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ENCLOSURE (B) 18

STUDIES ON CATALYSTS
FOR COAL HYDROGENATION

by

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SUMMARY

The catalyst used in the Bergius process, as applied to the hydrogenation of Japanese brown coals, was investigated and a mixed catalyst of the composition Fe₂O₃ : S : Sn(OH)₂ (100 : 17 : 1) was found to be the most suitable for the purpose.

I. INTRODUCTION

The catalyst employed in the Bergius process at the Naval Fuel Depot was ZnCl₂.H₂O, but owing to difficulties in supply, this investigation for finding a suitable catalyst composed of cheaper substitute materials was undertaken. This project was started in 1940 and completed in 1943.

II. DETAILED DESCRIPTION

A. Materials Used

1. Coal Brown coal from the Agochi district, Korea, was ground to powder of 60 mesh, and showed the following composition:

Water.....	15.5%	C.....	68.23%
Ash.....	8.2%	H.....	7.35%
V.m.....	43.6%	S.....	0.73%
F.c.....	32.7%	N.....	1.56%
		Ash.....	9.49%

2. Tar The tar, used to make the paste, was that fraction of dephenolated low temperature tar boiling from 270° to 320°. The dephenolated tar was prepared by washing with 10% caustic soda solution.

d₂₀.....1.037

Benzene Insol..... 1.7%

Composition

C.....	86.75%
H.....	8.55%
N.....	0.85%
S.....	0.17%
Ash.....	0.1%

Distillation Test

I.B.P. (90°)

90-270°..... 4.3%

270-300°..... 11.1%

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300-350°	31.0%
350-	52.2%

3. Hydrogen Hydrogen, of 99% purity was obtained by electrolysis of water.

4. Catalyst The following catalysts were tested.

- a. $ZnCl_2 \cdot 3H_2O$,
- b. MoO_3 , Na_2MoO_3 , MoO_3 with C, $H_2[MoO_3(C_2O_4)(H_2O)] \cdot H_2O$,
- c. $Sn(C_2O_4)_2 \cdot 3H_2O$, $Sn(C_2O_4)_4 \cdot 3H_2O$, $Sn(C_2H_2O_2)_2 \cdot 2H_2O$,
- d. $Sn(C_2H_2O_2)_4 \cdot 2H_2O$, $SnCl_2 \cdot 2H_2O$, $SnCl_4$, $Sn(OH)_2$, $Sn(OH)_4$,
- e. $Sn(C_{17}H_{35}CO_2)_4$,
- f. $Na_2MoO_4/SnCl_4(4 : 1)$, $MoO_3/SnCl_2(4 : 1)$
- g. Fe_2O_3 , $Fe(C_2O_4)_2 \cdot 2H_2O$, $Fe_2(C_2O_4)_3 \cdot 2H_2O$,
- h. $Fe_2(C_2O_4)_3 \cdot 2H_2O/NH_4Cl(10 : 1)$, $Fe(C_2O_4)_2 \cdot 2H_2O/NH_4Cl(10:1)$,
- i. $Fe(SO_4)_2$, $Fe_2(SO_4)_3$, FeS ,
- j. $Fe_2O_3/S(4 : 1)$, $Fe_2O_3/S(10 : 1)$, $Fe_2O_3/Sn(OH)_2(100 : 1)$,
- k. Fe Stearate Soap/ $Sn(OH)_2(100 : 1)$, $Fe_2O_3/S/Sn(OH)_2(100:17:1)$,
- l. $Zn(C_2O_4)_2 \cdot 3H_2O$, $Zn(C_2H_3O_2)_2 \cdot 3H_2O$, $Zn(C_2H_3O_2)_2 \cdot 3H_2O/NH_4Cl(10:1)$,
- m. $Pb(C_2H_3O_2)_2 \cdot 3H_2O$, $Pb(C_2H_3O_2)_2 \cdot 3H_2O/NH_4Cl(10 : 1)$.

The catalysts were prepared from the metallic chloride or nitrate by precipitation and mixing of the components. They were dried at 110°C and powdered.

B. Apparatus

A cast iron cylindrical autoclave of 2.4 litres capacity was used. It was equipped with a thermometer and manometer, and was heated externally by electric resistance, and mounted to rotate horizontally.

C. Procedures

A paste was made by mixing oil and coal in the weight ratio of 1 : 1.

In each experiment, 150gms of the paste and 4.5gms of the catalyst to be tested were put into the autoclave, and hydrogen was introduced, from a cylinder, to produce 100 atmospheres of pressure at 0°C. The autoclave was heated at a rate of 2°C/min, to the required temperature and kept at this temperature for one hour. The changes in pressure during the reaction were observed at intervals of five minutes. When the reaction was finished, the volume and the density of the gas in the apparatus were measured and the chemical compositions of the gas, liquid and, solid reaction

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products were determined by the usual methods.

D. Experimental Results

Experimental results are summarized in Table I(B)18. The data are presented only for the most promising of the catalysts.

III. CONCLUSIONS

The simple catalysts which gave the best results were, $ZnCl_2 \cdot 2H_2O$, MoO_3 , $Sn(OH)_2$, and $Sn(OH)_4$.

The mixed catalyst which may be recommended in any respect was $Fe_2O_3 : S : Sn(OH)_2$ (100 : 17 : 1). This catalyst was suitable for commercial usage and was better than $ZnCl_2 \cdot 2H_2O$, previously used commercially due to a higher yield of tar and no corrosion difficulties. The cost of this mixed catalyst is slightly higher than $ZnCl_2 \cdot 2H_2O$ due to tin content. It was prepared by mixing commercial grade ferric oxide (prepared by precipitation of $Fe(OH)_3$ and subsequent calcining), commercial grade sulphur and $Sn(OH)_2$ in the weight ratio of 100 : 17 : 1. The $Sn(OH)_2$ was prepared by precipitation from a 1 N solution of $SnCl_2$ with 10% $NaOH$, and drying in an oven at $110^\circ C$. This catalyst was used at the Fushun S.M.R. coal hydrogenation plant on the basis of these experiments and satisfactory results were obtained.

Table I(B)18
CATALYSTS FOR COAL HYDROGENATION

Exp. No.	Catalyst											
	ZnO, 2ZnO	Mo O ₃	Sn(CrO ₄) ₂ ·3H ₂ O	Sn(OH) ₂	Fe ₂ O ₃	Fe ₂ O ₃	Fe ₂ O ₃	Fe ₂ O ₃	Fe ₂ O ₃	Fe ₂ O ₃	Sn(OH) ₂	Sn(OH) ₂
	1	2	3	4	5	6	7	8	9	10	11	12
Temp. (°C)	400	420	420	450	375	400	385	400	400	410	420	400
Press. (mm), kg/cm ²	260	277	287	298	270	270	275	278	282	260	260	292
Press. Drop, kg/cm ²	29	30	28	30	27.0	36.0	32	37	24.5	16.0	19.5	26
Yield (liquid and solids) (gm)	133	127	85.7	129.6	96.8	130.4	117.7	125.5	104.0	-	-	113.5
Yield (by wt% of parts)	87	85	37	86	64	86.9	78.7	83.6	69.3	-	-	75.6
Water (wt% of tot. liquid)	24.5	25.7	27.5	28.9	25.0	26.3	25.3	25.3	23.7	13.0	13.0	24.3
Tar (<120°)	10.5	11.3	3.0	6.8	2.6	8.2	7.1	11.1	4.9	4.2	5.6	5.9
Tar (120 - 150°)	12.2	13.6	10.4	12.2	10.5	15.5	11.8	11.1	9.3	16.3	18.1	10.3
Tar (>150°)	26.6	24.3	35.6	29.8	36.1	30.9	32.7	29.3	39.8	57.9	54.6	20.7
Residues	24.5	13.9	12.6	11.5	16.5	9.7	11.2	11.3	16.1	7.4	6.0	12.9
CO ₂	1.8	1.8	1.7	0.9	2.2	1.8	2.2	2.0	2.4	0.6	0.6	2.1
CO	0.7	0.6	0.8	1.0	0.4	0.8	0.6	1.0	1.1	0.8	1.0	1.0
C ₆ H ₆	0.7	0.8	0.6	0.4	0.4	0.8	0.6	1.2	1.0	0.8	0.6	0.7
Acetylene	87.5	86.9	89.8	89.8	90.6	86.1	91.2	89.1	90.2	90.0	89.0	90.6
C ₆ H ₅ OH	4.9	6.1	1.6	3.9	1.5	4.7	2.9	2.9	2.2	4.9	5.8	2.6
n	1.2	1.2	1.0	1.2	2.0	2.0	2.0	2.0	1.5	2.7	2.0	1.5
Hydrogen consumed (gm)	7.7	8.0	7.5	7.7	7.0	9.3	7.6	9.1	6.6	4.9	5.7	6.8
Hydrogen (H ₂ /total, wt%)	37.3	38.8	36.4	37.3	33.9	45.1	36.9	44.2	32.0	24.2	28.4	33.0
Hydrogen (H ₂ /pure carbon in product, wt%)	6.7	6.9	6.5	6.7	6.1	8.1	6.6	7.9	5.8	8.3	9.6	5.9
Total of Tar (total liquid product minus dissolved)	65.0	64.6	61.0	64.2	64.4	70.8	67.9	70.6	56.5	84.9	83.9	61.9