al ₂ O ₃)	Feed Compo- sitions** %
Conditions: Temp., of	1000	1000	1000	1050	1000	1050	C5 4.8
Pressure psig	0	0	0	0	0	0	C6 8.7
WHSV	1	0.5	0.5	3.5	1.0	0.5	C7 10.1
TOS Hrs	1.5	3.0	3.0	3.5	1.0	1.5	C8 13.1
							C9 10.8
Selectivity, g/100g Feed							C10 9.1
Gaseous Product	44	43	40	40	56	51	C11 7.6
BTX	36	40	41	41	33	38	C12 6.5
Total Aromatics	52	55	59	59	39	46	C13 5.3
							C14 4.4
Prod. Distribution* wt %							C15 3.9
C4-	44.1	43.0	39.7	39.7	56.1	50.7	C16 3.1
C5-C6	3.5	1.6	1.2	1.2	3.5	2.2	C17 2.6
BZ	10.6	14.1	16.0	16.0	11.1	14.6	C18 2.1
Toluene	17.9	18.7	18.7	18.7	16.2	17.5	C19 1.7
EB	0.7	0.7	0.8	0.8	0.7	0.8	C20-C29 5.2
Xylenes	7.7	7.5	6.6	6.6	6.0	5.7	C30-C40 1.0
C9+ Aromatics	15.4	14.3	17.1	17.1	6.4	8.4	TOTAL 100.0
Total	99.9	99.9	100.1	100.1	100.0	99.9	

* On-line analysis; H₂ not analyzed.

** Contains less than 1% BTX, and approx. 10% oxygenates.

CLAIMS:

1. A process for producing a mixture of hydrocarbons rich in benzene, toluene and xylene which comprises:
 - (a) converting a fossil fuel to a synthesis gas;
 - (b) converting the synthesis gas by Fischer-Tropsch reaction to a product containing oxygenates and hydrocarbons;
 - (c) contacting said Fischer-Tropsch product with a catalyst comprising a metal-promoted porous crystalline zeolite having a constraint index within the range of 1 to 12 and a silica to alumina ratio of at least 12 to produce an effluent stream rich in benzene, toluene and xylene; and
 - (d) removing benzene, toluene and xylene from said effluent stream.
2. The process of Claim 1 wherein the metal of said catalyst composition of (c) comprises zinc, cadmium, mercury, aluminum, gallium, indium, thallium, iron, cobalt, nickel, ruthenium, rhodium, palladium, osmium, iridium, platinum or a mixture of two or more of these.
3. The process of Claim 1 or Claim 2 wherein the suitable conversion conditions of (c) include a temperature of from 250° to 650°C, a pressure of from 1×10^5 to 30×10^5 pascal and a WHSV of from 0.1 to 10..
4. The process of any preceding Claim wherein said zeolite of (c) is selected from ZSM-5, ZSM-11, ZSM-12, ZSM-23, ZSM-35, ZSM-36, and ZSM-48.
5. The process of Claim 4 wherein said zeolite of (c) is in the acid form.





DOCUMENTS CONSIDERED TO BE RELEVANT			
Category	Citation of document with indication, where appropriate, of relevant passages	Relevant to claim	CLASSIFICATION OF THE APPLICATION (Int. Cl. 3)
X	<p style="text-align: center;">---</p> US-A-4 076 761 (CHANG et al.) *Claims*	1,3-5	C 07 C 15/04 C 07 C 15/06 C 07 C 15/08 C 07 C 1/20
X	<p style="text-align: center;">---</p> GB-A-1 446 252 (MOBIL OIL CORPORATION) *Claims*	1,3-5	
P,X	<p style="text-align: center;">---</p> DE-A-3 113 838 (I.C.I.) *Claims; pages 10-12* <p style="text-align: center;">-----</p>	1,3-4	
			TECHNICAL FIELDS SEARCHED (Int. Cl. 3) C 07 C 15/00 C 07 C 1/00
The present search report has been drawn up for all claims			
Place of search THE HAGUE		Date of completion of the search 02-03-1983	Examiner VAN GEYT
CATEGORY OF CITED DOCUMENTS X : particularly relevant if taken alone Y : particularly relevant if combined with another document of the same category A : technological background O : non-written disclosure P : intermediate document T : theory or principle underlying the invention E : earlier patent document, but published on, or after the filing date D : document cited in the application L : document cited for other reasons & : member of the same patent family, corresponding document			