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ENCLOSURE (B)

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ENCLOSURE (B) 1

STUDIES ON THE PRODUCTION OF
DIESEL FUEL BY LIQUID SO_2 EXTRACTION

by

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SUMMARY

This investigation was begun in order to obtain a high cetane rating diesel fuel with low pour-point from petroleum kerosenes by the Edeleanu Process. The most significant results were that the aromatic hydrocarbons were for the most part removed from the kerosenes and the raffinate gave about 60-70 cetane rating.

I. INTRODUCTION

It was well known that the aromatic hydrocarbon components decreased the cetane value of petroleum oil. Accordingly, in order to obtain high cetane diesel fuel oil from petroleum, it was necessary to remove the aromatic hydrocarbon from the crude oil. In our laboratory, various kinds of petroleum oils were extracted under various conditions. This work was carried out by Naval Eng. Lieut. S. SONODA, C. NISHIMURA Naval Eng. Y. FUJIEDA and others, during the period Apr., 1942-Sept., 1944.

II. DETAILED DESCRIPTION

A. Test Procedures

Liquid SO_2 was inserted into a 3 liter flask which was maintained at the required temperature by dry ice. The mixture of one liter sample and liquid SO_2 in various ratios was mixed with a stirrer for 30 minutes, then, the raffinate and extract respectively were allowed to flow into the SO_2 evaporator, where SO_2 was evaporated by heating up to $80^\circ C$ electrically. The diagram of extraction apparatus is given in Figure 1(B)1.

The properties of the products were determined by the ordinary methods. The method of measuring the spontaneous ignition temperature was mainly that of J. S. Lewis (Japanese Chem. Soc., 1558, (1927)), as shown in Figure 2(B)2. The sample oil (0.1cc) was first introduced into a reaction vessel (240cc pyrex glass tube), and the vessel was evacuated. The vessel was heated at the rate of $4^\circ C/min.$, after which CO_2 free air was introduced into it. The increase in vapour pressure in the vessel was recorded every minute. The spontaneous ignition temperature was measured, at the time when a sudden ebullition of gas occurred in the mercury manometer, caused by the ignition and burning of the sample in the vessel.

B. Experimental Results

1. Petroleum sample from various sources were extracted with 100 wt % of liquid SO_2 at temperature $-10^\circ C$. The results are given in Table I(B)1. According to this table, it was concluded that paraffinic petroleum kerosenes were more suitable than aromatic ones, for providing diesel fuel of high cetane rating.
2. Tarakan kerosene (aromatic) and Sanga Sanga kerosene (paraffinic), both obtained from Borneo, were extracted with 100% of liquid SO_2 at temperature $-20^\circ C$. These results were given in Table II(B)1, Figure 3(B)1, Table III(B)1 and Figure 4(B)1. The appreciable tendencies in these results were as follows:

- a. The extraction effect for Tarakan kerosene was not appreciable.
- b. The effect for Sanga Sanga kerosene was recognized to be appreciable.

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c. The extraction effect increased with higher boiling point in the same kerosene.

3. A pilot plant which was begun on 15 August, 1945, had a capacity of 100 liters per hour; the flow sheet was exactly the same as the so-called Edeleanu Process.

The pre-cooled kerosene raw stock was fed into the bottom of the extractor, and the pre-cooled liquid SO₂ descended from the top in a spray, and the solvent and oil were mixed with each other in counter current, the solvent extracting the aromatic hydrocarbons from the oil. The optimum conditions for operating the extraction tower were :

Extraction temperature -25°C
 Extraction pressure atmospheric
 Solvent ratio 100%

The remaining SO₂ in the raffinate and extract oils was removed by heating the SO₂ extractors up to temperature 80°C. However, many difficulties in operation were experienced, due to the leakage of SO₂ from valve glands and packings of plunger pumps employed. The properties of raw stock and raffinate produced from the preliminary operation are given in Table IV(B)1. Roughly, the yield of raffinate was thought to be about 70%.

III. CONCLUSION

In the research laboratory experiments, it was recognized that it was possible to remove the great part of the aromatic hydrocarbons from petroleum

The extraction effects increased almost proportionally with the increase of boiling range and paraffinicity of the raw kerosenes.

In the pilot plant operations, many difficulties were experienced, chiefly due to the leakage of SO₂ gas from valve glands. It was found to be very difficult to operate the Edeleanu Plant with packing materials produced in Japan.

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Table I(B)1
PROPERTIES OF RAFFINATE*

| Sample | Yield (%) | Sp. gr (15°C) | Viscosity (R-1.30°C) | Flash pt (°C) | Pour. pt (°C) | Cetane Value |
|--------------------------------------|-----------|---------------|----------------------|---------------|---------------|--------------|
| Bahrain (204-365°C) | 86.2 | 0.8093 | 33.0 | none | -24 | 64.0 |
| Oha (259-372°C) | 82.4 | 0.8834 | 52.1 | none | -29 | 45.4 |
| Kettleman Hills (50% topped residue) | 85.0 | 0.8194 | 31.8 | none | -40 | 54.5 |
| Midway (200-350°C) | 72.5 | 0.8534 | 38.0 | none | -26 | 49.5 |
| Tarakan (200-300°C) | | 0.8606 | 34.6 | none | -30 | 49.0 |
| Innai, Japan (200-300°C) | 88.0 | 0.8582 | 34.8 | none | -50 | 39.3 |
| California (200-300°C) | 77.5 | 0.8474 | | none | -45 | 48.3 |
| Tarakan (F.D.-60%) | 72.4 | 0.8965 | 44.6 | none | -33 | 41.7 |
| California (217-385°C) | 71.9 | 0.8603 | | none | | 48.2 |
| Mexico (200-350°C) | | 0.8191 | 36.4 | none | -12 | 65.7 |
| Sumatra (164-255°C) | 88.4 | 0.7951 | 30.0 | none | -44 | 51.2 |
| Tarakan (105-356°C) | 67.5 | 0.8571 | | none | -1 | 45.4 |

*Extraction Temp - 10°C
Solvent ratio 100%

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Table II(B)1
EXTRACTION EFFECTS FOR TABLAKAN KEROSENE

| | 200 ~ 220 | | 230 ~ 250 | | 260 ~ 280 | | 290 ~ 310 | | 320 ~ 340 | | 350 ~ 370 | | 380 ~ 400 | | 410 ~ 430 | |
|-------------------------|-----------|--------|-----------|--------|-----------|--------|-----------|--------|-----------|--------|-----------|--------|-----------|--------|-----------|--------|
| | A | B | A | B | A | B | A | B | A | B | A | B | A | B | A | B |
| Sp. wt. (20°C) | 0.8021 | 0.8009 | 0.8011 | 0.8007 | 0.8013 | 0.8009 | 0.8011 | 0.8007 | 0.8013 | 0.8009 | 0.8011 | 0.8007 | 0.8013 | 0.8009 | 0.8011 | 0.8007 |
| Specific Gravity (20°C) | 0.8021 | 0.8009 | 0.8011 | 0.8007 | 0.8013 | 0.8009 | 0.8011 | 0.8007 | 0.8013 | 0.8009 | 0.8011 | 0.8007 | 0.8013 | 0.8009 | 0.8011 | 0.8007 |
| Distill. Pt. (°C) | 32.8 | 32.8 | 34.0 | 34.0 | 34.8 | 34.8 | 35.6 | 35.6 | 36.4 | 36.4 | 37.2 | 37.2 | 38.0 | 38.0 | 38.8 | 38.8 |
| Boiling Pt. (°C) | 34.0 | 34.0 | 35.2 | 35.2 | 36.0 | 36.0 | 36.8 | 36.8 | 37.6 | 37.6 | 38.4 | 38.4 | 39.2 | 39.2 | 40.0 | 40.0 |
| Flash Pt. (°C) | 34.0 | 34.0 | 35.2 | 35.2 | 36.0 | 36.0 | 36.8 | 36.8 | 37.6 | 37.6 | 38.4 | 38.4 | 39.2 | 39.2 | 40.0 | 40.0 |
| Auto. Ign. Pt. (°C) | 42.8 | 42.8 | 44.0 | 44.0 | 44.8 | 44.8 | 45.6 | 45.6 | 46.4 | 46.4 | 47.2 | 47.2 | 48.0 | 48.0 | 48.8 | 48.8 |
| Smoke Point (mm/100) | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 |
| Sp. wt. (20°C) | 0.8021 | 0.8009 | 0.8011 | 0.8007 | 0.8013 | 0.8009 | 0.8011 | 0.8007 | 0.8013 | 0.8009 | 0.8011 | 0.8007 | 0.8013 | 0.8009 | 0.8011 | 0.8007 |
| Specific Gravity (20°C) | 0.8021 | 0.8009 | 0.8011 | 0.8007 | 0.8013 | 0.8009 | 0.8011 | 0.8007 | 0.8013 | 0.8009 | 0.8011 | 0.8007 | 0.8013 | 0.8009 | 0.8011 | 0.8007 |
| Distill. Pt. (°C) | 32.8 | 32.8 | 34.0 | 34.0 | 34.8 | 34.8 | 35.6 | 35.6 | 36.4 | 36.4 | 37.2 | 37.2 | 38.0 | 38.0 | 38.8 | 38.8 |
| Boiling Pt. (°C) | 34.0 | 34.0 | 35.2 | 35.2 | 36.0 | 36.0 | 36.8 | 36.8 | 37.6 | 37.6 | 38.4 | 38.4 | 39.2 | 39.2 | 40.0 | 40.0 |
| Flash Pt. (°C) | 34.0 | 34.0 | 35.2 | 35.2 | 36.0 | 36.0 | 36.8 | 36.8 | 37.6 | 37.6 | 38.4 | 38.4 | 39.2 | 39.2 | 40.0 | 40.0 |
| Auto. Ign. Pt. (°C) | 42.8 | 42.8 | 44.0 | 44.0 | 44.8 | 44.8 | 45.6 | 45.6 | 46.4 | 46.4 | 47.2 | 47.2 | 48.0 | 48.0 | 48.8 | 48.8 |
| Smoke Point (mm/100) | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 |

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Table III(B)1
EXTRACTION EFFECTS FOR SANGA SANGA KEROSENE

| | 200 ~ 220 | | 230 ~ 250 | | 260 ~ 280 | | 290 ~ 310 | | 320 ~ 340 | | 350 ~ 370 | | 380 ~ 400 | | 410 ~ 430 | |
|-------------------------|-----------|--------|-----------|--------|-----------|--------|-----------|--------|-----------|--------|-----------|--------|-----------|--------|-----------|--------|
| | A | B | A | B | A | B | A | B | A | B | A | B | A | B | A | B |
| Sp. wt. (20°C) | 0.7964 | 0.7952 | 0.7964 | 0.7952 | 0.7964 | 0.7952 | 0.7964 | 0.7952 | 0.7964 | 0.7952 | 0.7964 | 0.7952 | 0.7964 | 0.7952 | 0.7964 | 0.7952 |
| Specific Gravity (20°C) | 0.7964 | 0.7952 | 0.7964 | 0.7952 | 0.7964 | 0.7952 | 0.7964 | 0.7952 | 0.7964 | 0.7952 | 0.7964 | 0.7952 | 0.7964 | 0.7952 | 0.7964 | 0.7952 |
| Distill. Pt. (°C) | 27.2 | 27.2 | 28.0 | 28.0 | 28.8 | 28.8 | 29.6 | 29.6 | 30.4 | 30.4 | 31.2 | 31.2 | 32.0 | 32.0 | 32.8 | 32.8 |
| Boiling Pt. (°C) | 28.0 | 28.0 | 28.8 | 28.8 | 29.6 | 29.6 | 30.4 | 30.4 | 31.2 | 31.2 | 32.0 | 32.0 | 32.8 | 32.8 | 33.6 | 33.6 |
| Flash Pt. (°C) | 28.0 | 28.0 | 28.8 | 28.8 | 29.6 | 29.6 | 30.4 | 30.4 | 31.2 | 31.2 | 32.0 | 32.0 | 32.8 | 32.8 | 33.6 | 33.6 |
| Auto. Ign. Pt. (°C) | 36.8 | 36.8 | 37.6 | 37.6 | 38.4 | 38.4 | 39.2 | 39.2 | 40.0 | 40.0 | 40.8 | 40.8 | 41.6 | 41.6 | 42.4 | 42.4 |
| Smoke Point (mm/100) | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 |
| Sp. wt. (20°C) | 0.7964 | 0.7952 | 0.7964 | 0.7952 | 0.7964 | 0.7952 | 0.7964 | 0.7952 | 0.7964 | 0.7952 | 0.7964 | 0.7952 | 0.7964 | 0.7952 | 0.7964 | 0.7952 |
| Specific Gravity (20°C) | 0.7964 | 0.7952 | 0.7964 | 0.7952 | 0.7964 | 0.7952 | 0.7964 | 0.7952 | 0.7964 | 0.7952 | 0.7964 | 0.7952 | 0.7964 | 0.7952 | 0.7964 | 0.7952 |
| Distill. Pt. (°C) | 27.2 | 27.2 | 28.0 | 28.0 | 28.8 | 28.8 | 29.6 | 29.6 | 30.4 | 30.4 | 31.2 | 31.2 | 32.0 | 32.0 | 32.8 | 32.8 |
| Boiling Pt. (°C) | 28.0 | 28.0 | 28.8 | 28.8 | 29.6 | 29.6 | 30.4 | 30.4 | 31.2 | 31.2 | 32.0 | 32.0 | 32.8 | 32.8 | 33.6 | 33.6 |
| Flash Pt. (°C) | 28.0 | 28.0 | 28.8 | 28.8 | 29.6 | 29.6 | 30.4 | 30.4 | 31.2 | 31.2 | 32.0 | 32.0 | 32.8 | 32.8 | 33.6 | 33.6 |
| Auto. Ign. Pt. (°C) | 36.8 | 36.8 | 37.6 | 37.6 | 38.4 | 38.4 | 39.2 | 39.2 | 40.0 | 40.0 | 40.8 | 40.8 | 41.6 | 41.6 | 42.4 | 42.4 |
| Smoke Point (mm/100) | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 | 14.2 |

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Table IV(B)
 PROPERTIES OF RAW MATERIALS AND PRODUCTS

| | Kerosene (Sanga Sanga 200-260°C) | Product (Paraffinate) |
|----------------------------|-------------------------------------|--------------------------|
| Yield (%) | | 70 |
| Sp. Gr. (15/15°C) | 0.8187 | 0.8129 |
| Viscosity (R-1 30°C sec) | 30.6 | 29.9 |
| Flash pt. (°C) | 58.5 | 69.0 |
| Pour pt. (°C) | -33.0 | -39.5 |
| Conradson's carbon (%) | Trace | Trace |
| Ash (%) | Trace | Trace |
| Impurities (%) | Trace | Trace |
| Cetane Value | 43.1 | 65.0 |
| Aniline pt. | 67.3 | 75.5 |
| Sp. Ignit. Temp (°C) | 293 | 225 |
| Unsat. and arom. (%) | 55.0 | 13.0 |
| Naphthene and Paraffin (%) | 45.0 | 87.0 |

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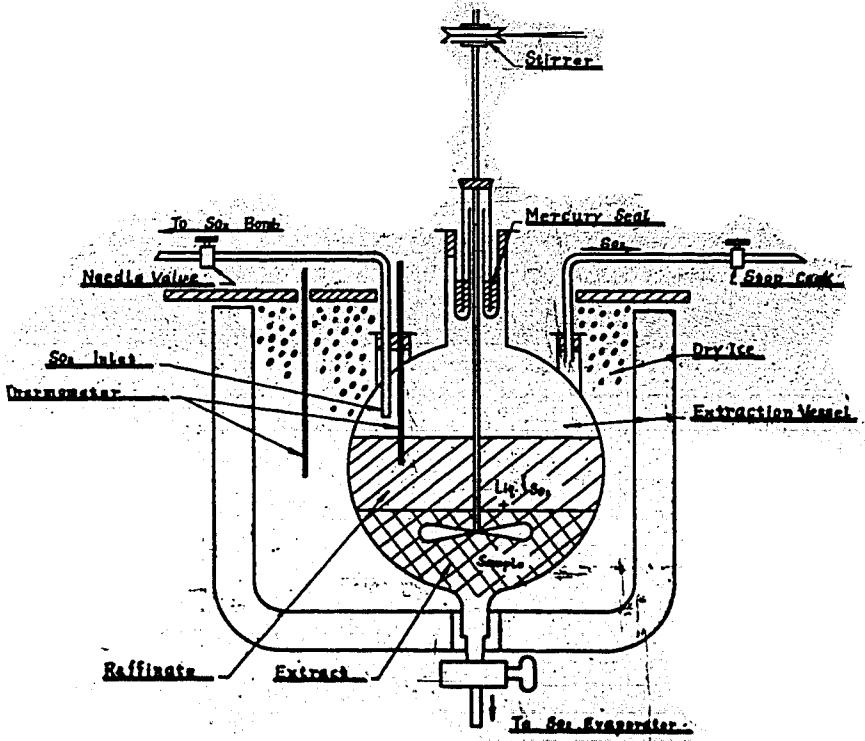


Figure 1(B)
DIAGRAM OF EXTRACTION APPARATUS

ENCLOSURE (B)

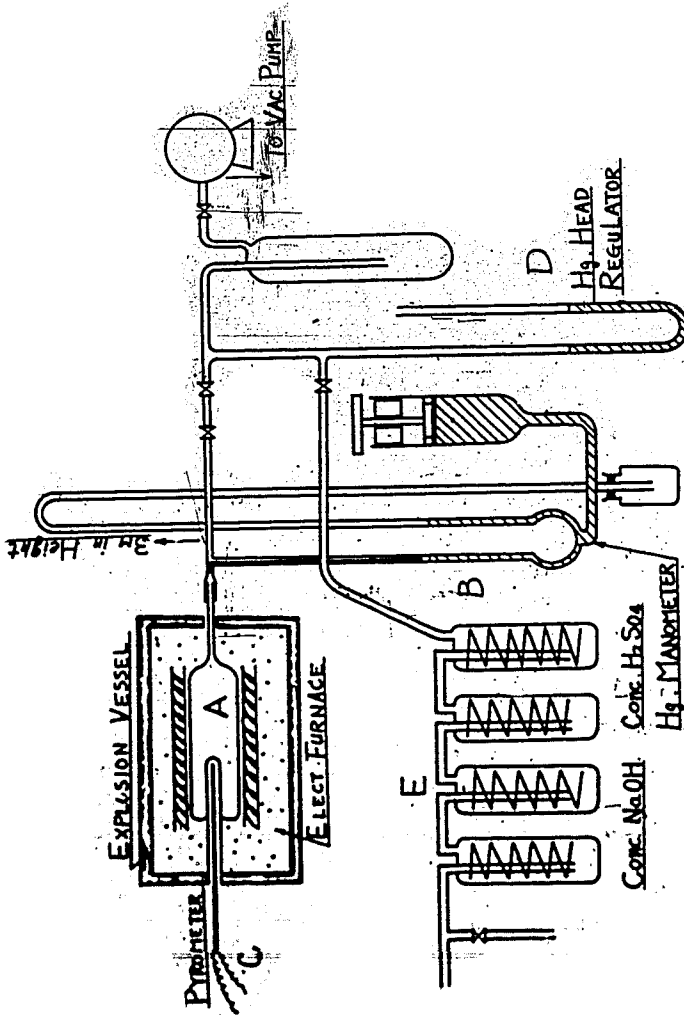


Figure 2(A):
APPARATUS FOR MEASURING SPONTANEOUS IGNITION TEMPERATURE

ENCLOSURE (B)1

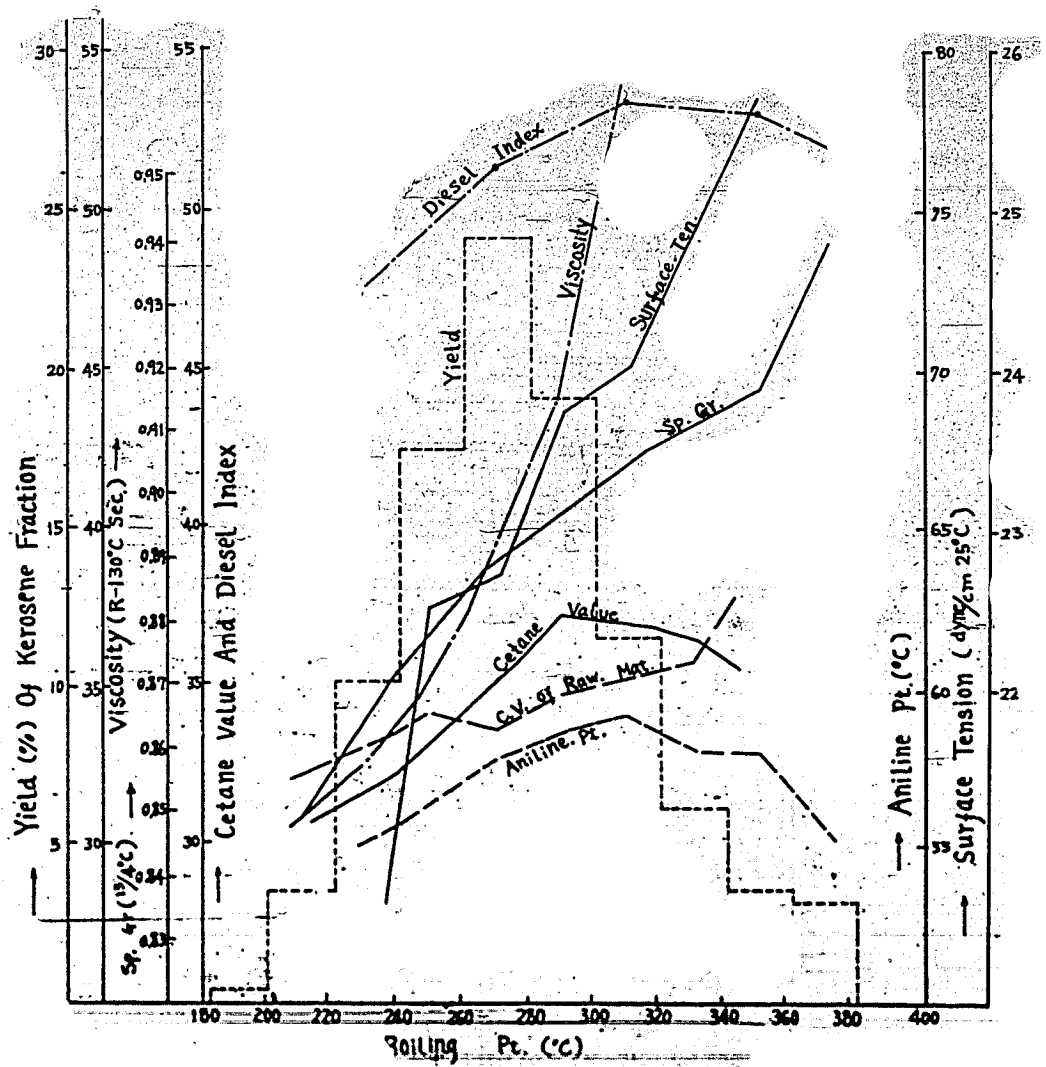


Figure 3(B)1
RELATIONS BETWEEN B.P. OF TARIKAR REFINERS' RAFFINATE AND ITS DIESEL PROPERTIES

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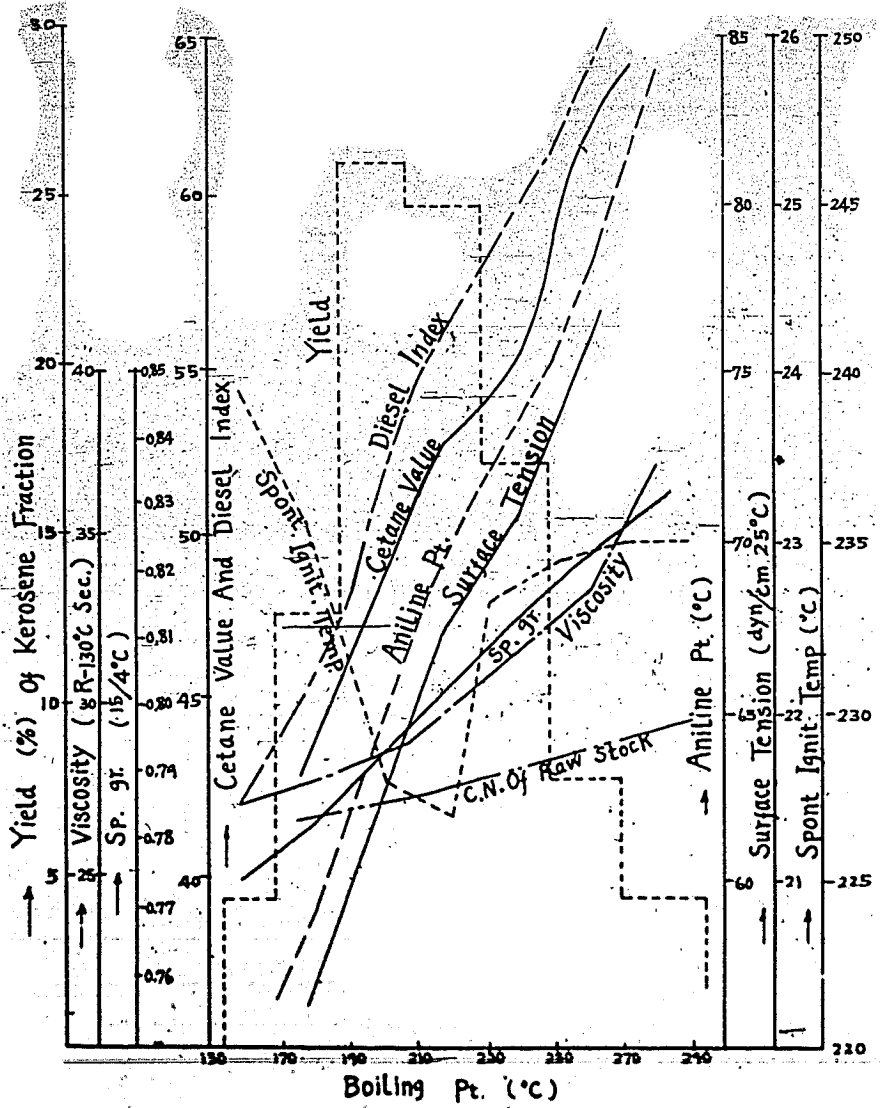


Figure 4(B)1
 RELATIONS BETWEEN B.P. OF SANCA SANCA
 KEROSENE RAFFINATE AND ITS DIESEL PROPERTIES