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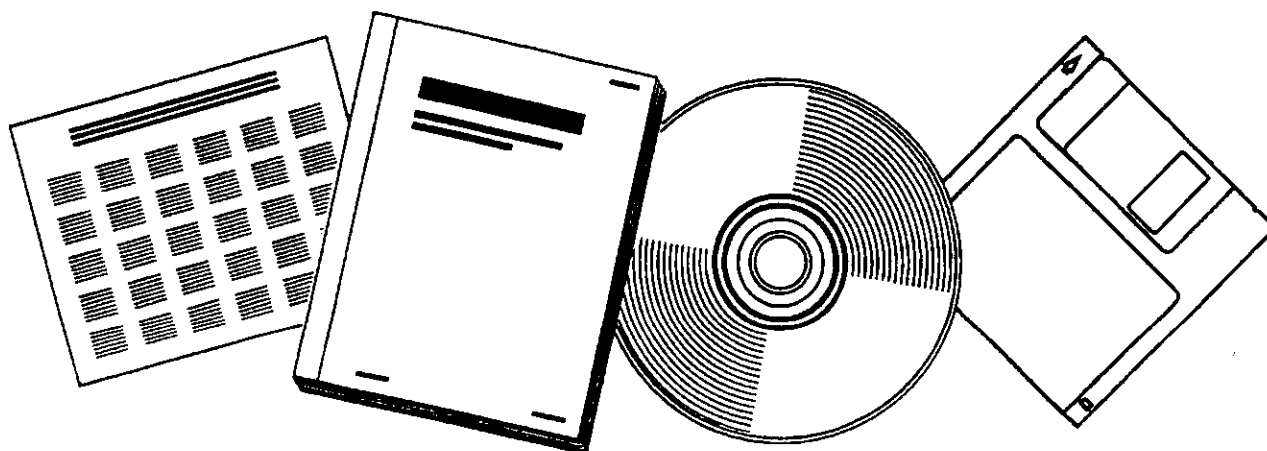
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**DEVELOPMENT OF A STABLE COBALT-RUTHENIUM  
FISCHER-TROPSCH CATALYST. TECHNICAL  
PROGRESS REPORT NO. 10, JANUARY 1,  
1992--MARCH 31, 1992**

UOP, INC.  
DES PLAINES, IL

1992



U.S. DEPARTMENT OF COMMERCE  
National Technical Information Service

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DE-AC/PC/89869--79

# DEVELOPMENT OF A STABLE COBALT-RUTHENIUM FISCHER-TROPSCH CATALYST

Contract DE-AC22-89PC89869

Technical Progress Report No. 10  
(1/1/92 - 3/31/92)

by

Robert R. Frame and Hemant B. Gala

UOP  
25 E. Algonquin Road  
Des Plaines, Illinois

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OFC ON November 9, 1993.

# DEVELOPMENT OF A STABLE COBALT-RUTHENIUM FISCHER-TROPSCH CATALYST

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## Contract Objective

The objective of this contract is to examine the relationship between catalytic properties and the function of cobalt Fischer-Tropsch catalysts and to apply this fundamental knowledge to the development of a stable cobalt-based catalyst with a low methane-plus-ethane selectivity for use in slurry reactors.

## Contract Tasks

Task 1.0: Project Management Report

Task 2.0: Reference Cobalt Catalyst

Task 3.1: Modifier Role for Ruthenium

Task 3.2: Particle Size Effects with Ruthenium

**Task 4.1: Identification of the Synergy between Cobalt and a Second Bimetallic Element, such as Ruthenium**

**Task 4.2: Development of a Bimetallic Catalyst**

**Task 5.0: Demonstration of Stability**

### **Experimental**

The fixed bed pilot plant, the catalyst testing procedure, and the calculations for conversion and selectivities were previously described in the technical progress report covering the period of 3/16/88 to 6/16/88 for Contract DE-AC22-87PC79812. Conversions and hydrocarbon selectivities were calculated using data from an on-line gas chromatography (GC) analyzer. Alcohol selectivities were calculated using data from an on-line boiling point GC analyzer, which analyzed the liquid product.

At the start of an experiment, 13 g of catalyst (> 40 mesh in size) is loaded in the fixed-bed reactor with 160 g of diluent. In most runs quartz sand (60 to 80 mesh in size) is used as the diluent. For runs 63 and 67,  $\alpha$ -alumina (40 to 80 mesh in size) was used as the diluent. Catalyst 585R2796 (Run 67) and 305R0160 (Run 77), prepared on carbotrap B support were 170 to 325 mesh in size. The diluent is used because of the very exothermic nature of the Fischer-Tropsch reactions. Experimental catalysts were screened by a three condition screening test (Table 1) wherein the initial condition (least strenuous) was the same as used for the reference catalyst. This will allow for a direct performance comparison with the reference catalyst. Since none of the catalysts were as active as the reference, the second and third conditions were used to provide higher conversions so that selectivities could be compared to the reference catalyst at comparable conversions. For cobalt catalysts methane selectivity is lower at higher conversion. One goal of the current work is to develop high activity catalysts which exhibit low methane

selectivity. All the catalysts evaluated with the exception of the reference catalyst contained ruthenium. A few also contained manganese and zirconium which were also on the reference catalyst (Table 2).

For runs discussed in this report, the run summary plots of conversions and selectivities as a function of hours-on-stream are attached. From these plots data were abstracted to prepare tabular summaries which allow comparison of catalyst performance (Tables 3 and 4).

#### Scope of Work During Reporting Period

Screening of experimental catalysts continued during this quarter. The reference catalyst, TC 211, was prepared under an earlier Union Carbide contract with the DOE (DOE-AC22-84PC70028) and consists of cobalt, manganese and zirconium deposited on a special Y zeolite-derived support. It exhibits good activity and low methane selectivity (Table 3 and 4). During that contract, this catalyst was found to be very stable.

The initial goal of this project is to identify suitable support materials for cobalt-ruthenium based Fischer-Tropsch catalysts. As reported in the previous two quarterly reports, several promising materials have emerged: magnesium oxide, 50/50 alumina/titania, and carbon. All are very pure; in particular, free of sulfur.

In this quarter, additional catalysts that were supported on these three promising materials were evaluated. The STEM apparatus was inoperable for most of this time period, thus only a minimal amount of catalyst characterization was done.

## Results and Discussion

### Runs 63, 69 and 72

These three runs employed magnesium oxide-supported catalysts. Runs 63 (catalyst 585R2757) and 69 (catalyst 585R2810) were discussed in previous reports from this project (Reports 7-9 covering the period of April to December, 1991). The hourly run summary data for Run 72 (catalyst 305R0142) are in Appendix A, Figures 1-8.

None of the catalysts supported on magnesium oxide were as active as the reference TC 211 catalyst at condition 1. At Condition 3 in Run 69 the conversion was close to the reference catalyst at Condition 1; the methane selectivity was 11.1% compared to 7.0% for the reference catalyst. Although these catalysts exhibited the lowest methane selectivities of all the experimental catalysts herein, they were still more methane selective than the reference catalyst. All of the catalysts were more selective to alcohols than the reference catalyst (Table 4). The reverse micelle impregnation method did not appear to be much less selective to methane than a similar catalyst prepared by an aqueous impregnation (Run 63 vs Run 72). There was at best a slight activity advantage for the reverse micelle catalyst.

### Runs 68 and 73

These two runs used catalysts prepared on 50/50 alumina/titania. Run 68 (catalyst 585P2775) was discussed in a previous technical progress report from this project (Report No. 9 covering the period October to December, 1991). The hourly run summary data for Run 73 (catalyst 305R0134) are in Appendix A, Figures 9-16.

The alumina/titania-supported catalysts both produced high levels of methane. There did not seem to be an advantage to the reverse micelle catalyst preparation route from the standpoint of either activity or selectivity at Condition 1. At Condition 2 the reverse micelle catalyst was more active and less selective for methane than the aqueous catalyst. These two catalysts also were more selective to alcohols than the reference catalyst. The alumina/titania catalysts seemed to be slightly more active than the magnesium oxide ones at Condition 1.

#### Runs 67 and 77

These two runs used catalysts supported on Carbotrap B which is a high purity, fine mesh carbon. Run 67 (catalyst 585R2796) was discussed in previous technical reports of this project (Reports 7 and 8 covering the period July to September, 1991). The hourly run summary data for Run 77 (catalyst 305R0160) are in Appendix A, Figures 17-24.

Catalyst 305R0160 (Run 77) was the most active of the experimental catalysts screened for this report, in spite of this it was not as active as the reference catalyst. These catalysts also exhibited high selectivity to methane at all test conditions. Catalyst 305R0160 was the only one of the experimental catalysts which exhibited the low alcohol selectivity of the reference catalyst. Comparison of runs 67 and 77 indicate that reverse micelle impregnation of Carbotrap B did not produce a catalyst that is less selective to methane at condition 1 than simple aqueous impregnation.

#### Summary and Implications for Further Work

In this report and the three before it progress has been reviewed toward finding a support for cobalt/ruthenium-based Fischer-Tropsch catalysts. Of the support materials investigated three have so

far shown promise: magnesium oxide, carbon and 50/50 alumina/titania. However, as yet catalysts supported on these three materials have proven inferior to the reference TC 211 Y zeolite-supported catalyst with regard to both activity and selectivity. Ruthenium is considered to be a promoter of activity, however, if this effect is manifested in the experimental catalysts it is not enough to make the catalysts more active than the ruthenium free reference catalyst. The advantages due to reverse micelle are, so far, minimal at best.

When the experimental catalysts were operated at higher conversions through evaluation at Conditions 2 and 3, the magnesium oxide-supported catalysts appeared to be closest to the desired low methane selectivity of the reference catalyst at similar conversion.

The catalysts prepared on the above supports were not superior to the reference catalyst TC 211. Since the main objective of the current contract is to determine whether cobalt/ruthenium catalysts can be prepared which are superior to cobalt only catalysts, the Y zeolite support will be used in the future. In this special Y zeolite-derived support crystallite size is controlled by the pore size distribution. Thus, the catalyst development objective of controlling the crystallite size will be achieved.

In the following quarters, work carried out on the cobalt and cobalt/ruthenium catalysts supported on the Y zeolite-derived support will be reported.



**Table 1**  
Operating Conditions for the Three Condition Test

Key Variables	Condition 1	Condition 2	Condition 3
Pressure, psig	287	287	287
Temperature, °C	211	231	231
FEED RATE, (NL/hr g Co)	4.9	4.9	2.5

**Table 2**  
Composition of Catalyst Precursors  
by Atomic Absorption Spectroscopy and Stem

Run No.	Catalyst No.	Support	AAS, wt-%	Crystallites Size, Å	Element. Anal., wt-%
65	TC 211	Steamed, acid-washed Y zeolite	Co, 8.3; Mn, 1.3; Zr, 1.0	50-100	Co, 19.9; Mn, 3.7; Zr, 3.7
63	585R2757 <sup>1</sup>	Ultra pure MgO	Co, 7.3; Mn, 0.61; Zr, 0.93; Ru, 1.2		
69	585R2810 <sup>2</sup>	Ultra pure MgO	Co, 8.0; Ru, 0.84	100-200	Co, 14.4; Ru, 1.0
72	305R0142 <sup>2</sup>	Ultra pure MgO	Co, 7.5; Mn, 0.60; Zr, 0.90; Ru, 0.17		
68	585R2775 <sup>1</sup>	Al <sub>2</sub> O <sub>3</sub> /TiO <sub>2</sub> , 50/50	Co, 2.7; Ru, 0.49		
73	305R0134 <sup>2</sup>	Al <sub>2</sub> O <sub>3</sub> /TiO <sub>2</sub> , 50/50	Co, 7.5; Ru, 0.3		
67	585R2796 <sup>1</sup>	Carbotrap B	Co, 5.8; Ru, 1.0		
77	305R0160 <sup>2</sup>	Carbotrap B	Co, 13.6; Ru, 1.1		

<sup>1</sup> Reverse micelle impregnation

<sup>2</sup> Aqueous impregnation

**Table 3**  
**Activity and Hydrocarbon Selectivity of Catalysts**

Run No.	Test Conditions	CO Conv., %	Hydrocarbon Selectivity, %				
			C <sub>1</sub>	C <sub>2</sub>	C <sub>3</sub> =	C <sub>2</sub>	C <sub>3</sub> =
65	1	58	7	0.6	0	1.7	2.0
63	1	18	15	0	0	2.5	7.0
69	1	10	13	0	0	3.0	5.0
	2	30	13	1.3	0.3	2.4	5.5
	3	50	11	1.5	0.8	1.2	6.2
72	1	8	19	3.0	0	4.5	9.0
	2	28	16	2.6	0.6	3.5	7.5
	3	99	9	1.7	0	3.1	1.0
68	1	20	21	5.2	0	8.5	2.5
	2	33	35	6.0	0	11.0	1.3
73	1	20	15	3.0	0	4.0	1.0
	2	22	75	13.0	0	22.0	2.0
	3	100	37	6.0	0	8.0	0
67	1	25	22	1.8	0	3.5	4.2
	2	50	20	1.9	0	4.0	3.7
	3	60	18	1.8	0	3.7	3.5
77	1	40	15	1.1	0	2.5	3.3
	2	75	20	1.9	0	3.6	4.0
	3	90	24	2.0	0	5.0	4.2

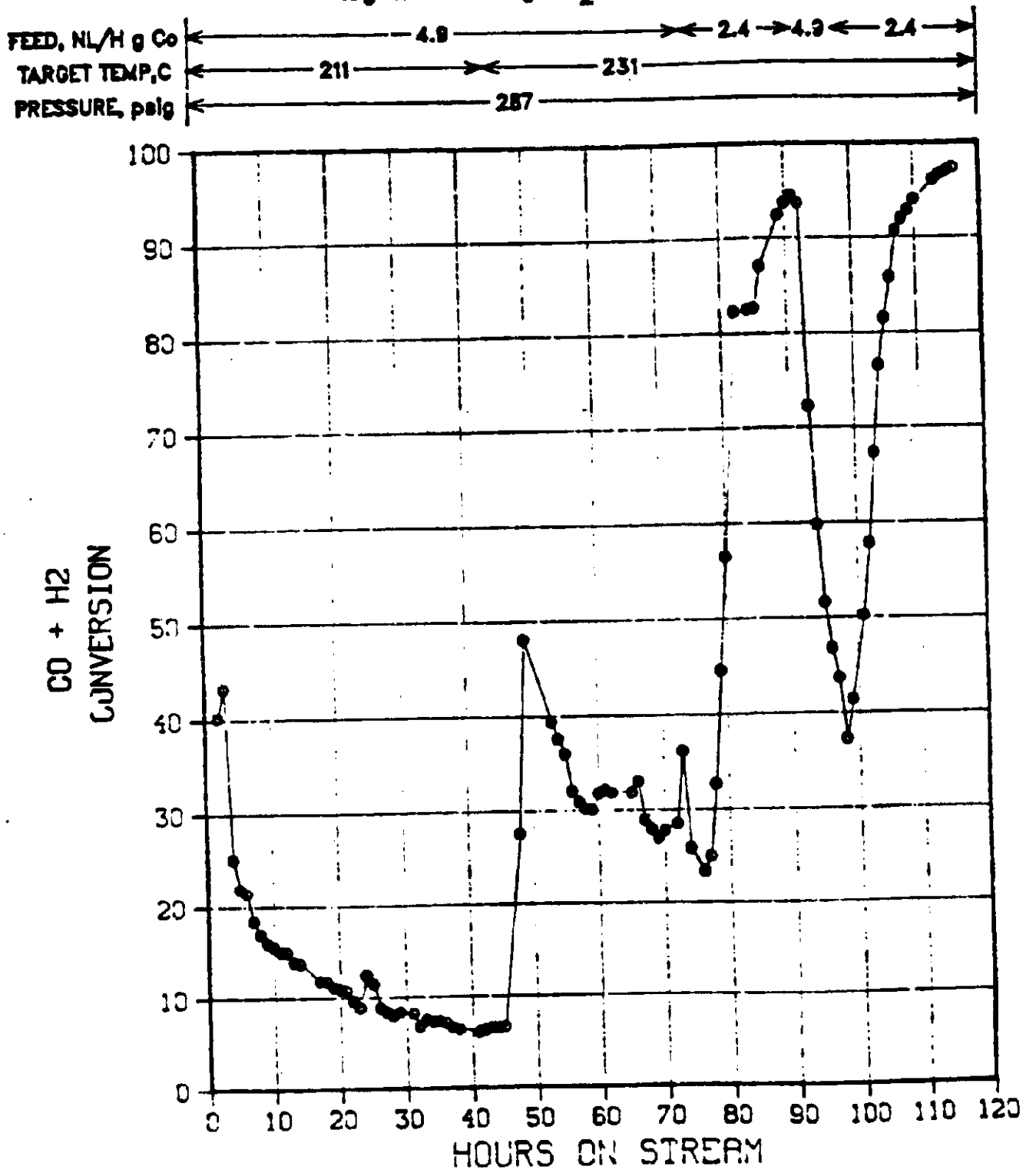
**Table 4**  
**Activity and Alcohol Selectivity of Catalysts**

Run No.	Test Conditions	CO Conv., %	Alcohol Selectivity, %		
			C <sub>1</sub>	C <sub>2</sub>	C <sub>3</sub>
65	1	58	0.5	0.2	0.2
63	1	13	1.6	0	1.0
69	1	10	2.5	0.5	1.6
	2	30	2.4	0.5	1.5
	3	50	1.5	0.5	1.5
72	1	8	0	0	0
	2	28	0	0	0
	3	99	2.0	0.7	1.5
68	1	20	3.8	1.0	1.8
	2	33	3.8	1.5	3.0
73	1	20	0.1	1.0	1.0
	2	22	6.0	4.0	6.0
	3	100	0	0	0
67	1	25	4.0	2.5	7.5
	2	50	2.0	1.1	2.5
	3	60	2.0	1.0	2.5
77	1	40	0.3	0.2	0.3
	2	75	0.3	0.2	0.4
	3	90	0.2	0.15	0.2

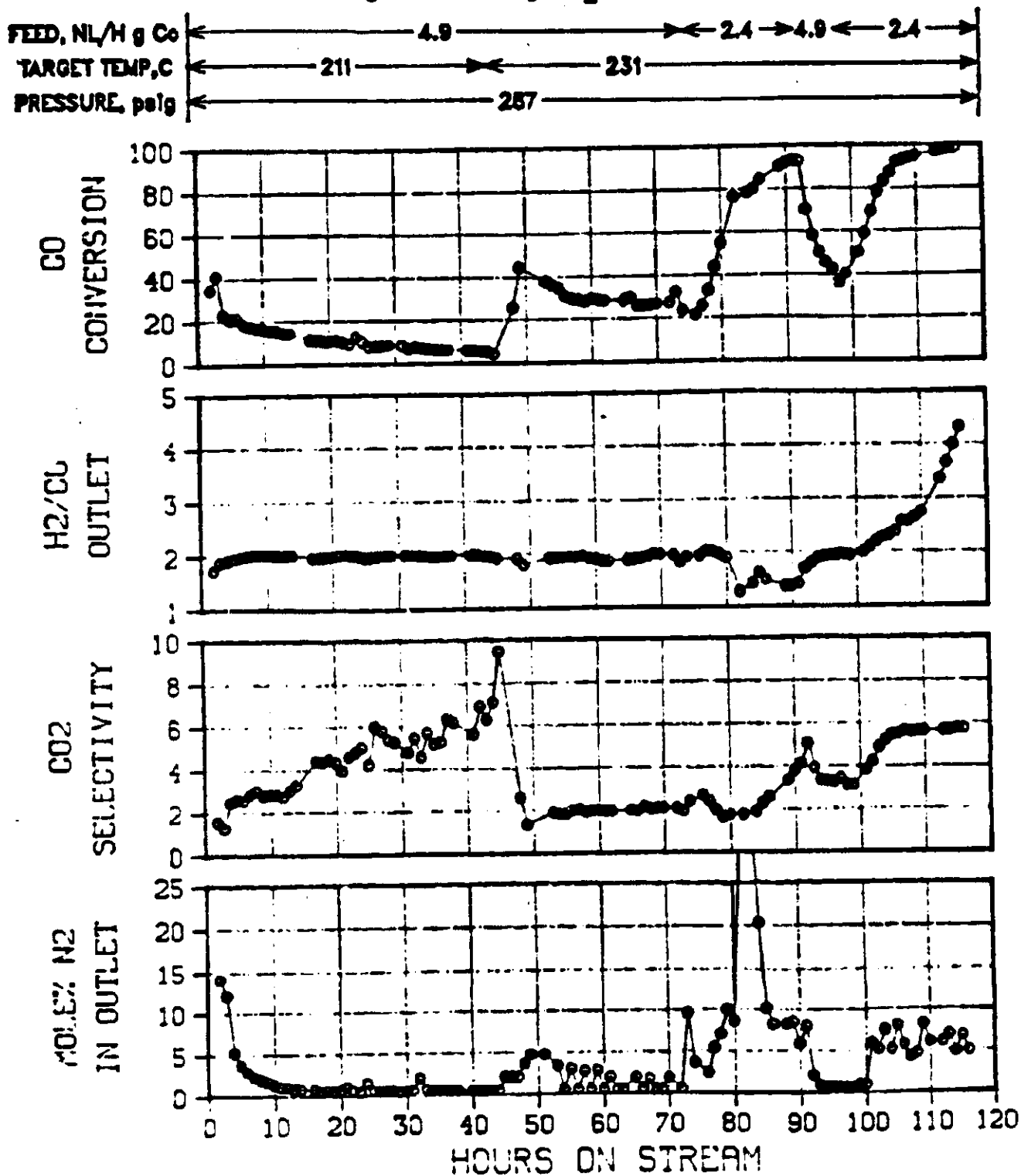
**APPENDIX A**  
**CATALYST PERFORMANCE DATA**  
**RUN SUMMARY**

Figure 1

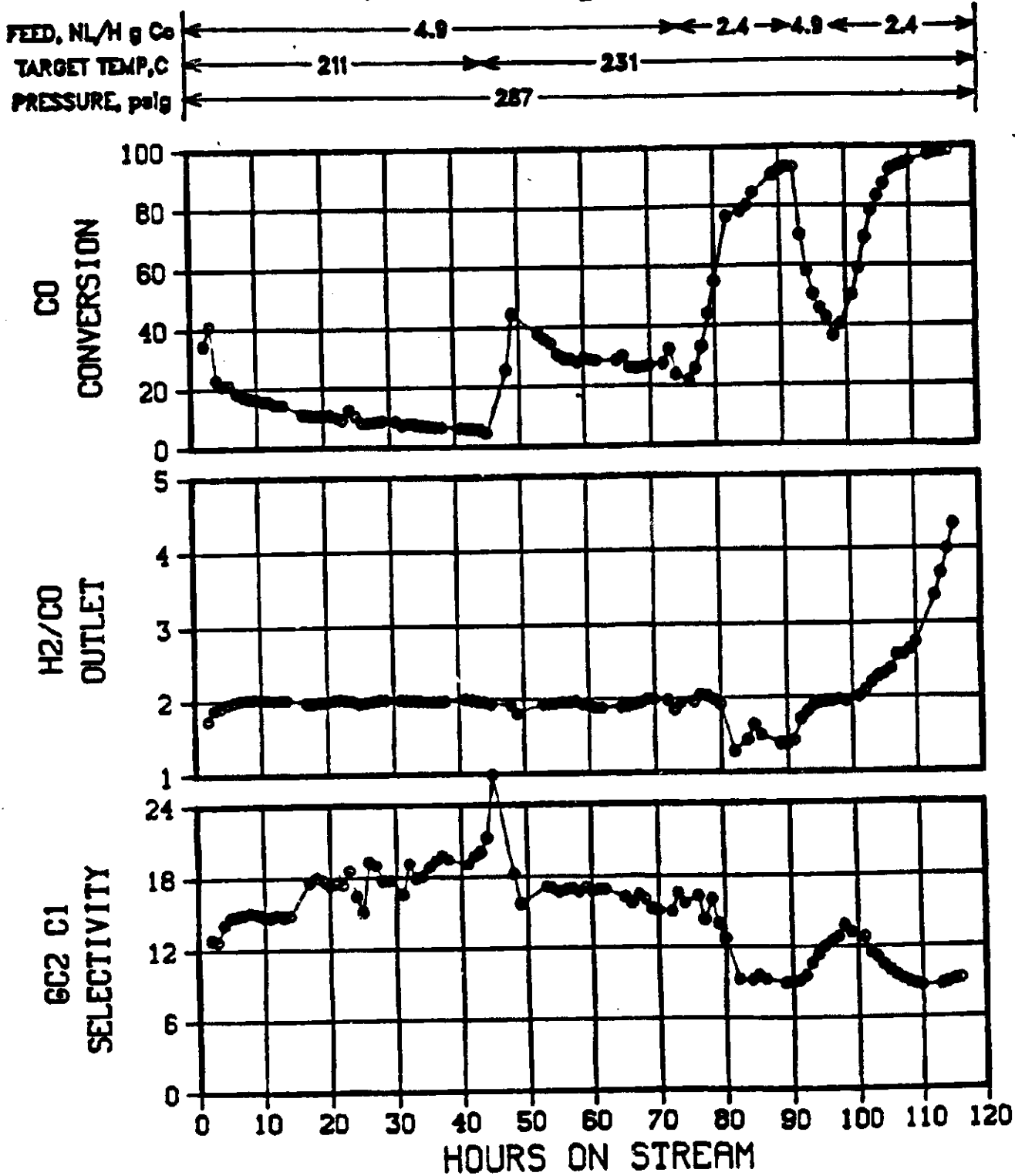
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13g Active in 160g SiO<sub>2</sub> sand



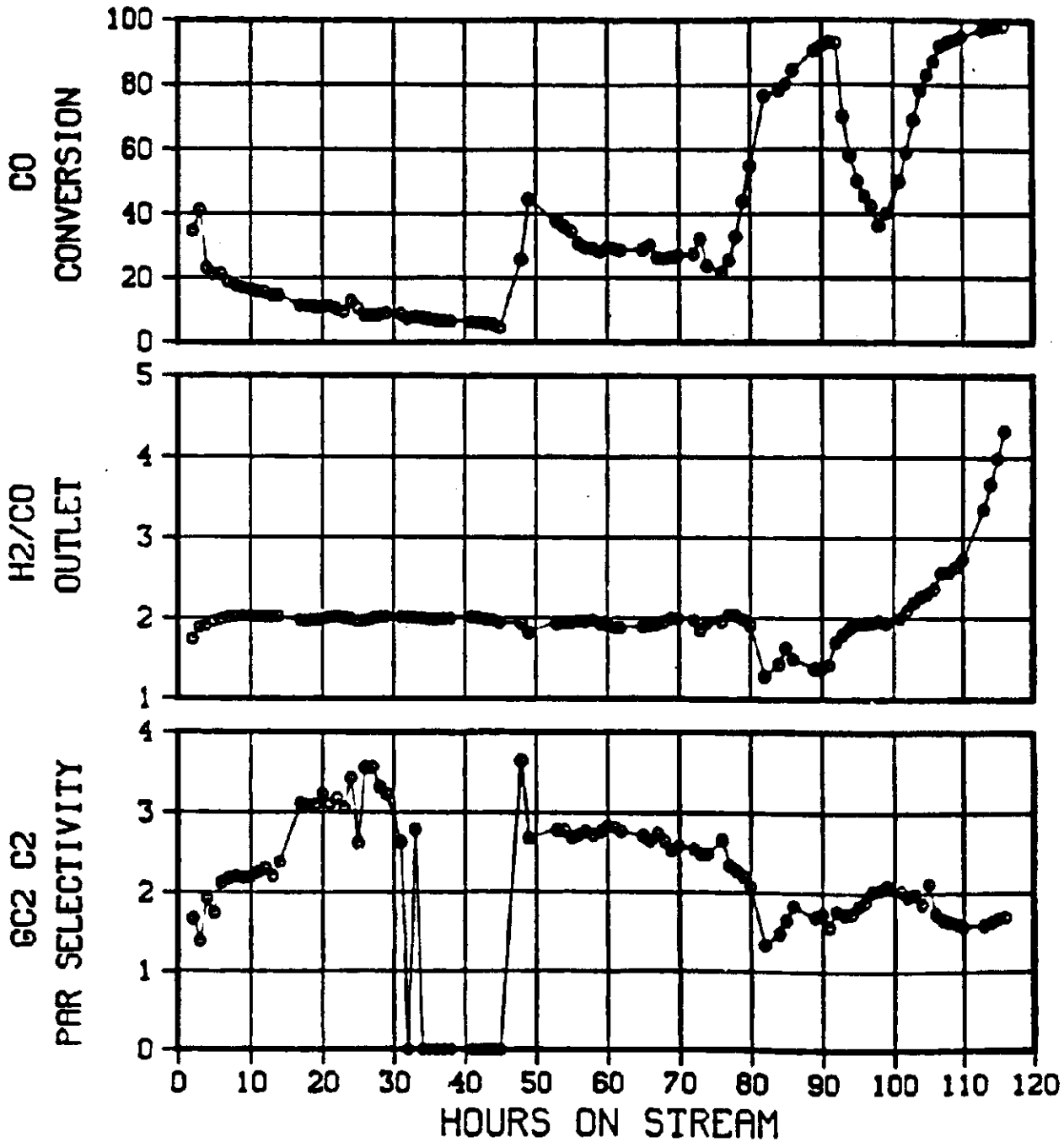
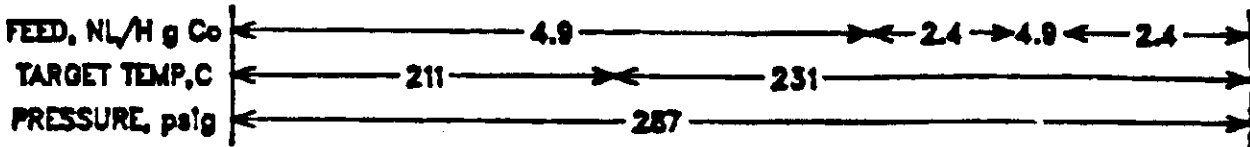
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 13g Active in 160g SiO<sub>2</sub> sand



PLT 700A RUN 72 Co,Ru,Mn,Zr on MgO  
 6531-134 w/7.45% Co via eq. Impreg 2:1 H<sub>2</sub>:CO in feed  
 13g Active in 160g SiO<sub>2</sub> sand

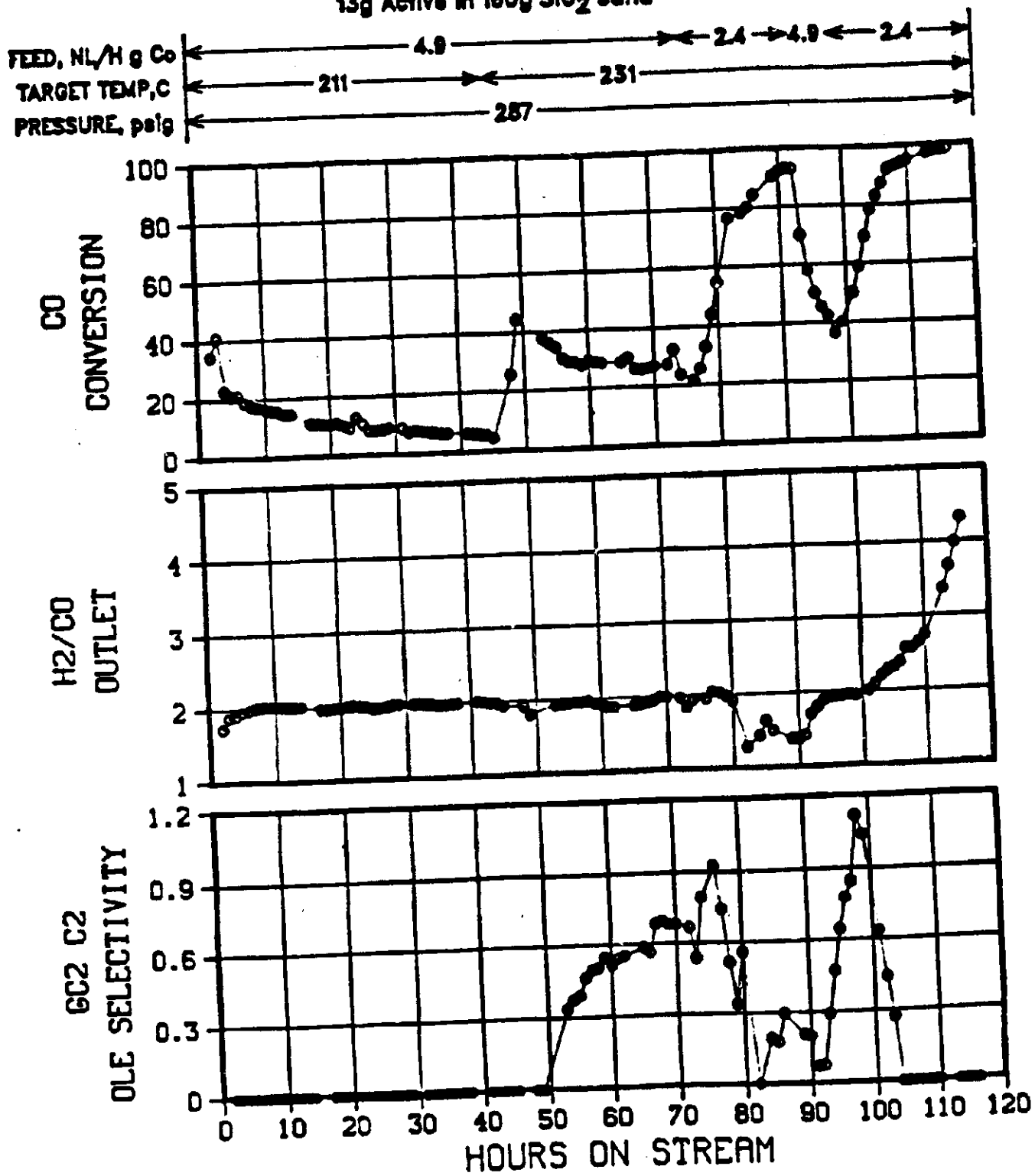


PLT 700A RUN 72 Co,Ru,Mn,Zr on MgO  
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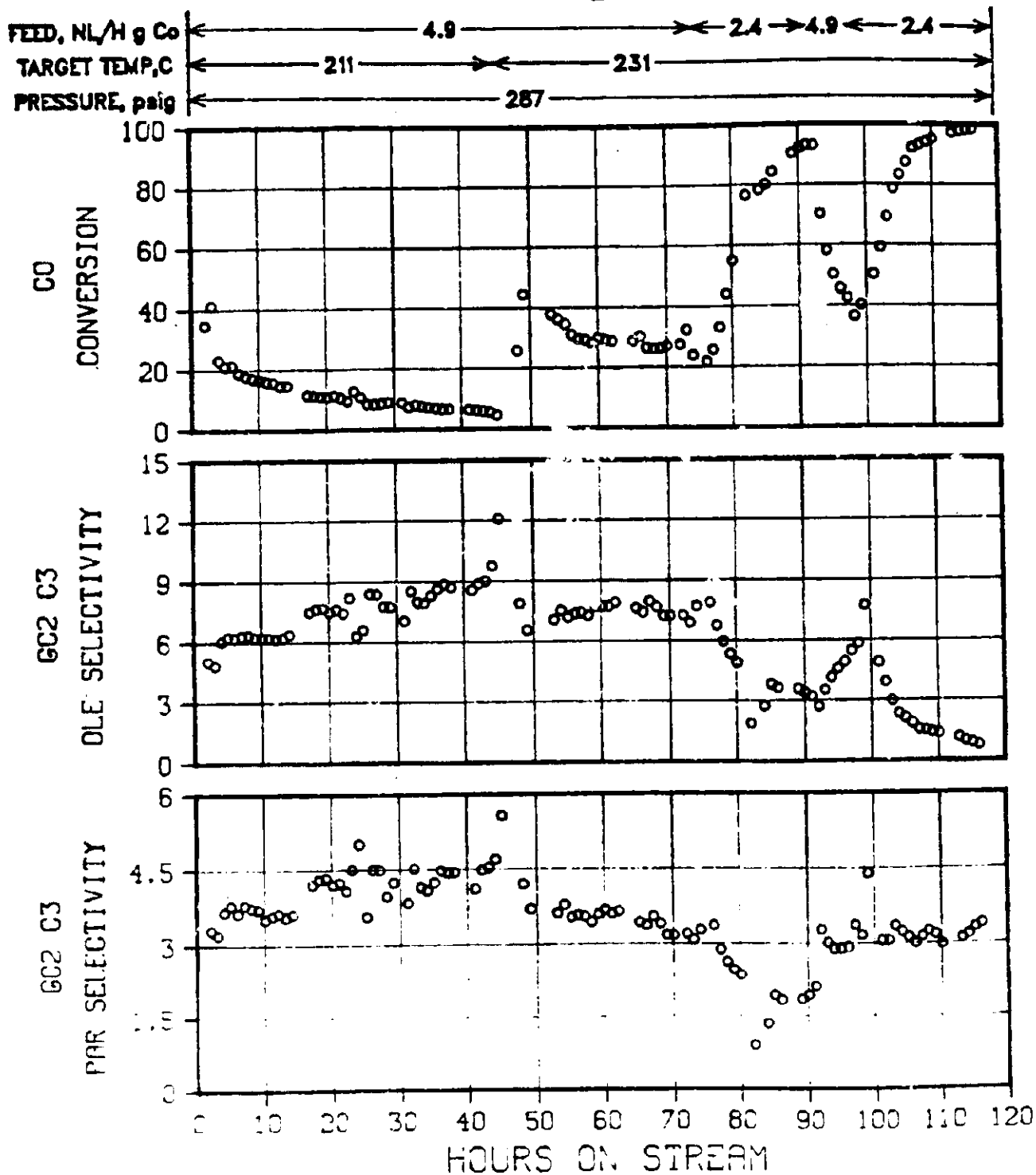




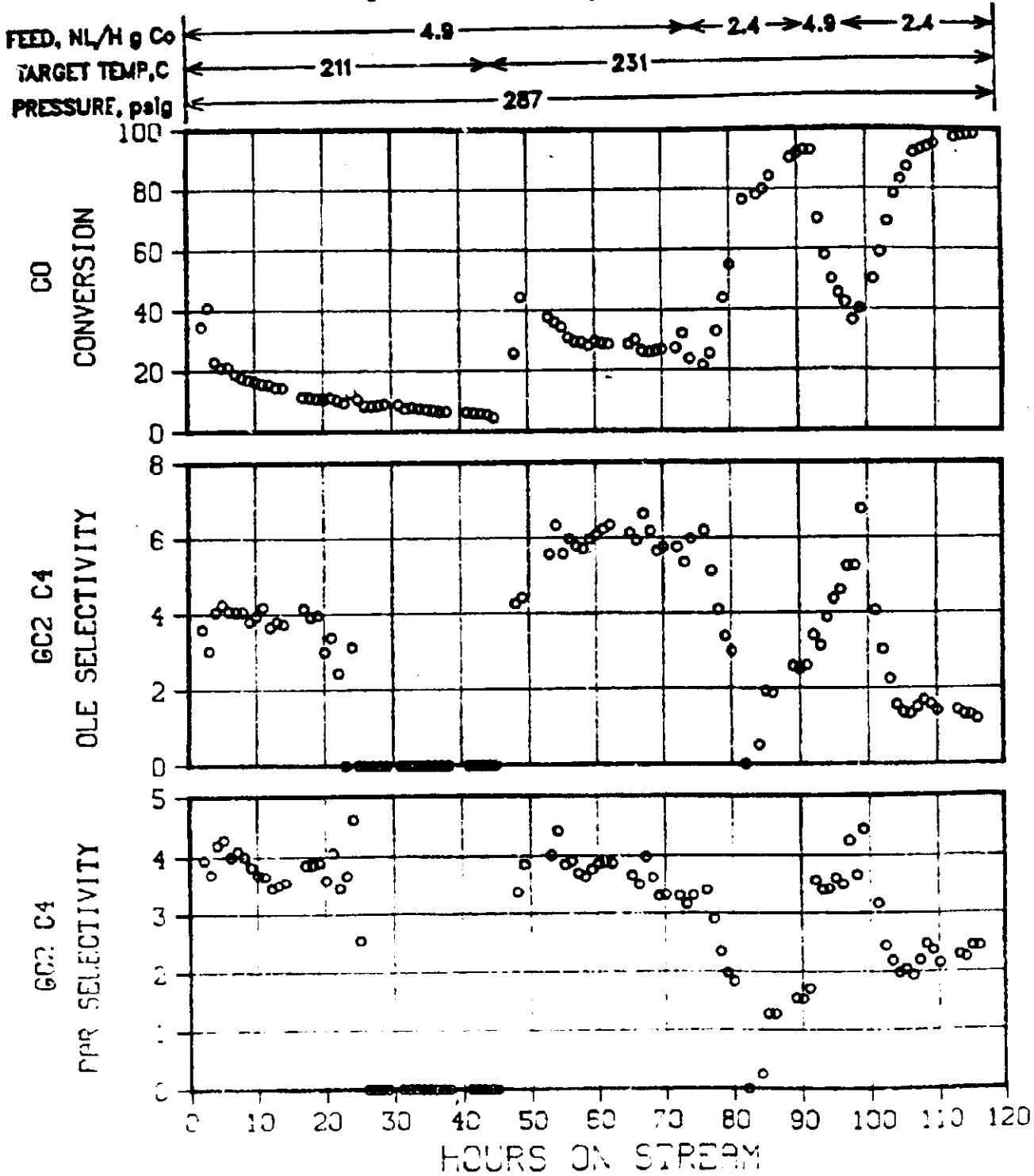
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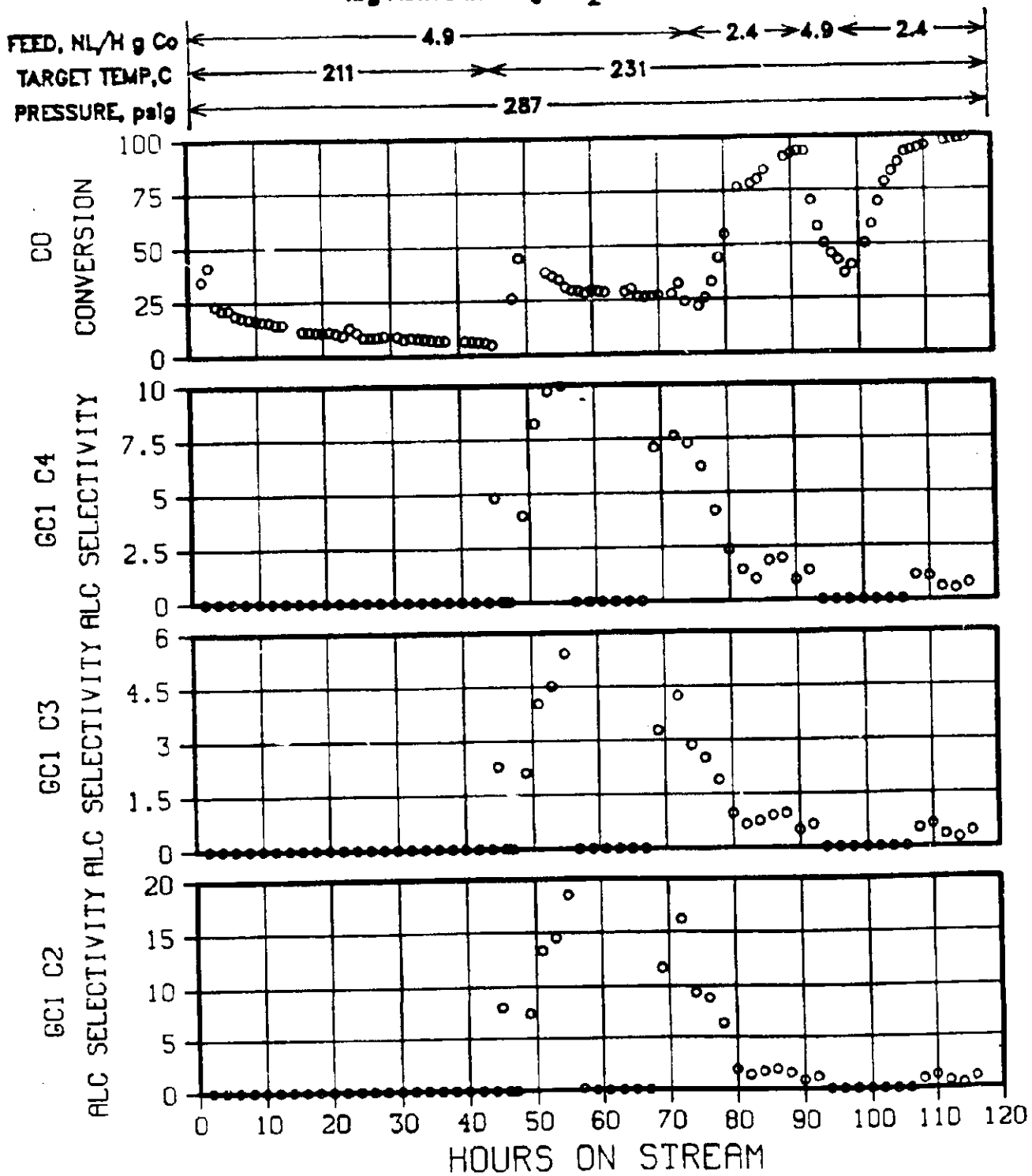
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PLT 700A RUN 72 Co,Ru,Mn,Zr on MgO  
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 13g Active In 160g SiO<sub>2</sub> sand



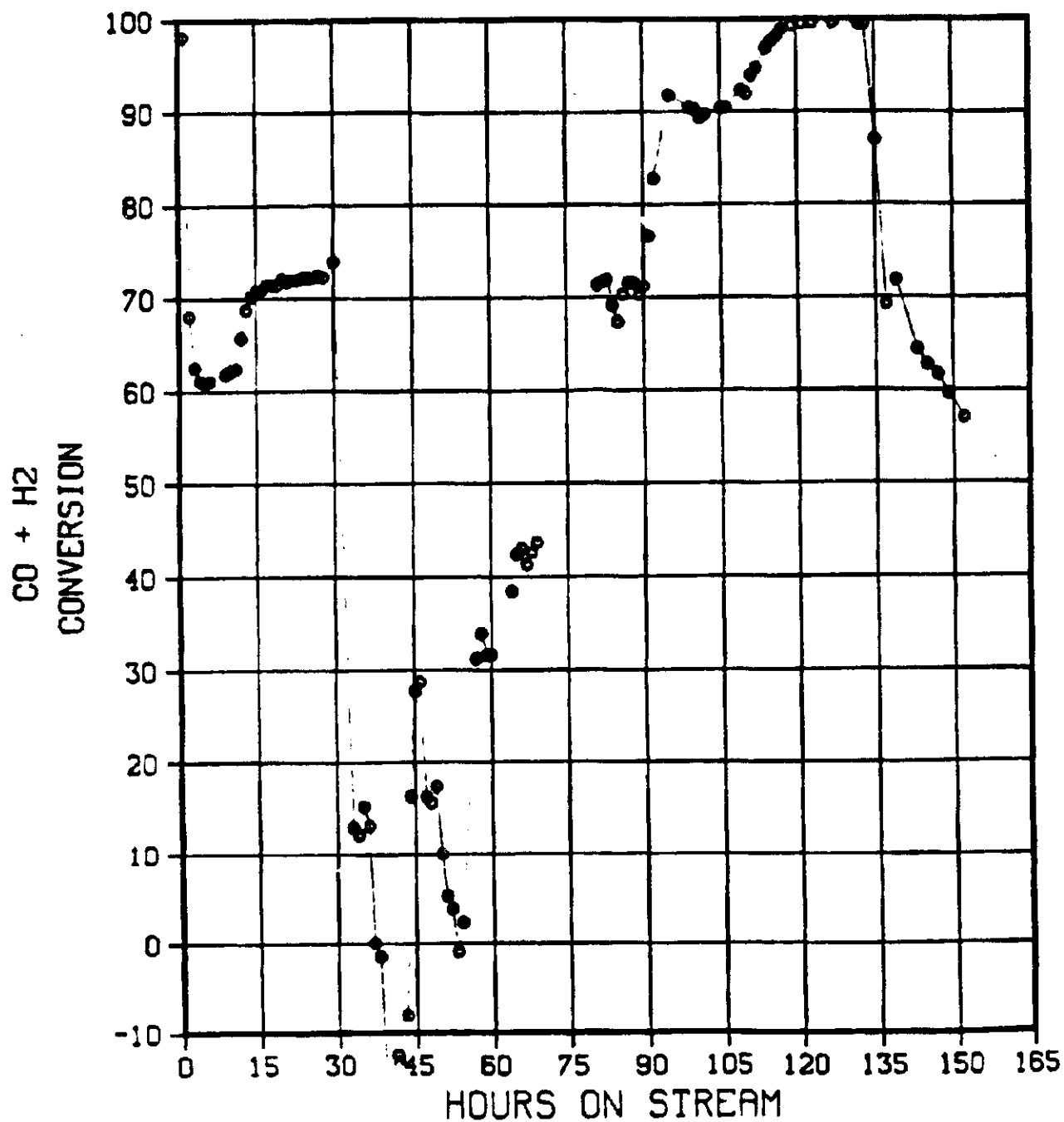
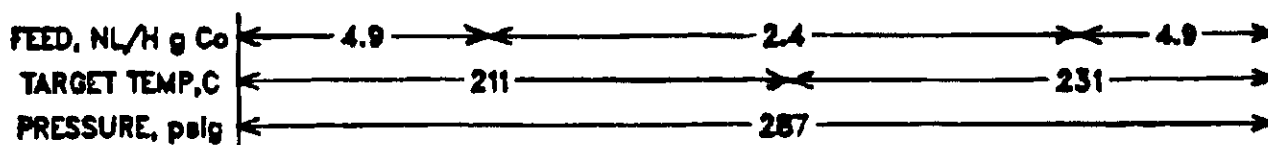
PLT 700A RUN 72 Co,Ru,Mn,Zr on MgO  
 6531-134 w/7.45% Co via aq. Impreg 2:1 H<sub>2</sub>:CO In feed  
 13g Active In 160g SiO<sub>2</sub> sand



# PLT 70JA RUN 73 Co,Ru on 50/50 Al<sub>2</sub>O<sub>3</sub>/TiO<sub>2</sub>

6531-134 w/7.45% Co via aq. Impreg 2:1 H<sub>2</sub>:CO In feed

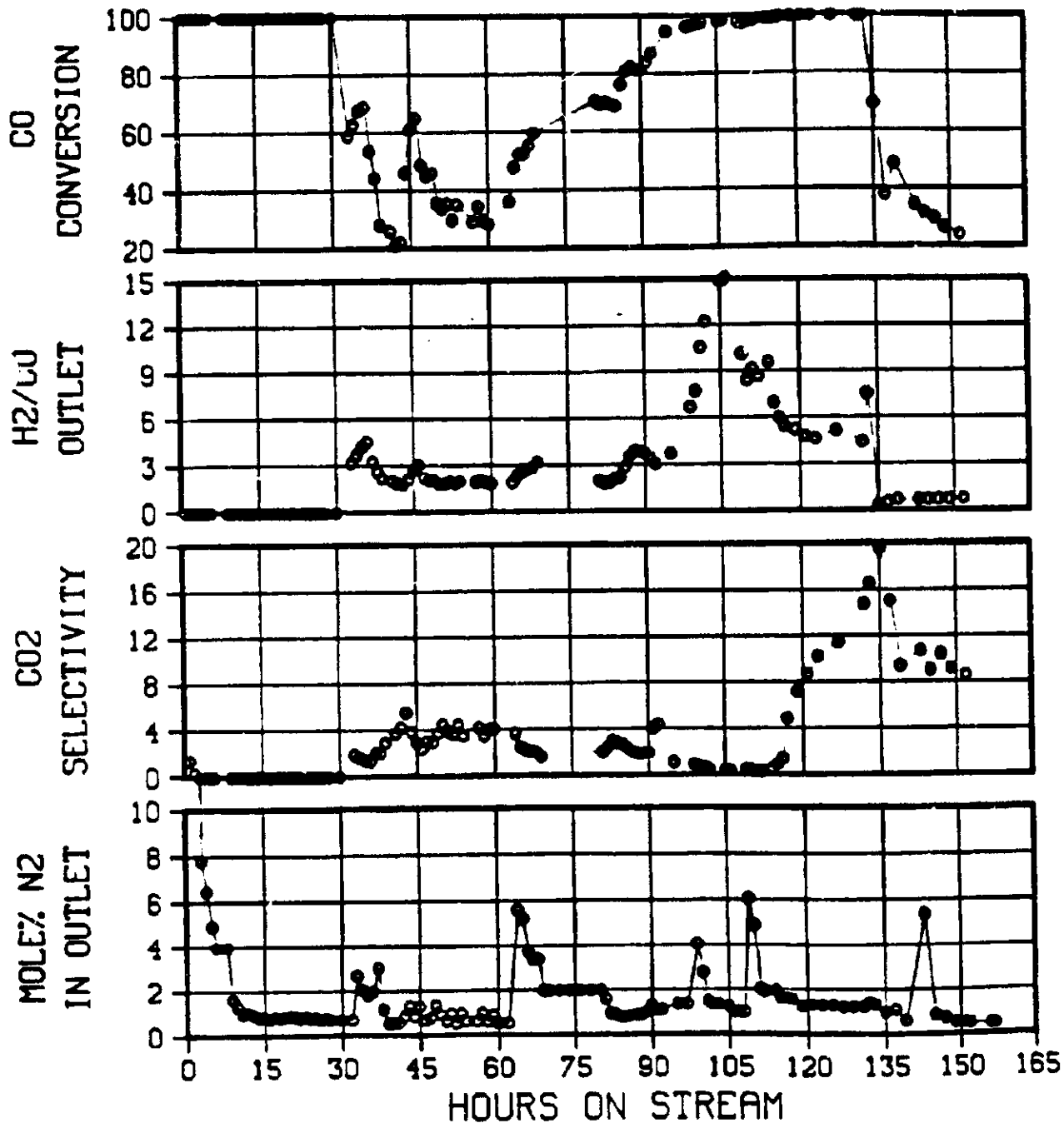
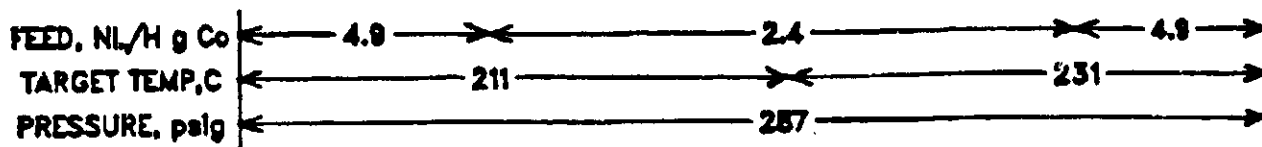
13g Active in 160g SiO<sub>2</sub> sand



# PLT 700A RUN 73 Co,Ru on 50/50 Al<sub>2</sub>O<sub>3</sub>/TiO<sub>2</sub>

6531-134 w/7.45% Co via aq. Impreg 2:1 H<sub>2</sub>:CO in feed

13g Active in 160g SiO<sub>2</sub> sand



PLT 700A RUN 73 Co,Ru on 50/50 Al<sub>2</sub>O<sub>3</sub>/TiO<sub>2</sub>

8531-134 w/7.45% Co via aq. Impreg 2:1 H<sub>2</sub>:CO In feed

13g Active in 180g SiO<sub>2</sub> sand

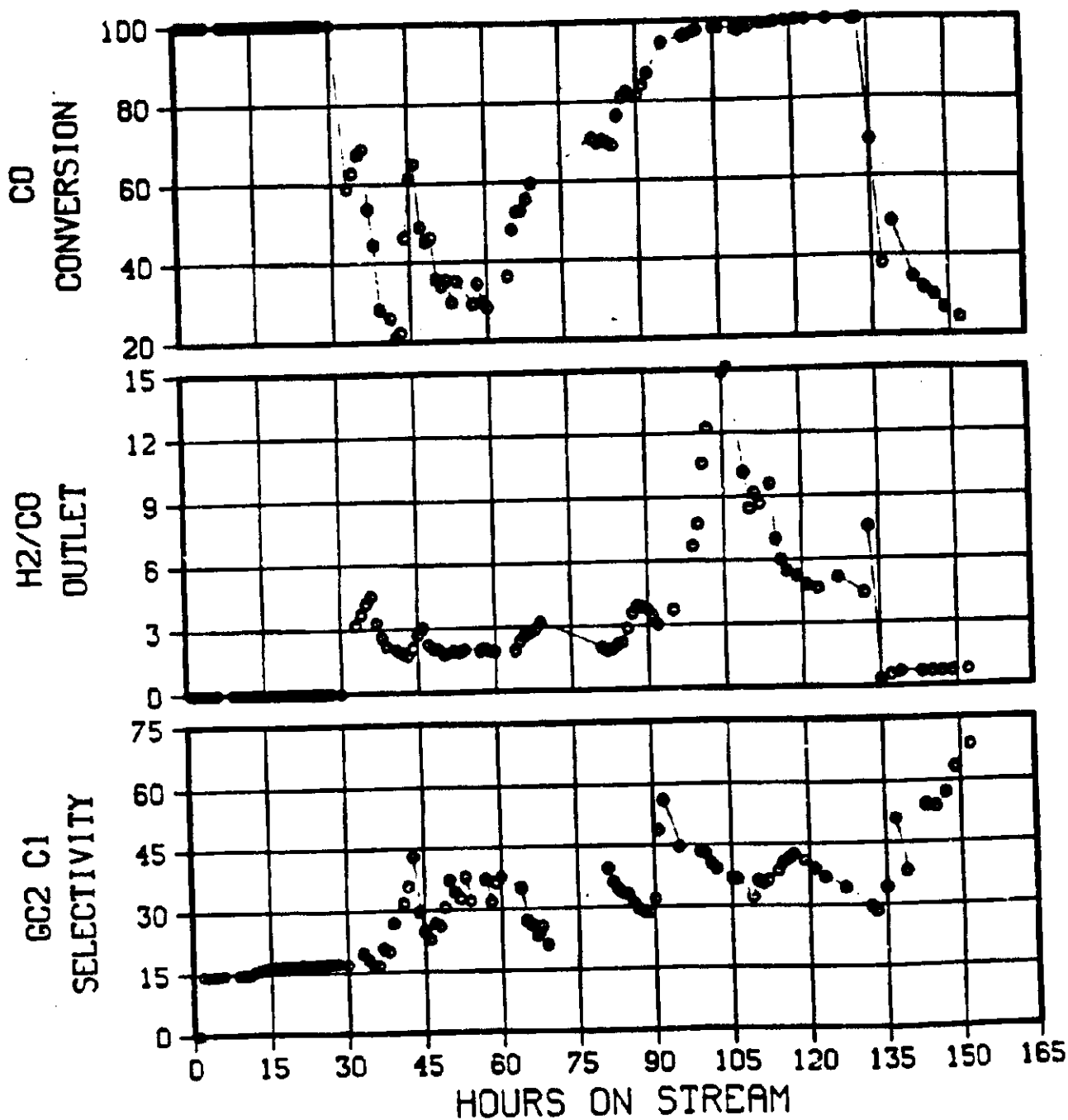
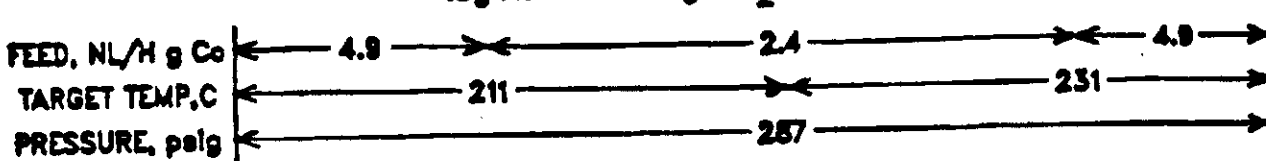


Figure 12

### PLT 700A RUN 73 Co,Ru on 50/50 Al<sub>2</sub>O<sub>3</sub>/TiO<sub>2</sub> 6531-134 w/7.45% Co via aq. Impreg 2:1 H<sub>2</sub>:CO in feed 13g Active in 160g SiO<sub>2</sub> sand

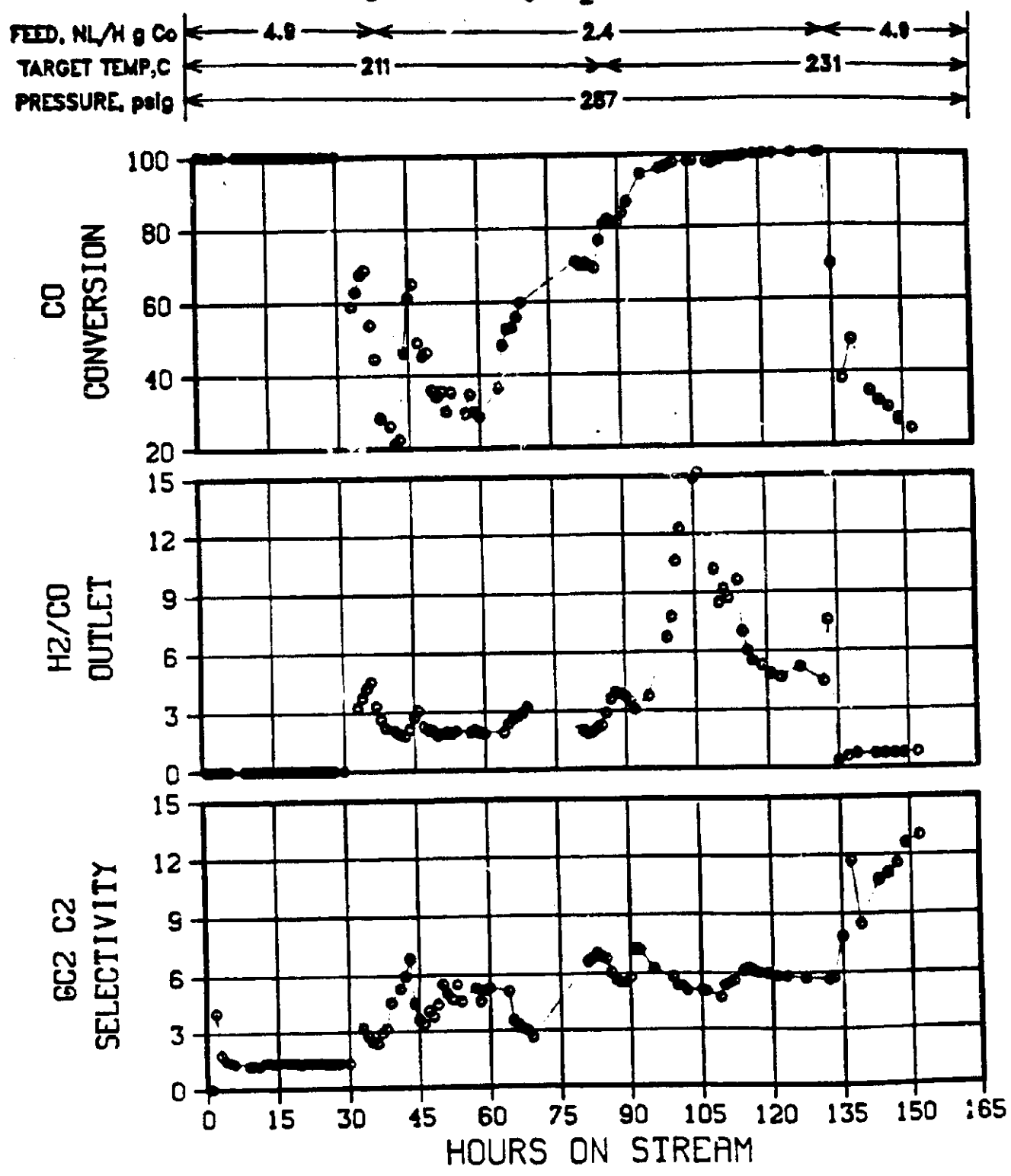




Figure 13

### PLT 700A RUN 73 Co,Ru on 50/50 Al<sub>2</sub>O<sub>3</sub>/TiO<sub>2</sub> 6531-134 w/7.45% Co via aq. Impreg 2:1 H<sub>2</sub>:CO In feed 13g Active In 160g SiO<sub>2</sub> sand

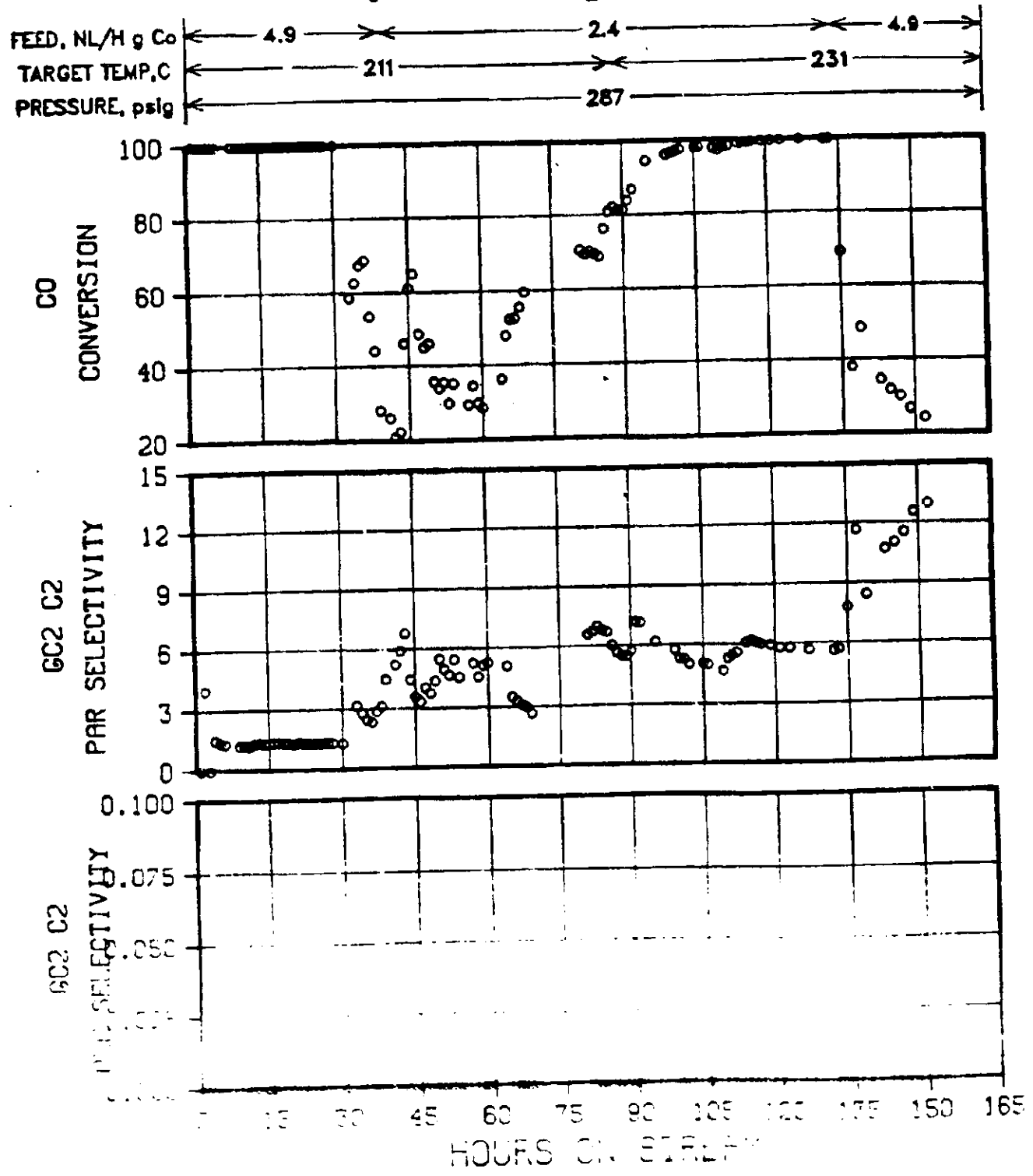


Figure 14

PLT 700A RUN 73 Co,Ru on 50/50 Al<sub>2</sub>O<sub>3</sub>/TiO<sub>2</sub>  
6531-134 w/7.45% Co via aq. impreg 2:1 H<sub>2</sub>:CO in feed  
13g Active in 160g SiO<sub>2</sub> sand

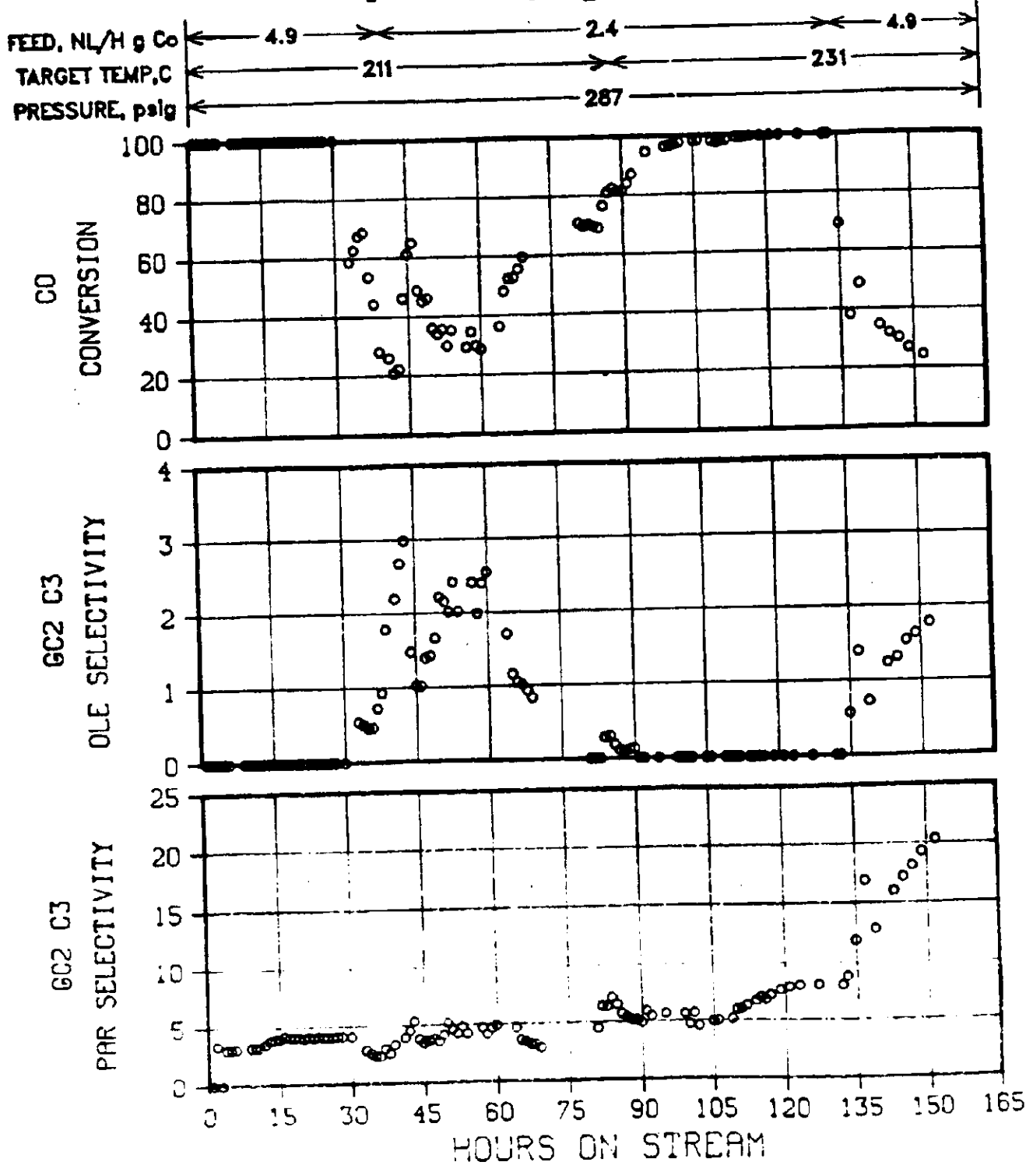


Figure 15

### PLT 700A RUN 73 Co,Ru on 50/50 Al<sub>2</sub>O<sub>3</sub>/TiO<sub>2</sub>

6531-134 w/7.45% Co via aq. Impreg 2:1 H<sub>2</sub>:CO In feed

13g Active in 160g SiO<sub>2</sub> sand

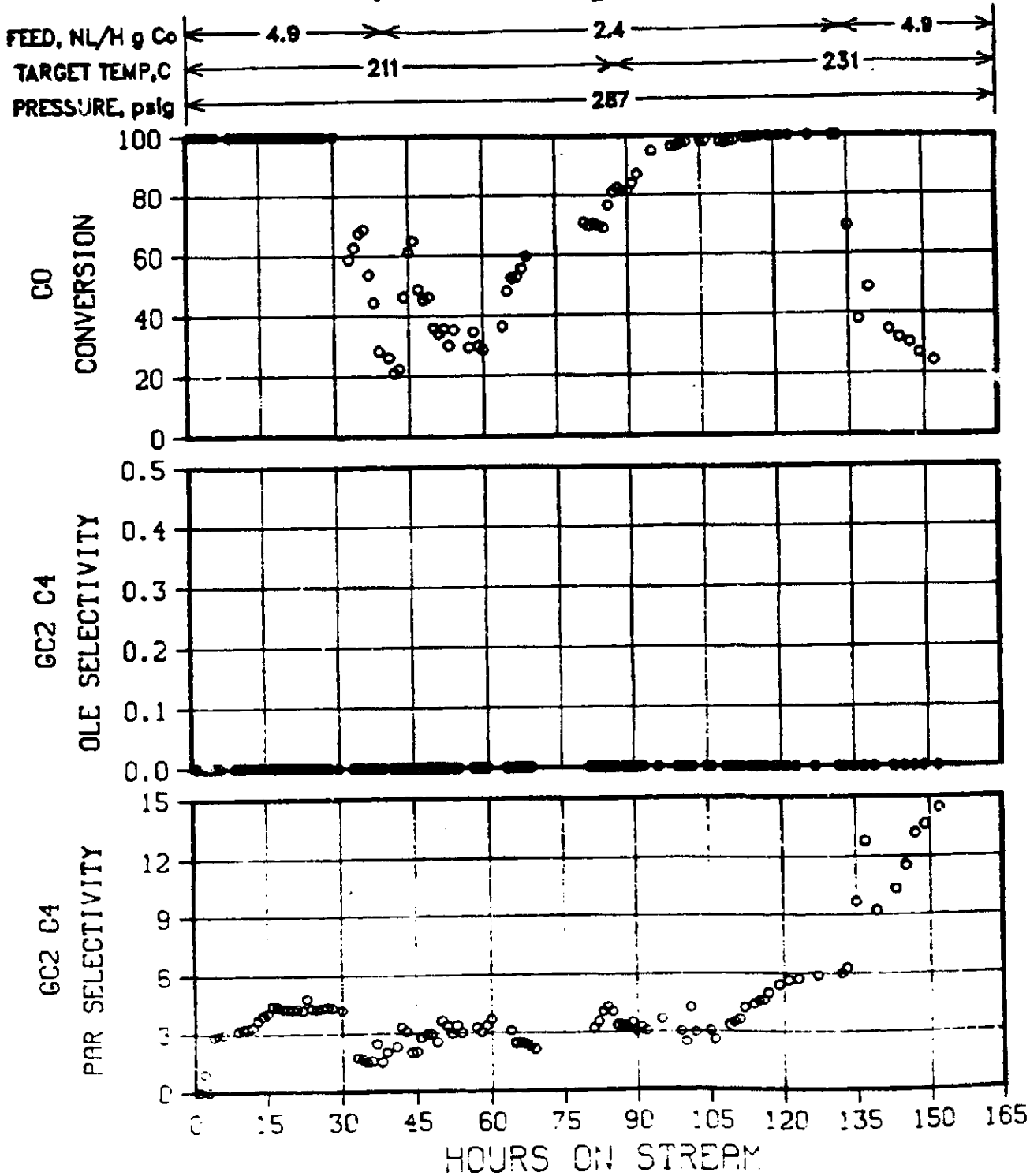
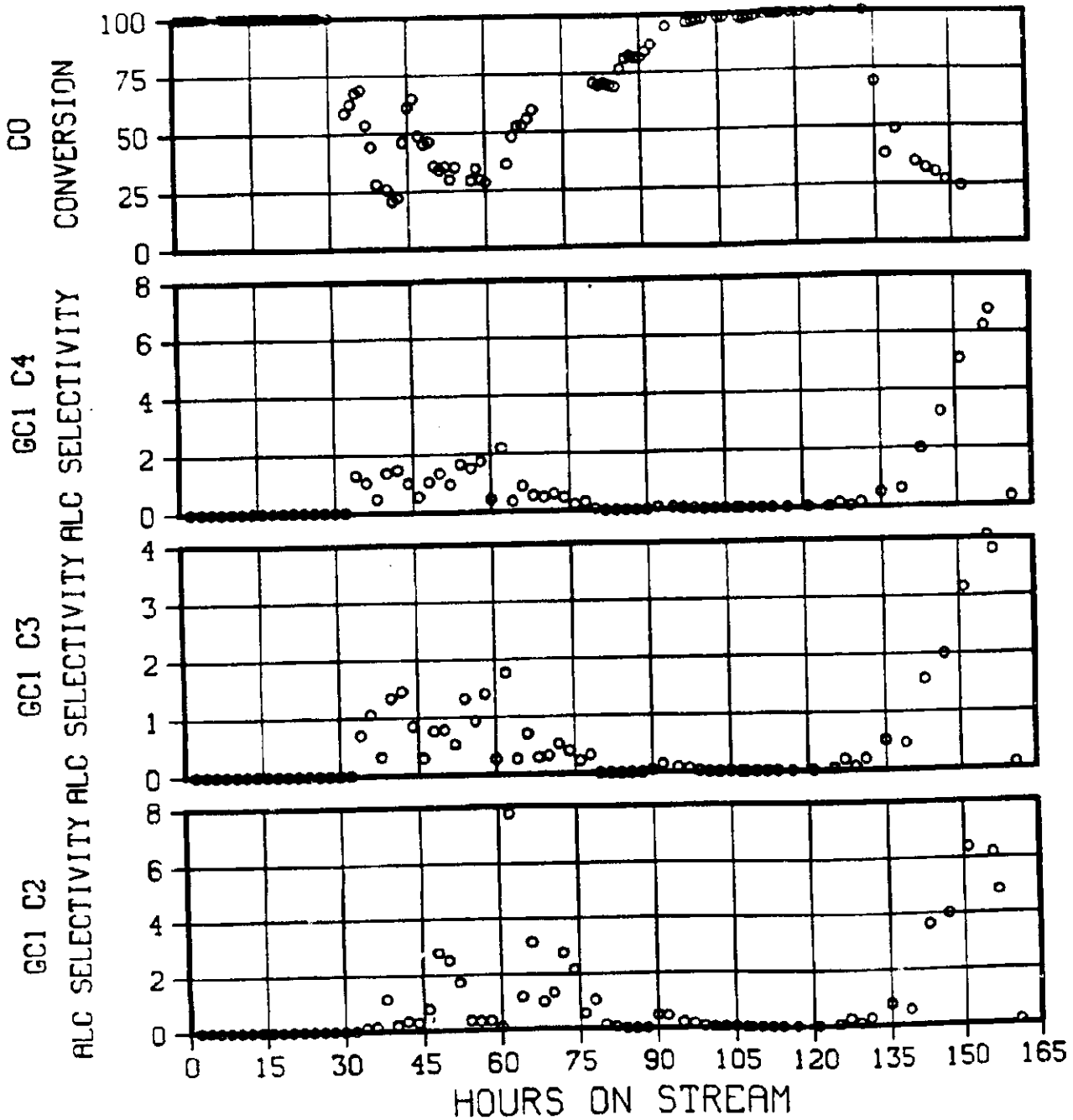
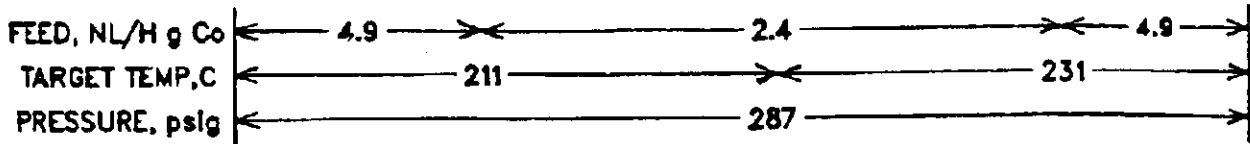


Figure 1b

PLT 700A RUN 73 Co,Ru on 50/50 Al<sub>2</sub>O<sub>3</sub>/TiO<sub>2</sub>  
6531-134 w/7.45% Co via aq. impreg 2:1 H<sub>2</sub>:CO in feed  
13g Active in 160g SiO<sub>2</sub> sand



PLT 700A RUN 77 Co,Ru on Carbotrap B  
 6531-160 w/13.6 % Co via aq. Impreg 2:1 H<sub>2</sub>:CO in feed  
 13g active in 160g quartz sand

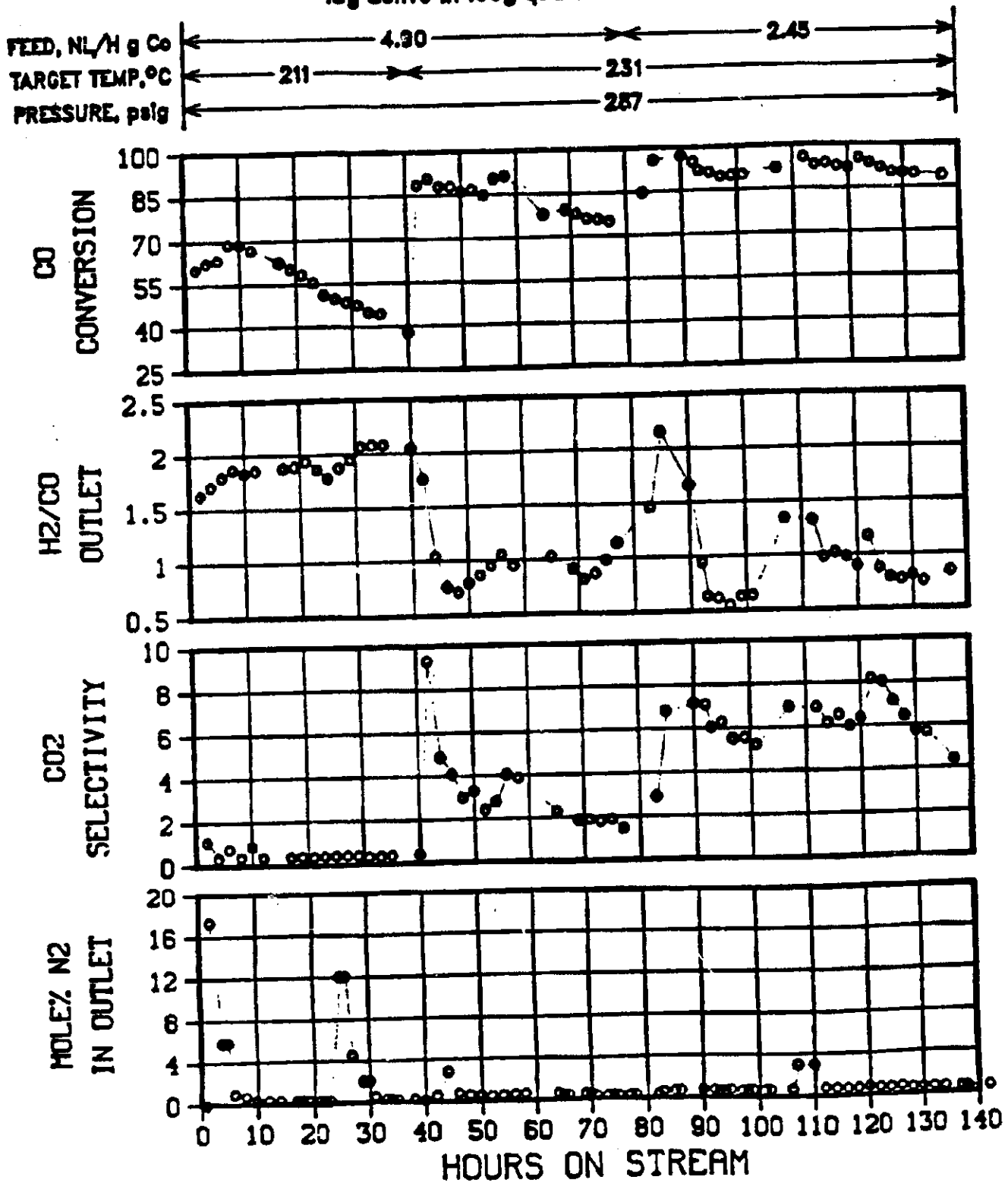
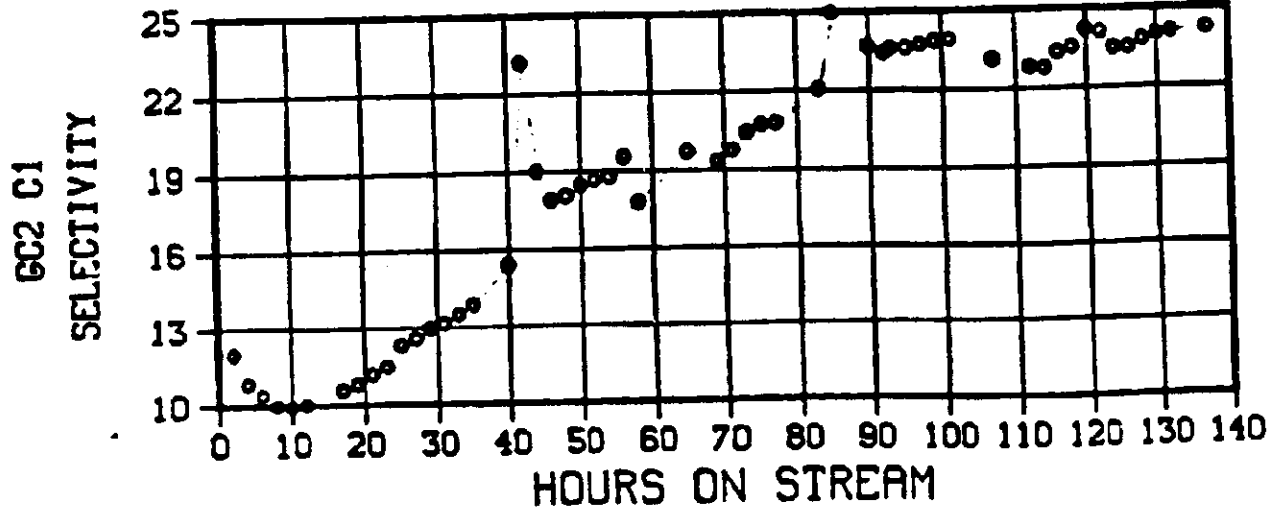
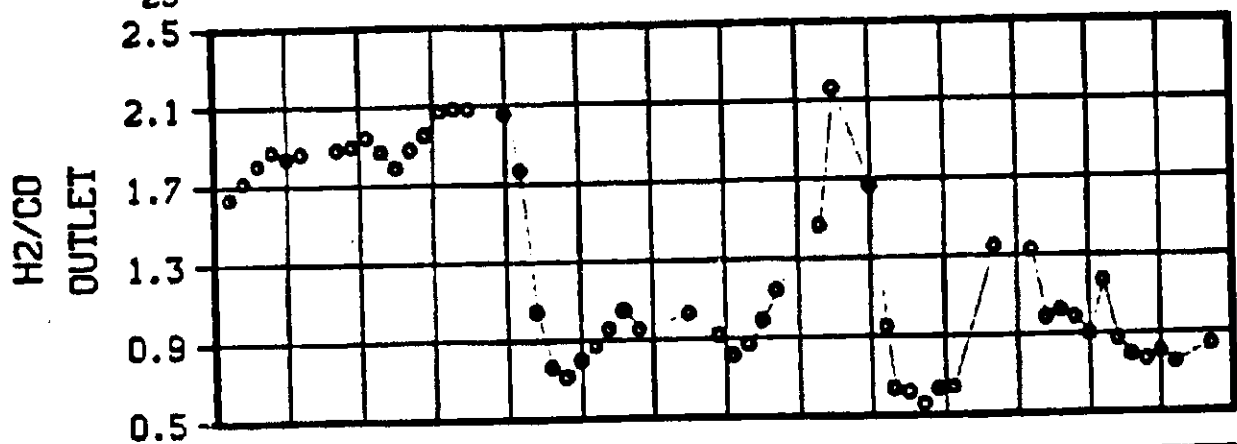
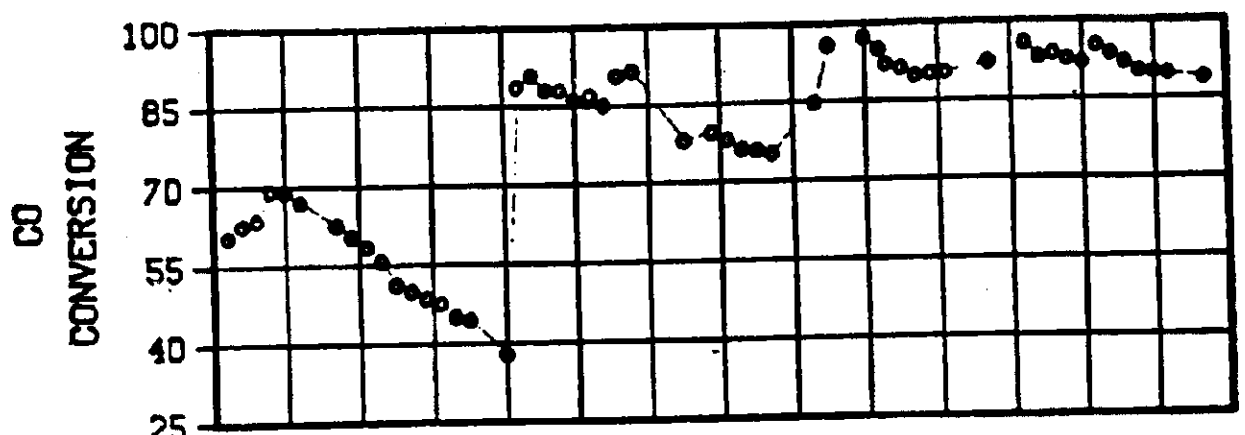
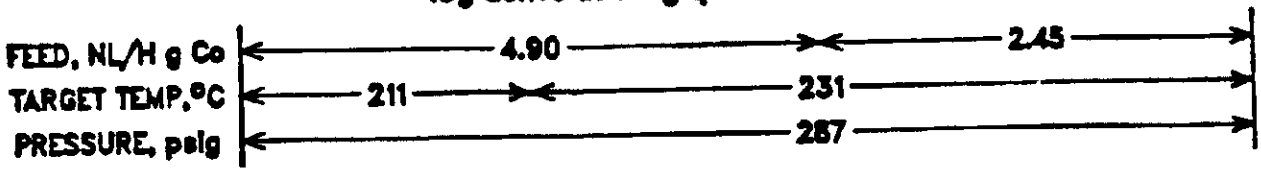


Figure 13

### PLT 700A RUN 77 Co,Ru on Carbotrap B

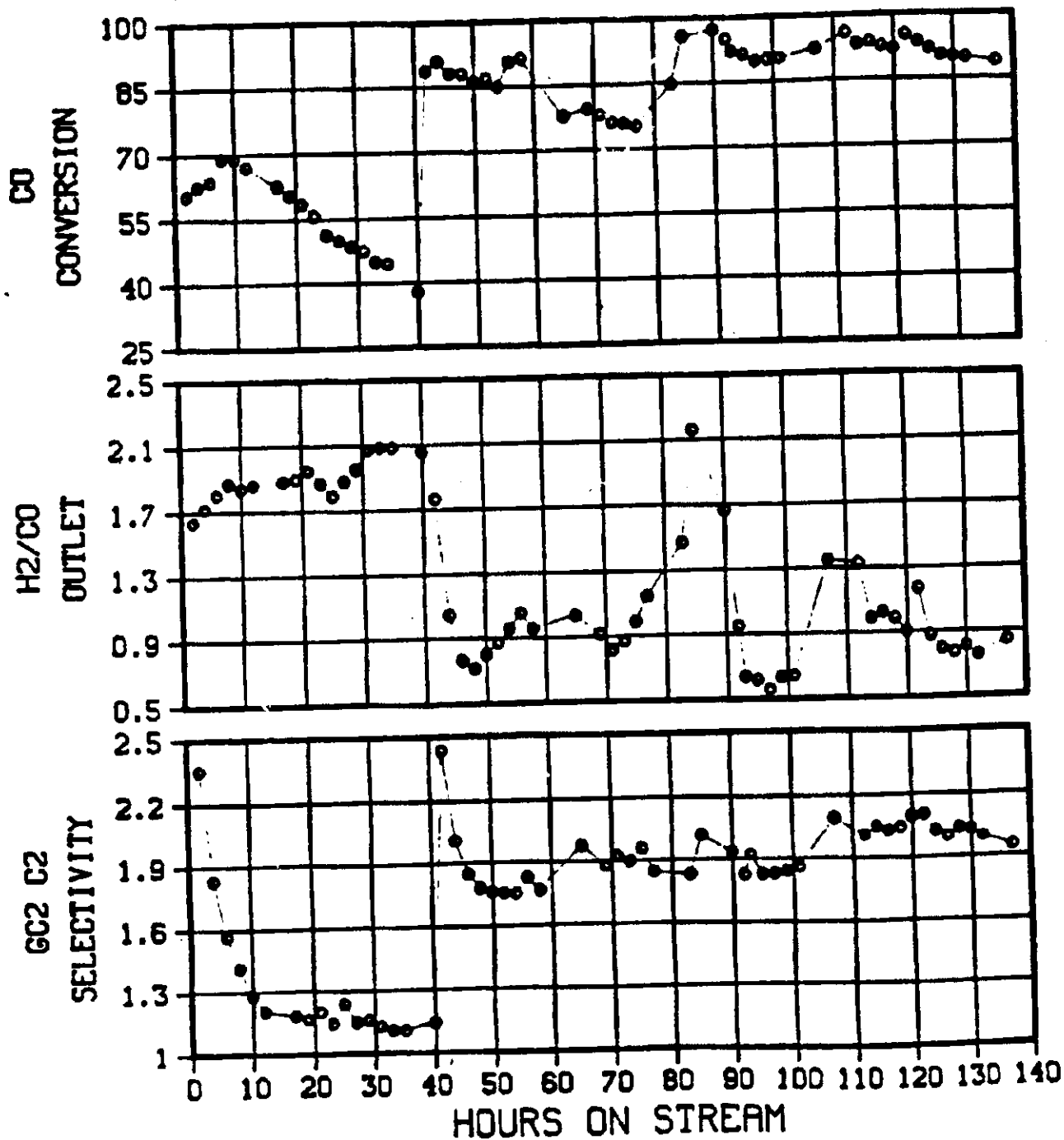
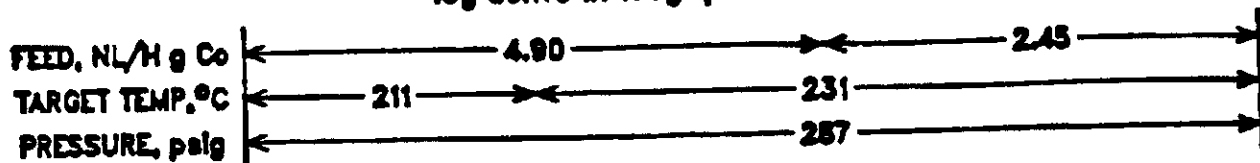
6531-160 w/13.6 % Co via aq. Impreg 2:1 H<sub>2</sub>:CO in feed  
13g active in 160g quartz sand



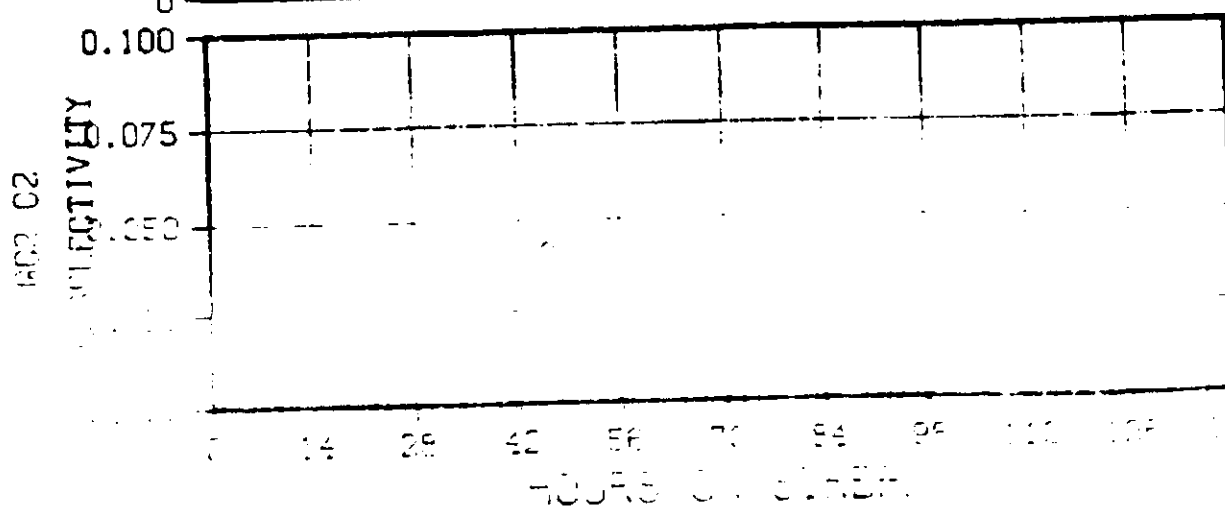
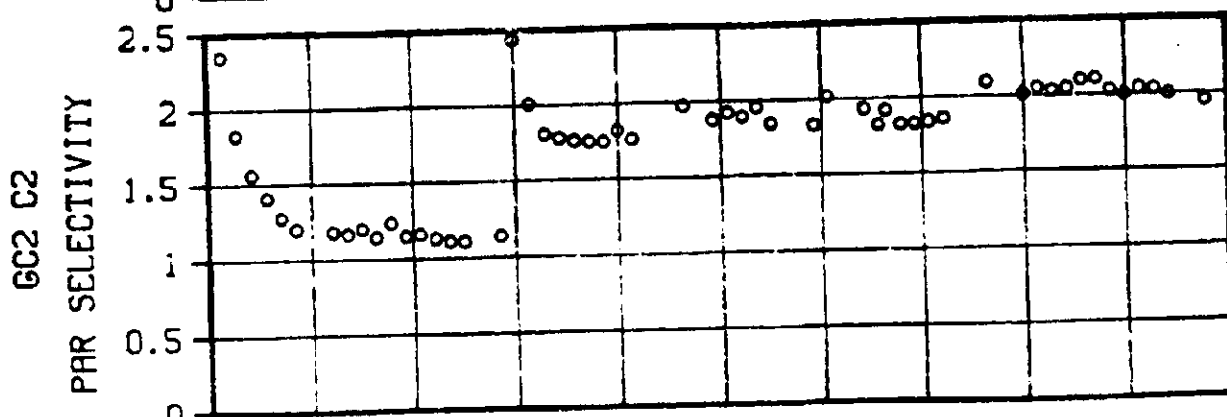
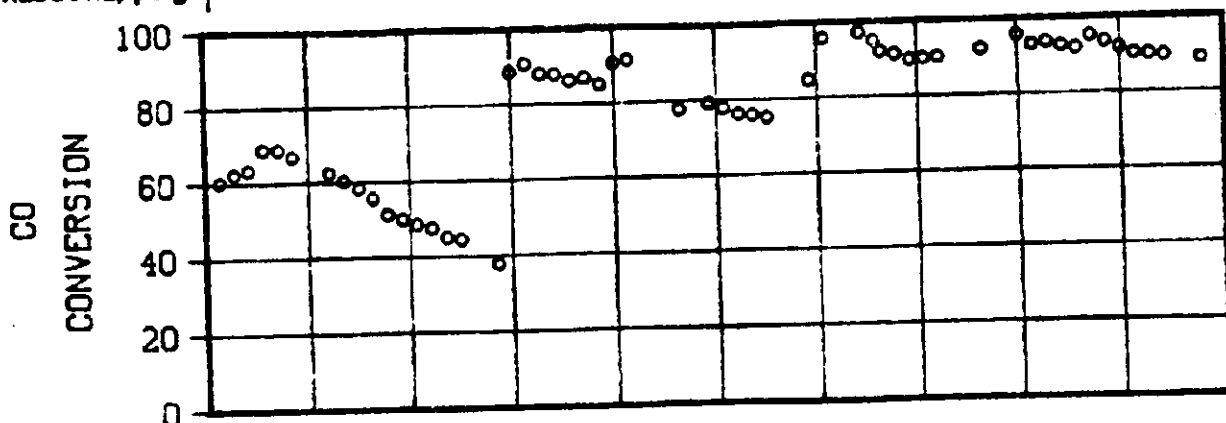
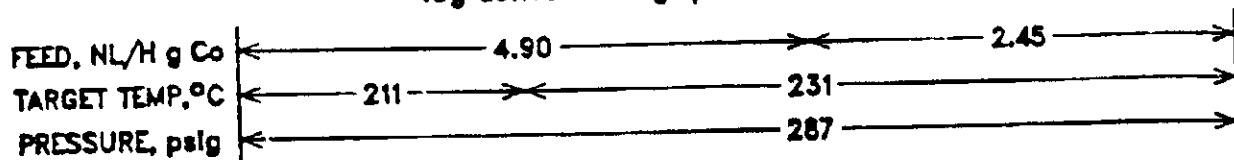
# PLT 700A RUN 77 Co,Ru on Carbotrap B

6531-160 w/13.6 % Co via eq. Impreg 2:1 H<sub>2</sub>:CO in feed

13g active in 160g quartz sand



PLT 700A RUN 77 Co,Ru on Carbotrap B  
 6531-160 w/13.6 % Co via aq. Impreg 2:1 H<sub>2</sub>:CO in feed  
 13g active in 160g quartz sand





PLT 700A RUN 77 Co,Ru on Carbotrap B  
 6531-160 w/13.6 % Co via eq. Impreg 2:1 H<sub>2</sub>:CO in feed  
 13g active in 160g quartz sand

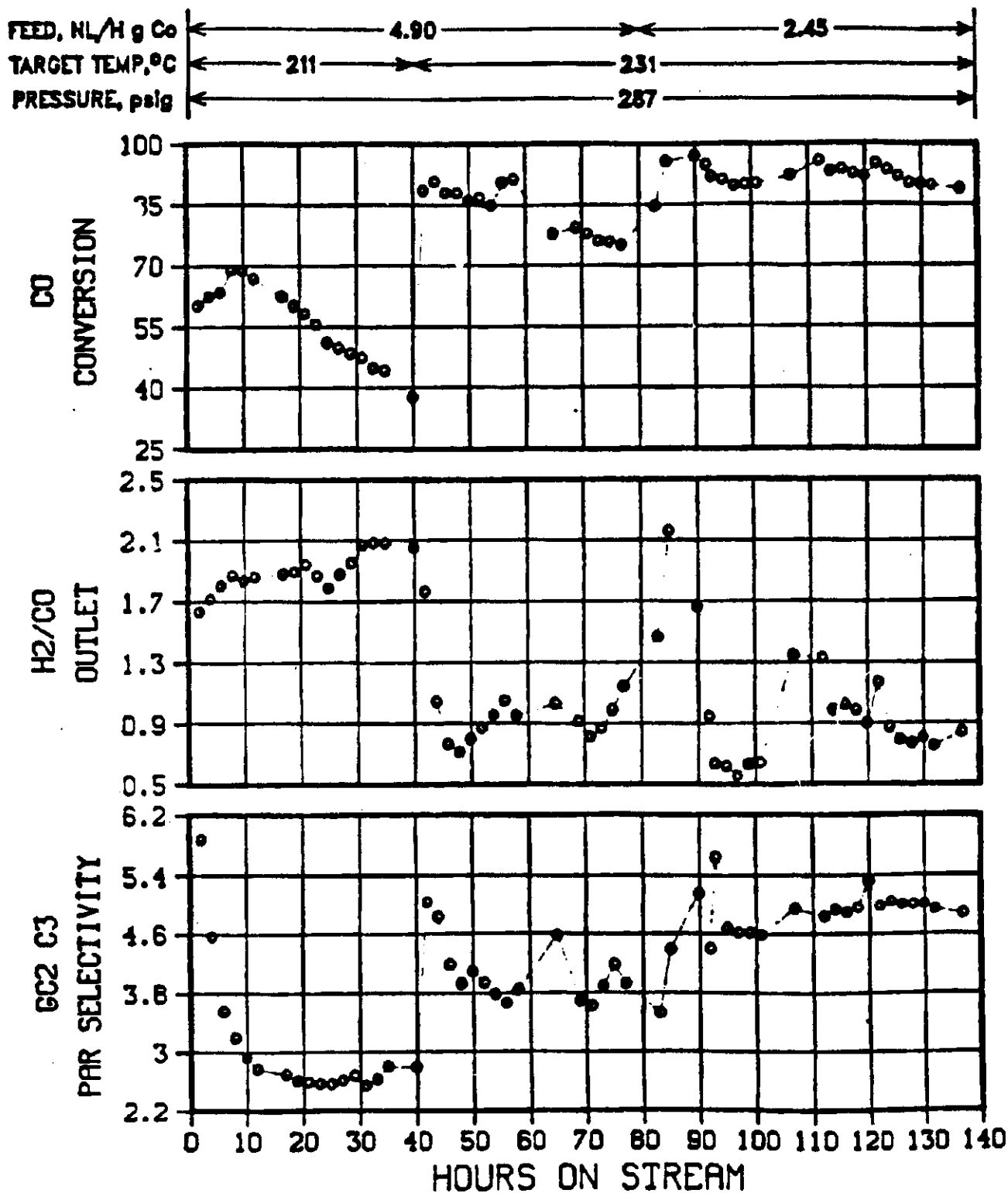


Figure 22

PLT 700A RUN 77 Co,Ru on Carbotrap B  
6531-160 w/13.6 % Co via aq. Impreg 2:1 H<sub>2</sub>:CO In feed  
13g active in 160g quartz sand

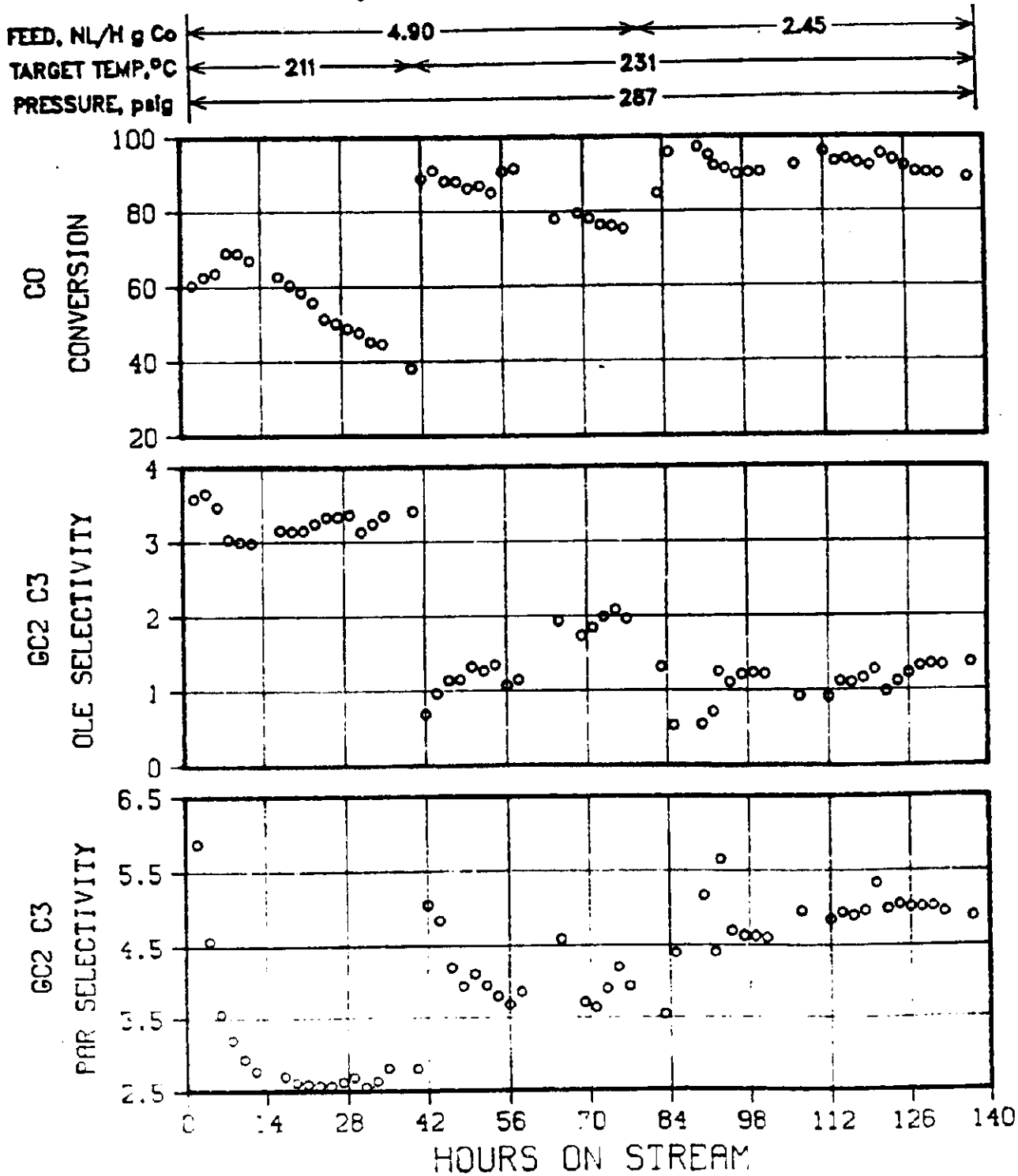
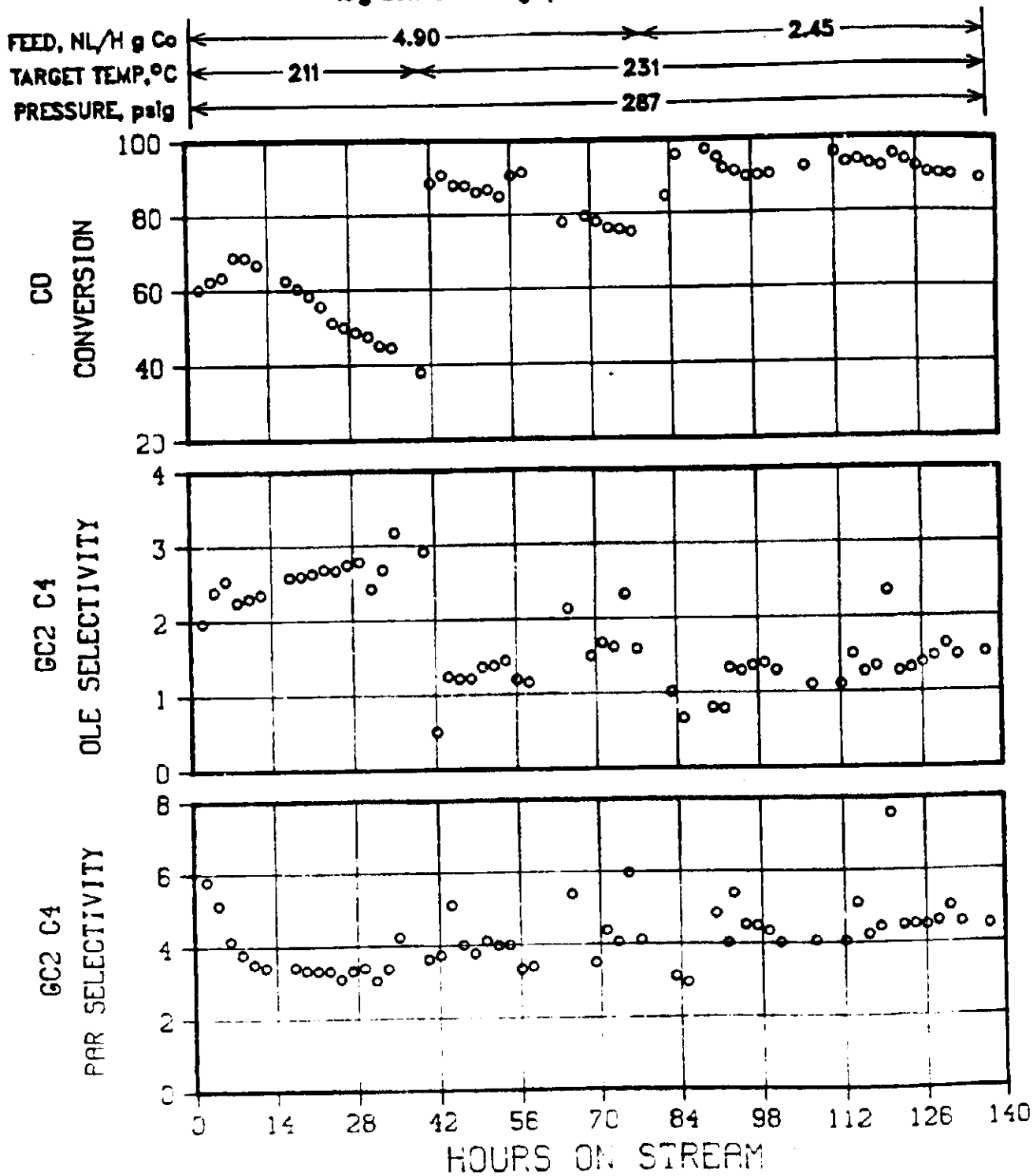


Figure 23

### PLT 700A RUN 77 Co,Ru on Carbotrap B

6531-160 w/13.6 % Co via aq. Impreg 2:1 H<sub>2</sub>:CO In feed  
13g active in 160g quartz sand



# PLT 700A RUN 77 Co,Ru on Carbotrap B

6531-160 w/13.6 % Co via aq. impreg 2:1 H<sub>2</sub>:CO in feed

13g active in 160g quartz sand

