Appendices

Appendix A – WKE Case

Appendix B – TXU Case

Appendix C – BB Power Report on Boiler Penetraions

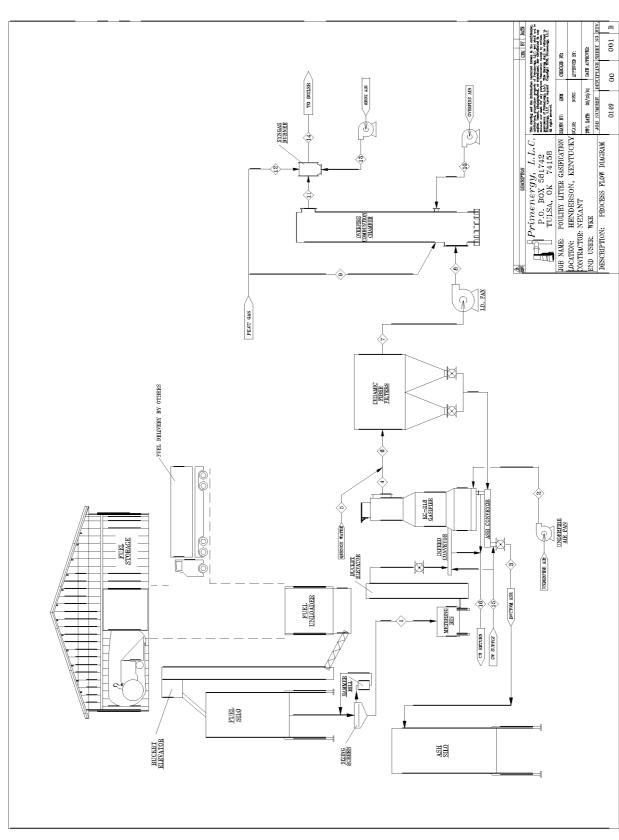


Table A-1 Reid Plant Single KC-18 Material and Energy Balance

| Stream ID | 1 | 2 | 3 | 4 | 2 | 9 | 7 | 8 | 6 |
|---------------------------------|----------|----------|----------|----------|--------|---------|---------|---------|-------|
| Stream | GASIFIER | GASIFIER | GASIFIER | GASIFIER | QUENCH | HGF | HOT GAS | OI | PILOT |
| Name | FEED | COMB | BOTTOM | SYNGAS | WATER | INLET | FILTER | FAN | GAS |
| | | AIR | ASH | | | SYNGAS | EXHAUST | EXHAUST | |
| Pressure, psig ("w.cg) | | (20.0) | 1 | (-0.25) | 50 | (-0.50) | (-10.0) | (8.0) | 30 |
| Temperature, °F | 22 | 08 | 300 | 1550 | 22 | 1400 | 1382 | 1382 | 27 |
| Molecular Weight (lb/lbmole) | - | 28.68 | 67.17 | 24.95 | 18.02 | 24.69 | 24.66 | 24.66 | 16.04 |
| Component | H/ql | 4/qı | lb/h | lb/h | ų/qj | ų/qj | lb/h | lb/h | lb/h |
| Carbon | 4,617 | | 467 | | | | | | |
| Hydrogen | 527 | | | | | | | | |
| Nitrogen | 463 | | | | | | | | |
| Oxygen | 3,416 | | | | | | | | |
| Sulfur | 83 | | | | | | | | |
| Chlorine | 0 | | | | | | | | |
| Fuel Gas | | | | | | | | | 23 |
| Carbon Monoxide | | | | 3,819 | | 3,819 | 3,819 | 3,819 | |
| Carbon Dioxide | | | | 9,207 | | 9,207 | 9,207 | 9,207 | |
| Hydrogen | | | | 421 | | 421 | 421 | 421 | |
| Water (v) | | 267 | | 5,412 | | 9/2/9 | 6,576 | 6,576 | |
| Nitrogen | | 20,853 | | 21,316 | | 21,316 | 21,316 | 21,316 | |
| Oxygen | | 6,313 | | | | | | | |
| Sulfur Dioxide | | | | 166 | | 166 | 166 | 166 | |
| Hydrogen Chloride | | | | 0 | | | | | |
| Ash | 3,494 | | 3,961 | 70 | | 20 | | | |
| Lime | | | | | | | | | |
| Water (I) | 4,200 | | | | 1,164 | | | | |
| TOTAL | 16,800 | 27,433 | 4,428 | 40,410 | 1,164 | 41,574 | 41,505 | 41,505 | 23 |

Table A-1 Reid Plant Single KC-18 Material and Energy Balance (contd.)

| Stream ID | 1 | 2 | ε | 4 | 5 | 9 | 2 | 8 | 6 |
|--|----------|----------|----------|----------|--------|---------|---------|---------|--------|
| Stream | GASIFIER | GASIFIER | GASIFIER | GASIFIER | QUENCH | HGF | HOT GAS | al | PILOT |
| Name | FEED | COMB | BOTTOM | SYNGAS | WATER | INLET | FILTER | FAN | GAS |
| | | AIR | ASH | | | SYNGAS | EXHAUST | EXHAUST | |
| Pressure, psig ("w.cg) | | (20.0) | | (-0.25) | 50 | (-0.50) | (-10.0) | (8.0) | 30 |
| Temperature, °F | 77 | 80 | 300 | 1550 | 77 | 1400 | 1382 | 1382 | 77 |
| Molecular Weight (Ib/Ibmole) | | 28.68 | 67.17 | 24.95 | 18.02 | 24.69 | 24.66 | 24.66 | 16.04 |
| Component | lb/h | lb/h | lb/h | lb/h | lb/h | lb/h | y/al | lb/h | lb/h |
| TOTAL | 16,800 | 27,433 | 4,428 | 40,410 | 1,164 | 41,574 | 41,505 | 41,505 | 23 |
| AVAILABLE ENERGY VALUE (LHV-Hv), Btu/lb | 4,196 | | 14,100.0 | 953.9 | | 927.1 | 928.7 | 928.7 | 21,502 |
| AVAILABLE ENERGY, MMBtu/h | 70.50 | | 9.9 | 38.5 | 0.0 | 38.5 | 38.5 | 38.5 | 0.5 |
| FLOW RATE, scfm (gpm) | | 6,050 | | 10,243 | (2.33) | 10,652 | 10,644 | 10,644 | 6 |
| FLOW RATE, acfm | | 6,283 | | 39,593 | | 38,100 | 37,701 | 37,701 | 6 |
| | | | | | | | | | |

Table A-1 Reid Plant Single KC-18 Material and Energy Balance (contd.)

| Stream ID | 10 | 11 | 12 | 13 | 14 | 15 | 16 |
|------------------------------|----------|----------|-------|--------|---------|----------|----------|
| Stream | OVERFIRE | OVERFIRE | PILOT | REOX | COMB | GASIFIER | GASIFIER |
| Name | COMB | SYNGAS | GAS | COMB | PROD TO | COOLING | CW |
| | AIR | | | AIR | BOILER | WATER | RETURN |
| Pressure, psig ("w.cg) | (13.0) | (7.0) | 30 | (13.0) | (6.0) | 09 | 10 |
| Temperature, °F | 80 | 2400 | scfm | 80 | 2330 | 110 | 165 |
| Molecular Weight (Ib/Ibmole) | 28.68 | 26.96 | 16.04 | 28.68 | 28.02 | 18.02 | 18.02 |
| Component | lb/h | h/dl | lb/h | y/q | h/dl | lb/h | lb/h |
| Carbon | | | | | | | |
| Hydrogen | | | | | | | |
| Nitrogen | | | | | | | |
| Oxygen | | | | | | | |
| Sulfur | | | | | | | |
| Chlorine | | | | | | | |
| Fuel Gas | | | 23 | | | | |
| Carbon Monoxide | | 633 | | | | | |
| Carbon Dioxide | | 14,276 | | | 15,335 | | |
| Hydrogen | | 200 | | | | | |
| Water (v) | 157 | 8,756 | | 245 | 10,844 | | |
| Nitrogen | 12,257 | 33,574 | | 19,099 | 52,673 | | |
| Oxygen | 3,711 | | | 5,782 | 3,737 | | |
| Sulfur Dioxide | | | | | | | |
| Hydrogen Chloride | | | | | | | |
| Ash | | | | | | | |
| Lime | | | | | | | |
| Water (I) | | | | | | 26,738 | 26,738 |
| TOTAL | 16,125 | 57,440 | 23 | 25,125 | 82,588 | 26,738 | 26,738 |

Table A-1 Reid Plant Single KC-18 Material and Energy Balance (contd.)

| Stream ID | 10 | 11 | 12 | 13 | 14 | 15 | 16 |
|--|----------|----------|--------|--------|---------|----------|----------|
| Stream | OVERFIRE | OVERFIRE | PILOT | KEOX | COMB | GASIFIER | GASIFIER |
| Name | COMB | SYNGAS | GAS | COMB | PROD TO | COOLING | CW |
| | AIR | | | AIR | BOILER | WATER | RETURN |
| Pressure, psig ("w.cg) | (13.0) | (7.0) | 30 | (13.0) | (0.9) | 09 | 10 |
| Temperature, °F | 80 | 2400 | scfm | 80 | 2330 | 110 | 165 |
| Molecular Weight (Ib/Ibmole) | 28.68 | 26.96 | 16.04 | 28.68 | 28.02 | 18.02 | 18.02 |
| Component | lb/h | h/dl | lb/h | 4/ql | y/ql | lb/h | lb/h |
| TOTAL | 16,125 | 57,440 | 23 | 25,125 | 82,588 | 26,738 | 26,738 |
| AVAILABLE ENERGY VALUE (LHV-Hv), Btu/lb | | 229.0 | 21,502 | | | 0.0 | 1.0 |
| AVAILABLE ENERGY, MMBtu/h | | 13.2 | 0.5 | | | 0.0 | 1.5 |
| FLOW RATE, scfm (gpm) | 3,556 | 13,478 | 6 | 5,541 | 18,642 | (53.5) | (53.5) |
| FLOW RATE, acfm | 3,693 | 74,129 | 8 | 5,754 | 100,031 | | |
| | | | | | | | 1 |

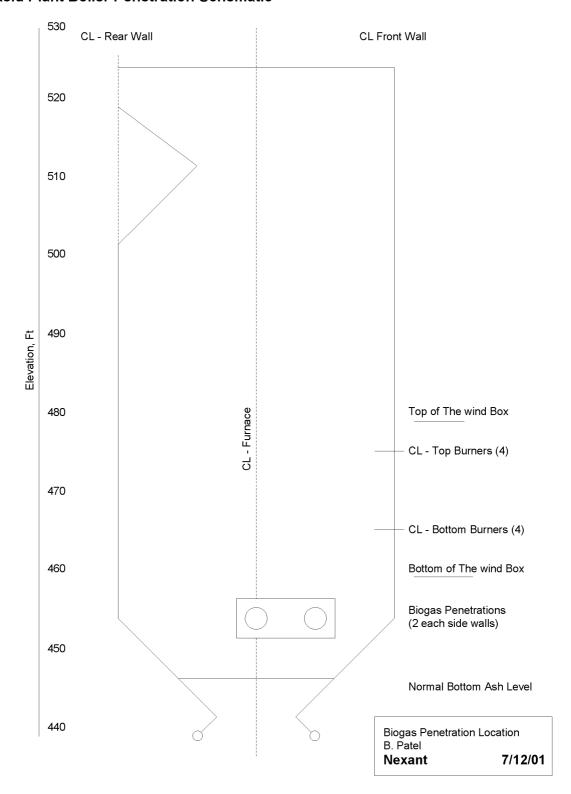
Table B-2 Reid Plant Cost Sensitive Analysis

| Case | | Base Case | 7 | က | 4 | 2 | 9 | 2 | ∞ |
|--------------|--------|--------------|--------------|--------------|---|--------------|--------------|--------------|--------------|
| | | | | | | | | | |
| Litter Cost | \$/ton | \$ 12 | 8 \$ | \$ 10 | \$ 12 | 9 \$ | \$ 8 | \$ 10 | \$ 12 |
| Ash Credits | \$/Ton | (9) \$ | (9) \$ | \$ (8) | \$ (10) | \$ (12) | \$ (12) | \$ (14) | \$ (16) |
| Capital Cost | | 000'005'6 \$ | \$ | \$ 9,500,000 | 000'0006'8 \$ 000'006'8 \$ 000'006'8 \$ 000'006'8 \$ 000'005'6 \$ 000'006'8 | 000'006'8 \$ | \$ 8,900,000 | 000'006'8 \$ | \$ 8,900,000 |
| WKE Cost | | \$ 4,750,000 | \$ 4,750,000 | \$ 4,750,000 | 4,750,000 \$ 4,750,000 \$ 4,750,000 \$ 4,450,000 \$ 4,450,000 \$ 4,450,000 \$ 4,450,000 | \$ 4,450,000 | \$ 4,450,000 | \$ 4,450,000 | \$ 4,450,000 |
| | | | | | | | | | |
| | | | | | | | | | |
| Interest | % | 7.5% | 7.5% | 7.0% | 7.0% | %0'. | 7.5% | 7.0% | %0.7 |
| Period | Years | 10.0 | 10.0 | 15.0 | 15.0 | 15.0 | 10.0 | 10.0 | 10.0 |
| | | | | | | | | | |
| Power Cost | | | | | | | | | |
| Fuel | c/kwh | 1.74 | 1.12 | 1.35 | 1.58 | 0.56 | 0.87 | 1.10 | 1.33 |
| O&M | c/kwh | 1.03 | 1.03 | 1.03 | 1.03 | 1.03 | 1.03 | 1.03 | 1.03 |
| Capital | c/kwh | 2.39 | 2.39 | 1.80 | 1.80 | 1.69 | 2.24 | 2.19 | 2.19 |
| | | | | | | | | | |
| Total | c/kwh | 5.17 | 4.54 | 4.18 | 4.41 | 3.28 | 4.14 | 4.32 | 4.55 |

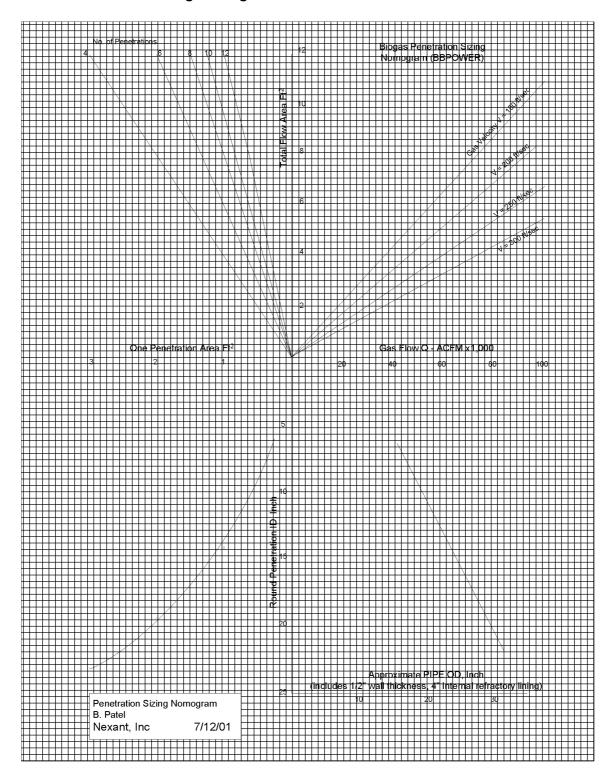
Table A-2 Electrical Power Consumption

| SYSTEM MOTOR LIST & | ELECTR | RICAL RI | EQUIREN | /IENT | |
|--|--------|----------|---------|--------|-------|
| | MOTOR | | | | ELEC. |
| | SIZE | QTY | QTY | OPR | USAGE |
| ITEM | Нр | SUPL. | OPRTG | FACTOR | Kw |
| Fuel Receiving Hopper | 15 | 1 | 1 | 0.40 | 4.5 |
| Fuel Receiving Hopper Discharge Conveyor | 15 | 1 | 1 | 0.40 | 4.5 |
| Storage Silo Bucket Elevator | 20 | 1 | 1 | 0.40 | 6.0 |
| Separation Screen | 5 | 1 | 1 | 0.40 | 1.5 |
| Hammermill | 50 | 1 | 1 | 0.40 | 14.9 |
| Hammermill Air System | 15 | 1 | 1 | 0.40 | 4.5 |
| Silo Unloader | 15 | 1 | 1 | 0.40 | 4.5 |
| Silo Discharge Conveyor | 10 | 1 | 1 | 0.40 | 3.0 |
| Metering Bin Discharge Screw | 5 | 1 | 1 | 0.50 | 1.9 |
| Bucket Elevator | 5 | 1 | 1 | 0.50 | 1.9 |
| Fuel Feed Rotary Valve | 5 | 1 | 1 | 0.50 | 1.9 |
| Fuel Infeed Auger | 5 | 1 | 1 | 0.50 | 1.9 |
| Agitator | 5 | 1 | 1 | 0.50 | 1.9 |
| Ash Discharge Auger #1 | 3 | 1 | 1 | 0.50 | 1.1 |
| Ash Discharge Auger #2 | 3 | 1 | 1 | 0.50 | 1.1 |
| Ash Cooling Auger | 5 | 1 | 1 | 0.50 | 1.9 |
| Underfire Air Fan | 40 | 1 | 1 | 0.85 | 25.5 |
| Cooling Water Pump | 10 | 2 | 1 | 0.38 | 2.8 |
| Syngaas Compressor | 100 | 1 | 1 | 0.65 | 48.6 |
| Fly Ash Discharge Valve | 1 | 2 | 2 | 0.50 | 0.7 |
| Final Ash Conveyor | 10 | 1 | 1 | 0.50 | 3.7 |
| ID Fan | 250 | 1 | 1 | 0.83 | 155.3 |
| Overfire Air Fan | 10 | 1 | 1 | 0.50 | 3.8 |
| Reox/Recycle Fan | 10 | 1 | 1 | 0.55 | 4.1 |
| Air Compressor | 100 | 1 | 1 | 0.50 | 37.4 |
| Miscellaneous Electrical Usage | | | | | 2.0 |
| Total | 567.0 | | | | 340.6 |

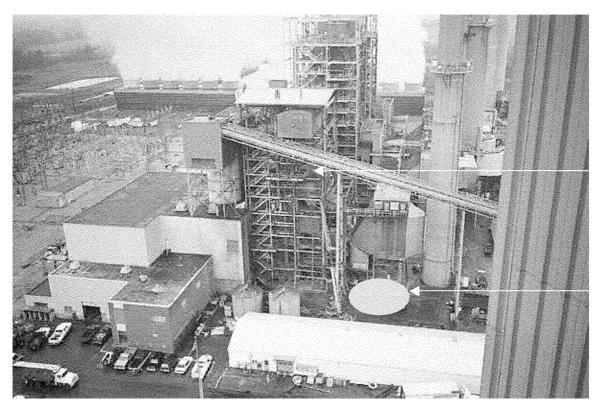
Reid Plant Boiler Penetration Schematic



Boiler Penetration Sizing Nomogram



Proposed Gasifier Location at Reid Plant



Reid Plant Boiler

Proposed Gasifier Location

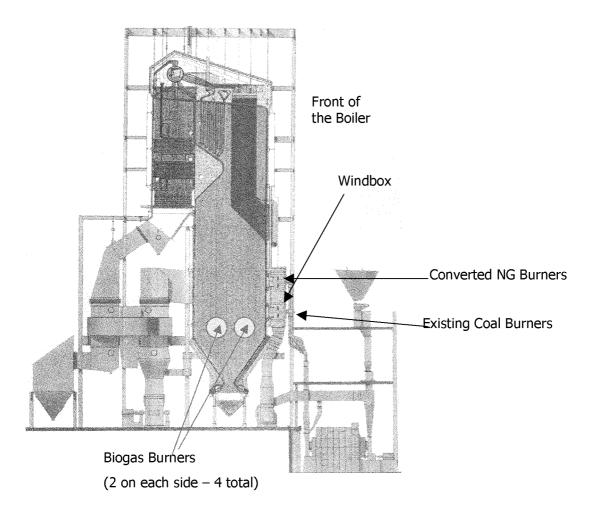
Fuel Receiving and Storage

Fuel



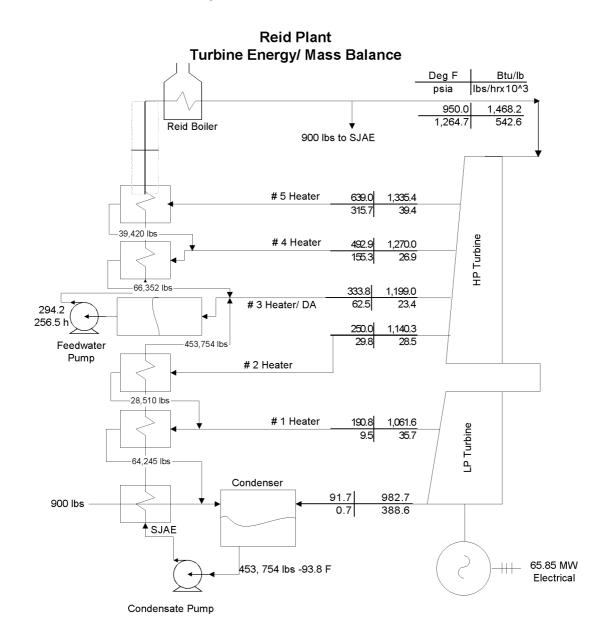
Fuel Storage

Reid Plant Boiler Penetrations



- Four Penetrations
- 2 on each side of the boiler
- Just below the lower windbox line
- Pressure at the burner –10"-12" of WC
- Velocity at the burner 150~300 ft/sec
- Flow 70,000~100,000 scfm

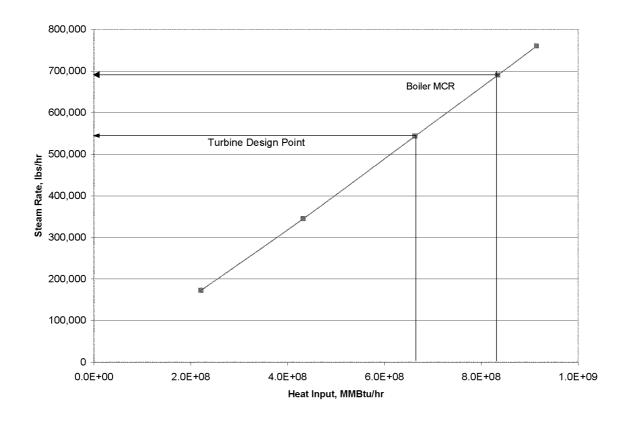
Reid Plant Turbine Energy Balance Turbine Name Plate Data by GE

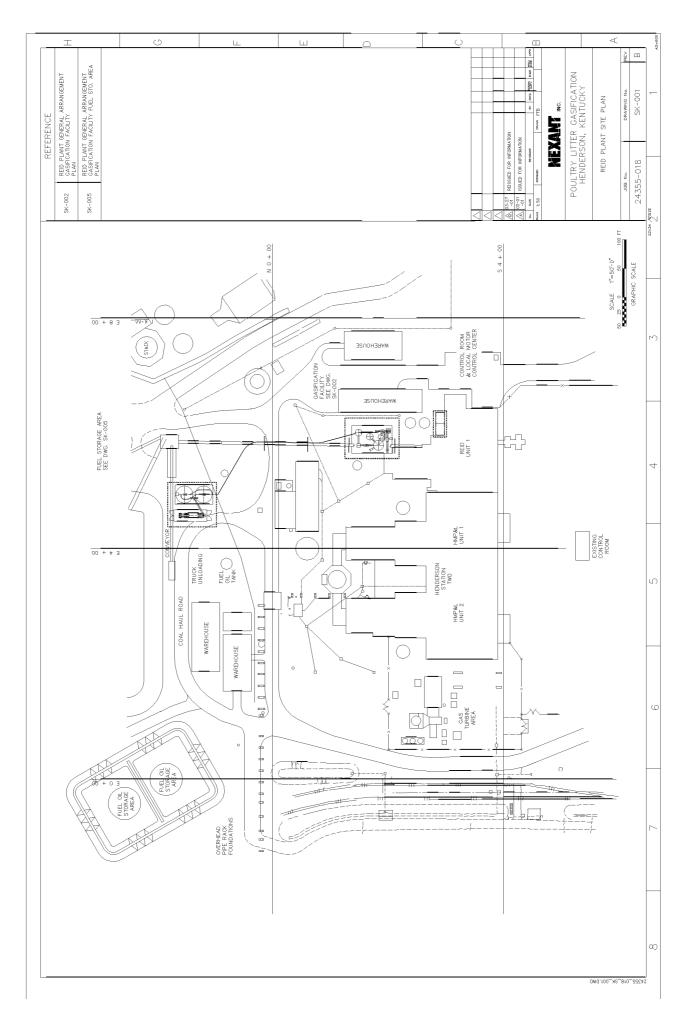


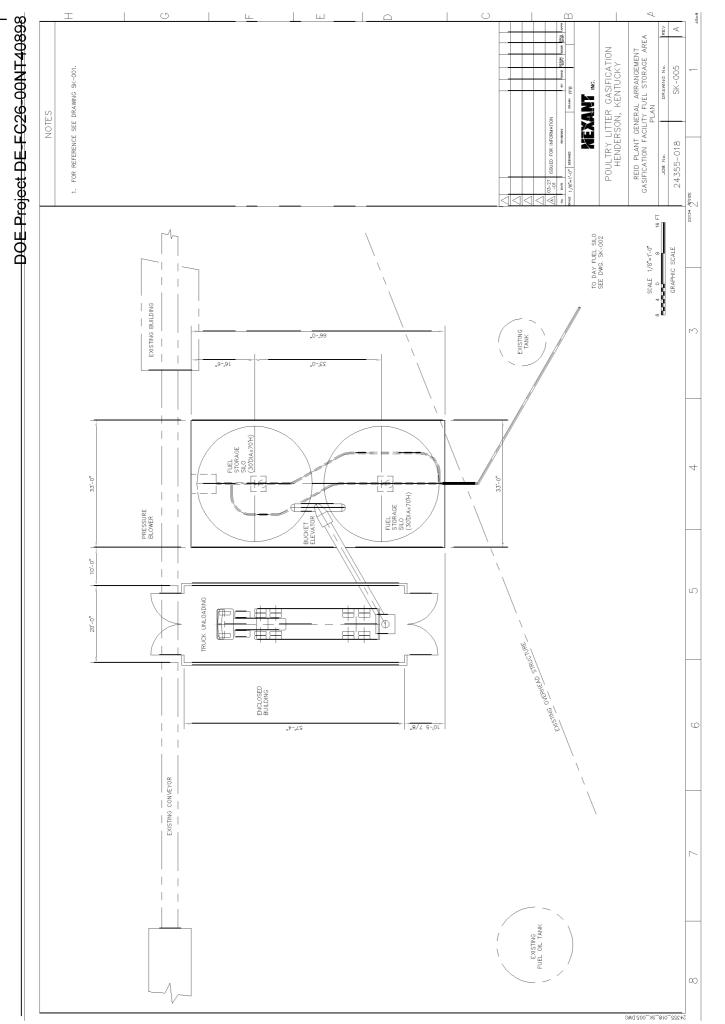
Ref: GE Design Case @ 65.85 MW Gross Turbine Output

B. Patel/ 3/23/01
Nexant Inc.

Turbine Design Point steam Load v/s Boiler heat Input







Appendix B - TXU Case

Appendix B- TXU Case

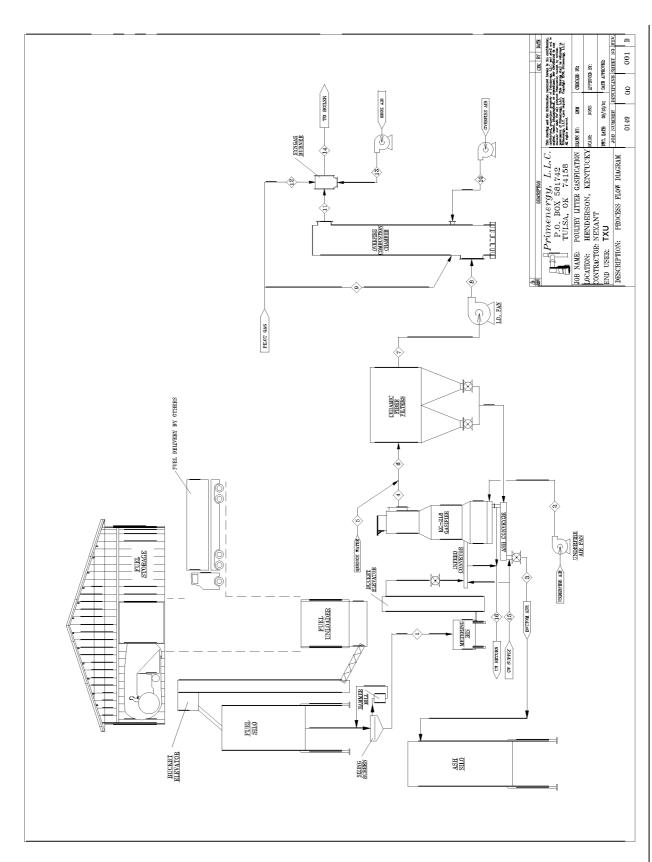


Table B-1 Material and Energy Balance for Monticello Case

| Stream ID | 1 | 2A | 3 | 4 | 5 | 9 | 7 | 8 | 8A | 6 | 10 | 11 |
|------------------------------|---------|----------|----------|--------|----------|---------|----------------|----------|----------|----------|--------|---------|
| Stream | BROILER | HEATED | GASIFIER | QUENCH | SYNGAS | HEAT | QI | OVERFIRE | HEATED | OVERFIRE | HEATED | COMB |
| Name | LITTER | GASIFIER | BOTTOM | WATER | SCRUBBER | ЕХСН | FAN | & REOX | OVERFIRE | SYNGAS | REOX | PROD TO |
| | | AIR | ASH | | EXHAUST | EXHAUST | EXHAUST | AIR | AIR | | AIR | BOILER |
| Pressure, psig ("w.cg) | - | (20.0) | | 50 | (-10.0) | (-13.0) | (8.0) | (15.0) | (12.0) | (7.0) | (12.0) | (0.9) |
| Temperature, °F | 77 | 650 | 300 | 77 | 1400 | 662 | 662 | 77 | 650 | 2400 | 650 | 2379 |
| Molecular Weight (Ib/Ibmole) | 1 | 28.68 | 75.25 | 18.02 | 24.39 | 24.39 | 24.39 | 28.68 | 28.68 | 27.56 | 28.68 | 28.33 |
| Component | lb/hr | lb/hr | lb/hr | lb/hr | lb/hr | lb/hr | lb/hr | lb/hr | lb/hr | lb/hr | lb/hr | lb/hr |
| Carbon | 10,151 | | 927 | | | | | | | | | |
| Hydrogen | 1,019 | | | | | | | | | | | |
| Nitrogen | 1,041 | | | | | | | | | | | |
| Oxygen | 7,135 | | | | | | | | | | | |
| Sulfur | 221 | | 111 | | | | | | | | | |
| Chlorine | | | | | | | | | | | | |
| Carbon Monoxide | | | | | 10,293 | 10,293 | 10,293 | | | 1,200 | | |
| Carbon Dioxide | | | | | 17,628 | 17,628 | 17,628 | | | 31,914 | | 33,799 |
| Hydrogen | | | | | 971 | 971 | 971 | | | 329 | | |
| Water (v) | | 510 | | | 10,795 | 10,795 | 10,795 | 435 | 435 | 16,966 | 480 | 20,386 |
| Nitrogen | | 39,813 | | | 40,854 | 40,854 | 40,854 | 33,982 | 33,982 | 74,836 | 37,490 | 112,326 |
| Oxygen | | 12,053 | | | | | | 10,287 | 10,287 | | 11,349 | 8,053 |
| Sulfur Dioxide | | | | | 221 | 221 | 221 | | | | | |
| Ash | 4,216 | | 4,110 | | | | | | | | | |
| Water (I) | 7,927 | | | 1,928 | | | | | | | | |
| TOTAL | 31,710 | 52,376 | 5,147 | 1,928 | 80,761 | 80,761 | 80,761 | 44,704 | 44,704 | 125,245 | 49,319 | 174,564 |
| | | | | | | | | | | | | |

Appendix B- TXU Case

Table B-1 Material and Energy Balance for Monticello Case (contd.)

| Stream ID | 1 | 2A | 3 | 4 | 5 | 9 | 7 | 8 | 8A | 6 | 10 | 11 |
|--|---------|----------|----------|--------|----------|---------|---------|----------|-----------------|----------|--------|---------|
| Stream | BROILER | HEATED | GASIFIER | QUENCH | SYNGAS | HEAT | al | OVERFIRE | HEATED | OVERFIRE | HEATED | COMB |
| Name | LITTER | GASIFIER | BOTTOM | WATER | SCRUBBER | ЕХСН | FAN | & REOX | & REOX OVERFIRE | SYNGAS | REOX | PROD TO |
| | | AIR | ASH | | EXHAUST | EXHAUST | EXHAUST | AIR | AIR | | AIR | BOILER |
| Pressure, psig ("w.cg) | | (20.0) | | 50 | (-10.0) | (-13.0) | (8.0) | (15.0) | (12.0) | (7.0) | (12.0) | (0.9) |
| Temperature, °F | 77 | 650 | 300 | 77 | 1400 | 662 | 662 | 77 | 650 | 2400 | 650 | 2379 |
| Molecular Weight (lb/lbmole) | 1 | 28.68 | 75.25 | 18.02 | 24.39 | 24.39 | 24.39 | 28.68 | 28.68 | 27.56 | 28.68 | 28.33 |
| Component | lb/hr | lb/hr | lb/hr | lb/hr | lb/hr | lb/hr | lb/hr | lb/hr | lb/hr | lb/hr | lb/hr | lb/hr |
| TOTAL | 31,710 | 52,376 | 5,147 | 1,928 | 80,761 | 80,761 | 80,761 | 44,704 | 44,704 | 125,245 | 49,319 | 174,564 |
| AVAIL ENERGY VALUE (LHV-Hv), Btu/lb | 4,537 | | | | 1,181 | 1,181 | 1,181 | | | 178 | | |
| AVAILABLE ENERGY MMBtu/hr | 143.85 | | 13.06 | | 95.35 | 95.35 | 95.35 | | | 22.32 | | |
| SENSIBLE ENERGY MMBtu/hr | | 7.47 | | | 35.43 | 14.90 | 14.90 | | 6.37 | 93.47 | 7.03 | 122.86 |
| FLOW RATE, scfm (gpm) | | 11,551 | | (3.86) | 20,940 | 20,940 | 20,940 | 9,859 | 9,859 | 28,743 | 10,877 | 38,968 |
| FLOW RATE, acfm | | 24,656 | | | 74,899 | 45,190 | 45,190 | 10,181 | 21,045 | 158,087 | 23,217 | 212,766 |

Appendix B- TXU Case

Table B-2 Electrical Usage for Monticello Case

| SYSTEM MOTOR LIST 8 | & ELECT | RICAL RI | EQUIREM | 1ENT | |
|--|---------|----------|---------|--------|-------|
| | MOTOR | | | | ELCTL |
| | SIZE | QTY | QTY | OPRTG | USAGE |
| ITEM | Нр | SUPLD | OPRTG | FACTOR | Kw |
| Fuel Receiving Hopper | 15 | 1 | 1 | 0.40 | 4.5 |
| Fuel Receiving Hopper Discharge Conveyor | 15 | 1 | 1 | 0.40 | 4.5 |
| Storage Silo Bucket Elevator | 20 | 1 | 1 | 0.40 | 6.0 |
| Separation Screen | 5 | 1 | 1 | 0.40 | 1.5 |
| Hammer mill | 50 | 1 | 1 | 0.40 | 14.9 |
| Hammer mill Air System | 15 | 1 | 1 | 0.40 | 4.5 |
| Silo Unloader | 15 | 2 | 2 | 0.40 | 9.0 |
| Silo Discharge Conveyor | 10 | 2 | 2 | 0.40 | 6.0 |
| Metering Bin Discharge Screw | 5 | 2 | 2 | 0.50 | 3.7 |
| Bucket Elevator | 5 | 2 | 2 | 0.50 | 3.7 |
| Fuel Feed Rotary Valve | 5 | 2 | 2 | 0.50 | 3.7 |
| Fuel Infeed Auger | 5 | 2 | 2 | 0.50 | 3.7 |
| Agitator | 5 | 2 | 2 | 0.50 | 3.7 |
| Ash Cooling Auger | 5 | 2 | 2 | 0.50 | 3.7 |
| Underfire Air Fan | 50 | 2 | 2 | 0.79 | 58.9 |
| Cooling Water Pump | 15 | 2 | 1 | 0.70 | 7.9 |
| Syngaas Compressor | 150 | 1 | 1 | 0.75 | 84.0 |
| Fly Ash Discharge Valve | 1 | 4 | 4 | 0.50 | 1.5 |
| Final Ash Conveyor | 10 | 1 | 1 | 0.50 | 3.7 |
| Ash Bucket Elevator | 10 | 1 | 1 | 0.50 | 3.7 |
| ID Fan | 250 | 2 | 2 | 0.69 | 256.1 |
| Reox / Overfire Air Fan | 60 | 2 | 2 | 0.73 | 65.6 |
| Air Compressor | 25 | 1 | 1 | 0.75 | 14.0 |
| Miscellaneous Electrical Usage | | | | | 5.0 |
| Total | | | | | 573.7 |

Table B-2 Texas Lignite Analysis (Monticello Boiler Fuel)

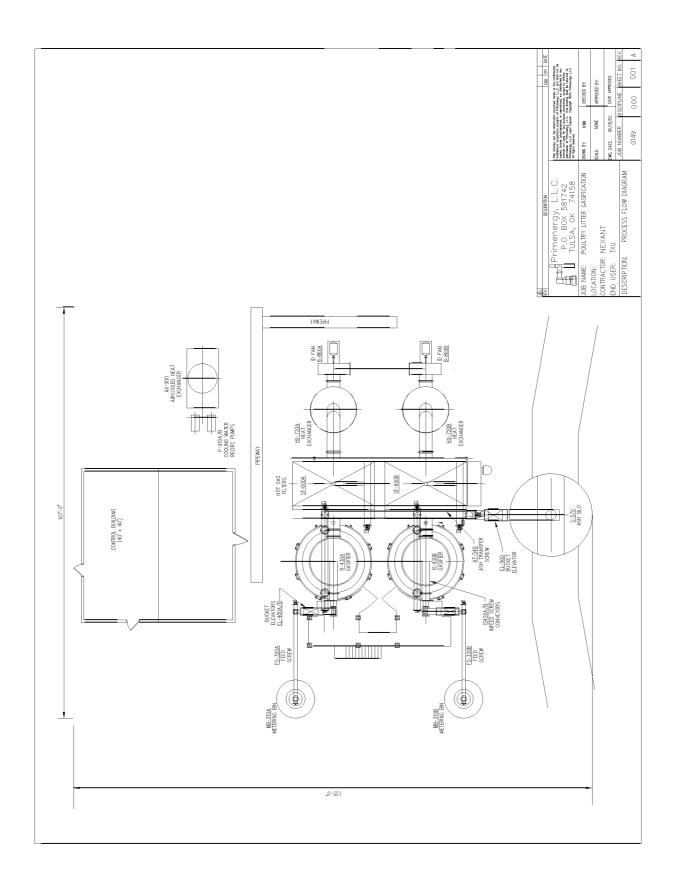
| Texas Lignite | Value | Units |
|---------------|----------------|----------------|
| Fuel HHV | 15 738 (6,767) | kJ/kg (Btu/lb) |
| С | 39.20 | % |
| H | 2.99 | |
| 0 | 11.04 | |
| Ν | 0.58 | |
| S | 0.61 | |
| Ash | 14.31 | |
| Moisture | 31.27 | |
| Total | 100.00 | |

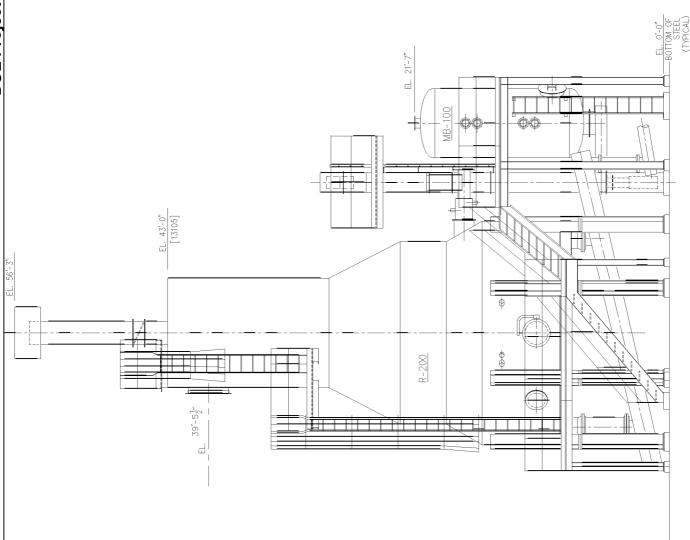
Table B-3 Monticello Boiler Design Data

| Monticello Unit 1 & 2 | Units | Control Point | MCR |
|-----------------------------------|-------|---------------|---------------|
| Fuel | | Texas Lignite | Texas Lignite |
| | | | |
| Evaporation | lbs/h | 3,200,000 | 4,025,000 |
| FW Temp | F | 478 | 501 |
| FW Pressure (calc) | psig | 3,750 | 4,068 |
| SH Outlet Temp | F | 1,005 | 1,005 |
| SH Outlet Press | psig | 3,595 | 3,825 |
| SH Pressure Drop | psig | 141 | 222 |
| | | | |
| Reheat Flow | lbs/h | 2,814,000 | 3,520,000 |
| Reheat inlet Temp | F | 550 | 572 |
| Reheat Inlet Press | psig | 542 | 682 |
| Reheat Outlet Temp | F | 1,005 | 1,005 |
| Reheater Press Drop | psig | 28 | 35 |
| Econmizer Press Drop | psi | 14 | 21 |
| Gas Drop - Furnace to Econ | "wg | 2.45 | 3.65 |
| Gas Drop Econ Outlet to AH Outlet | "wg | 4.80 | 6.85 |
| Gas Temp Entering AH | F | 805 | 860 |
| Gas Temp Leaving AH | F | 327 | 351 |
| Gas Temp Leaving AH | F | 311 | 336 |
| Air Temp Air Heater | F | 85 | 85 |
| Air Temp Leaving | F | 701 | 730 |
| Air Press Air Heater | "wg | 7.90 | 10.35 |
| Amb. Air Temp | F | 80 | 80 |
| Excess Air Econ | % | 20 | 20 |
| Fuel Fired | lbs/h | 681,000 | 836,000 |
| Efficiency | % | 82.69 | 82.06 |

Table B-4 Monticello Plant Sensitivity Case

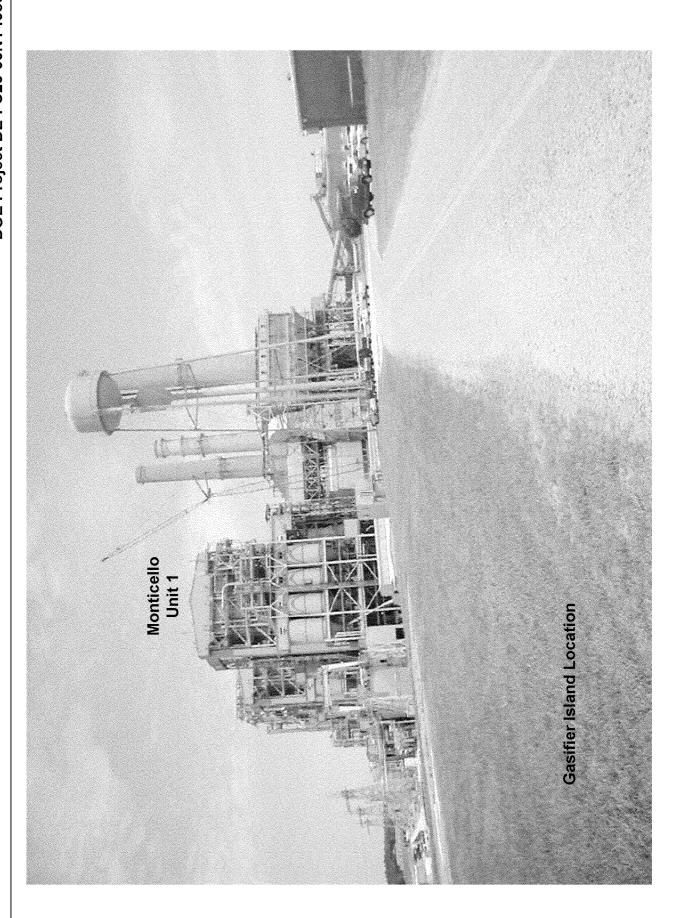
| Case | Litter Cost | Ash Credits | Capital Cost | TXU Cost Share | Interest | Period | Fuel | O&M | Capital | Total |
|--------------|----------------|----------------|--------------|-------------------|----------|--------|-------|-------|---------|-------|
| | \$/ton | \$/Ton | | | % | Years | c/kWh | c/kwh | c/kwh | c/kwh |
| Base Case | 8 | 0 | \$14,882,622 | \$14,882,622 | 7.5% | 10 | 1.00 | 0.78 | 2.69 | 4.47 |
| 2 | 8 | (6) | \$ 4,882,622 | \$14,882,622 | 7.5% | 10 | 0.83 | 0.78 | 2.69 | 4.30 |
| 3 | 8 | 0 | \$14,882,622 | \$ 7,441,311 | 7.5% | 10 | 1.00 | 0.78 | 1.34 | 3.13 |
| 4 | 6 | (6) | \$14,882,622 | \$14,882,622 | 7.5% | 10 | 0.58 | 0.78 | 2.69 | 4.05 |
| 5 | 6 | (6) | \$14,882,622 | \$ 7,441,311 | 7.5% | 10 | 0.58 | 0.78 | 1.34 | 2.71 |
| 6 | 4 | 0 | \$14,882,622 | \$14,882,622 | 7.5% | 10 | 0.50 | 0.78 | 2.69 | 3.97 |
| 7 | 4 | 0 | \$14,882,622 | \$ 7,441,311 | 7.5% | 10 | 0.50 | 0.78 | 1.34 | 2.63 |
| 8 | 0 | (6) | \$14,882,622 | \$14,882,622 | 7.5% | 10 | -0.17 | 0.78 | 2.69 | 3.30 |





Primenery Gasifier Elevation





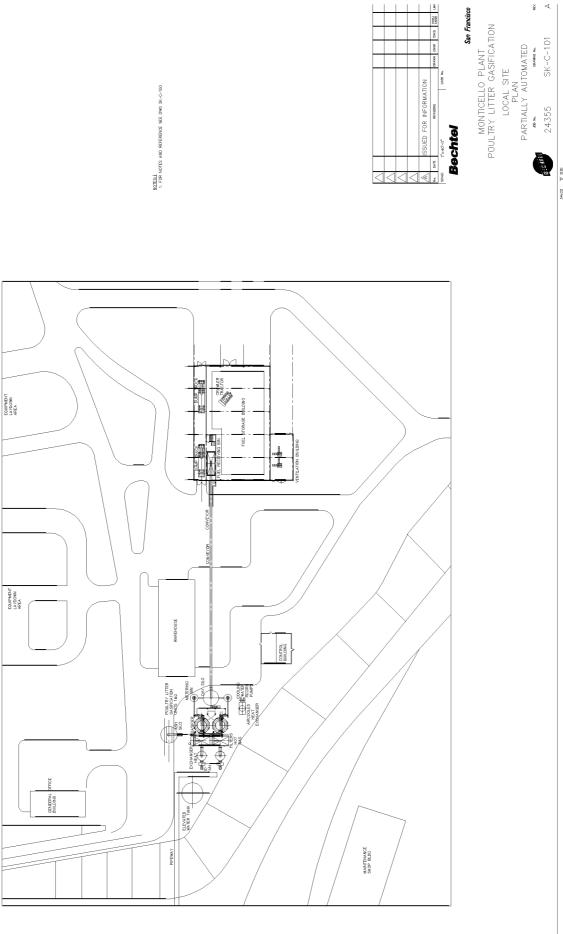
Prepared By Nexant, Inc.

SK-C-500

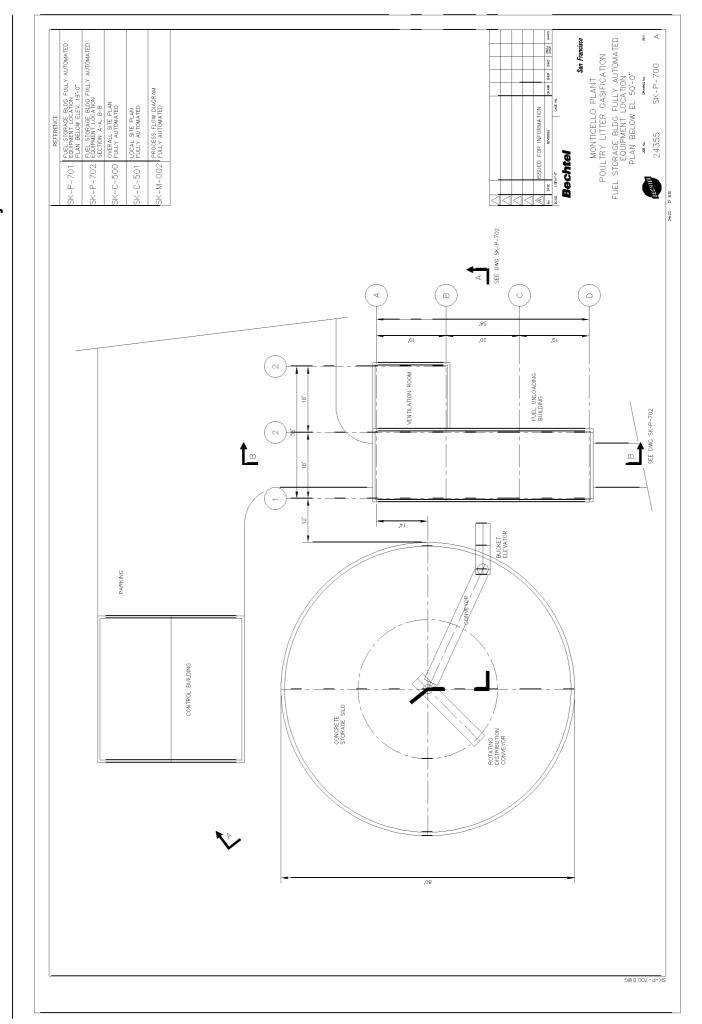
24355

San Francis

2K-C-201'DMC



2K-C-101'DMC



Appendix B -TXU Case

| Appendix C – BB Power Report | | |
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PRELIMINARY ENGINEERING STUDY FOR FEASIBILITY OF MODULAR BIO-GASIFIER HOT PRODUCER GAS INJECTION INTO PULVERIZED COAL FIRED FLAT WALL FURNACE

FOR:

NEXANT INC.

AT

WESTERN KENTUCKY ENERGY REID PLANT SEBREE POWER COMPLEX SEBREE, KENTUCKY

BBP CONTRACT No. 200756 Original Contract Riley Stoker Corp. B2502

Date Issued: 31 May 2001

PRELIMINARY ENGINEERING STUDY FOR FEASIBILITY OF MODULAR BIO-GASIFIER HOT PRODUCER GAS INJECTION INTO PULVERIZED COAL FIRED FLAT WALL FURNACE

FOR NEXANT INC. AT

WESTERN KENTUCKY ENERGY **REID PLANT** SEBREE POWER COMPLEX SEBREE, KENTUCKY

BBP CONTRACT NO. 200756 Original Contract Riley Stoker Corp. B2501

DATE ISSUED: 31 May 2001

Prepared By:

Sr. Staff Engineer

Boiler Design

Prepared By:

Sr. Consultant

Fuel Burning

Approved By:

Brian Vitalis

Manager

Boiler Design

BABCOCK BORSIG POWER

May 31, 2001

NEXANT, Inc. 45 Fremont Street, 7th Floor San Francisco, CA 94105-2210

Attn: Mr. Babul Patel

Subject:

Phase 1 Engineering Study for Feasibility of Modular Bio-Gasifier Hot

Producer Gas Injection into Pulverized Coal Fired Flat Wall Furnace

At Western Kentucky Energy, Reid Plant Sebree Power Complex, Sebree, Kentucky NEXANT, Inc. PO #0104-NEX-133

Original Contract Riley Stoker Corp, B2502

DB Riley Contract 200756

Dear Babul,

Thank you for using Babcock Borsig Power's engineering services; attached please find three copies of engineering's report that provides NEXANT assistance and recommendations in determining feasible locations, size, and number of penetrations required to flow syn gas into a pressurized type furnace.

As mentioned in today's conversation, once you have reviewed the report, call me a day ahead of time and I will set up a teleconference with engineering (Frank and Dick) to answer any questions that you may have.

Thank you for the opportunity to be of service to you, BBP looks forward to perhaps working with NEXANT on Phase 2 of this project.

Sincerely,

Babcock Borsig Power, Inc.

Liène Strachoures

Elaine K. Strzelewicz

Job Manager, Field Engineering and Services Department

CC: K. Davis, P. Knight/1, J. Scott/1, E. Vega/1

Babcock Borsig Power, Inc. Energy Systems and Services Division

Mailing Address:

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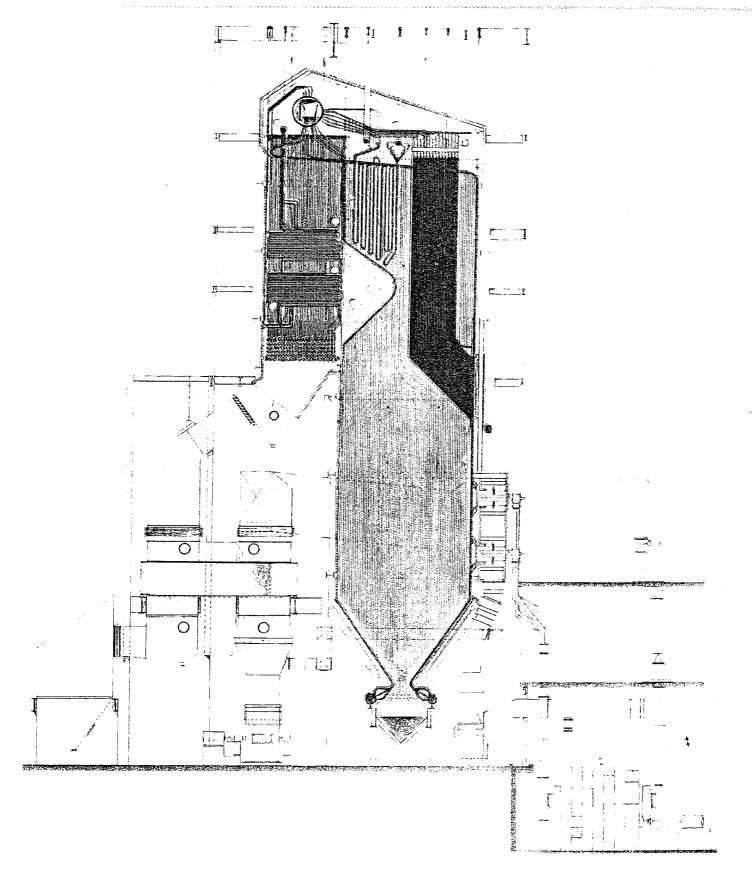
5 Neponset Street Worcester, MA 01606 Telephone: (508) 852-7100 (508) 852-7548

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WKE Reid Plant
BBP Contract 200756
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BIG RIVERS RURAL ELECTRIC COOPERATIVE CORP. SEBREE, KENTUCKY

690.000 lbs/hr—1475 psig design—1300 psig operating—955F Burns & McDonnell Engineering Co., Consulting Engineers

Nexant Inc. WKE Reid Plant BBP Contract 200756

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BBP Contract 200756

1.0 -INTRODUCTION AND BACKGROUND

1.1 Introduction

NEXANT, Inc. and its partners, Western Kentucky Energy and Primenergy, are working with DOE-NETL to develop a biomass cofiring project at the Western Kentucky Energy Reid Plant located near Henderson, Kentucky. The cofiring project is a proposal for the installation of modular bio-gasifier(s) adjacent to the existing boiler and injecting the hot producer gas from the gasifier into the boiler. As part of phase 1, Nexant is seeking assistance in modeling the expected boiler operation post gasifier(s) installation. The specific tasks for BBP (subcontractor scope of work) as a part of phase 1 are as follows:

- Determine feasible locations for boiler penetration(s) to minimize the impact on existing boiler equipment
- Size the penetrations
- Determine pressure requirements at the penetrations
- Provide preliminary recommendations on required stiffening/strengthening at the boiler penetrations.

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1.2 Background

The Western Kentucky Energy Reid Plant was designed by Riley Stoker Corporation under contract B-2502 (1962). It consists of one steam generating unit at a maximum continuous rating of 690,000 Lb/hr steam flow, 1300 psig outlet steam pressure, 955 °F outlet steam temperature, 440 °F feedwater temperature entering the economizer, while firing West Kentucky Bituminous coal. The boiler has two (2) Riley ball tube mills, eight (8) Riley type 60 flare burners, and one (1) Ljungstrom 25VIx48 air heater.