

TVA/OGM/CG-81/13

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TVA COAL-GASIFICATION
COMMERCIAL DEMONSTRATION PLANT PROJECT

VOLUME 6
PLANT BASED ON
GASIFIER
TEXACO

FINAL REPORT
November 1, 1980



Foster Wheeler Energy Corporation

110 South Orange Avenue, Livingston, New Jersey

PROCESS PLANTS DIVISION



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Table of Contents

Volume 6 Plant Based on Texaco Gasifier

Section		
1.0		<u>Introduction</u>
2.0		<u>Process Selection</u>
	2.1	Choice of Processing Sequence
	2.2	General Description of Flow
	2.3	Nominal Capacities of Processing Units
	2.4	Block Flow Diagram
3.0		<u>Baseline Design</u>
	3.1	<u>Section 100 Coal Preparation</u>
		Description of Flow
		List of Major Equipment
		Flow Diagram
	3.2	<u>Section 200 Air Separation Plant</u>
		Description of Flow
		Input/Output Major Stream Flows
		List of Major Equipment
		Flow Diagram
	3.3	<u>Section 300 Texaco Gasification System</u>
		Description of Flow
		Input/Output Major Stream Flows
		Flow Diagram
	3.4	<u>Section 400 Acid Gas Removal</u>
		Description of Flow
		Input/Output Major Stream Flows
		List of Major Equipment
		Flow Diagram



3.5 Section 600A - Clause Sulfur Recovery Plant

- Description of Flow
- List of Major Equipment
- Input/Output Major Stream Flows
- Flow Diagram

Section 600B - Sulfur Recovery Beavon Unit

- Description of Flow
- Input/Output Major Stream Flows
- List of Major Equipment
- Flow Diagram

Section 600C - Sulfur Prilling Unit

- Description of Flow
- List of Major Equipment
- Flow Diagram

3.6 Section 700 Sour Water Stripper and Waste Water Treatment

- Description of Flow
- Flow Diagram

3.7 Section 800 Slag Handling

- Description of Flow
- List of Major Equipment
- Flow Diagram

3.8 Section 1200 Utility Area

Raw Water Treatment and Storage

- Description of Flow
- List of Major Equipment
- Flow Diagram

Potable Water Treatment

- Description of Flow
- List of Major Equipment
- Flow Diagram

BFW Treatment

- Description of Flow
- List of Major Equipment
- Flow Diagram



Steam Generation

Description of Flow

List of Major Equipment

Flow Diagram

3.9 Section 1300 Cooling Water System

Description of Flow

List of Major Equipment

Flow Diagram

3.10 Section 1400 Flare

Description of Flow

List of Major Equipment

Flow Diagram

3.11 Section 1500 Waste Water Treatment

Description of Flow

List of Major Equipment

Flow Diagram

3.12 Section 2000 General Facilities

Ash & Slag Storage

By-products and Chemicals Storage

Firewater System

Sewage System

Power, Lighting and Communications

3.13 Section 2100 Buildings

4.0 Plant Requirements

4.1 Summary of Feed and Products

Tabulation of Feed and Products

Overall Material and Energy Balance

4.2 Steam Balance

Description of Flow

Steam Balance Diagram

4.3 Cooling Water Usage

Cooling Water Usage Diagram



4.4	<u>Power Requirements</u>
	Listing of Power Usage by Section
4.5	<u>Fuel Requirements</u>
	Discussion
4.6	<u>Catalysts and Chemicals Requirements</u>
	Catalyst & Chemical Cost
5.0	<u>Plant Layout</u>
	Key Plot Plan
	Elevations
6.0	<u>Environmental Assessment</u>
7.0	<u>Suggestions for Follow-on Work</u>
8.0	<u>Projections</u>
9.0	<u>Cost Estimates</u>
9.1	Investment Cost
9.2	Operating Cost
9.3	Sensitivity Analysis

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SECTION 1.0

INTRODUCTION

Form No. 130-171

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TVA Coal Gasification Study
Texaco Gasifier

INTRODUCTION

The baseline of a coal gasification plant producing medium Btu gas, based upon the Texaco gasification process is documented in this report.

The coal gasification plant consists of four identical modules, each with a capacity of approximately 4,800 tons of coal per day dry basis as delivered to the gasifiers. The entire plant (four modules) produces 1,195.0 Million Standard Cubic Feet per day of gas with a GHV value of approximately 285 Btu/SCF for a total heating value of about 341 billion Btu/day.

The plant location is the rural site of Murphy Hill, located along the Tennessee River, some 30 miles east of Huntsville, Alabama. Section 1 provides more detailed site information.

The desired product gas is a clean, medium-Btu gas suitable for pipeline distribution. The coal used for processing and for auxiliary boilers is a Kentucky No. 9 coal. The product gas specifications and the coal characteristics are listed in Section 2.

The site is accessible by barge and road, with the plant receiving coal primarily by barge. About 5 percent of plant needs are delivered by truck. The site will not be served by rail. The coal receiving facilities are sized to handle the entire needs of the plant.

Water needed for cooling and for process consumption will be drawn from the Tennessee River and will be treated by the plant water treatment facility. The plant will use closed loop cooling. Electricity will be furnished by TVA at the plant boundary.

The plant will be designed to meet all Federal, State, and local standards and guidelines.

A description of the plant by major sections is included as well as flow diagrams, stream balances and lists of major equipment. A key plot plan is presented in Section 5.



3.1 Choice of Processing Sequence

Process selection for the main processing units and support systems for the plant is determined by the characteristics of the Texaco gasification process and the results of specific studies carried out in Task 1. These studies considered the following questions:

- o Acid gas removal
- o Oxygen purity
- o Coal washing
- o Sulfur recovery

Support facilities studies include:

- o Equipment Drives
- o Gas Storage and Spaces
- o Gas Delivery Pressure
- o Effects of Scale
- o Effects of Load Change

It was concluded that the conceptual design of the coal gasification plant should be based on unwashed coal, 98 volume % oxygen, and production of sulfur by-product in the form of prilled elemental sulfur. The Selexol process was preferred to remove acid gas from raw coal gas.

The general processing sequence for the plant based on the Texaco gasifier reflects the characteristics of the gasifier. Pulverized coal is gasified under super atmospheric pressure with oxygen. Gasification occurs at high temperature (about 2500°F), and the gas produced is rich in carbon monoxide and hydrogen. Because of the high gasification temperature, the raw gas contains only small amounts of methane and essentially no oil, tar or phenols. As a result, the main processing units downstream of the gasification section consist only of gas cooling and acid gas removal.

Foster Wheeler established capacity factors to be used in the conceptual design of the various plant sections with the exception of gasification which is based on information supplied by the Texaco Development Corporation. The capacity factors, which were defined as the ratio of design capacity to normal material balance, reflected expected variations in coal feed analyses. In addition, Foster Wheeler selected spare trains and/or back-up systems to achieve an expected on-stream factor of about 90% for a module. The capacity factors are given in Foster Wheeler's supplement to TVA's Design Criteria. On-stream factor considerations are given in the discussion in Section 3.6 Volume 2 Study Assessments and Process Selection.

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2.1 Choice of Processing Sequence (cont'd)

Process selection depends upon economics, experience with the process application and upon the characteristics of the Texaco gasifier. In addition to the selection of the process units, there is also the problem of selection of the process configuration involving the arrangement of units, number of trains, multiple part-capacity equipment items all integrated with the optimum plant capacity. Some configuration limitations are due to the state of development of the gasifier, some to equipment size and scale limitations as well as product demand variation and high risk, high maintenance items.

Block Flow Diagram

Drawing No. 54099-4-50-35-1 is a block flow diagram illustrating a coal conversion MBC plant using the Texaco gasifier. As shown in the diagram, coal, air, and water are the only raw materials entering the plant. Medium-Btu gas is the only product leaving the plant together with by-products of sulfur, carbon dioxide and slag.

The accompanying Process Block Flow Diagram provides an overview of the main processing units selected for preparing medium Btu gas based on incorporating Texaco's gasification reactor. A brief review of the schematic which traces the flow of raw materials into finished product is furnished below, as well as a more detailed description of each individual unit.



2.1 Choice of Processing Sequence (Cont'd)

Raw coal is received from barges and is transported to coal storage piles. The coal is crushed, pulverized, slurried and fed to the gasifier, where it is reacted with oxygen from the air separation plant. The gasifier product gas is cooled and scrubbed free of solids, after which the acid gas components, CO_2 , H_2S and COS , are removed in the Selexol unit. Slag emanating from the gasifier is removed to a slag disposal area; waste water generated from various processing units is treated by steam stripping. The hydrogen sulfide removed in the acid gas treating step is further processed to recover saleable sulfur, in-primed form. The resulting clean medium Btu gas is sent to the distribution system.

Support facilities common to these various units include: utilities waste water treating, flare/incineration, and cooling tower.



2.2.

General Description of FlowSection 100 - Coal Receipt and Handling

Coal is delivered by barge to the plant as essentially 3" x 0 material. Coal is unloaded from the barges, broken to remove over-size pieces, and transferred to live storage or dead storage as required. Provision is made for receipt of about 5% of the coal by truck. During normal operation of plant, coal is reclaimed from live storage and delivered to a coal crusher which reduces the size to 1/2" x 0 as required for Section 300.

Section 200 - Air Separation Plant

Oxygen as required for gasification in the Texaco gasifier is produced as a 98% by volume oxygen stream from the air separation plants. The Texaco gasification process requires approximately 4,424 tons per day of oxygen to gasify 4,800 TPD of Kentucky Number 9 coal per module. The coal feed is expressed on a dry basis.

Principal components of the air separation plant are:

- o Air compression to a pressure of approximately 75 psig
- o Low temperature air fractionation
- o Oxygen compression to a pressure of about 980 psig for the Texaco gasifiers

Liquid oxygen storage (24 hour consumption in one module) and high pressure gaseous oxygen storage (15 minutes consumption in one module) are provided as back-up supply of oxygen during short term outages of the air separation plant. Storage is provided in order to insure the required 90% operating factor for the plant.

The air separation plant produces nitrogen which is used for inert gas blanketing, instrument service, purges and other miscellaneous services. Liquid nitrogen storage of 250 tons is provided as a back-up nitrogen supply. Liquid nitrogen vaporization rate of 30 tons per hour has been used to meet the estimated plant needs with a delivery pressure of 100 psig.

Section 300 - Coal Gasification

Section 300 includes all of the equipment specified by the Texaco Development Corporation for the Texaco coal gasification process. Sized coal 1/2" x 0 is delivered to a coal feed bin included in Section 300. The coal is then pulverized in a rod mill using a wet grinding technique. The discharge from the mill is then fed to a slurry makeup system which



produces a coal/water slurry of proper consistency for pumping to the gasifiers. Coal fines and dirty water streams recovered downstream of the gasification system are recycled to the mill in order to minimize any carbon losses from the plant.

The coal/water slurry is pumped into the gasifier where it is gasified at high temperatures. With oxygen, the gasifier operating pressure is 750 psig which meets the final product gas requirements of 600 psig at battery limits without further compression. The gasifier effluent, which contains molten ash and the hot product gas, flows through a cooling section which generates 900 psig steam. Slag is discharged from the bottom of the gasification unit through a lock hopper system and discharged as a wet product to battery limits.

The partially cooled gas next flows through a three-stage scrubbing system for carbon removal. The scrubbed gas of a temperature of approximately 286°F then flows to a COS hydrolysis unit which is not included in the scope of Texaco's supply. The gas from the hydrolysis system is returned to the Texaco unit, Section 300, at a temperature of about 330°F and is then cooled to a final temperature of 110°F. The gas stream at this point contains less than 1 ppm by weight of carbon and flows to the sulfur removal system.

Various water streams, including water condensed from the gas, is collected and processed to clarify the water for the use in the process. A waste stream of about 300 gpm per module is sent to Section 700 for waste treatment. Recovered carbon is recycled to the wet coal grinding system.

Section 400 - Acid Gas Removal

The raw medium Btu gas from Section 300 contains sulfur compounds which must be removed. The bulk of the sulfur from the coal is as hydrogen sulfide with a smaller portion as carbonyl sulfide. COS is hydrolyzed in a catalytic reactor at a temperature of about 330°F. This reduces the COS content to about 13 ppm volume. Allied's Selsol process has been picked as suitable for removal of the H₂S for this particular application. This process uses a solvent consisting of dimethyl ether of polyethylene glycol (DMPEG), can be designed to provide a high degree of selectivity between hydrogen sulfide and carbon dioxide, and also has dehydration capabilities thus allowing the gas to meet the moisture specification of 7 lbs/MMSCF without further drying. This process is a physical absorption process and the relatively high partial pressure of H₂S is a factor in making this process attractive for the present plant design.



Carbon dioxide removal is also required in addition to H₂S removal in order to meet the GHV requirement of 285 Btu's per standard cubic foot in the purified product gas. Accordingly, design capacity has been provided in the Selexol unit to remove the required amount of CO₂.

The purified gas from the Selexol unit is delivered directly to battery limits at about 600 psig. No further treatment nor compression is required to meet the specifications for this plant.

Section 500 - Treated Gas Compression

This section is not required for this process.

Section 600 - Sulfur Recovery

In accordance with the Task I recommendation, sulfur compounds in the acid gas stream are converted to elemental sulfur using a Claus process followed by a Beavon tail gas treating unit. The hydrogen sulfide concentration in the acid gas stream from the Selexol unit is about 18.5%. Accordingly, a split flow variation of the Claus process is used to obtain over 95% conversion of H₂S to elemental sulfur. The low H₂S concentration in the acid gas requires that the Claus plant be provided with supplemental fuel. Product gas is used for this purpose.

In order to limit the sulfur emissions from the Sulfur Recovery Section, the Beavon sulfur recovery process is used to treat the tail gas. Overall sulfur recovery is increased to about 99.9% which meets sulfur recovery unit emission standards of 200 ppm or less of sulfur compounds in treated tail gas.

Molten elemental sulfur produced in the Claus and Beavon units is converted to solid prills in a Chemsourc sulfur prilling process. In this operation molten sulfur is sprayed into a circulating stream of water. Solid prills of uniform size are produced and then separated from the water stream. De-watered prills are sent to storage for eventual shipment from the site.

Section 700 - Sour Water Stripping

The water condensed during cooling of the gas stream from the Texaco gasifiers is contaminated with small amounts of sulfites, cyanides, thiocyanates, formates, ammonia and solids. While much of the water is recycled, a portion must be withdrawn from the system for waste water treatment. The waste water is treated with iron sulfate and lime, is clarified, filtered, and then flows through an ammonia stripper, which removes the ammonia stream for disposal. The water from the ammonia stripper is neutralized and then flows to a biological oxidation clarifier before final

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discharge to sewer.

Section 800 - Ash and Slag Handling

In the Texaco gasifier approximately 100% of the coal ash is converted to an inert slag. This material is discharged through equipment provided in Section 300. The slag discharge screens in Section 300 discharge on to conveyor and the material is then conveyed to a 56 hour slag pile before final discharge to the long-term slag storage pile. Fines accumulated in the screens' sumps are recycled to the coal pulverizers.

Section 1200 - Utility Area

The utility Area includes:

- o Raw water storage and treatment
- o Potable water treatment
- o BFW and condensate treatment
- o Steam generation
- o Plant and instrument air inert gas

Raw water is taken from the river, filtered and softened. This water is used for cooling tower makeup and for process water makeup as well as for feed for boiler feed water treatment. A portion of the softened water is further treated by chlorination to provide potable water.

Softened water is treated by ion exchange to provide water of satisfactory quality for use as boiler feed water in the high pressure steam systems. Recovered condensate is treated in an ion exchange system to "polish" the water for reuse in steam generation.

The Texaco coal gasification waste heat boilers normally generate adequate steam for operation of the plant. Foster Wheeler coal fired fluidized bed boilers are supplied for startup purposes. The high pressure steam generated in the Texaco waste heat boilers is saturated and must be superheated before prior use. A coal fired fluidized bed boiler super heater is provided for this purpose. Sulfur dioxide emissions are controlled in the Foster Wheeler fluid bed boilers by the addition of limestone which captures sulfur dioxide produced during combustion. The spent limestone is sent to long-term solid waste storage.

Plant and instrument air systems are based on the use of nitrogen produced as the byproduct in the Air Separation section.

Form No. 130-171



Section 1300 - Cooling Water System

Cooling water used in process heat exchangers and exhaust steam condensing systems is cooled in mechanical draft cooling towers. Blow-down from the cooling water is treated for recovery of chromates and then sent to Waste Water Treatment.

Section 1400 - Flare and Incineration

Flares are provided to handle startup and emergency disposal of gas. An incinerator is provided to handle disposal of any combustible wastes or gases which can not be flared.

Section 1500 - Waste Water Treatment

Waste water collected in the plant based on the Texaco gasifiers is comprised of cooling tower blowdown, water treatment and steam generation blowdowns, and sanitary treatment effluent. In addition, water runoff from coal storage piles and long-term solid waste storage piles is added to the waste water.

The treatment system provided for waste water includes API separator, air floatation, surge basin and activated sludge biological oxidation systems and final holding ponds. Water from these final ponds is discharged to the river.

Section 2000 - General Facilities

General facilities for the coal gasification plant include:

- o Long-term solid waste storage
- o Byproducts and chemicals storage
- o Power, lighting and communications
- o Roads and fences
- o Firewater systems
- o Sewage plant
- o Interconnecting piping

Storage of solid wastes accumulated over a 20 year period is provided. The major byproduct storage for the plant other than waste solids is elemental sulfur prills. Chemicals storage includes water chemicals, solvents and



limestone. The water system is based on drawing water from the river. The raw water storage tank serves as fire water reservoir as described in Section 1200.

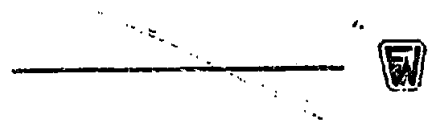
Section 2100 - Buildings

Buildings are provided as required in TVA's Design Criteria, Section 1, Paragraph 1.3.

Section 2200 - Dock Facilities

Dock facilities are provided to receive and handle barges delivering coal and barges handling sulfur shipments.

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2.3 NOMINAL CAPACITIES OF PROCESSING UNITS



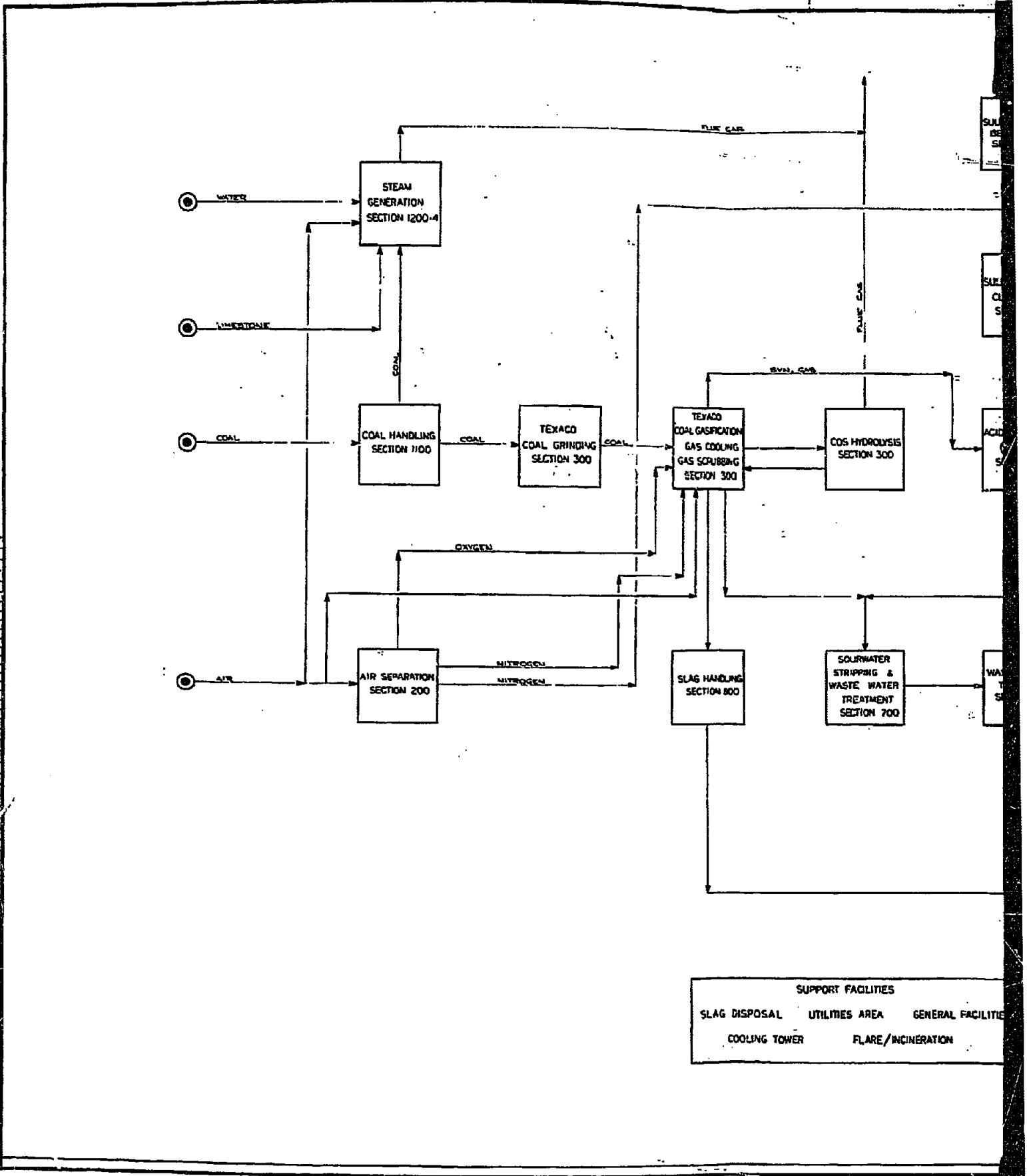
Nominal Capacities of Processing Units

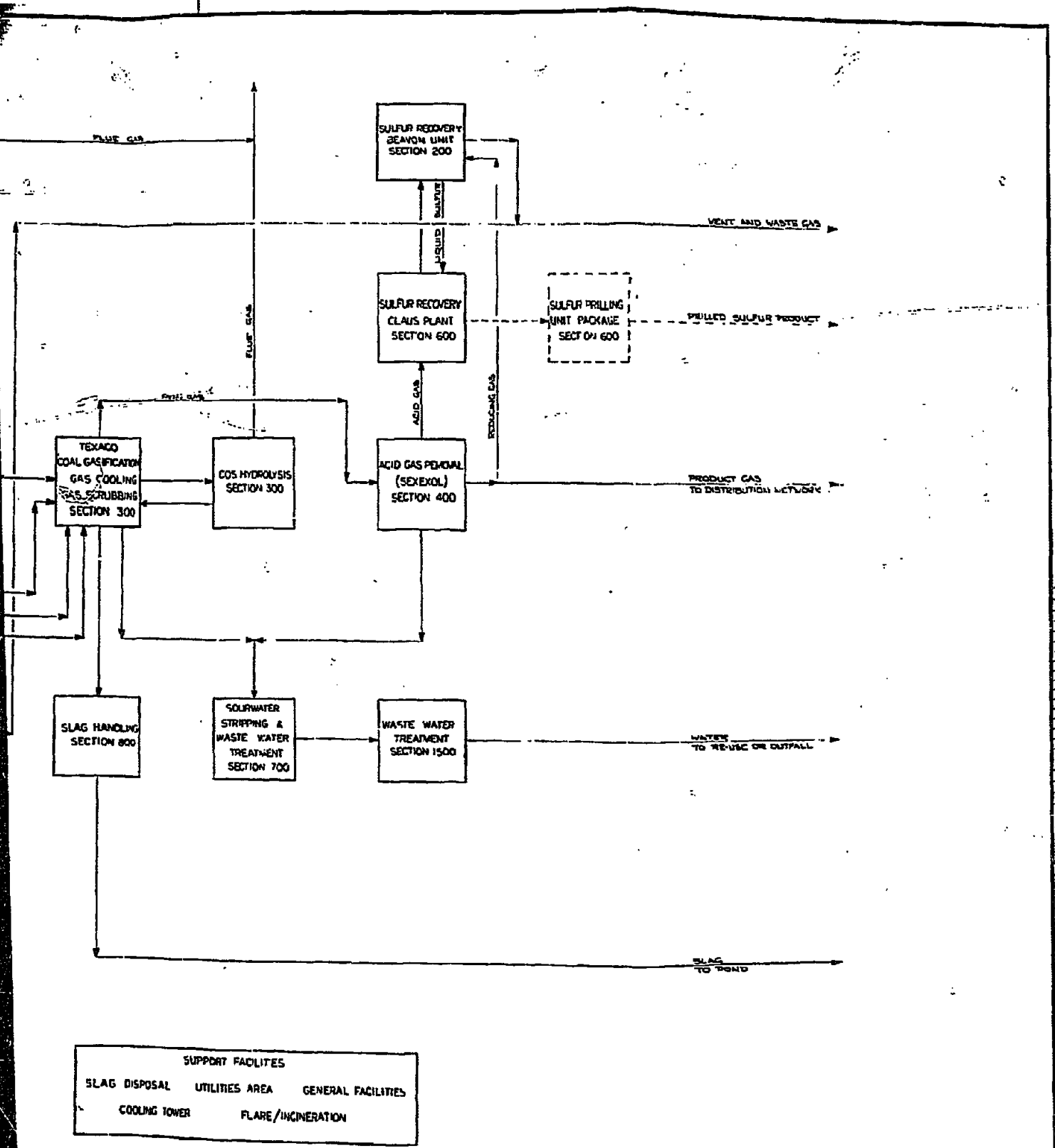
Process Unit	Units	Nominal Capacity	
		1 Module	4 Modules
100 Coal Handling and Preparation	TPD	5,642.5	22,570
200 Air Separation Oxygen Production	TPD	4,424	17,696
300 Coal Gasification	TPD	5,000	20,000
400 Acid Gas Removal Gas Processed	MMSCFD	324.7	1,298.8
500 Product Gas Compressor	MMSCFD	-	-
600 Sulfur Recovery	LTPD	196	784
700 Sour Water Stripping	GPM	500	2,000
800 Ash Handling	TPD	750	3,000
900 Phenol Recovery	TPD	-	-
1000 Ammonia Recovery	TPD	-	-
1200 Utilities Area			
Raw Water Treatment	GPM		24,400
Potable Water Treatment	GPM		300
BFW Treatment	GPM		2,240
Condensate Treatment	GPM		7,600
Steam Generation	TPD		34,858
Flue Gas Cleaning	MMSCFD	-	-
1300 Cooling Water System			
Cooling Water Circulation	GPM	175,000	700,000
Blow Down Treatment	GPM		4,000
1400 Flare	MMBTU/HR	2,000	8,000
1500 Waste Water Treatment	GPM		4,320

Form No. 130 1-1



2.4 BLOCK FLOW DIAGRAM





SUPPORT FACILITIES

SLAG DISPOSAL UTILITIES AREA GENERAL FACILITIES

COOLING TOWER FLARE/INCINERATION

...BLOCK FLOW DIAGRAM
 TVA COAL GASIFICATION STUDY
 TEXACO GASIFIERS ONE MODULE

AMERICAN OVERSEAS CORPORATION
 CHEMICAL PROCESSING DIVISION
 MOBILE, ALABAMA, U.S.A.

DATE: 08-11-58 34099 078-34099-35-1-50-0



TVA Coal Gasification Study
Texaco Gasifier

SECTION DESCRIPTION

3.1

SECTION 100-COAL PREPARATION

A. Reference Material:

- . Process Flowsheet FWEC Dwg. No. 54099-35-1-50-1
- . Elevation Drawing FWEC Dwg. No. 54099-35-1-01-1
- . Equipment List

B. Description of Flow

The unit is designed to receive and store coal, and transport it to four (4) coal gasification modules.

3" x 0" coal (8" maximum lump) is received in 1500 ton barges, and removed by barge unloader 35-UD101. Coal is then conveyed to unloader surge bin 35-TK101. Prior to entering the surge bin, tramp iron is removed by unloader magnetic separator 35-S101. Then the coal is conveyed from the surge bin to sampling station 35-SS101 and 35-SS102. Incoming inventory will be determined by sampling station feed weigh scales 25-WS101 and 35-WS102.

Coal will also be received by trucks, dumping into truck receiving hopper 35-TK102 in 25 ton batches. Coal is then conveyed directly to sampling station 35-SS101 and 35-SS102. Prior to sampling, tramp iron is removed by truck receiving magnetic separator 35-S102. Incoming inventory in this case will be determined by truck weigh scale 35-WS103.

Upon sampling, all coal drops to vibrating screens 35-SN101, 35-SN102, 35-SN103 and 35-SN104, where oversized lumps (+6") are conveyed directly to loadout and 90 day open dead storage. Unders (-6") are conveyed either to dead storage or enclosed live storage in storage silos 35-TK103, 35-TK104, 35-TK105 and 35-TK106. Incoming inventory to dead storage is determined by load-out weigh scale 35-WS104. Incoming inventory to live storage is determined by silo feed weigh scale 35-WS105.

Live storage reclamation is handled by silo discharge feeders 35-FD104A-G, 35-FD105A-G, 35-FD106A-G and 35-FD107A-G, and the coal is conveyed to coal feed crushers 35-SR101, 35-SR102, 35-SR103 and 35-SR104. Dead storage reclamation is done by a front-end loader dumping coal into dead storage reclaim hoppers 35-TK107 and 35-TK108, then conveying to the coal feed crushers.

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TVA Coal Gasification Study
Texaco Gasifier

The crushers break the coal down to 1/2" x 0" particle size and discharges it to the gasifier feed conveyors 35-CR117A/B. The gasifier feed conveyors will transport the material to the overhead bunker fill conveyors 35-CR118A/B feeding the coal feed bins or to the steam generator transfer conveyors 35-CR120A/B, which conveys the material onto the steam generator fill conveyors 35-CR119A/B.

All equipment from the gasifier feed conveyors to the storage bunkers are provided with one operating and one spare train.

Limestone Storage

Limestone will be delivered to the plant site by barge, then loaded into trucks. The trucks will be equipped with pneumatic unloaders for unloading into the 5000 ton limestone storage silo. Limestone will be removed from the silo using vibrating bin bottom 35-BV101 and will be fed into a pneumatic transport line by 2 rotary feeders 35-FD110A/B leading the material to the steam generator limestone storage bunkers. The pneumatic transport line will be equipped with silencers before and after pneumatic transport blowers 35-B101A/B for noise suppression.

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TVA Coal Gasification Study

Barge Unloading System

A power winch system for barge pulling has been contemplated and included in Item UD-101, of the equipment list for Section 100, Coal Preparation. The barge puller is designed to move a line of coal laden barges, already moved, and eventually, a single barge only during the actual coal unloading operation of that barge.

Considering the scale of the Key Plot Plan, 1 in. = 400 Ft., the barge puller is not shown. It does not appear on the Process Flow Diagrams of Section 100, either, as it is an ancillary device which does not serve to clarify the movement and treatment of the product, coal, the principal purpose of the Process Flow Diagrams.

The cost of the barge puller is included as part of the hardware costs of equipment Item UD-101, for each of the coal gasification plants.

The foregoing comments apply as well to the barge cleanout system which consists of a small front end loader and a single bucket crane which loads the residual coal into a barge dedicated to the plant site for cleanout service. When it becomes full, the dedicated barge is moved into the unloading line and is then replaced by another of the empty barges.

Movement of single barges, other than those operated by the power winch, is effected by means of a 750 hp switch boat for which pricing provisions have been made in our estimate of plant costs.



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 CUSTOMER: TVA/TEXACO
 LOCATION: MURPHY HILLS, ALABAMA

SECTION NAME: COAL PREPARATION
 REF. DWG.: 54092-35-1-50-1
 CONTRACT NO.: 11-35-5409

SECTION NO.: 104
 PAGE NO.: 1 OF 3
 DATE: 6/30/80

EQUIPMENT SUMMARY

ITEM	DESCRIPTION	DEFINITION	DESIGN * TEMP. (°F)	DESIGN * PRESS. (PSIG)	CONSTRUCTION MATERIAL *
35-B101A/B	Pneumatic Transport Supply Blowers				
35-BV101	Vibrating Discharger	20 TPH			
35-CR101	Unloader Transfer Conveyor	Part of UD-101			
35-CR102	Surge Bin Feed Conveyor	84" Belt, 4,800 TPH			
35-CR103	Sampling Station Feed Conveyor	48" Belt, 1,600 TPH			
35-CR104	Sampling Station Feed Conveyor	48" Belt, 1,600 TPH			
35-CR105	Truck Receiving Transfer Conveyor	30" Belt, 125 TPH			
35-CR106	Oversize Coal Coll. Conveyor	30" Belt, 128 TPH			
35-CR107	Oversize Coal Transfer Conveyor	30" Belt, 128 TPH			
35-CR108	Screen Collecting Conveyor	48" Belt, 1,600 TPH			
35-CR109	Screen Collecting Conveyor	48" Belt, 1,600 TPH			
35-CR110	Dead Storage Load-Out Conveyor	66" Belt, 3,200 TPH			
35-CR111	Silo Fill Conveyor	66" Belt, 3,200 TPH			
35-CR112	Silo Fill Conveyor	66" Belt, 3,200 TPH			
35-CR113	Silo Fill Conveyor	66" Belt, 3,200 TPH			
35-CR114	Silo Feed Conveyor	66" Belt, 3,200 TPH			
35-CR115	Silo Disch. Collecting Conveyor	48" Belt, 1,250 TPH			
35-CR116	Reclaim Collecting Conveyor	48" Belt, 1,250 TPH			
35-CR117A/B	Gasifier Feed Conveyor	48" Belt, 1,250 TPH EA.			
35-CR118A/B	Overhead Bunker Fill Conveyor	48" Belt, 1,250 TPH EA.			
35-CR119A/B	Steam Generator Fill Conveyors	48" Belt, 1,250 TPH EA.			
35-CR120A/B	Stm. Gen. Transfer Feed Conveyors	48" Belt, 1,250 TPH EA.			
35-DC101	Coal Preparation Dust Coll. Sys.				
35-DP101	Dust Suppression System				
35-F101	Silo Vent Filter				
35-F102	Silo Vent Filter				
35-F103	Silo Vent Filter				
35-F104	Silo Vent Filter				

* SHELL/TUBE WHERE APPLICABLE

11-35-5409-1

11-35-5409-1



FOSTER WHEELER ENERGY CORPORATION
 CUSTOMER: TWA/TEXACO
 LOCATION: MURPHY HILL, ALABAMA

SECTION NAME: COAL PREPARATION
 REF. DWG.: 54099-35-1-50-1
 CONTRACT NO.: 11-35-54099 REV.: 0

SECTION NO.: 100
 PAGE NO.: 2 OF 3
 DATE: 6/30/80

EQUIPMENT SUMMARY

ITEM	DESCRIPTION	DEFINITION	DESIGN * TEMP. (°F)	DESIGN * PRESS. (PSIG)	CONSTRUCTION MATERIAL #
35-F105	Silo Filter Separator				
35-FD101	Unloader Surge Bin Feeder	84" x 120", 1,600 TPH			
35-FD102	Unloader Surge Bin Feeder	84" x 120", 1,600 TPH			
35-FD103	Truck Receiving Feeder	24" x 42", 125 TPH			
35-FD104A-G	Silo Discharge Feeder	30" Belt, 3 @ 417 TPH, 4 @ 313 TPH			
35-FD105A-G	Silo Discharge Feeder	30" Belt, 3 @ 417 TPH, 4 @ 313 TPH			
35-FD106A-G	Silo Discharge Feeder	30" Belt, 3 @ 417 TPH, 4 @ 313 TPH			
35-FD107A-G	Silo Discharge Feeder	30" Belt, 3 @ 417 TPH, 4 @ 313 TPH			
35-FD108	Reclaim Hopper Discharge Feeder	48" x 72", 1,250 TPH			
35-FD109	Reclaim Hopper Discharge Feeder	48" x 72", 1,250 TPH			
35-FD110A/B	Rotary Feeders	20 TPH EA.			
35-S101	Unloader Magnetic Separator	84"			
35-S102	Truck Receiving Magnetic Separator	30"			
35-S103	Dead Storage Reclaim Mag. Sep.	48"			
35-S104	Live Storage Reclaim Mag. Sep.	48"			
35-SL101	Silencer				
35-SL102	Silencer				
35-SN101	Vibrating Screen	8' x 20' Single Deck, 800 TPH			
35-SN102	Vibrating Screen	8' x 20' Single Deck, 800 TPH			
35-SN103	Vibrating Screen	8' x 20' Single Deck, 800 TPH			
35-SN104	Vibrating Screen	8' x 20' Single Deck, 800 TPH			
35-SR101	Coal Feed Crusher	44 x 93, 1,250 TPH			
35-SR102	Coal Feed Crusher	44 x 93, 1,250 TPH			

* SHELL/TUBE WHERE APPLICABLE



FOSTER WHEELER ENERGY CORPORATION
 CUSTOMER: TVA/TEXACO
 LOCATION: MURPHY HILL, ALABAMA

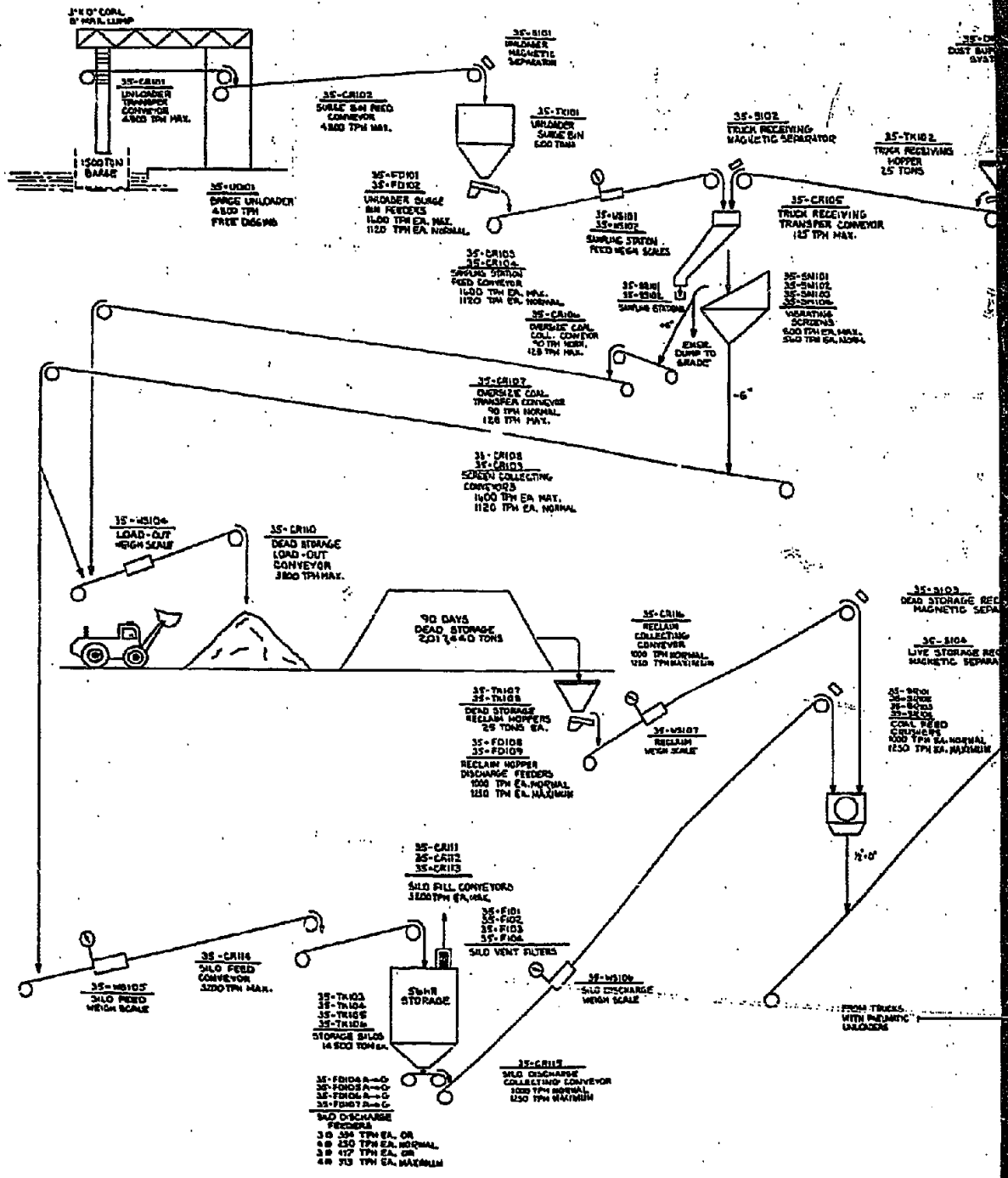
SECTION NAME: COAL PREPARATION
 REF. DWG.: 54099-35-1-50-1
 CONTRACT NO.: 11-35-54099 REV.: 0

SECTION NO.: 100
 PAGE NO.: 3 OF 3
 DATE: 5/30/80

EQUIPMENT SUMMARY

ITEM	DESCRIPTION	DEFINITION	DESIGN # TEMP. (°F)	DESIGN # PRESS. (PSIG)	CONSTRUCTION MATERIAL #
35-SR103	Coal Feed Crusher	44" X 93", 1,250 TPH			
35-SR104	Coal Feed Crusher	44" X 93", 1,250 TPH			
35-SS101	Sampling Station	2 - Stage, 1,600 TPH			
35-SS102	Sampling Station	2 - Stage, 1,600 TPH			
35-TK101	Unloader Surge Bin	600 Ton Capacity			
35-TK102	Truck Receiving Hopper	25 Ton Capacity			
35-TK103	Storage Silo	14,500 Ton Capacity			
35-TK104	Storage Silo	14,500 Ton Capacity			
35-TK105	Storage Silo	14,500 Ton Capacity			
35-TK106	Storage Silo	14,500 Ton Capacity			
35-TK107	Dead Storage Reclaim Hopper	25 Ton Capacity			
35-TK108	Dead Storage Reclaim Hopper	25 Ton Capacity			
35-TK109	Limestone Silo	5,000 Ton Capacity			
35UD101	Barge Unloader	4,800 TPH			
35-WS101	Sampling Station Fd. Weigh Scale	48" W, 1,600 TPH			
35-WS102	Sampling Station Fd. Weigh Scale	48" W, 1,600 TPH			
35-WS103	Truck Weigh Scale	10' X 60'			
35-WS104	Load-Out Weigh Scale	66" W, 3,200 TPH			
35-WS105	Silo Feed Weigh Scale	66" W, 3,200 TPH			
35-WS106	Silo Discharge Weigh Scale	48" W, 1,168 TPH			
35-WS107	Reclaim Weigh Scale	48" W, 1,168 TPH			

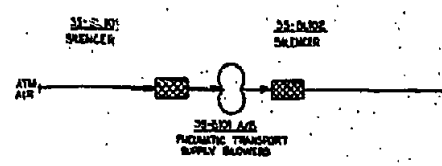
* SHELL/TREE WHEEL APPLICABLE

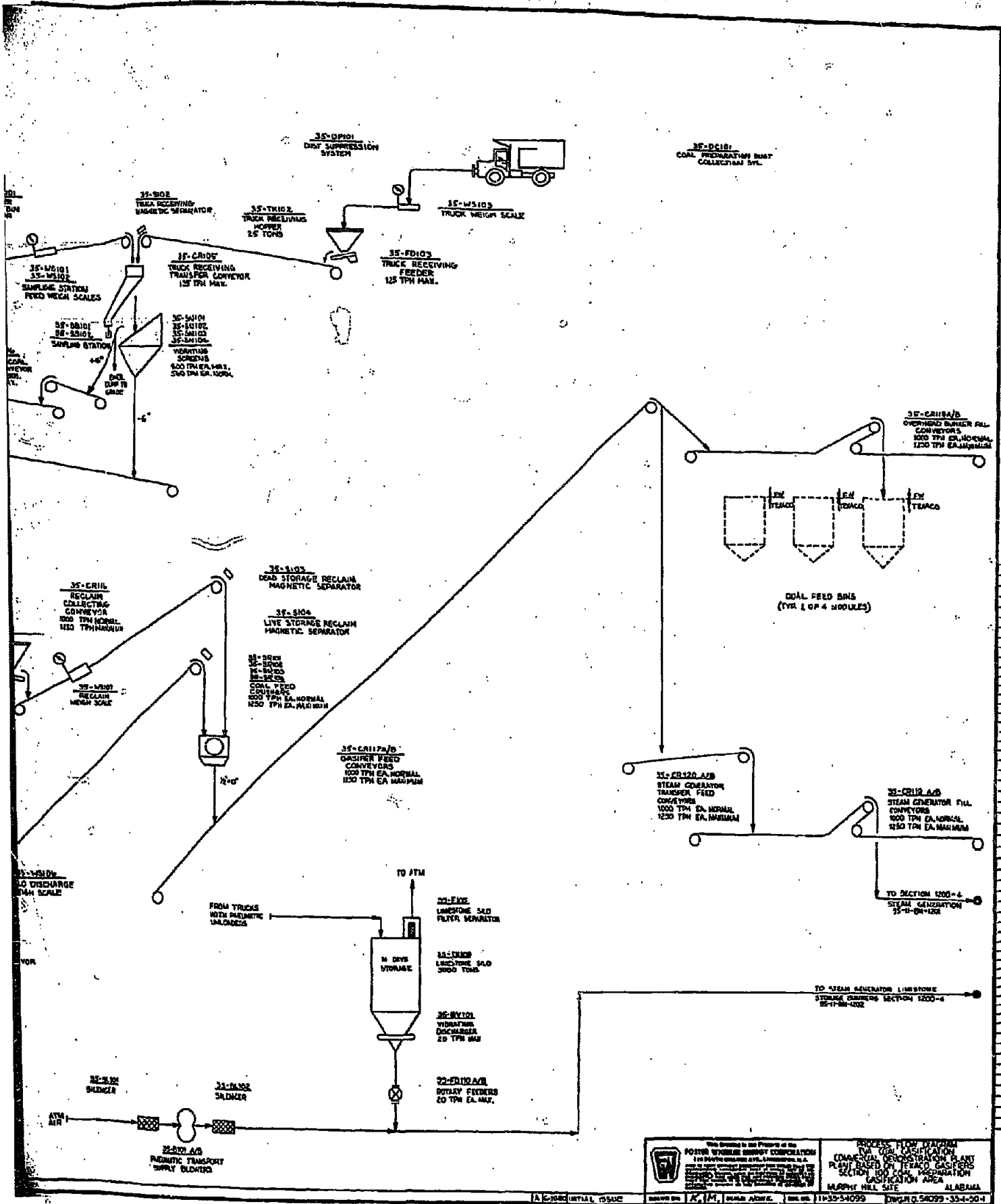


LEGEND

	INTERNAL BALANCE STREAM NUMBER		PROCESS STREAMS TO B.L.
	OPERATING TEMPERATURE °F		PROCESS STREAMS FROM B.L.
	OPERATING PRESSURE P148		

35-FD108A-D
35-FD108B-G
35-FD109A-C
35-FD109B-G
SLO DISCHARGE FEEDERS
3.0 354 TPH EA. OR
4.0 450 TPH EA. NORMAL
3.0 417 TPH EA. OR
4.0 373 TPH EA. MAXIMUM





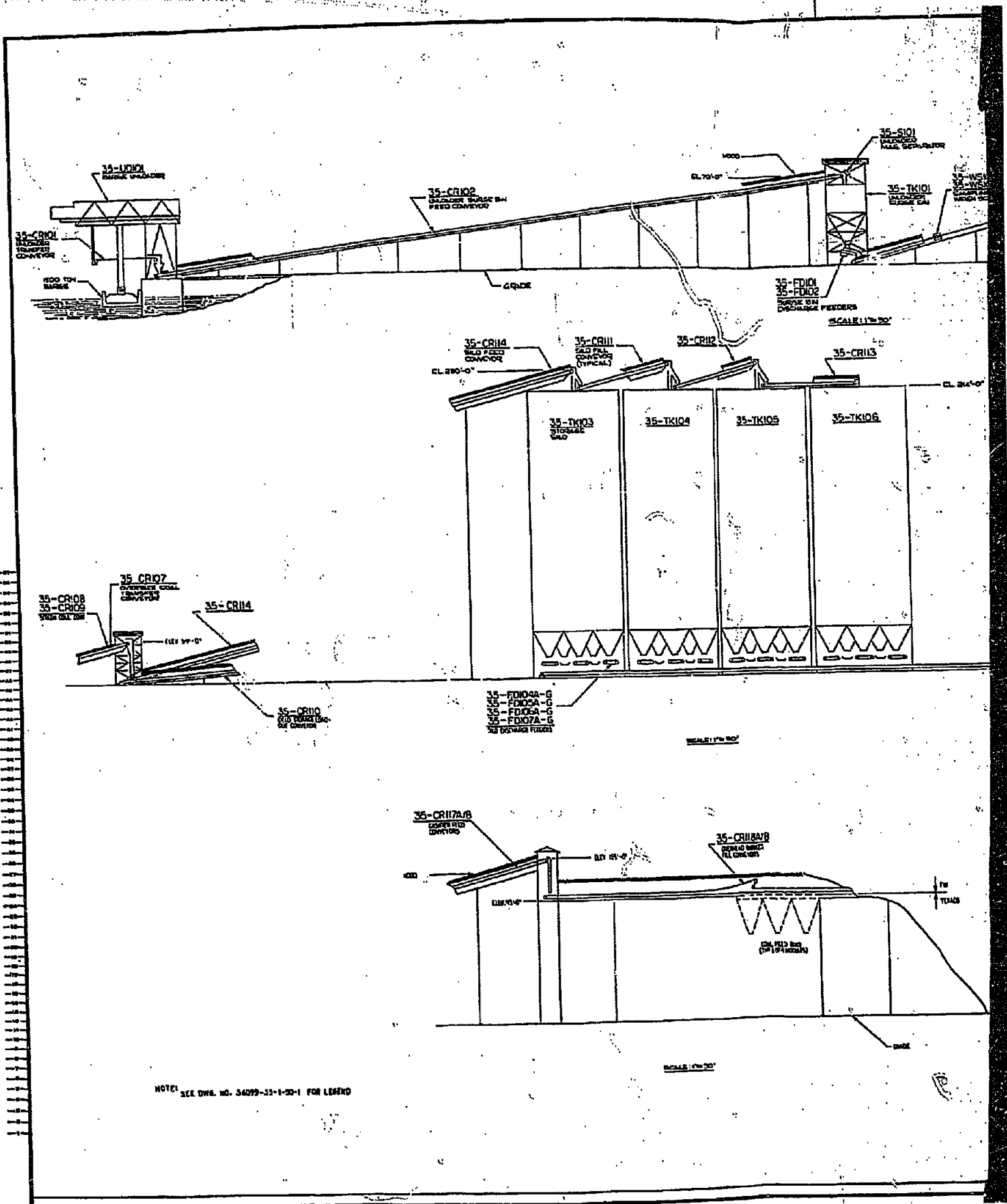
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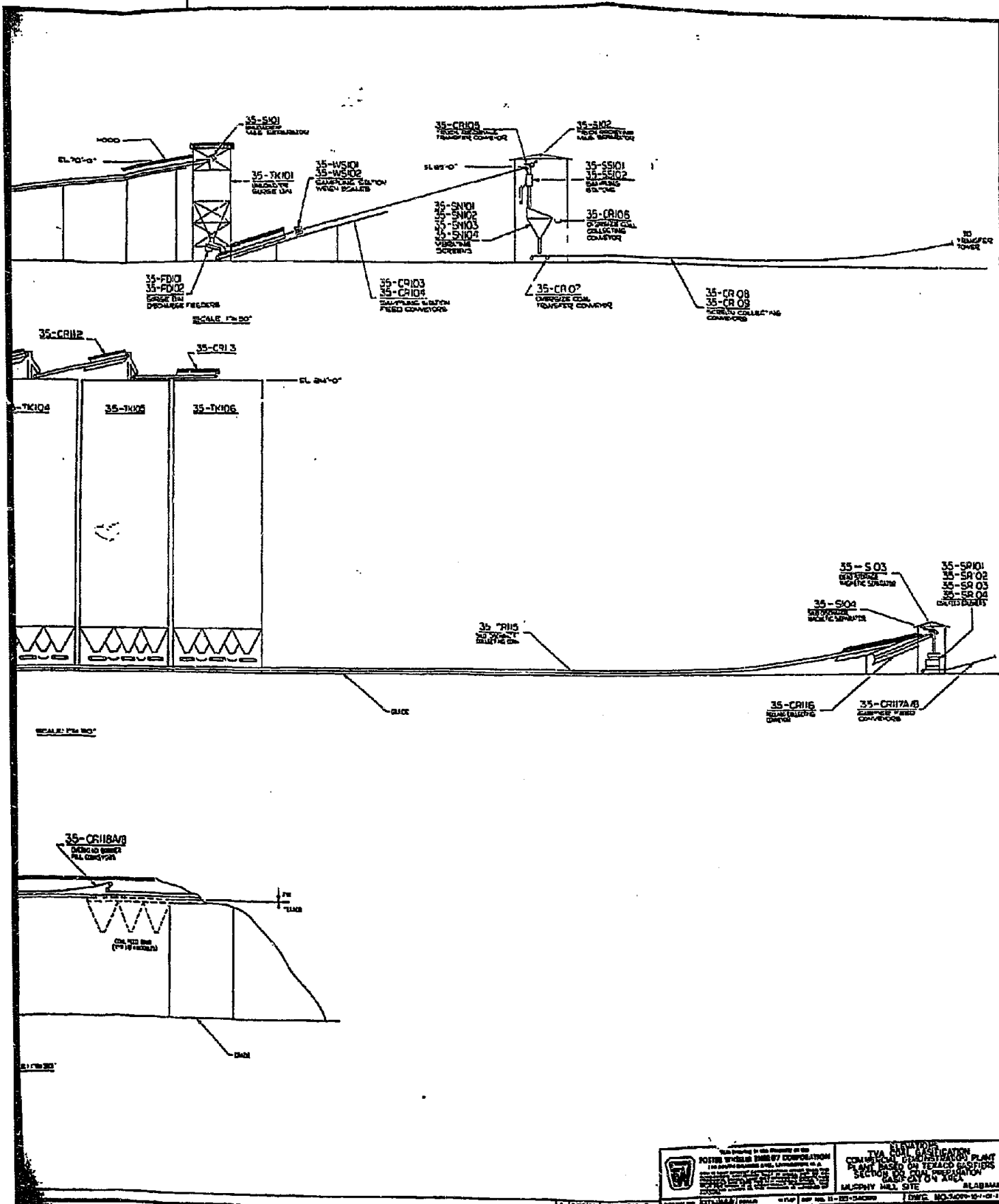
PROJECT: 1-17-1938
 DRAWING: 35-1-34099

MOBILE, ALABAMA

MURPHY HILL SITE ALABAMA

DRAWN BY: D. S. C. 35-1-34099-35-4-30-1





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TVA ENVIRONMENTAL RESTORATION PROGRAM
 COMMERCIAL UTILIZATION PLANT
 PLANT BASED ON TERACO EASTPUS
 SECTION ON COAL REFINERY
 MURPHY HILL SITE ALABAMA

A. CR103 | INITIAL STUDY | DRAWING NO. 11-251-24300 | DATE: 06/20/97

FOSTER WHEELER ENERGY CORPORATION



TVA coal Gasification Study
Texaco Gasifier

SECTION DESCRIPTION

3.2 SECTION 200 - AIR SEPARATION PLANT

A. Reference Material:

- . Process Flowsheet FWEC Drwg No. 54099-35-1-50-2
- . Equipment List
- . Input/Output Major Stream Flows

B. Description of Flow

Filtered air is compressed to approximately 90 PSIG in Air Compressors (35-12-C-201A/B). Intercoolers, an aftercondenser, and K.O. Drum are provided. Condensate leaving the K.O. Drum flows to the cooling tower. One Air Compressor is motor driven and one turbine driven per air plant.

Some compressed air is fed to the gasifier during startup. Normally compressed air is fed only to the Cold Box Package (35-12-PG-201).

The Cold Box Package produces nitrogen containing about 10 ppmv O₂ and oxygen of about 98 vol % O₂ purity. Waste nitrogen is vented through the Waste Nitrogen Silencer (35-12-SL-201) to atmosphere. Oxygen gas leaving the Cold Box Package is compressed to a pressure of about 900 PSIG by the Oxygen Compressor (35-12-C-202A/B). Intercoolers will be provided by the compressor manufacturer. A fraction of the compressed oxygen is sent to the Gasification Section 300. A smaller fraction is boosted to about 3,000 PSIG by the O₂ Storage Feed Compressor and flows to the Gaseous Oxygen Storage Tanks (35-11-TK-20A/B/C/D). Stored oxygen is provided to insure continuity of a gasifier operation during shut down air plant outages.

The liquid oxygen product leaving the Cold Box Package (35-12-PG-201) enters the Liquid Oxygen Storage Tank (35-11-TK-201). When required, liquid oxygen is vaporized in the Liquid Oxygen Vaporation Package (35-11-PG-204), then combined with oxygen from the O₂ Storage Feed Compressors in both air plants (two air plants per module). The combined gaseous oxygen stream enters the Gaseous Oxygen Storage Tanks.

Form No. 130-171

FOSTER WHEELER ENERGY CORPORATION



Liquid nitrogen leaves the Cold Box Package and enters the Liquid Nitrogen Storage Tank (35-11-TK-203). When required, liquid nitrogen is vaporized in the Nitrogen Vaporization Packages (35-11-PG-203A/B). Vaporized nitrogen from Nitrogen Package PG-203A is sent to the Gasifier in Section 300, while vaporized nitrogen from Nitrogen Vaporization Package PG-203B is used for Plant Instruments.

Gaseous nitrogen from the Cold Box Package, PG-201, enters the Plant Nitrogen Package (35-12-PG-202). Compressed nitrogen leaving the Knockout Drum at a pressure of about 585 PSIG is distributed to process users. A fraction of the compressed nitrogen utilized by plant instruments, the remainder used for purging, blanketing, coal system shutdown, coal treatment and coal feed system.



FOSTER WHEELER ENERGY CORPORATION
 CUSTOMER: TVA COAL GASIFICATION
 LOCATION: ALABAMA
 PLANT TYPE: TEXACO GASIFIER

SECTION NAME: AIR SEPARATION PLANT
 REF. DWG.: 54099-35-1-50-2
 CONTRACT NO.: 11-35-54099 REV.:

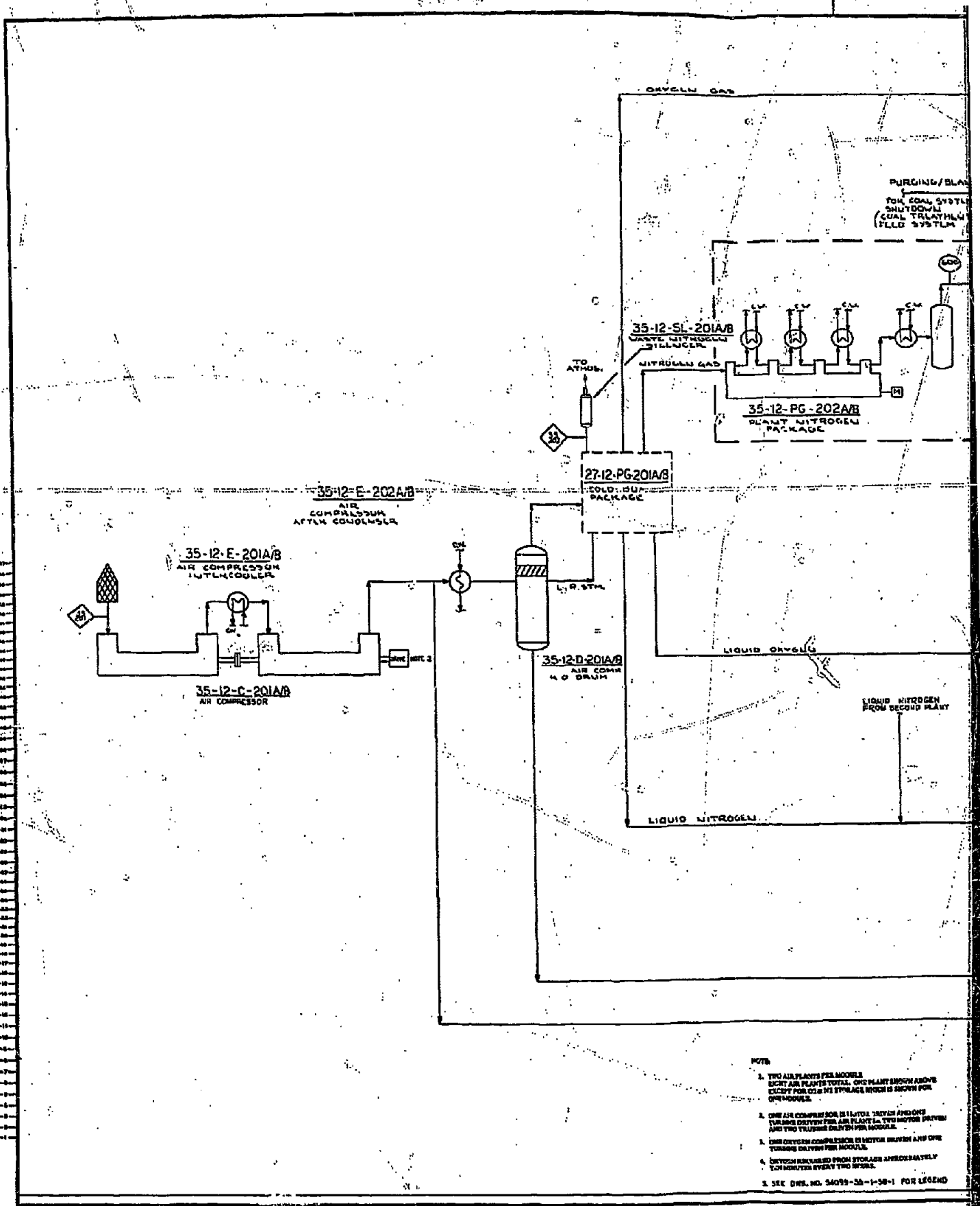
SECTION NO.: 200
 PAGE NO.: 1
 DATE:

STREAM NUMBER	35	201	35	202	35	203	35	204	35	205	35	206
STREAM DESCRIPTION	Air Intake	Nitrogen	Oxygen	Oxygen	Oxygen	Oxygen	Oxygen	Oxygen	Oxygen	Condensate	Nitrogen	Nitrogen
COMPONENTS	(MMW)	MOL/HR	MOL/HR	MOL/HR	MOL/HR	MOL/HR	MOL/HR	MOL/HR	MOL/HR	MOL/HR	MOL/HR	MOL/HR
HYDROGEN	2.016											
CARBON MONOXIDE	28.011											
CARBON DIOXIDE	44.011											
METHANE	16.043											
NITROGEN	28.014	42,984.76	40,841.9								2,142.86	
OXYGEN	32.000	11,518		11,518								
HYDROGEN SULFIDE	34.080											
CARBONYL SULFIDE	60.075											
AMMONIA	17.031											
HYDROGEN CYANIDE	27.026											
CHLORIDES	35.453											
SULFUR	32.066											
CARBON DISULFIDE	76.143											
SULFUR DIOXIDE	64.059											
ARGON	39.944	511.79	273.93		223.44							14.42
MERCAPTANS												
TOTAL DRY GAS		55,014.55	41,115.83		11,741.44							2,157.28
WATER	18.016	1,100.6										
TOTAL WET GAS		56,115.15										
		LBS/HR	LBS/HR	LBS/HR	LBS/HR	LBS/HR	LBS/HR	LBS/HR	LBS/HR	LBS/HR	LBS/HR	LBS/HR
TOTAL STREAM LBS/HR		1,613,022.4	1,155,087		377,501						60,606	
SOLIDS LBS/HR												
COAL												
ASH												
CARBON												
TOTAL SOLIDS										19,828.4		
WATER LIQUID												
TOTAL STREAM					240							
TEMPERATURE, °F		98										
MMSCFD DRY GAS												
DRY GAS GHV (BTU/SCF)												

TWO TRAINS PER MODULE (EXCEPT O₂ & N₂ STORAGE & VAPORIZATION)

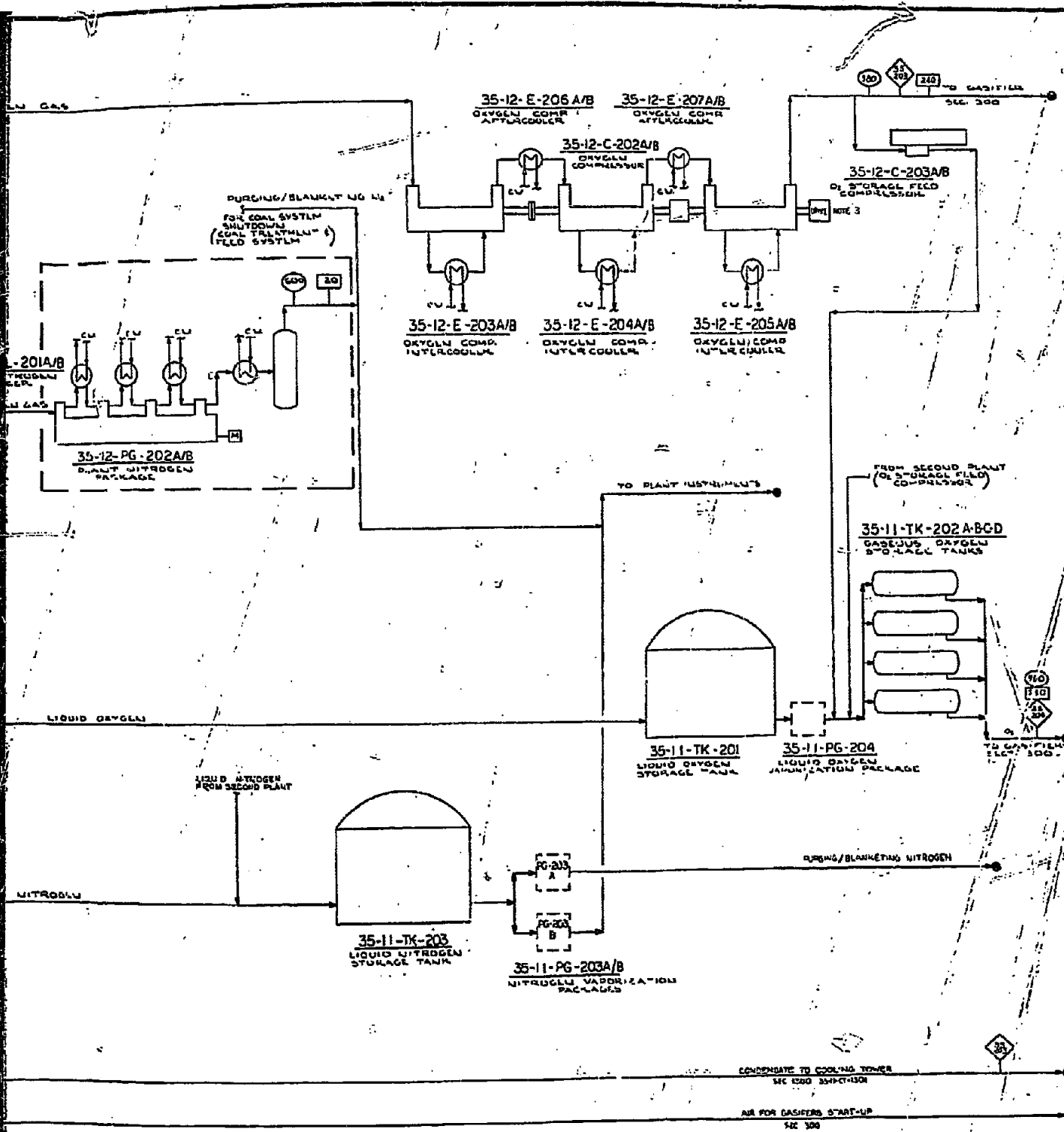
FOSTER WHEELER ENERGY CORP. PROCESS PLANTS DIVISION		CONTRACT NO. 11-35-54099		EQUIPMENT LIST		SECTION 200		TYPE OF UNIT AIR SEPARATION PLANT		PAGE 1 OF 2	
CLASS	ITEM NO	DESCRIPTION	FD#	REVISION DATE	REQ'N. NO. NO/MODULE	ORIGINAL	1	2	3	4	5
COMPRESSORS 35-12 -	C-201 A/B	AIR COMPRESSOR	2		2 - 50%						
	C-202 A/B	OXYGEN COMPRESSOR	2		2 - 50%						
	C-203 A/B	OXYGEN STORAGE FEED COMPRESSOR	2		2 - 50%						
DRUMS 35-12 -	D-201 A/B	AIR COMPRESSOR K.O. DRUM	2		2 - 50%						
EXCHANGERS 35-12 -	E-201 A/B	AIR COMPRESSOR INTERCOOLER	2		2 - 50%						
	E-202 A/B	AIR COMPRESSOR AFTER CONDENSER	2		2 - 50%						
	E-203 A/B	OXYGEN COMPRESSOR FIRST INTERCOOLER	2		2 - 50%						
	E-204 A/B	OXYGEN COMPRESSOR SECOND INTERCOOLER	2		2 - 50%						
	E-205 A/B	OXYGEN COMPRESSOR THIRD INTERCOOLER	2		2 - 50%						
	E-206 A/B	OXYGEN COMPRESSOR FIRST AFTERCOOLER	2		2 - 50%						
	E-207 A/B	OXYGEN COMPRESSOR SECOND AFTERCOOLER	2		2 - 50%						

CLASS	ITEM NO	DESCRIPTION	REVISION		ORIGINAL	TYPE OF UNIT					REV
			FD#	DATE		1	2	3	4	5	
SILENCER	35-12	WASTE NITROGEN SILENCER	2		2 - 50%						
TANKS	35-12	LIQUID OXYGEN STORAGE TANK	2		1 - 100%						
		GASEOUS OXYGEN STORAGE TANK	2		4 - 25%						
		LIQUID NITROGEN STORAGE TANK	2		1 - 100%						
PACKAGE	35-12	COLD BOX PACKAGE	2		2 - 50%						
		PLANT NITROGEN PACKAGE	2		2 - 50%						
		NITROGEN VAPORIZATION PACKAGE	2		2 - 50%						
		LIQUID OXYGEN VAPORIZATION PACKAGE	2		1 - 100%						



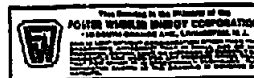
NOTE

1. TWO AIR PLANTS PER MODULE. EACH AIR PLANT TOTAL. ONE PLANT SHOWN ABOVE EXCEPT FOR O2 STORAGE WHICH IS SHOWN FOR ONE MODULE.
2. ONE AIR COMPRESSOR IS 1150 HP. OTHER TWO ARE 750 HP. TWO FOR AIR PLANTS. TWO MOTOR DRIVEN AND TWO TURBO DRIVEN PER MODULE.
3. ONE OXYGEN COMPRESSOR IS MOTOR DRIVEN AND ONE TURBO DRIVEN PER MODULE.
4. OXYGEN RECOVERED FROM STORAGE APPROXIMATELY 100 HOURS EVERY TWO WEEKS.
5. SEE DWS. NO. 34099-33-1-34-1 FOR LEGEND



NOTE:

1. TWO AIR PLANTS PER MODULE SHORT AIR PLANT TOTAL. ONE PLANT SHOWN ABOVE ESCAPE FOR ONE B PISTON PACKAGE WHICH IS SHOWN FOR ONE MODULE.
2. ONE AIR COMPRESSOR IS MOTOR DRIVEN AND ONE TURBINE DRIVEN PER AIR PLANT IN TWO MOTOR DRIVEN AND TWO TURBINE DRIVEN PER MODULE.
3. ONE OXYGEN COMPRESSOR IS MOTOR DRIVEN AND ONE TURBINE DRIVEN PER MODULE.
4. DRIVEN REQUIRED FROM STORAGE APPROXIMATELY TEN MINUTES EVERY TWO HOURS.
5. SEE Dwg. No. 3499-35-1-50-1 FOR LEGEND



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PROCESS FLOW DIAGRAM
 TVA COAL GASIFICATION STUDY
 SECTION 200 AIR SEPARATION PLANT
 TEXACO GASIFIERS

FOSTER WHEELER ENERGY CORPORATION



TVA Coal Gasification Study
Texaco Gasifier

SECTION DESCRIPTION

3.3 SECTION 300 - TEXACO GASIFICATION SYSTEM

A. Reference Material:

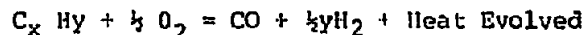
- Process Flowsheets FWEC Dwg. No. 54099-35-4-50-3A
- Input/Output Major Stream Flows

B. Description of Flow

Sized coal ($\frac{1}{2}$ " x 0) is delivered to a Coal Feed Bin. The Coal flows to the Belt Scale, and then to the Coal Feeding Belt, which conveys the coal (dry basis) at an average rate of 400,000 lbs/hr into a Mill. The Mill pulverizes the coal using wet grinding technique. Make-up water is continuously added to the Mill. Pulverized coal is discharged by gravity into the Mill Sump, where additional water is added. The coal slurry is pumped to a Slurry Make-up Tank. Coal/water slurry of proper consistency is produced in the Make-up Tank.

Coal fines and dirty water streams recovered downstream of the gasification system are recycled to the Mill in order to minimize any carbon losses from the plant. The slurry is pumped into the Slurry Mix Tank. When the tank is full, coal slurry is pumped into the Slurry Run Tank.

The coal slurry flows to the Gasifier where a controlled flow of oxygen from battery limit is introduced. The oxygen burns the coal to a synthetic gas containing largely H_2 and CO by the basic reaction:



The process burner directs the products of combustion down into the gasifier.

The gasifier effluent, which contains molten ash and the hot product gas, flows through a Radiant Cooler, and then through a Convection Cooler, which generates 900 psig steam. The hot gas is scrubbed of soot and slag. The slag falls to the bottom of the radiant cooler and into the Lock Hopper. The Lock Hopper is operated on a 30 minute automatic cycle. The slag slurry leaving the hopper is screened to remove the larger sizes from the fines and water in Slag Screen. The slag is delivered to battery limits and the fines and water are collected in Startup Quench Water Sump. The fines are pumped to the battery limits for disposal by Sump Pump. The Sump Pump is also used to flush the slag hopper and to supply quench water during preheat of the gasifier.



The partially cooled gas flows through a Heat Exchanger, to heat the BFW to 375°F. The cooled gas next flows through a scrubbing system for carbon removal. The scrubbed gas of a temperature of approximately 280°F then flows to COS Hydrolysis Unit (FWEC Dwg. 54099-35-1-50-7) to reduce the COS concentration in the gas before entering the Acid Gas Removal Section. The gas from COS hydrolysis system is returned to Gasification Section. Most of the water vapor is condensed by first passing the syngas through coolers. All of the condensate is recirculated through the carbon scrubbing system. Syngas from the cooler flows to the Acid Gas Removal System, Section 400.

The carbon water from the gasifier and scrubbers is cooled in the Carbon Water Precooler before it enters the Clarifier. In the clarifier, carbon solids are concentrated and recycled to the wet coal grinding system. The overflow from the clarifier enters the Gray Water Drum, where the water is further clarified and sent to various process units within the Gasification Section. A waste stream is sent to the Section 700 for waste treatment.



FOSTER WHEELER ENERGY CORPORATION
 CUSTOMER: **TVA COAL GASIFICATION**
 LOCATION: **ALABAMA**
 PLANT TYPE: **TEXACO GASIFIER**

SECTION NAME: **COAL GRINDING**
 REF. DWG.: **54099-35-1-50-3A**
 CONTRACT NO.: **11-35-54099** REV.:

SECTION NO.: **300**
 PAGE NO.: **1 OF 3**
 DATE:

STREAM NUMBER	35	301	35	303	15	304
STREAM DESCRIPTION	Raw Coal		Make-up Water	Lack Hopper Effluent		
COMPONENTS (MW)	MOL/HR	MOL/HR	MOL/HR	MOL/HR	MOL/HR	MOL/HR
HYDROGEN	2.016					
CARBON MONOXIDE	28.011					
CARBON DIOXIDE	44.011					
METHANE	15.043					
NITROGEN	28.014					
OXYGEN	32.000					
HYDROGEN SULFIDE	34.080					
CARBONYL SULFIDE	60.075					
AMMONIA	17.031					
HYDROGEN CYANIDE	27.026					
CHLORIDES	35.453					
SULFUR	32.066					
CARBON DISULFIDE	76.143					
SULFUR DIOXIDE	64.059					
ARGON	39.844					
MERCAPTANS						
TOTAL DRY GAS						
WATER	18.016					
TOTAL WET GAS						
		LBS/HR		LBS/HR		LBS/HR
TOTAL STREAM LBS/HR						
SOLIDS LBS/HR						
COAL	400,000					
ASH						
CARBON						
SOOT						
TOTAL SOLIDS	400,000					
WATER LIQUID						
TOTAL STREAM	400,000					
TEMPERATURE, °F						
MMSCFD DRY GAS						
DRY GAS GRV (BTU/SCF)						



FOSTER WHEELER ENERGY CORPORATION
 CUSTOMER: TVA COAL GASIFICATION
 LOCATION: ALABAMA
 PLANT TYPE: TEXACO GASIFIER

SECTION NAME: GASIFICATION
 REF. DWG: 54099-35-1-50-3A
 CONTRACT NO.: 11-35-54099 REV:

SECTION NO.: 300
 PAGE NO.: 2 OF 3
 DATE:

STREAM NUMBER	35	311	35	315	316
STREAM DESCRIPTION	Oxygen			SYN Gas	Flashed Gas
COMPONENTS	(MM)	MOL/HR	MOL/HR	MOL/HR	MOL/HR
HYDROGEN	2.016			12,268.78	
CARBON MONOXIDE	28.011			16,380.06	
CARBON DIOXIDE	44.011			5,902.00	
METHANE	16.043			107.09	
NITROGEN	28.014			228.15	
OXYGEN	32.000	11,518		524.24	FLOW
HYDROGEN SULFIDE	34.080			1.6	
CARBONYL SULFIDE	60.076				
AMMONIA	17.031				
HYDROGEN CYANIDE	27.026				
CHLORIDES	36.463				
SULFUR	32.086				
CARBON DISULFIDE	76.143				
SULFUR DIOXIDE	64.059			223.44	INTERMITTENT
ARGON	38.944	223.44			
MERCAPTANS					
TOTAL DRY GAS				35,635.36	
WATER	18.016			49.25	
TOTAL WET GAS		11,711.44		35,684.61	
		LBS/HR	LBS/HR	LBS/HR	LBS/HR
TOTAL STREAM LBS/HR		377,501		778,102	
SOLIDS LBS/HR					
COAL					
ASH					
CARBON					
SOOT					
TOTAL SOLIDS					
WATER LIQUID					
TOTAL STREAM		240		1.00	
TEMPERATURE, °F					
MMSCFD DRY GAS					
DRY GAS GHV (BTU/SCF)					



FOSTER WHEELER ENERGY CORPORATION
 CUSTOMER: TVA COAL GASIFICATION
 LOCATION: ALABAMA
 PLANT TYPE: TEXACO GASIFIER

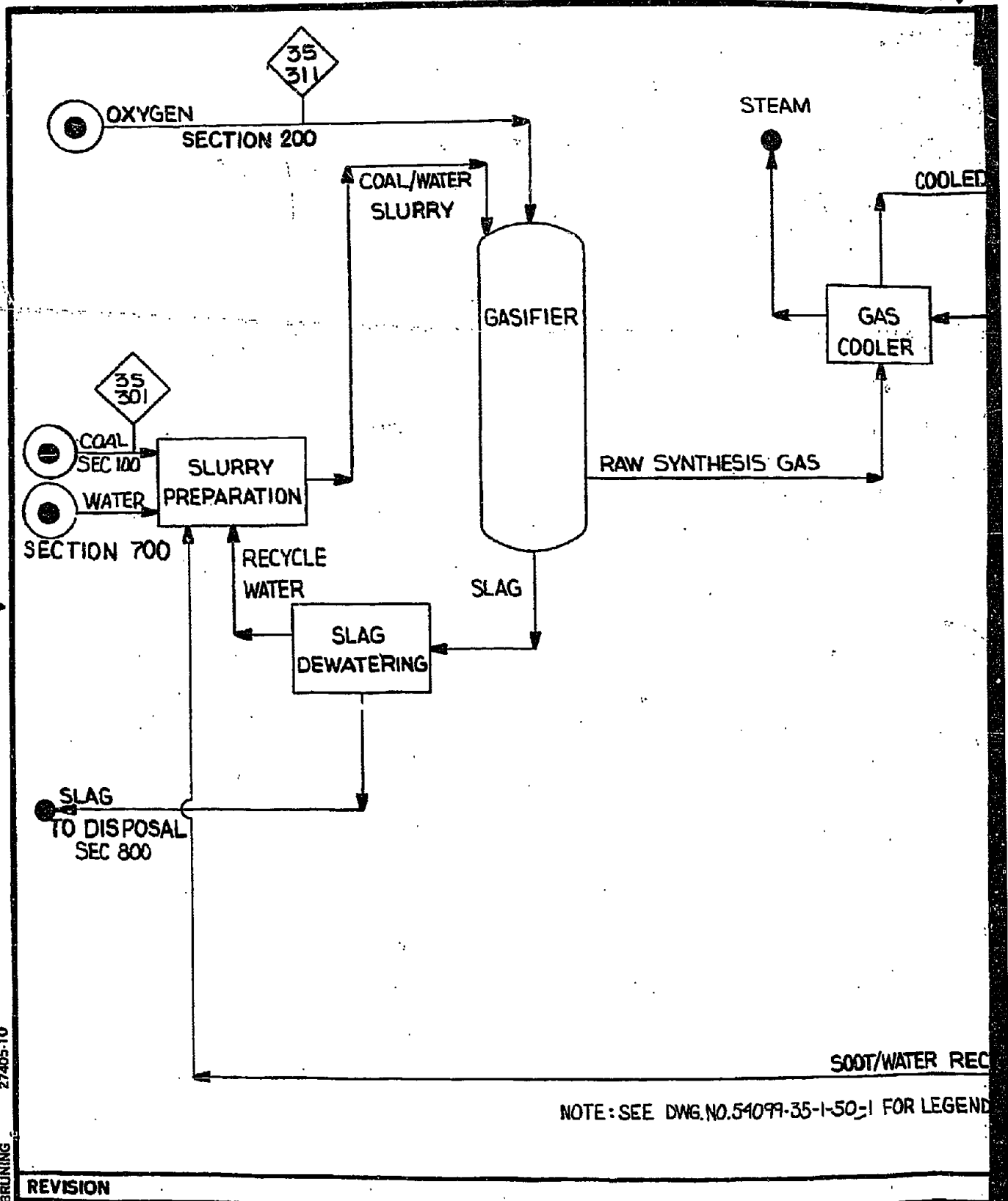
SECTION NAME: GASIFICATION
 REF. DWG.: 54099-35-1-50-3A
 CONTRACT NO.: 11-35-54099 REV:

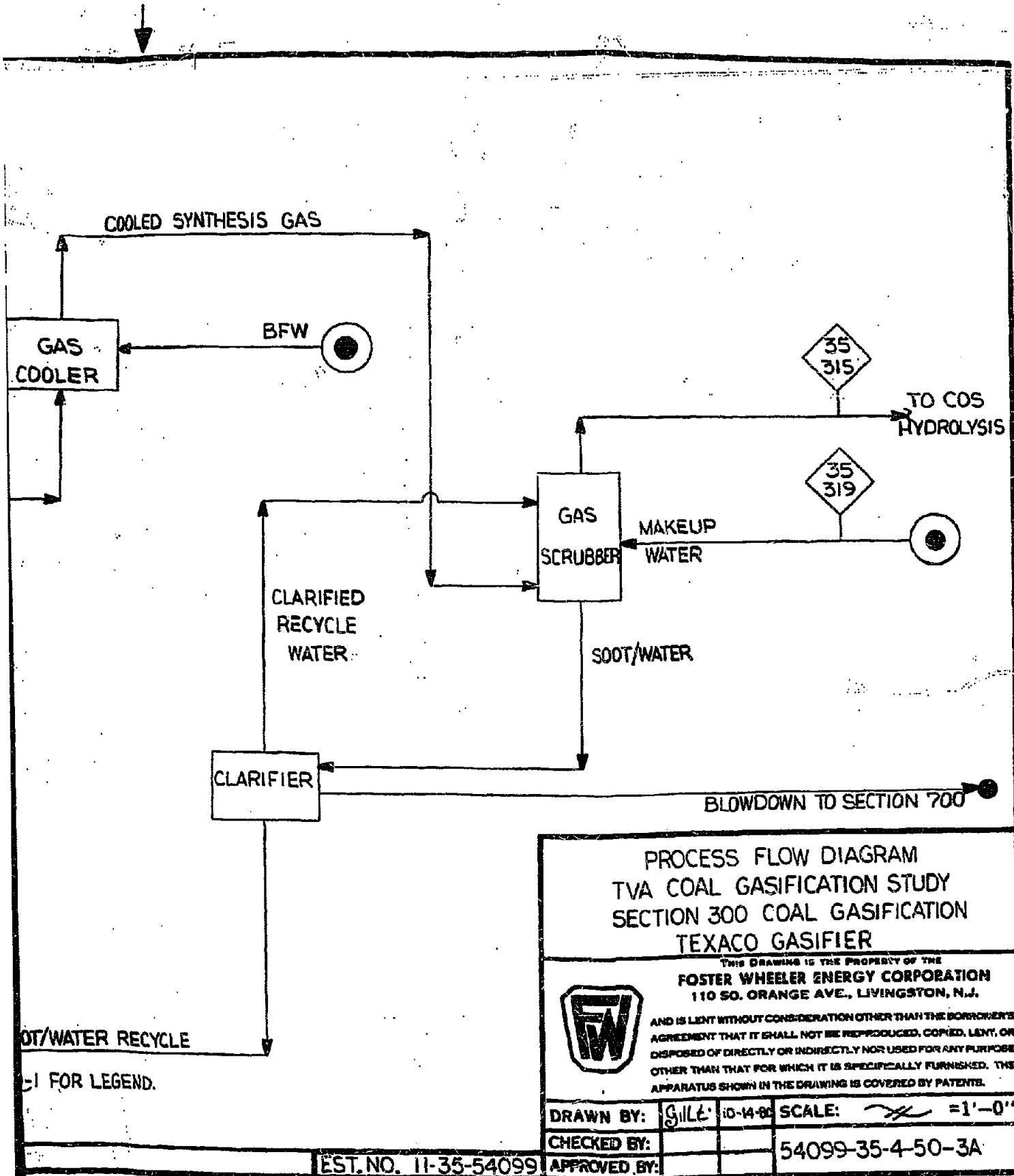
SECTION NO.: 300
 PAGE NO.: 3 OF 3
 DATE:

STREAM NUMBER			35	319			
STREAM DESCRIPTION			Make-up Water				
COMPONENTS	(MW)	MOL/HR	MOL/HR	MOL/HR	MOL/HR	MOL/HR	MOL/HR
HYDROGEN	2.016						
CARBON MONOXIDE	28.011						
CARBON DIOXIDE	44.011						
METHANE	16.043						
NITROGEN	28.014						
OXYGEN	32.000						
HYDROGEN SULFIDE	34.080						
CARBONYL SULFIDE	60.075						
AMMONIA	17.031						
HYDROGEN CYANIDE	27.026						
CHLORIDES	35.463						
SULFUR	32.066						
CARBON DISULFIDE	76.143						
SULFUR DIOXIDE	64.059						
ARGON	39.944						
MERCAPTANS							
TOTAL DRY GAS							
WATER	18.016						
TOTAL WET GAS		LBS/HR	LBS/HR	LBS/HR	LBS/HR	LBS/HR	LBS/HR
TOTAL STREAM LBS/HR							
SOLIDS LBS/HR							
COAL							
ASH							
CARBON							
TOTAL SOLIDS							
WATER LIQUID							
TOTAL STREAM							
TEMPERATURE, °F							
MMSCFD DRY GAS							
DRY GAS GHV (BTU/SCF)							

201,358.37

85





PROCESS FLOW DIAGRAM
 TVA COAL GASIFICATION STUDY
 SECTION 300 COAL GASIFICATION
 TEXACO GASIFIER

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CHECKED BY:			54099-35-4-50-3A	
APPROVED BY:				



TVA Coal Gasification Study
Texaco Gasifier

SECTION DESCRIPTION

SECTION 300 - COS HYDROLYSIS

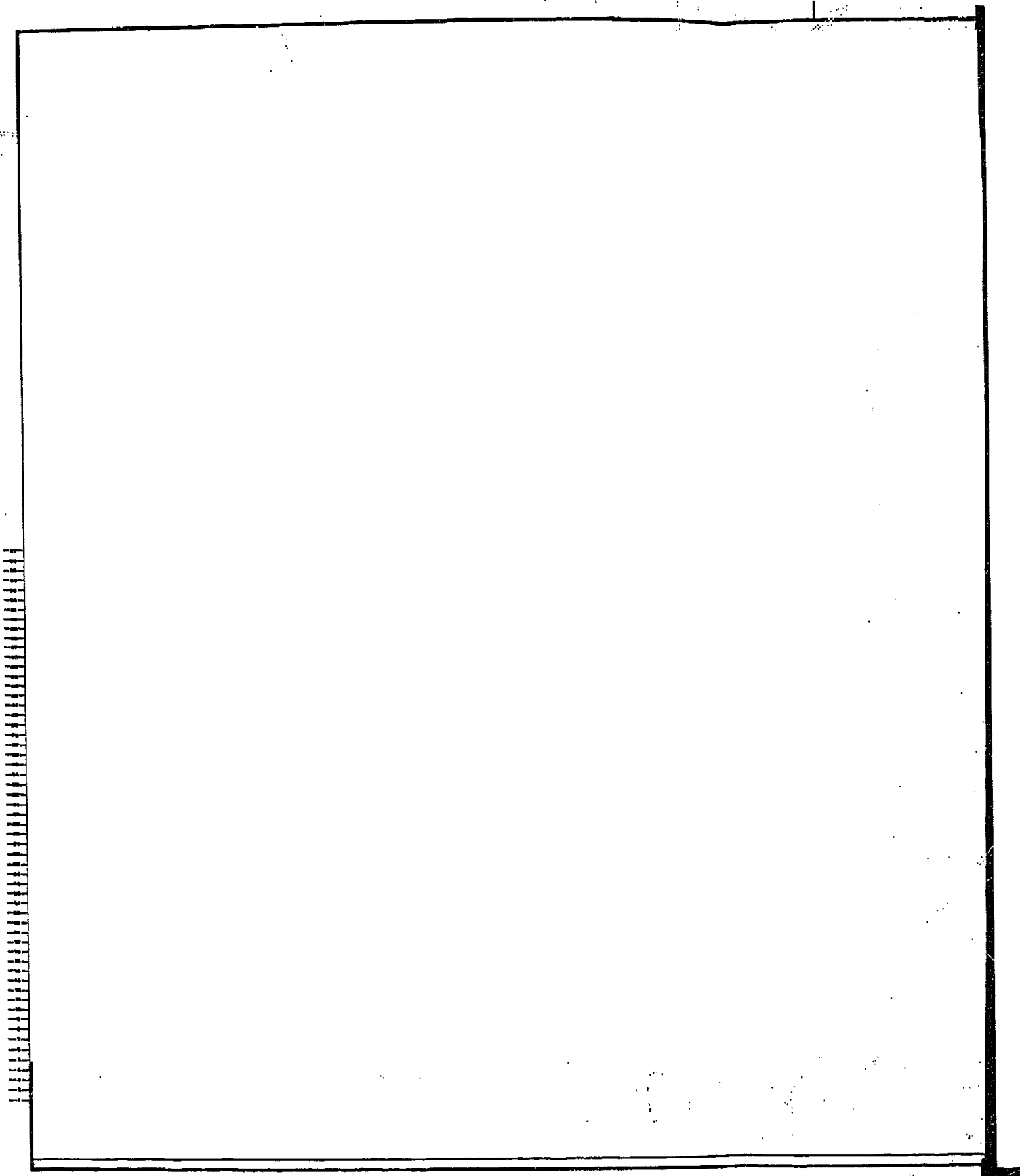
A. Reference Material:


- . Process Flowsheet FWEC Dwg. No. 54099-35-1-50-7
- . Equipment Summary List

B. Description of Flow:

The scrubbed syngas downstream of the carbon scrubber flows to the COS Reactor Feed Preheater E-301. The gas is heated from 280 °F to 333 °F temperature to avoid pore condensation in the reactor.

The COS Reactor R-301, converts the bulk of COS in the raw gas to H₂S using the Halder Topsoe CKA Catalyst. The conversion of COS to H₂S in the hydrolysis unit decreases the utility requirements and size of the Selexol unit. The raw gas leaving the reactor enters the syngas airfan cooler.



	<p>This document is the property of the FOSTER WHEELER ENERGY CORPORATION 1100 NORTH BRIDGE ST., PITTSBURGH, PA. 15222 © 1984 Foster Wheeler Energy Corporation All rights reserved.</p>	<p>PROCESS FLOW DIAGRAM TVA COAL GASIFICATION STUDY SEC.300,COS HYDROLYSIS TEXACO GASIFIER</p>
<p>DESIGNED BY: [A.B.C.]</p>	<p>DATE: 1/21/84</p>	<p>DWG. NO: 6058354-507</p>

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TVA Coal Gasification Study
Texaco Gasifier

SECTION DESCRIPTION

3.4

SECTION 400 - ACID GAS REMOVALA. Reference Material

Process Flow Diagram: FWEC Dwg. No. 54099-35-1-50-8
Equipment List
Input/Output Major Stream Flows

B. Description of Flow

The purpose of this section is to remove sulfur compounds from the raw gas. Raw gas from Gas Scrubbing (Section 300) combines with process recycle gas from the Recycle Gas Compressor (35-11-C-401) and is then cooled by heat exchange with product gas in the Feed-Product Gas Exchanger (35-11-E-401). Water condensed from the raw gas is separated in the H₂S Absorber K.O. Drum (35-11-D-401). Raw gas leaving the H₂S Absorber K.O. Drum (35-11-D-401) flows to the H₂S Absorber (35-11-T-401) where cold lean Selexol solvent physically absorbs H₂S, residual COS and some CO₂. Product gas leaving the top of the H₂S Absorber is heated in the Feed-Product Gas Exchanger (35-11-E-401). Most of the product gas flows to the Plant Battery Limit and the remainder to the Beavon Unit, Section 600, to be utilized as a reducing gas. The product gas contains less than 100 ppmv H₂S and less than 30 ppmv COS.

The Selexol solvent leaving the bottom of the H₂S Absorber flows directly to the H₂S Flash Drum (35-11-D-402). Most of the absorbed CO₂ and sour gases are flashed, then compressed in the Recycle Gas Compressor (35-11-C-401), and then combined with the raw gas feed entering the Feed-Product Gas Exchanger. Make-up solvent is added to the H₂S stripper bottom. Fresh solvent is stored in a Solvent Storage Tank (35-11-TK-401).

Solvent leaving the bottom of the H₂S Flash Drum is pumped to the H₂S Stripper Preheater (35-11-E-402). The Stripper Preheater is heated with hot lean solvent pumped from the bottom of the H₂S Stripper (35-11-T-401). Preheated solvent enters the H₂S Stripper for removal of acid gases. Stripper bottoms are reboiled in the H₂S Stripper Reboiler (35-11-E-403) heated with 85 PSIG steam. Vapors leaving the H₂S Stripper overhead are condensed in the H₂S Stripper Condenser (35-11-E-404) then enters the Stripper Recycle Drum (D-403). Condensate is totally recycled back to the Stripper, while the Acid Gases flow to the Sulfur Recovery Claus Plant (Section 600). Hot lean solvent is pumped from the bottom of the H₂S Stripper and cooled in the H₂S Stripper Preheater as described earlier. The solvent is chilled in Selexol Refrigeration Package (35-11-PG-401), then enters the top of the H₂S Absorber.



FOSTER WHEELER ENERGY CORPORATION
 CUSTOMER: TVA COAL GASIFIER
 LOCATION: ALABAMA
 PLANT TYPE: TEXACO GASIFIER

SECTION NAME: ACID GAS REMOVAL
 REF. DWG.: 54099-35-1-50-8
 CONTRACT NO.: 11-35-54099REV:

SECTION NO.: 400
 PAGE NO.: 1
 DATE:

STREAM NUMBER	35	401	35	402	35	403	35	404
STREAM DESCRIPTION	SYN Gas	Product Gas	Acid Gas	Make-up Water	MOL/HR	MOL/HR	MOL/HR	MOL/HR
COMPONENTS	(MMW)	MOL/HR	MOL/HR	MOL/HR	MOL/HR	MOL/HR	MOL/HR	MOL/HR
HYDROGEN	2.016	12,268.78	12,267.81			1.15		
CARBON MONOXIDE	28.011	16,380.06	16,369.76			10.14		
CARBON DIOXIDE	44.011	5,902.00	3,604.0			2,297.48		
METHANE	16.043	107.09	106.72			0.33		
NITROGEN	28.014	228.15	228.15					
OXYGEN	32.000							
HYDROGEN SULFIDE	34.080	524.24	0.006			523.24		
CARBONYL SULFIDE	60.075	1.6	0.332			1.26		
AMMONIA	17.031							
HYDROGEN CYANIDE	27.026							
CHLORIDES	35.453							
SULFUR	32.065							
CARBON DISULFIDE	76.143							
SULFUR DIOXIDE	64.059							
ARGON	39.944	223.49	223.49					
MERCAPTANS								
TOTAL DRY GAS								
WATER	18.016	49.25	2.08			133.5		
TOTAL WET GAS		35,714.85	32,802.35			2,966.62		
		LBS/HR	LBS/HR			LBS/HR		LBS/HR
TOTAL STREAM LBS/HR		779,194	658,969			121,719		
SOLIDS LBS/HR								
COAL								
ASH								
CARBON								
TOTAL SOLIDS								
WATER LIQUID								
TOTAL STREAM		110	92			110		
TEMPERATURE, °F								
MMSCFD DRY GAS								
DRY GAS CHV (101/SCF)								

ONE TRAIN PER MODULE

FOSTER WHEELER ENERGY CORP. PROCESS PLANTS DIVISION		CONTRACT NO. 11-35-54099		EQUIPMENT LIST		SECTION 400		TYPE OF UNIT ACID GAS REMOVAL (SELEXOL)					PAGE 1 OF 3		
CLIENT TVA - COAL GASIFICATION STUDY				REVISION DATE		ORIGINAL		1	2	3	4	5	REV		
LOCATION ALABAMA				FD#		REQ'N. NO. NO/MODULE									
CLASS	ITEM NO	DESCRIPTION													
COMPRESSOR 35-11	C-401	RECYCLE GAS COMPRESSOR				1 - 100%									
DRUMS 35-11	D-401	H ₂ S ABSORBER K.O. DRUM				1 - 100%									
	D-402	H ₂ S FLASH DRUM				1 - 100%									
	D-403	STRIPPER RECYCLE DRUM				1 - 100%									
EXCHANGERS 35-11	E-401	FEED PRODUCT GAS EXCHANGER				1 - 100%									
	E-402	H ₂ S STRIPPER PREHEATER				1 - 100%									
	E-403	H ₂ S STRIPPER REBOILER				1 - 100%									
	E-404	H ₂ S STRIPPER CONDENSER				1 - 100%									



FOSTER WHEELER ENERGY CORP.
PROCESS PLANTS DIVISION

CONTRACT NO.
11-35-54099

EQUIPMENT LIST

SECTION
400

TYPE OF UNIT
ACID GAS REMOVAL (SELEXOL)

CLASS	ITEM NO	DESCRIPTION	FD#	REVISION	DATE	REQ'N. NO./NO./MODULE	ORIGINAL	TYPE OF UNIT					REV
				1	2			3	4	5			
PUMPS	35-11 -												
	P-401A/B	LEAN SOLUTION PUMP				2 - 100%							
	-												
	P-402A/B	H ₂ S STRIPPER RECYCLE PUMP				2 - 100%							
	-												
	P-403A/B	SOLVENT SUMP PUMP				2 - 100%							
	-												
TANK	35-11 -												
	TK-401	SOLVENT STORAGE TANK				1 - 100%							
	-												
	TK-402	SOLVENT SUMP				1 - 100%							
	-												

ONE TRAIN PER MODULE

EQUIPMENT LIST

SECTION 400

TYPE OF UNIT
ACID GAS REMOVAL (SELEXOL)

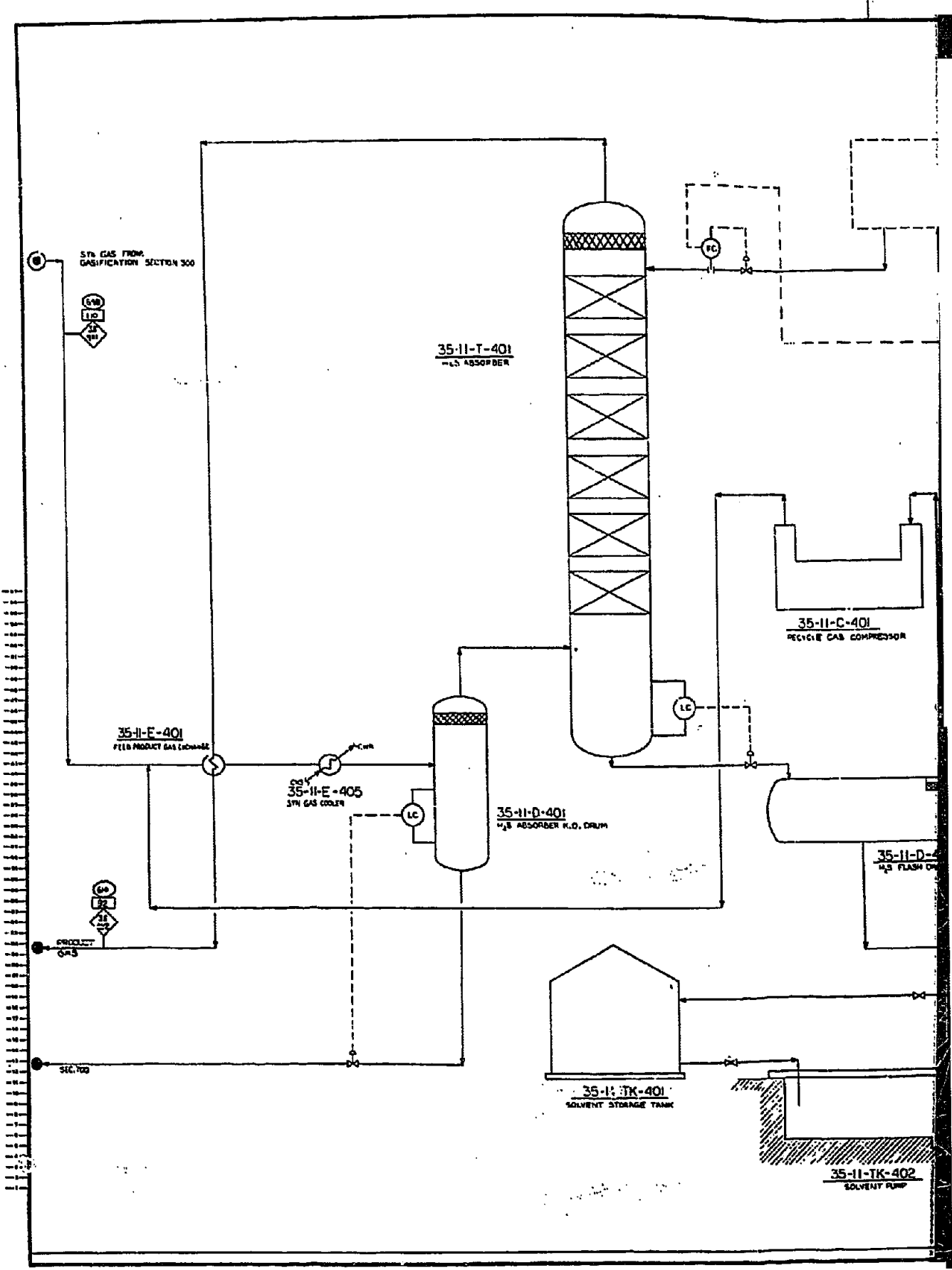
PAGE 3 OF 3

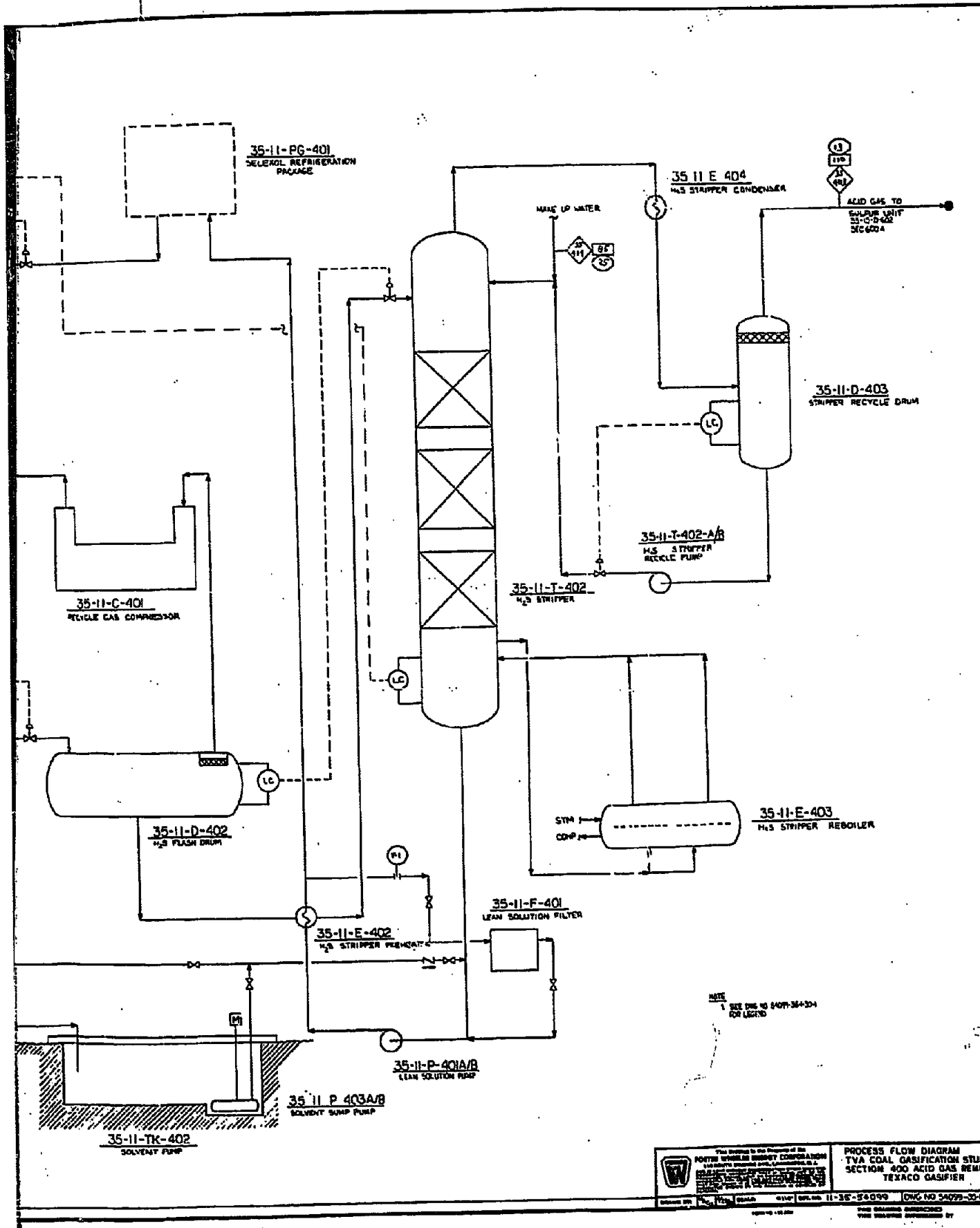
FOSTER WHEELER ENERGY CORP.
PROCESS PLANTS DIVISION
CONTRACT NO.
11-35-54099

CLIENT TVA - COAL GASIFICATION STUDY

LOCATION ALABAMA

CLASS	ITEM NO	DESCRIPTION	REV. NO.	REVISION DATE	REQ'D NO. NO/MODULE	ORIGINAL	1	2	3	4	5	REV
TOWERS 35-11 --	T-401	H ₂ S ABSORBER			1 - 100%							
	T-402	H ₂ S STRIPPER			1 - 100%							
FILTER 35-11 --	F-401	LEAN SOLUTION FILTER			1 - 100%							
PACKAGES ITEM: 35-11 --	PG-401	SELEXOL REFRIGERATION PACKAGE			1 - 100%							





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 PROCESS FLOW DIAGRAM
 TVA COAL GASIFICATION STUDY
 SECTION 400 ACID GAS REMOVAL
 TEXACO GASIFIER
 THIS DRAWING APPROVED BY
 THE ENGINEER RESPONSIBLE FOR THE DESIGN



TVA Coal Gasification Study
Texaco Gasifier

SECTION DESCRIPTION

3.5 SECTION 600A - CLAUS SULFUR RECOVERY PLANT

A. Reference Material

Process Flowsheet FWEC Drawing No. 54099-35-1-50-9

Equipment List

Input/Output Major Stream Flows

B. Description of Flow

Acid gas from the Selexol Unit Stripper Recycle Drum flows through K.O. Drum and enters the Muffle Furnace (H-601). Hydrogen sulfide is partially (about one-third) oxidized to sulfur dioxide, utilizing air fed by the Process Air Blower (B-601). Medium pressure steam is generated in the Waste Heat Boiler (E-601) and is the major source of 150 psig steam for process use (refer to 54099-35-1-50-151).

Gases leaving the Waste Heat Boiler flow to a three stage Claus reactor system, consisting of R-601, 602, and 603, where sulfur dioxide reacts catalytically with the remaining hydrogen sulfide, producing elemental sulfur and water. The Claus Unit is about 96% efficient in removal of sulfur compounds from acid gas. Treated tail gas leaving the Claus Unit flows to the Beavon Unit (in series with the Claus Unit) for further reduction of sulfur compounds from the gas and recovery as elemental sulfur. Total normal sulfur production from Claus and Beavon Units combined is about 198 T/D per module.

Gas leaving each Claus Reactor (stage) is cooled below about 300°F to condense sulfur before entering the next stage or flowing to the Beavon Unit. A third Reactor Preheater, E-606, is provided for optimum operation in the third stage.

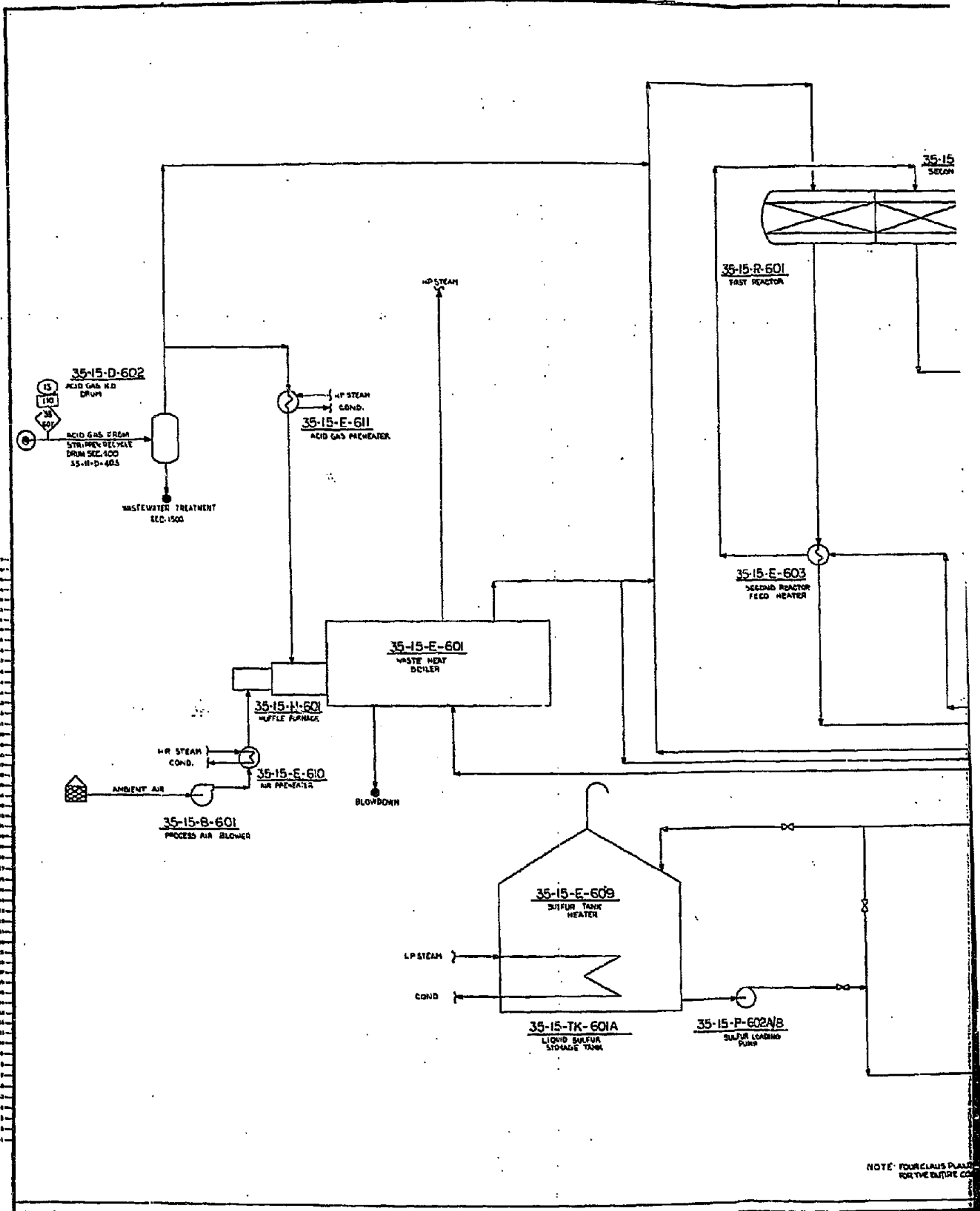
Liquified (condensed) sulfur flows to a Sulfur Pit, X-601, and may be stored in the Liquid Sulfur Storage Tank, TK-601A, for sale as a liquid product or prilled in the Sulfur Prilling Unit

Low pressure steam is generated during gas cooling to recover sulfur. Boiler blowdown streams will be used as cooling tower makeup as shown on 54099-35-1-50-151.

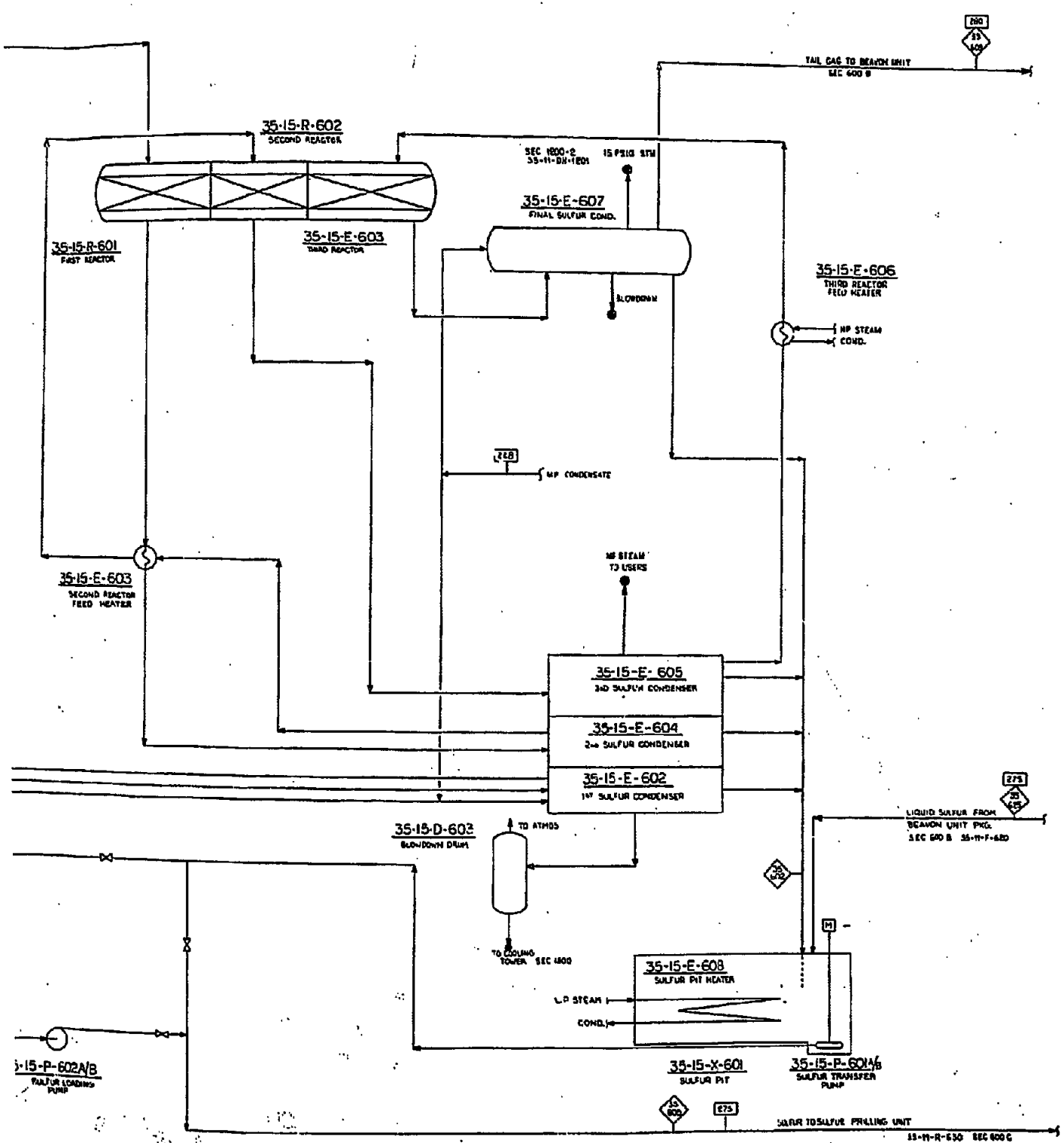
ONE TRAIN PER MODULE PLUS ONE SPARE TRAIN FOR ENTIRE PLANT

FOSTER WHEELER ENERGY CORP. PROCESS PLANTS DIVISION		CONTRACT NO. 11-35-54099		EQUIPMENT LIST				PAGE 1 OF 2	
CLIENT	TVA - COAL GASIFICATION STUDY	SECTION	600	ORIGINAL	1	2	3	4	5
LOCATION	ALABAMA	REVISION	DATE	REQ'D. NO.	NO/MODULE	FD#	DESCRIPTION	ITEM NO	REV
BLOWER	35-15					8	PROCESS AIR BLOWER	B-601	
DRUMS	35-15					8	ACID GAS K.O. DRUM	D-601	
						8	BLOWDOWN DRUM	D-602	
EXCHANGER	35-15					8	WASTE HEAT BOILER	E-601	
						8	1st SULFUR CONDENSER	E-602	
						8	SECOND REACTOR FEED HEATER	E-603	
						8	2ND SULFUR CONDENSER	E-604	
						8	3RD SULFUR CONDENSER	E-605	
						8	THIRD REACTOR FEED HEATER	E-606	
						8	FINAL SULFUR CONDENSER	E-607	
						8	SULFUR PIT HEATER	E-608	
	35-15					8	SULFUR TANK HEATER	E-609	
						8	AIR PREHEATER	E-610	
							ACID GAS PREHEATER	E-611	
	35-15					8	MUFFLE FURNACE	H-601	

FOSTER WHEELER ENERGY CORP. PROCESS PLANTS DIVISION		CONTRACT NO. 11-35-54099		EQUIPMENT LIST				PAGE 2 OF 2				
CLIENT	TVA - COAL GASIFICATION STUDY	SECTION	600	TYPE OF UNIT				1	2	3	4	5
LOCATION	ALABAMA	REVISION	DATE	FD#	REQ'N. NO.	NO/MODULE	1	2	3	4	5	
CLASS	ITEM NO	DESCRIPTION									REV	
PUMPS												
35-15 -	P-601	SULFUR TRANSFER PUMP	8			2 - 100%						
-	P-602	SULFUR LOADING PUMP	8			2 - 100%						
REACTORS												
35-15 -	R-601	FIRST REACTOR	8			1 - 100%						
-	R-602	SECOND REACTOR	8			1 - 100%						
-	R-603	THIRD REACTOR	8			1 - 100%						
TANKS												
35-15 -	TK-601	LIQUID SULFUR STORAGE TANK	8			1 - 100%						
-	X-601	SULFUR PIT	8			1 - 100%						



NOTE: FOUR CLAS PLANT FOR THE ENTIRE CO.



NOTE: SEE DWG. NO. 34099-36-1-80-1 FOR LEGEND

NOTE: FOUR CLAUSTRAL PLUS ONE SPARE UNIT ARE REQUIRED FOR THE ENTIRE COAL CONVERSION PLANT

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	DWG. NO. 34099-36-1-80-1	DATE: 01-25-80



TVA Coal Gasification Study
Texaco Gasifier

SECTION DESCRIPTION

SECTION 600B- SULFUR RECOVERY BEAVON UNIT

A. Reference Material:

- . Process Flow Diagram: FWEC Dwg. No. 54099-35-1-50-10
- . Equipment List
- . Input/Output Major Stream Flows

B. Description of Flow

Essentially all the sulfur compounds contained in the tail gas flowing from the Sulfur Recovery Claus Plant (Section 600) to the Beavon Unit are converted by hydrogenation to hydrogen sulfide in the Beavon Reactor, R-620. Product reducing gas from Section 400 serves to reduce the sulfur oxides to H_2S .

The tail gas to the Reactor (35-11-R-620) is preheated in the Reactor Effluent Exchanger, 35-11-E-620, reduced, then cooled in the Reactor Effluent Cooler, E-621. Boiler feedwater is the coolant on the shell side of the Reactor Effluent Cooler. Tail gas from the Beavon Unit flows to the bottom of the H_2S Absorber (35-11-T-620). Most of the H_2S contained in the tail gas is absorbed by the Stretford solution, which circulates countercurrent to the gas entering the Absorber. Clean gas is vented to atmosphere from the top of the Absorber. The Stretford solution leaving the bottom flows to the Oxidizer Pit, 35-11-X-620. The absorbed sulfur, mostly H_2S , is oxidized to elemental sulfur, as is reduced Stretford solution, by air admitted by the Aerator, 35-11-M-620. Vent gases (air) leaving the Oxidizer Pit are released to atmosphere. The resulting

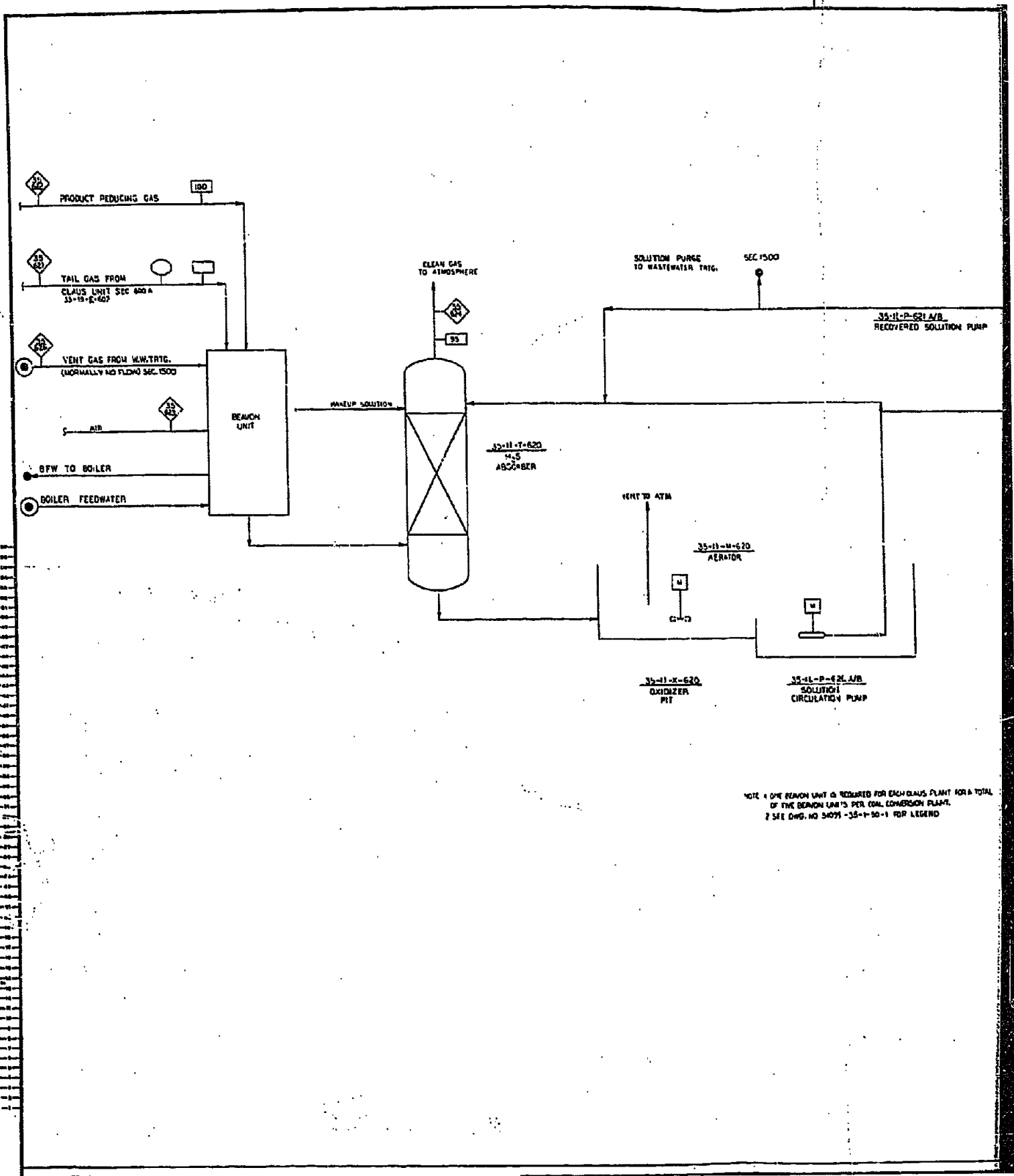
B. Description of Flow (cont'd)

frothy solution is circulated by the Solution Circulation Pump, P-620A/B, to the H₂S Absorber. A portion of the circulating stream is filtered in the Sulfur Filter, F-620, to recover elemental sulfur. Filtrate enters the Recovered Solution Drum (35-11-D-620) and also is recycled to the top of the H₂S Absorber by P-621A/B.

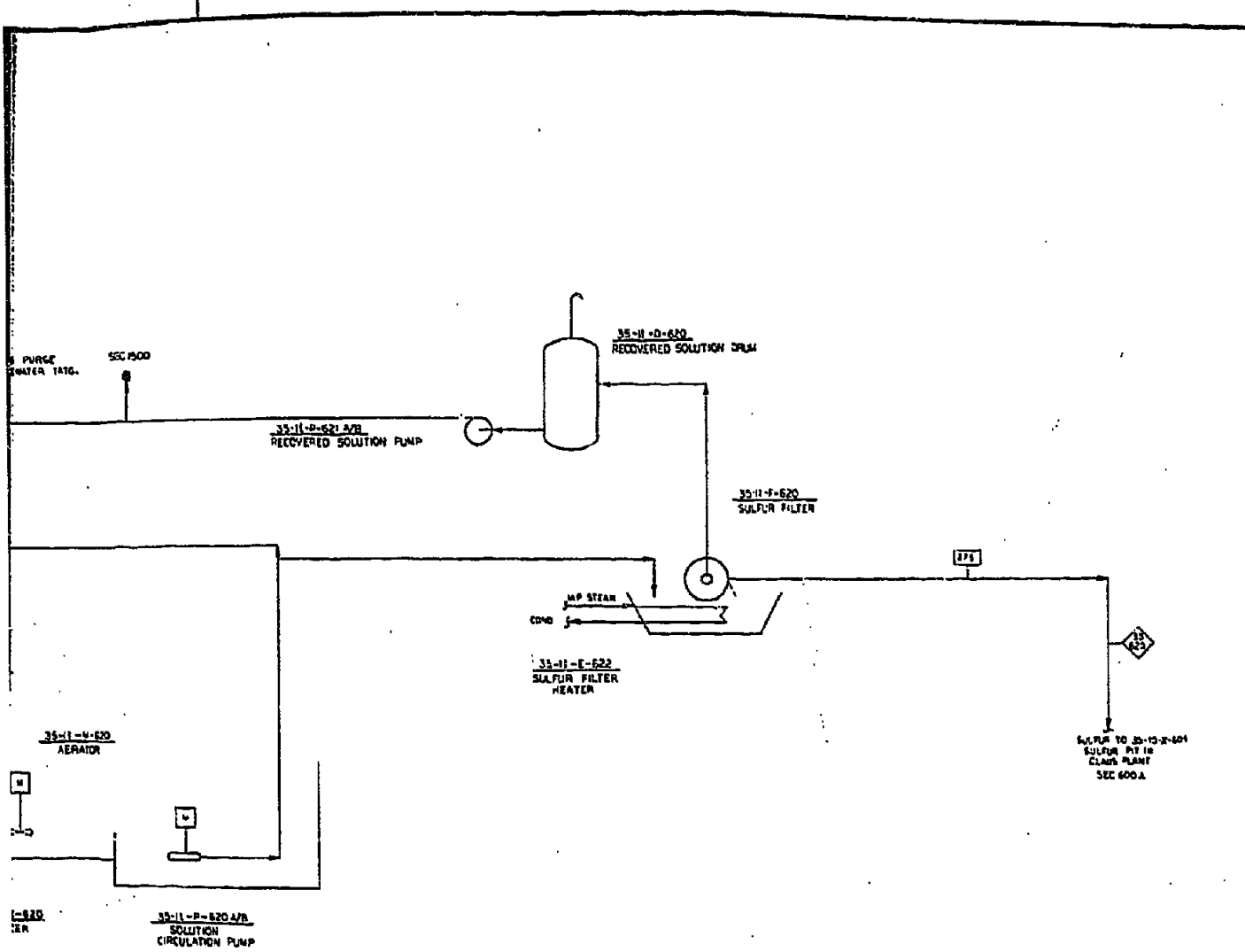
Liquid sulfur flows to the Sulfur Pit (X-601) in the Claus Plant (Section 600). A small portion of the recycled solution is purged to Wastewater Treating (Section 1500) or to drums. Makeup Stretford solution, stored in drums, is pumped intermittently as an aqueous solution to the top of the H₂S Absorber to replace purged solution. It may be necessary to direct vent gas, normally no flow, from Waste Water Treating (Section 1500) to the Beavon Unit for reduction of sulfur compounds.

FOSTER WHEELER ENERGY CORP. PROCESS PLANTS DIVISION		CONTRACT NO. 11-35-54099		EQUIPMENT LIST					PAGE 1 OF 1	
CLIENT TVA - COAL GASIFICATION STUDY				SECTION 600		TYPE OF UNIT SULFUR RECOVERY-BEAVON UNIT				
LOCATION ALABAMA				REVISION DATE		ORIGINAL			REV	
CLASS	ITEM NO	DESCRIPTION	FD%	REQ N. NO./MODULE						
DRUM 35-11	D-620	RECOVERED SOLUTION DRUM	10	1 - 100%						
FILTER 35-11	F-620	SULFUR FILTER	10	1 - 100%						
EXCHANGERS 35-11	E-620	REACTOR FEED EFFLUENT EXCHANGER	10	1 - 100%						
	E-621	REACTOR EFFLUENT COOLER	10	1 - 100%						
	E-622	SULFUR FILTER HEATER	10	1 - 100%						
MIXER 35-11	M-620	AERATOR	10	1 - 100%						
PUMPS 35-11	P-620	SOLUTION CIRCULATION PUMP	10	2 - 100%						
	P-621	RECOVERED SOLUTION PUMP	10	2 - 100%						
TOWER 35-11	T-620	H ₂ S ABSORBER	10	1 - 100%						
REACTOR 35-11	R-620	REACTOR	10	1 - 100%						
TANK 35-11	X-620	OXIDIZER PIT	10	1 - 100%						

FORM NO. 195-660



NOTE: 1 ONE BEAMON UNIT IS REQUIRED FOR EACH CLAUS PLANT FOR A TOTAL OF FIVE BEAMON UNITS PER COAL CONVERSION PLANT.
 2 SEE DWG. NO 34091-35-1-50-1 FOR LEGEND



NOTE 1. ONE BEAM UNIT IS REQUIRED FOR EACH CLEAN PLANT FOR A TOTAL OF FIVE BEAM UNITS PER COAL CONVERSION PLANT.
 2. SEE DIAG NO 34079-35-Y-30-1 FOR LEGEND

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	DRAWING NO. 35-11-620 SHEET NO. 1 OF 1	11 20 1973 (REV. 11-20-73)



TVA Coal Gasification Study
Texaco Gasifier

SECTION DESCRIPTION

SECTION 600C - SULFUR PRILLING UNIT

A. Reference Material

- . Process Flowsheet FWEC Dwg. No. 54099-35-1-50-11
- . Equipment List

B. Description of Flow

The molten sulfur is fed to the top of Prilling Reactor, R-630, where it is distributed on a plate containing a number of nozzles.

Sulfur from the molten pool on the plate flows down through the nozzles into a short air space where surface tension causes the individual flow streams to break up and contract into spheres. The latter then drop into a pool of temperature controlled process water where the prills are completely solidified and cooled.

The process water enters the reactor through a series of inlet nozzles located along the straightside of the reactor. This provides precise water flow control and allows for control of the surface movement of the water.

A grizzly screen is located near the bottom of the Prilling Reactor to catch large pieces of sulfur which are swept away.

Sight glasses are provided on the reactor to observe both the nozzle plate and the bottom screen. Manways are located on the reactor to gain access to the grate and the nozzle plate.

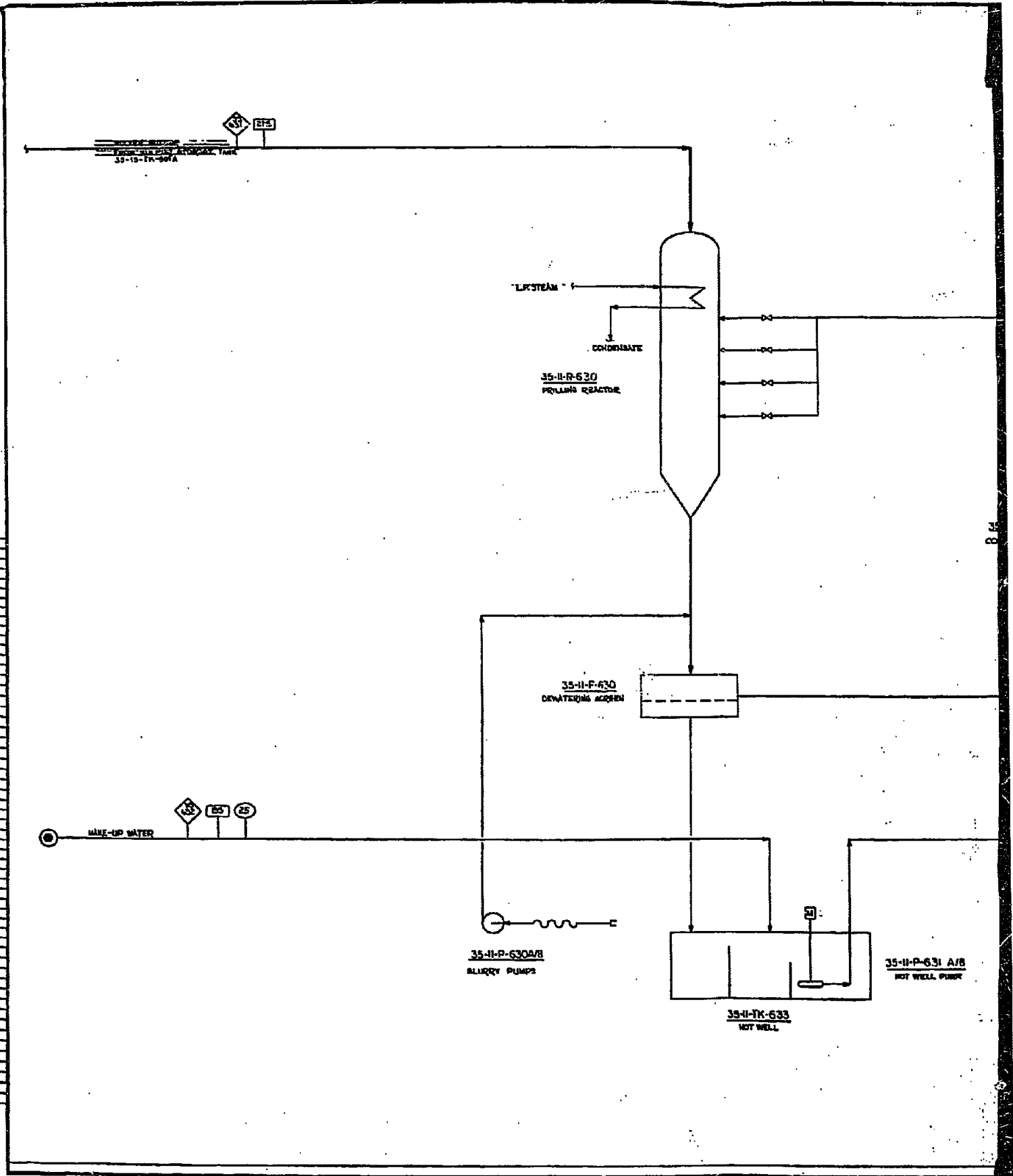
From the reactor, the water slurry of cooled solid sulfur prills flows on to Dewatering Screen, F-630, which is located directly under the reactor. This screen separates the bulk of the water from the sulfur prills.

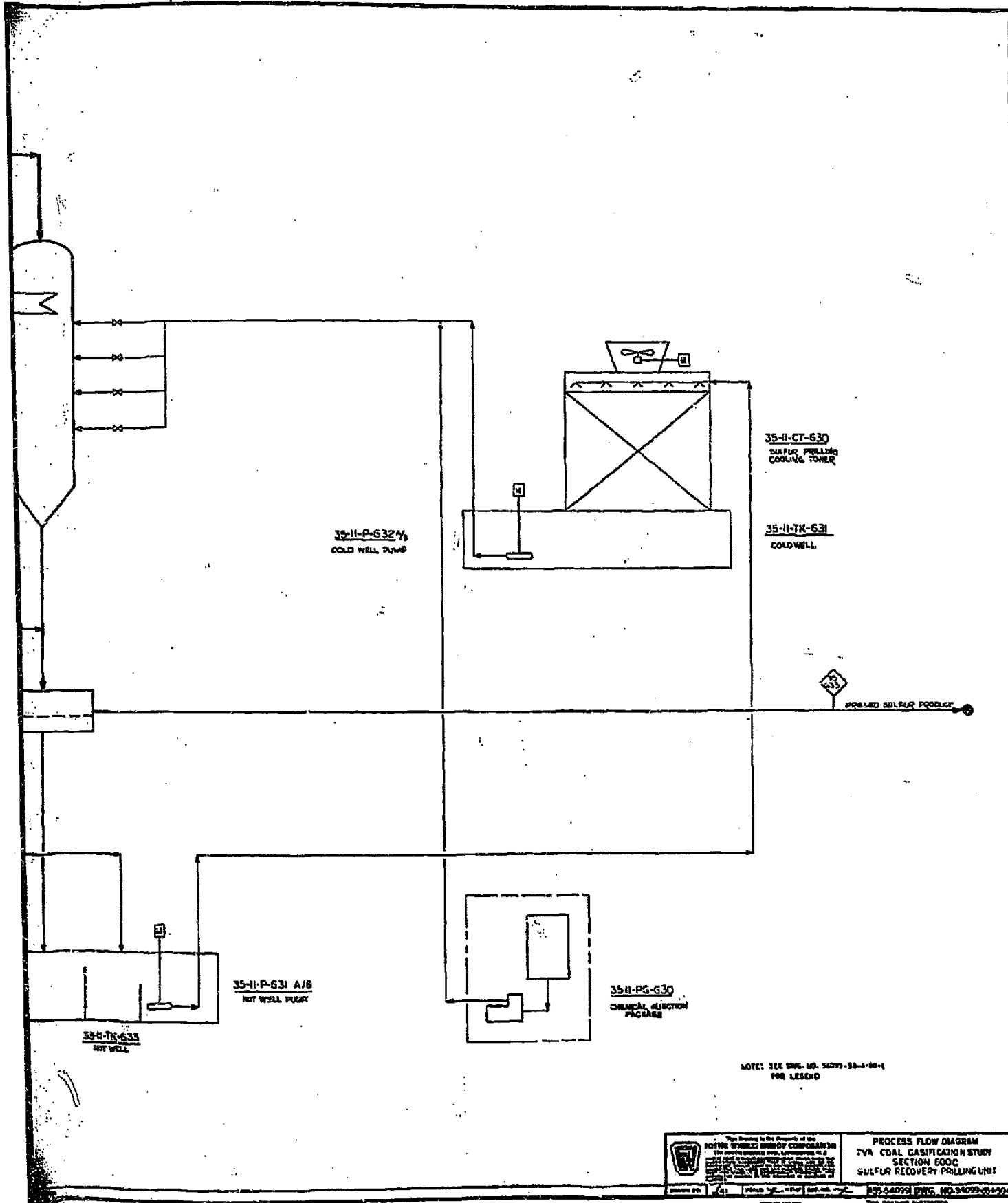
Water from F-630 flows by gravity into the Hotwell, TK-633. The Hotwell is a two-compartment vessel. The water enters the first compartment and overflows a weir before entering the second compartment. This will allow any sulfur fines in the water to settle in the first compartment. Any solids trapped in TK-633 can be pumped out, using the Slurry Pump, P-630A/B.



Make-up water flow to the system is controlled by the level in the Hotwell. The Hotwell Pump, P-631A/B pumps the water from the Hotwell to the Cooling Tower, CT-630, which is packaged type cooling tower. The temperature of the water from the tower is controlled by on/off control of the fan motor. The water from the water cooler drains to the Cold Well, TK-631, and is pumped from the Cold Well to the prill reactor by the Cold Well Pump, P-632A/B.

FOSTER WHEELER ENERGY CORP. PROCESS PLANTS DIVISION		CONTRACT NO. 11-35-54099		EQUIPMENT LIST				SECTION 600		TYPE OF UNIT SULFUR PRILLING			PAGE 1 OF 1	
CLIENT TVA - COAL GASIFICATION STUDY				REVISION		ORIGINAL		1	2	3	4	5		
LOCATION ALABAMA				DATE		REQ'N. NO. NO/MODULE								REV
CLASS	ITEM NO	DESCRIPTION	FD#	REVISION	DATE	REQ'N. NO.	NO/MODULE							
SCREEN	F-630	DEWATERING SCREEN	10			1 - 100%								
PUMPS	P-630	SLURRY PUMP	10			2 - 100%								
	P-631	HOT WELL PUMP	10			2 - 100%								
	P-632	COLD WELL PUMP	10			2 - 100%								
REACTOR	R-630	PRILLING REACTOR	10			1 - 100%								
COOLING TOWER	CT-630	SULFUR PRILLING COOLING TOWER	10			1 - 100%								
TANKS	TK-630	HOT WELL	10			1 - 100%								
	TK-631	COLD WELL	10			1 - 100%								
PACKAGE ITEMS	PG-630	CHEMICAL INJECTION PACKAGE	10			1 - 100%								





NOTE: SEE ENG. NO. 34079-30-1-00-1 FOR LEGEND

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	<p>335-54093 DWG. NO. 34079-30-1-00-1</p> <p>This Drawing pertains to the Contract referenced by the Contract Reference on the Drawing</p>



TVA Coal Gasification Study
Texaco Gasifier

SECTION DESCRIPTION

3.6 SECTION 700 - SOUR WATER STRIPPER & WASTE WATER TREATMENT

A. Reference Material:

- Process Flow sheet FWEC Dwg. No. 54099-35-4-50-12A

B. Description of Flow:

The process flow for the Blowdown Wastewater Treatment section is described below.

Blowdown from the clarifier in Section 300 is flashed and stripped with steam. The overhead vapors are partially condensed and the condensate is returned to Section 300. The non-condensibles are water scrubbed in the Neutralization Unit. The flashed liquid is sent to the Chemical Mix Reaction Unit where most of the impurities are chemically precipitated. Any vapor formed in the reactor is sent to the neutralization system, while the reacted wastewater flows to clarification. From the clarifier, the sludge, after dewatering, is sent to landfill. The clarified water is then steam stripped. Stripped vapor is sent to boiler fire box, and the stripper bottom liquid is neutralized.

After neutralization, the liquor flows to Aeration and Biological Oxidation. The digested sludge from biological oxidation is filtered and then disposed of as landfill. The clean water from the biox system is used as cooling tower make-up water.

P

FOSTER WHEELER ENERGY CORPORATION



TVA Coal Gasification Study
Texaco Gasifier

SECTION DESCRIPTION

3.7 SECTION 800-SLAG HANDLING

A. Reference Material:

- Process Flowsheet FWEC Dwg. No. 54099-35-1-50-13
- Equipment List

B. Description of Flow

Slag

This unit is designed to receive slag from any or all of twenty (20) Texaco Gasification Units, and mechanically transport the slag to an on-site landfill area.

Slag from each gasifier is dewatered by a screen and discharged to one of the slag transfer conveyors 35-CR805A/B. It is then conveyed to a slag conveyor 35-CR806, and transferred to a 56 hour slag pile at the onsite landfill area.

Slag is also captured in the grinding section of each module by a clarifier screen. This slag is dumped onto a clarifier screen transfer conveyor 35-CR801A/B, 35-CR802A/B, 35-803A/B or 35-CR804A/B. It is then transferred to the slag transfer conveyors and conveyed to the landfill.

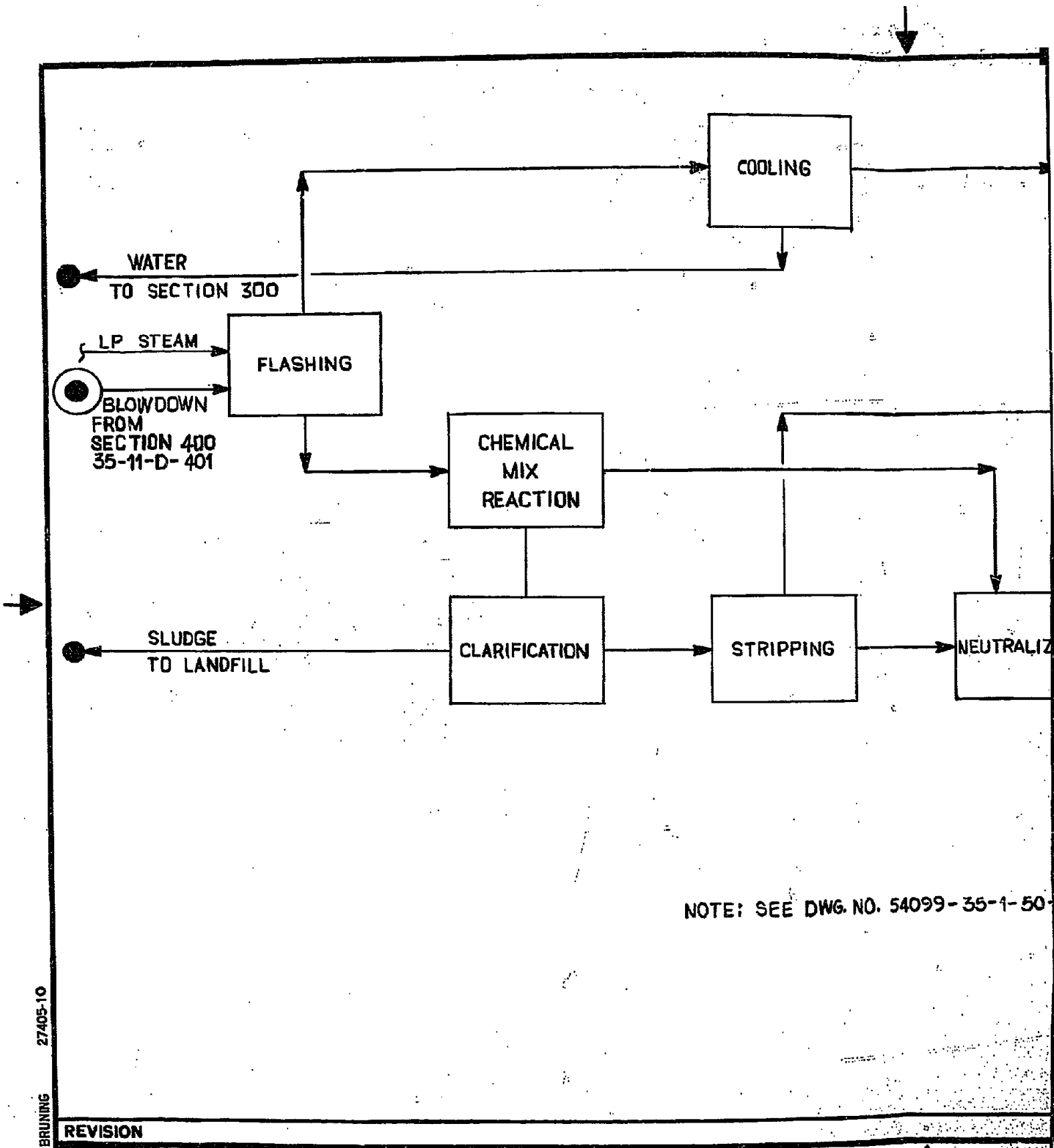
Spent Bed

Spent bed from the spent bed coolers in section 1200 is fed into a pneumatic transport line by rotary feeders 35-FD801A-J. The material is then conveyed up to the filter separator 35-F801 by pneumatic transport blowers 35-B801A/B. The pneumatic transport line will be equipped with silencers before and after the pneumatic transport blowers 35-B801A/B for noise suppression.

The filter separator will remove the forced air from the material and discharge it into the atmosphere. Meanwhile, the spent bed falls into the spent bed storage silo 35-TK801. Later, the material will be removed from the silo and brought to the disposal site by trucks.

Flyash

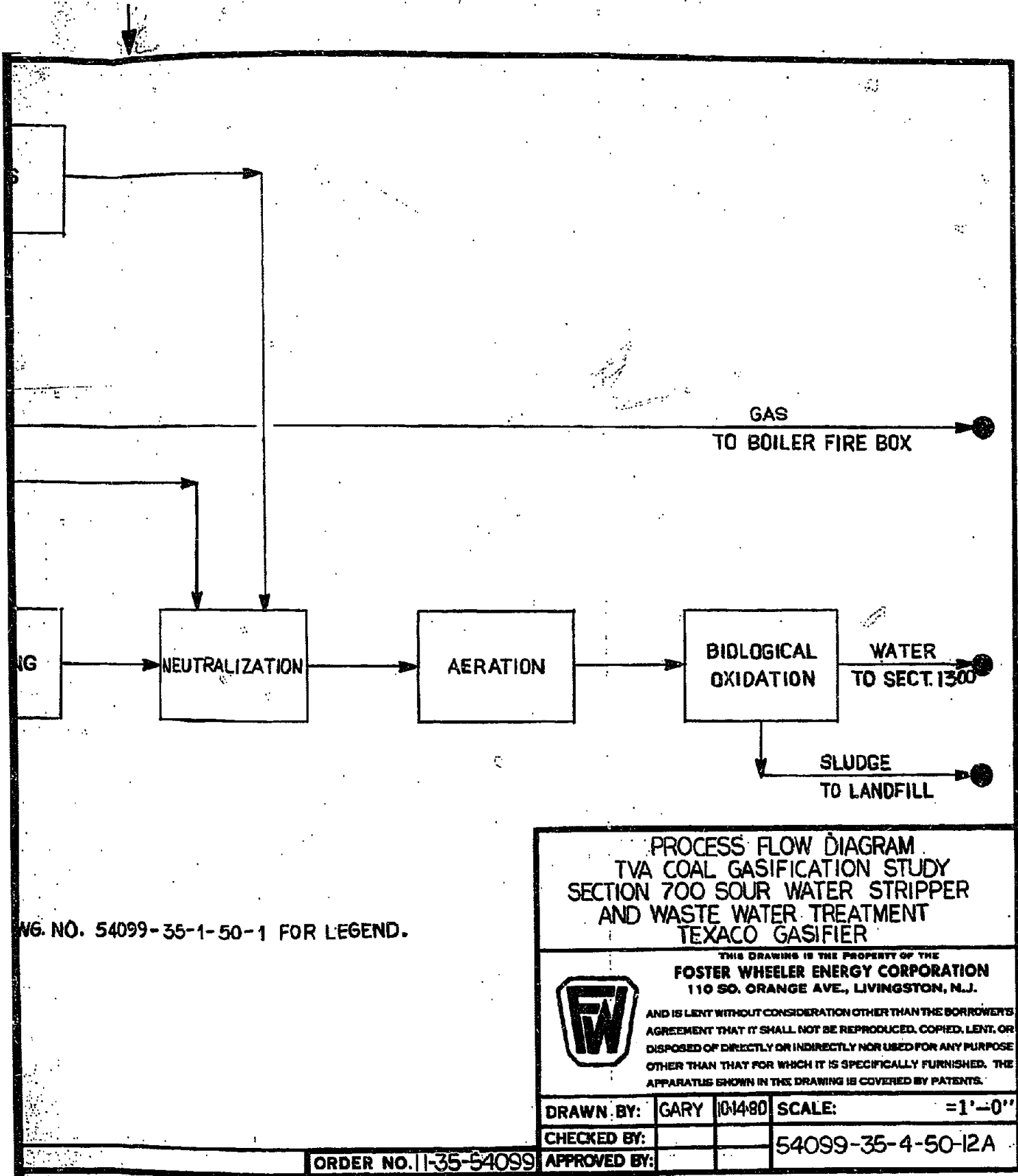
Flyash from baghouses will be drawn into filter separator 35-F802 by flyash centrifugal blower 35-B802. The air will be discharged to the atmosphere and the flyash will drop into the flyash storage silo 35-TK802. Flyash will be removed from the silo by flyash mixer conditioner 35-M801 which will also blend the flyash with water to create a uniform dust free mixture for clean disposal. The flyash/water mixture will be brought to the disposal site by trucks.



NOTE: SEE DWG. NO. 54099-35-1-50-

BRUNING 27405-10

REVISION

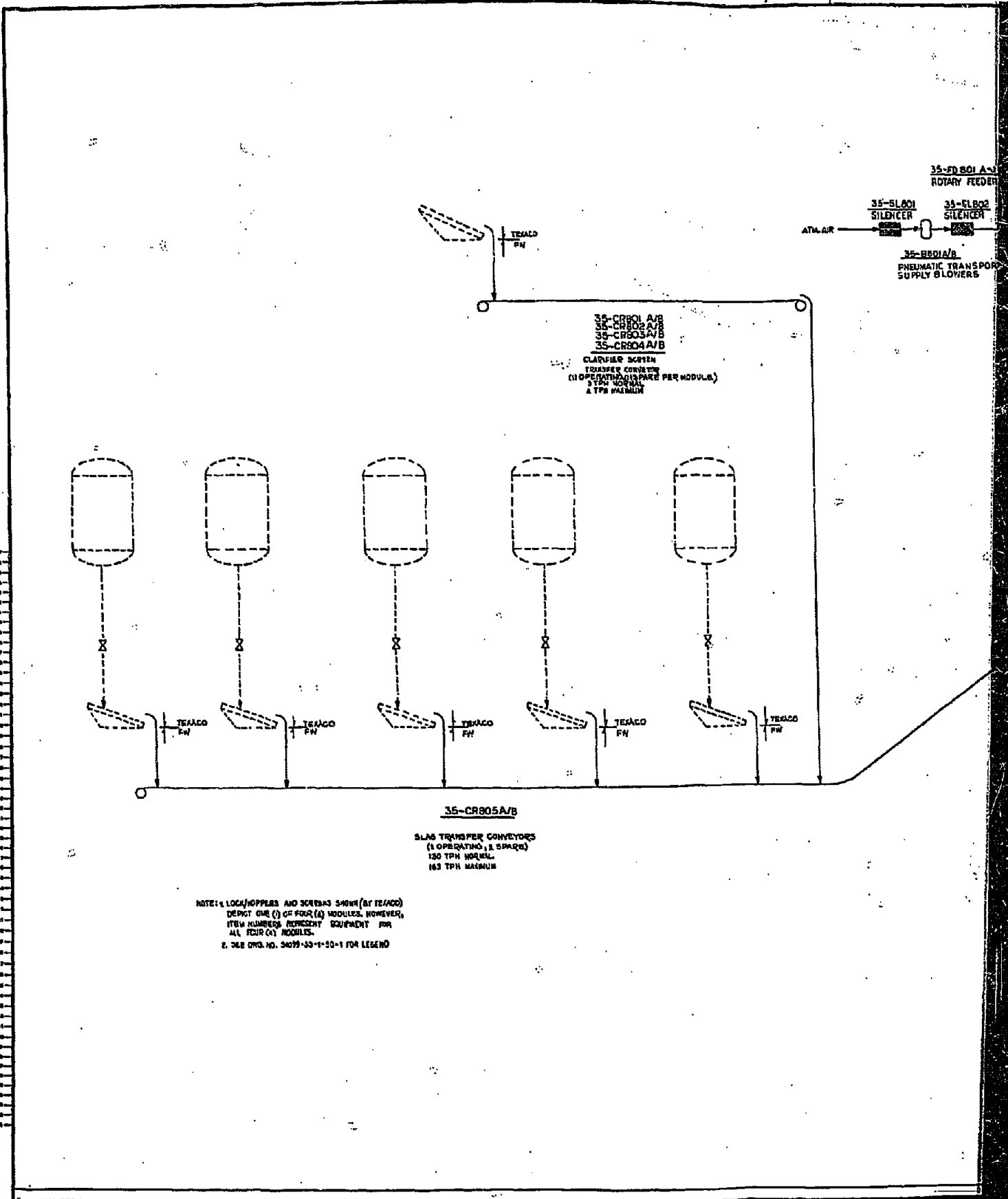


FOSTER WHEELER ENERGY CORPORATION
 SECTION NAME: SLAG HANDLING
 SECTION NO.: 800
 CUSTOMER: TVA/TEXACO
 REF. DWG.: 54092-35-1-50-10
 LOCATION: MURPHY HILL, ALABAMA
 CONTRACT NO.: 11-35-54099 REV.: 0
 DATE: 6/30/90

EQUIPMENT SUMMARY

ITEM	DESCRIPTION	DEFINITION	DESIGN * TEMP. (°F)	DESIGN * PRESS. (PSIG)	CONSTRUCTION MATERIAL *
35-B801A/B	Pneumatic Transport Supply Blowers				
35-B802A/B	Flyash Centrifugal Blower				
35-CR801A/B	Clarifier Screen Transfer Con.	24" Belt, 4 TPH			
35-CR802A/B	Clarifier Screen Transfer Con.	24" Belt, 4 TPH			
35-CR803A/B	Clarifier Screen Transfer Con.	24" Belt, 4 TPH			
35-CR804A/B	Clarifier Screen Transfer Con.	24" Belt, 4 TPH			
35-CR805A/B	Slag Transfer Conveyor	30" Belt, 163 TPH			
35-CR106	Slag Conveyor	30" Belt, 163 TPH			
35-F801	Filter/Separator				
35-F802	Filter/Separator				
35-FD801A	Rotary Feeder				
35-FD801B	Rotary Feeder				
35-FD801C	Rotary Feeder				
35-FD801D	Rotary Feeder				
35-FD801E	Rotary Feeder				
35-FD801F	Rotary Feeder				
35-FD801G	Rotary Feeder				
35-FD801H	Rotary Feeder				
35-FD801I	Rotary Feeder				
35-FD801J	Rotary Feeder				
35-M801	Flyash Mixer Conditioner				
35-SL801	Silencer				
35-SL802	Silencer				
35-TR801	Spent Bed Storage Silo	105 tons			
35-TR802	Flyash Storage Silo	210 tons			

* SHELL/TUBE WHERE APPLICABLE



35-FD 801 A/B
 ROTARY FEEDER

35-BL001
 SILENCER

35-BL002
 SILENCER

ATM. AIR

35-HB01A/B
 PNEUMATIC TRANSPOR
 SUPPLY BLOWERS

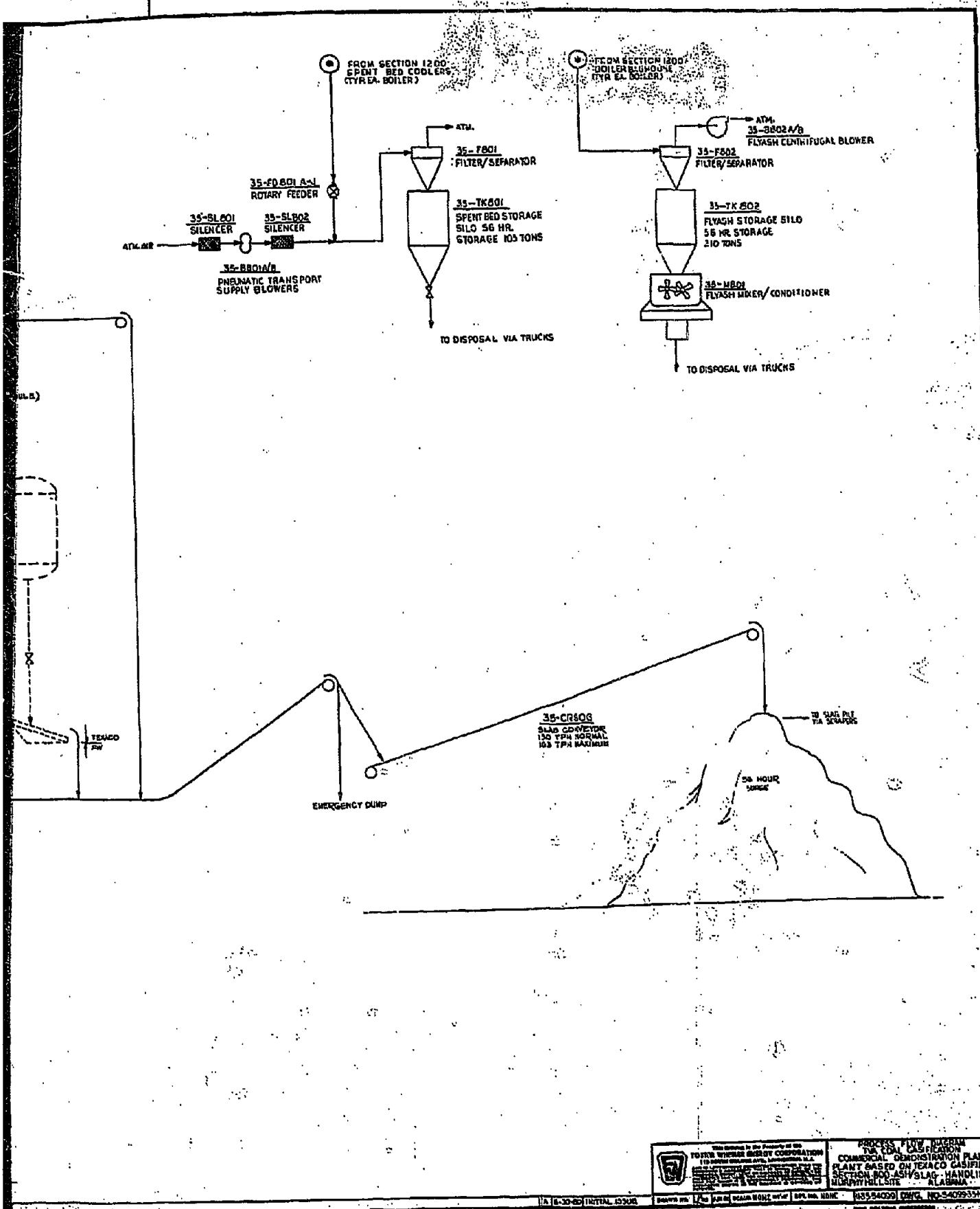
35-CR01A/B
 35-CR02A/B
 35-CR03A/B
 35-CR04A/B

CLASSIFIER SCREEN
 TRANSFER CONVEYOR
 (110 OPERATING, 113 PAKE PER MODULE,
 174 NORMAL
 178 MAXIMUM)

35-CR05A/B

SLAG TRANSFER CONVEYORS
 (1 OPERATING, 1 SPARE)
 130 TPH NOMINAL
 163 TPH MAXIMUM

NOTE: 1. LOGS/HOPPERS AND SCREENS SHOWN (BY TEACO)
 DEPICT ONE (1) OF FOUR (4) MODULES, HOWEVER,
 ITEM NUMBERS REFERENT EQUIPMENT FOR
 ALL FOUR (4) MODULES.
 2. SEE DWG. NO. 3409-33-1-50-1 FOR LEGEND



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PROCESS FLOW DIAGRAM
 TGA CDA GAS FISSION
 COMMERCIAL DEMONSTRATION PLANT
 PLANT BASED ON TEXACO GASIFIERS
 SECTION 800 ASH/SLAG HANDLING
 MIDWAY HILLSITE ALABAMA



TVA Coal Gasification Study
Texaco Gasifiers

SECTION DESCRIPTION

3.8 Section 1200 Utility Area

Section 1200-1 Raw Water Storage & Treatment

A. Reference Material

Process Flowsheet FWEC Drawing No. 54099-35-1-50-14

Equipment Summary List

B. Description of Flow

Raw water makeup entering the plant battery limits is of excellent quality. It is river water of the following approximate analyses in milligrams per liter:

<u>Component</u>	<u>Concentration, Mg/liter</u>		
	<u>Median</u>	<u>Maximum</u>	<u>Minimum</u>
Silica (SiO ₂)	5	6	3
Calcium (Ca)	19	23	15
Magnesium (Mg)	3.8	4.8	2.0
Sodium (Na)	5.3	24	1
Bicarbonate (HCO ₃)	50	62	38
Sulfate (SO ₄)	9.9	16	6.3
Chloride (Cl)	8	31	3
Nitrate (NO ₃)	1.3	2.8	0
Disolved Solids (180°C)	84	160	56
Hardness, as CaCO ₃	62	76	49
pH (SU)	7.4	7.9	6.9
Color (PCU)	5	20	0
Iron	negligible		
Fluorides	negligible		

The Raw Water Storage Tank, TK-1208, also will serve as a reservoir of firewater. Therefore, it should always contain four hours of raw water storage at the peak usage of 4000 gpm per module x 4 modules,



even though the normal makeup is about 100 gpm (since water is recovered from wastewater treating and used as cooling tower makeup).

Raw water, after treatment, will be used for cooling tower makeup, as emergency potable and service water, and influent to the demineralizer package provided in SEC 1200-3 to produce water for H.P. boiler feedwater treating. A single train of raw water treating is provided to serve all four modules.

Raw water is lifted from the river by P-1208A/B/C and pumped into TK-1208. Raw water is pumped from TK-1208 to the above-ground Clarifier-Softeners, CL-1201A/B, two units arranged in parallel. Sludge (mud, silt, etc) will precipitate from the river water in these Clarifiers. Lime, alum and polyelectrolyte are added to the Clarifier feed-wells as required to reduce hardness to a low level and enhance flocculation of suspended solids. Sludge underflowing the Clarifiers is pumped to rotary vacuum or belt filters for concentration of solids. Polymer or lime are added in line in M-1201A/B to improve filtration rate. Filtrate is recycled to the Clarifiers. Concentrated solids are trucked to ash (slag) ponds.

Clarified water flows by gravity to Sandfilters, F-1202A/B, for polishing, reduction of suspended solids to a very low level (1-2 ppm). The filters are backwashed periodically, approximately every 12 to 16 hours, for about five minutes. Backwash also is recycled to the Clarifiers.

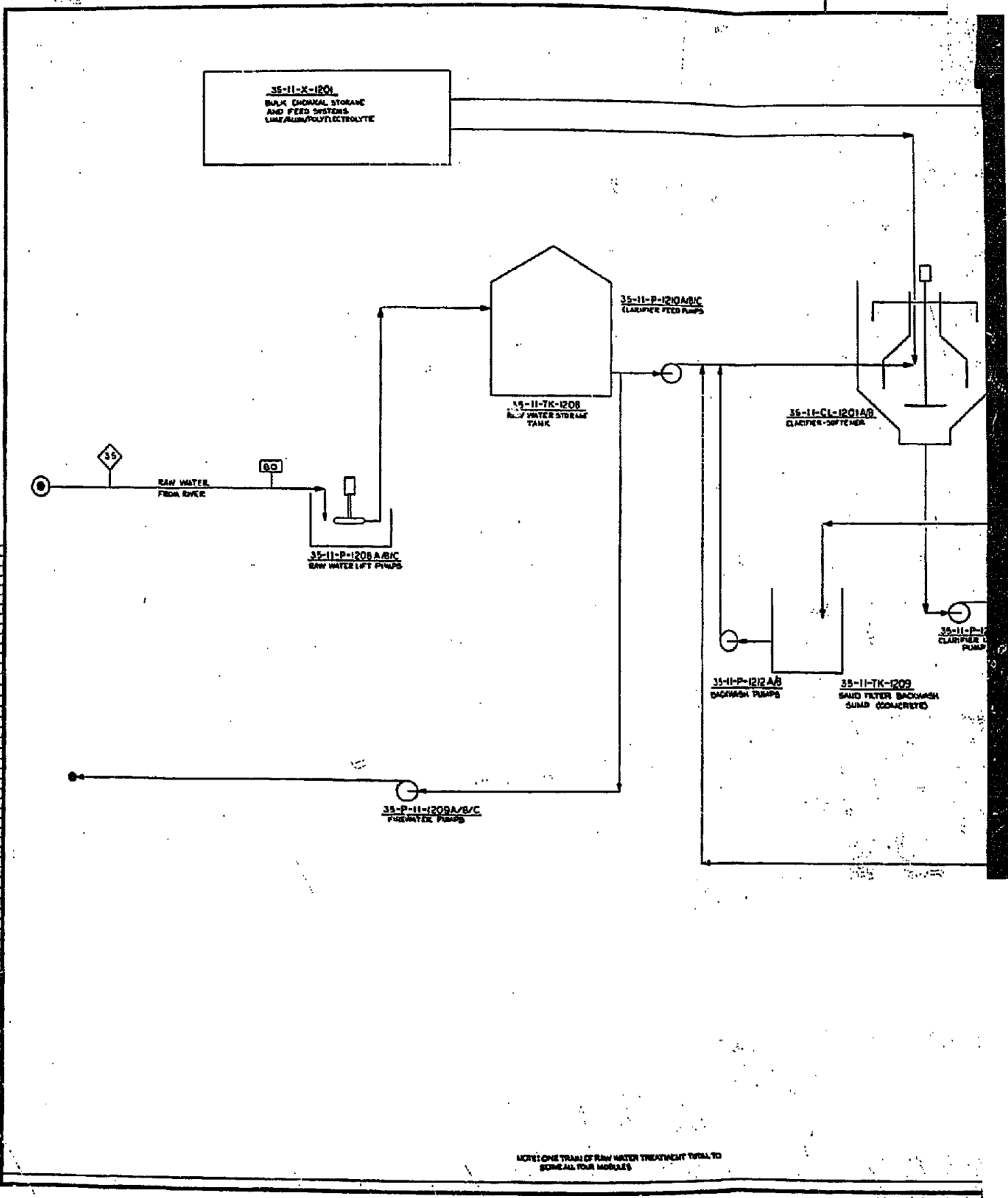
Treated water leaving the Clarified Water Sandfilters, F-1202A/B, flows to SEC 1200-3, SFW Treating (Demineralization).

1. TRAIN PER ALL 4 MODULES (PER PLANT)

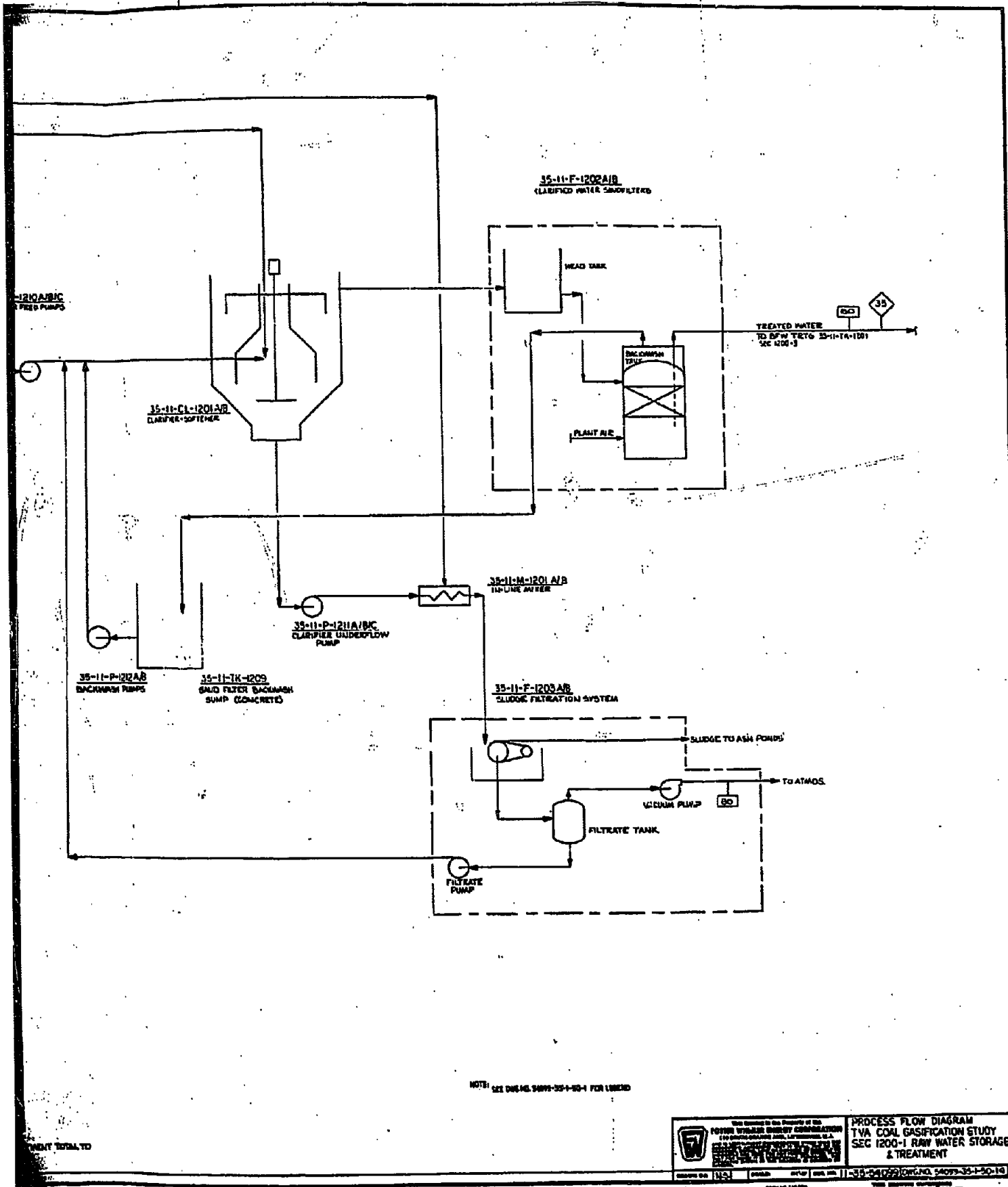
FOSTER WHEELER ENERGY CORP. PROCESS PLANTS DIVISION		CONTRACT NO. 11-35-54099		EQUIPMENT LIST					PAGE OF	
CLIENT TVA (COAL GASIFICATION STUDY)		LOCATION ALABAMA		SECTION 1200-1	TYPE OF UNIT			1	3	
				ORIGINAL	2	3	4	5		
CLASS	ITEM NO	DESCRIPTION	FD*	REVISION DATE	REQ'N. NO.	NO./PLANT			REV	
<u>CLARIFIER</u>										
35-11 -	CL-1201	CLARIFIER-SOFTENER	14			2-50%				
	A/B									
<u>FILTERS</u>										
35-11 -	F-1202	CLARIFIED WATER SANDFILTERS	14			2-50%				
	A/B									
35-11 -	F-1203	SLUDGE FILTRATION SYSTEM	14			2-100%				
	A/B									
<u>MIXER</u>										
35-11 -	M-1201	IN-LINE MIXER	14			2-100%				
	A/E									

1 TRAIN PER ALL 4 MODULES (PER PLANT)

CLASS	ITEM NO	DESCRIPTION	REV. NO. / PLANT	REVISION		DATE	SECTION	TYPE OF UNIT										
				FDY	REQ'D			1200-1	RAW WATER STORAGE/TREATMENT	1	2	3	4	5				
FOSTER WHEELER ENERGY CORP.		CONTRACT NO. 11-35-54099		EQUIPMENT LIST					PAGE OF 2 3									
PROCESS PLANTS DIVISION		TVA (COAL GASIFICATION STUDY)																
CLIENT		ALABAMA																
TANKS																		
35-11-	TK-1208	RAW WATER STORAGE TANK		14			1200-1											
35-11-	TK-1209	SANDFILTER BACKWASH SUMP		14			1200-1											
PUMPS																		
35-11-	P-1208	RAW WATER LIFT PUMPS		14														
	P-1209	FIREWATER PUMPS		14														
	P-1210	CLARIFIER FEED PUMPS		14														
	P-1211	CLARIFIER UNDERFLOW PUMP		14														
	P-1212	BACKWASH PUMPS		14														



NOTE ONE TRAIN OF RAW WATER TREATMENT TOTAL TO
SERVE ALL FOUR MODULES



NOTE: SEE DWG. NO. 3409-30-1-80-1 FOR LEGEND

MENT TOTAL TO

	This material is the Property of the FEDERAL ENERGY ADMINISTRATION 1775 Avenue of the Americas, New York, N.Y. 10019	PROCESS FLOW DIAGRAM TVA COAL GASIFICATION STUDY SEC 1200-1 RAW WATER STORAGE & TREATMENT
	GROUP NO. 11-3 SHEET NO. 11-31-340930-NO. 1409-30-1-80-1	



TVA Coal Gasification Study
Texaco Gasifiers

SECTION DESCRIPTION

3.8 SECTION 1200-2 - POTABLE WATER STORAGE & CONDENSATE TREATMENT

A. Reference Material

- . Process Flowsheet 54099-35-1-50-15
- . Equipment Summary List

B. Description of Flow

Potable water extracted downstream of the Activated Carbon Filter in the Demineralization Unit (Sec 1200-3) is chlorinated to kill micro-organisms, then stored in the Potable Water Drum, D-1210.

Medium pressure condensate and high pressure condensate collected from the various continuous users and various other miscellaneous intermittent users are flashed to 50 psig steam for process users. The low pressure condensate is then cooled to about 274° F in the Condensate/ Demin. Water Exchanger, E-1201, by exchanging heat with cold demineralized water. The latter stream feeds the Deaerator. Cooled condensate is further flashed in the Condensate Storage Tank, TK-1203 to 15 psig steam.

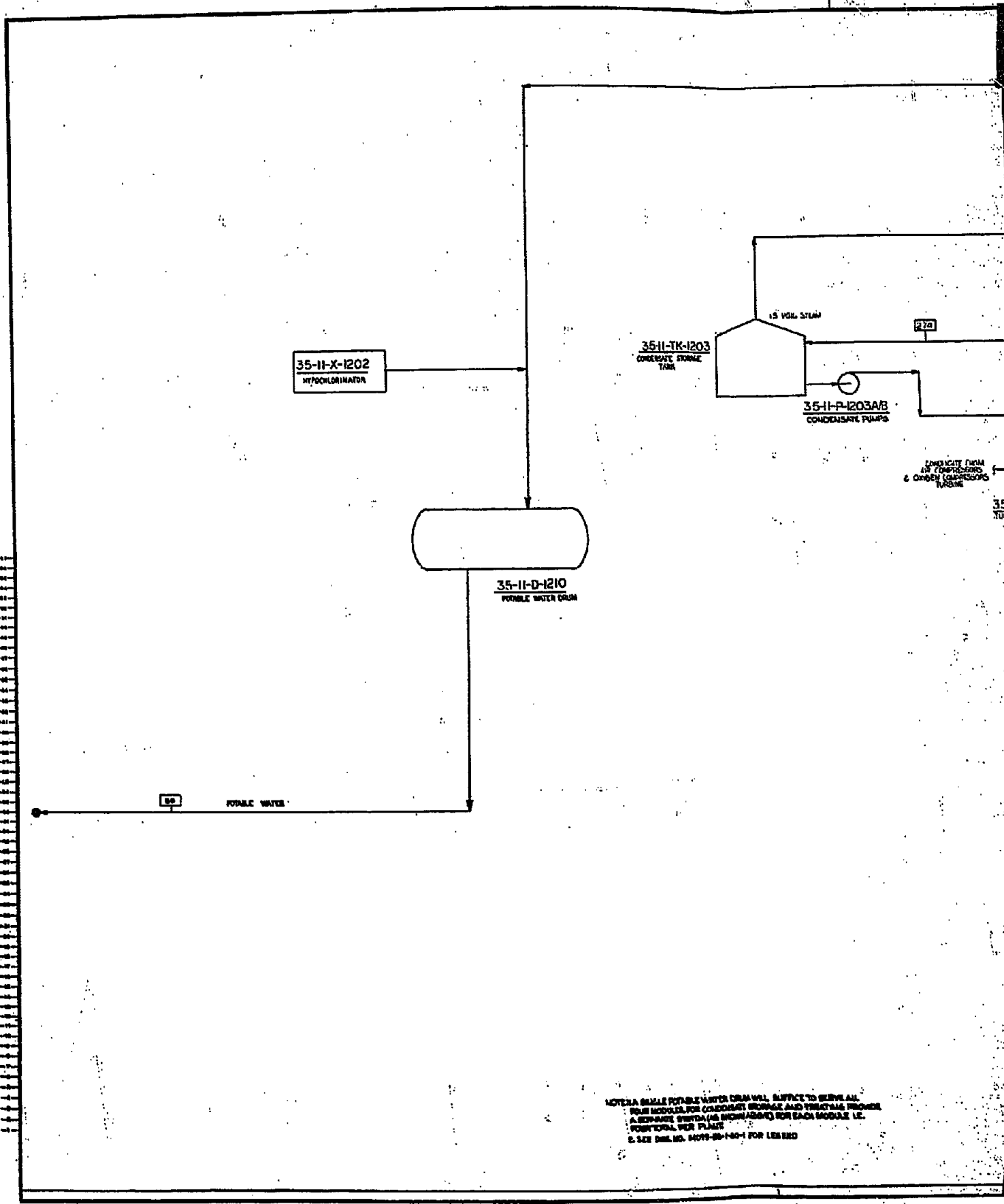
Condensate and steam recovery have been maximized in order to minimize raw water intake costs. Four hours of condensate hold-up is maintained to protect against possible leakage of a process stream into the condensate. Adequate hold-up permits condensate dumping until the source of the problem is located and a course of action is taken. Condensate from the Condensate Storage Tank, TK-1203, is pumped by Condensate Pumps, P-1203 A/B, to the Deaerator, DH-1201. Condensate from turbine drives on the Air Compressor, C-201, and Oxygen Compressor, C-202, enter the Deaerator as does condensate from the shell side of BFW preheater, E-1206. The required deaeration steam is provided by L.P. steam from the 50 psig steam header, M.P. steam from the 85 psig steam header, and to a lesser extent by flashed steam from the Condensate Storage Tank, TK-1203.



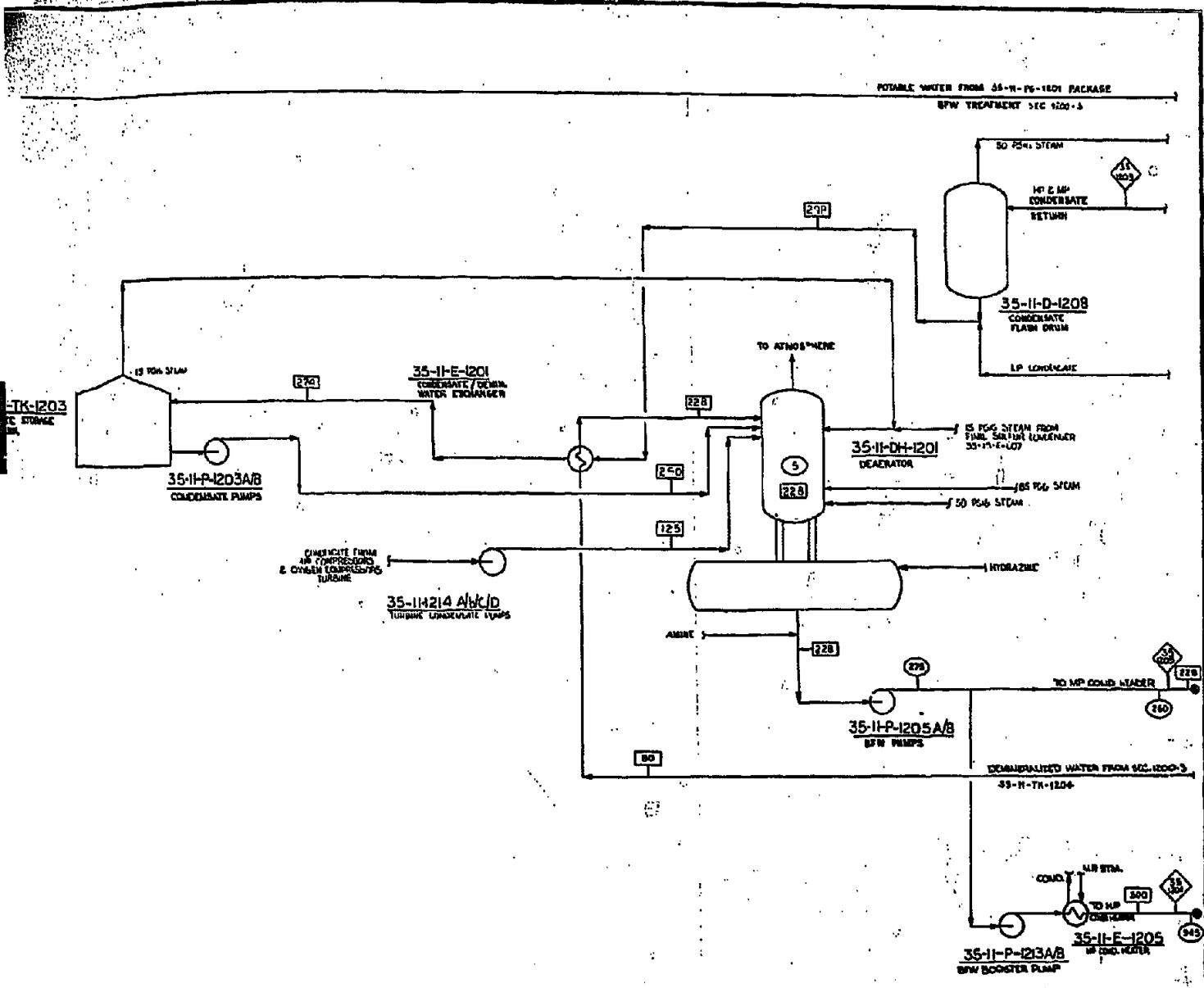
Deaeration is required to prevent corrosion in the various steam generation systems. The Deaerator, DH-1201, normally operates at 5 psig. Steam is used as the stripping medium and is vented to atmosphere, thereby removing gases entrained in BFW. Demineralized water makeup maintains the level in the deaerator storage drum.

Final oxygen control is maintained by chemical addition of hydrazine, an oxygen scavenger, directly to the deaerator. Amine is added in the form of morpholine to the boiler feed-water pump suction line to control corrosion of piping.

Deaerated BFW is pumped to the MP condensate header. A side-stream is withdrawn and boosted to a higher pressure by the BFW Booster Pump, P-1213A/B thereby providing high pressure (935 psig) BFW. This stream is preheated in the H.P. Condensate Heater, E-1206, before entering the HP condensate header.



NOTES: A SINGLE POTABLE WATER DRUM WILL SUFFICE TO SERVE ALL
 FOUR MODULES FOR CONDENSATE STORAGE AND TREATING PROVIDED
 A SEPARATE SHUT-OFF IS PROVIDED FOR EACH MODULE I.E.
 PORTABLE WATER VALVE
 SEE DRG. NO. 1409-20-140-1 FOR LEGEND



ALL WATER CONTAINS SUFFICIENT AMOUNTS OF CHLORINE TO DISINFECT AND TREATS PROVIDED BY THE DESIGN AND/OR FOR EACH MODULE IN PLANT.

35-N-16-1801 FOR LEGEND

 <p>Prepared by the University of the Atomic Energy Commission 120 Avenue, Islamabad, Pakistan</p>	<p>PROCESS FLOW DIAGRAM TMA COAL GASIFICATION STUDY SECTION 200-2 POTABLE WATER STORAGE AND CONDENSATE TREATMENT</p>
<p>Revised on: 10/11/77</p>	<p>35-N-16-1801 DWG. NO. 24000-201-5011</p>



TVA Coal Gasification Study
 Texaco Gasifiers

SECTION DESCRIPTION

3.8 SECTION 1200-3 BOILER FEEDWATER TREATMENT

A. Reference Material:

- . Process Flowsheet: 54099-35-1-50- 16
54099-35-1-50-151
- . Equipment Summary List:

B. Description of Flow


Treated river water at 75 - 80°F average, from Raw Water Treating, Sec 1200-1, is stored in TK-1201 (8 hour surge) then partly used as cooling tower and Gas Scrubbing (Sec 300) makeup. Most of the treated raw water undergoes additional treatment in a Demineralizer Package, PG-1201, to upgrade the water quality for use in the fluid bed boilers which generate high pressure superheated steam (935 psig/775°F). This demineralization system has an activated carbon filter to remove organic chlorides found in the river water in order to protect the downstream resin beds of the demineralizer. Cation exchangers (weak acid unit) reduce hardness and alkalinity; a degasifier removes carbon dioxide and reduces the load on the following mixed bed unit which removes silica and other anions. Demineralized undeaerated water is stored in the Demineralized Water Storage Tank, TK-1204, which provides about 8 hrs. hold-up. From this tank, the demineralized water is pumped through the Condensate/Demineralized Water Exchanger, E-1201, in Sec 1200-2.

Potable water is extracted downstream of the Demineralization Unit Activated Carbon Filter and flows to the Potable Water Drum, D-1210, in Sec 1200-2.

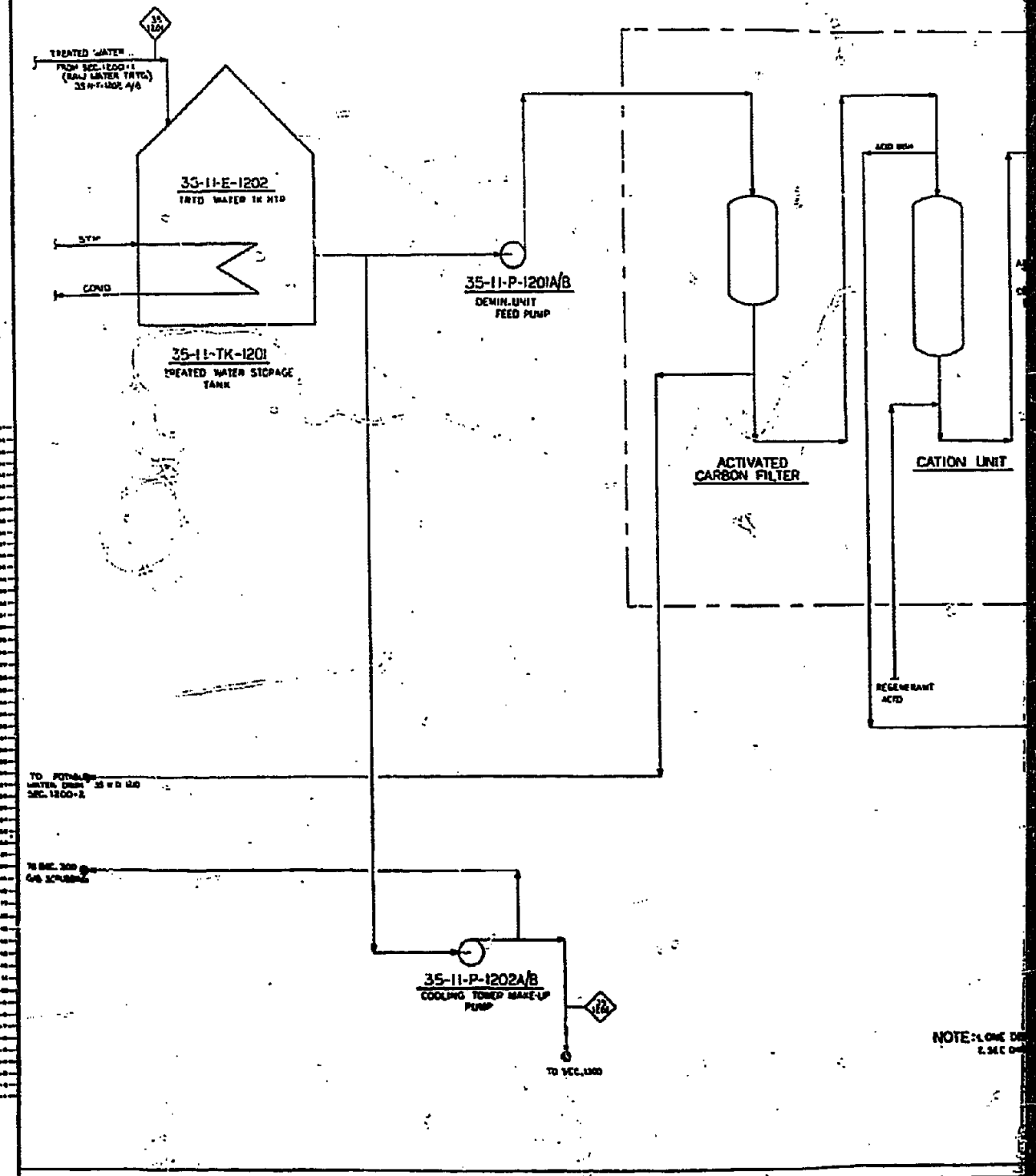
A Neutralization Tank, TK-1202, is provided to collect rinse and regenerant streams from the Demineralizer Package. These wash streams then are neutralized with 66° BE sulfuric acid or 50% caustic, as required. Wastes then are drained to the Clean Water Holding Basin, X-1506, located in the Wastewater Treatment Area, Sec 1500.

FORM NO. 135-904

1 TRAIN PER MODULE

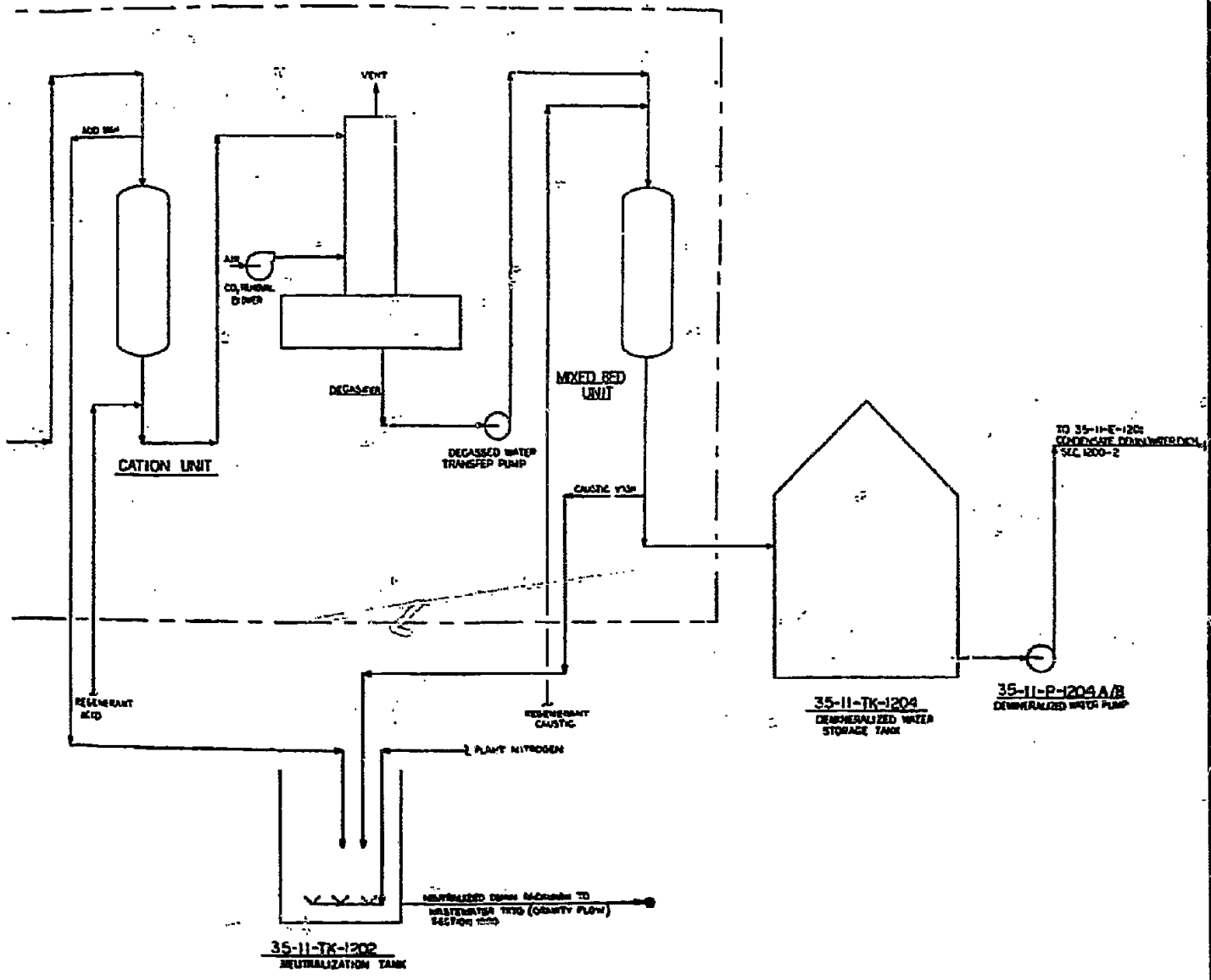
 FOSTER WHEELER ENERGY CORP. PROCESS PLANTS DIVISION		CONTRACT 11-35-54099 SECTION: 120C-3		NAME OF UNIT BFW TREATMENT			PAGE 1 OF 2			
CLIENT TVA (COAL GASIFICATION STUDY) LOCATION ALABAMA				REVISION DATE	ORIGINAL	1	2	3	4	5
CLASS	ITEM NO.	DESCRIPTION	EFD	RECYN. NO	NO./Module	REV.				
PACKAGE ITEM										
35-11-	PG-1201	DEMINEALIZER PACKAGE	16		1-100%					
EXCHANGERS										
35-11-	E-1202	TREATED WATER TANK HEATER	16		1-100%					
-	E-1203	WATER BACKWASH HEATER	16		1-100%					
-	E-1204	CAUSTIC STORAGE DRUM HEATER	16		1-100%					
DRUMS										
35-11-	D-1201	SULFURIC ACID STORAGE DRUM	16		1-100%					
-	D-1202	CAUSTIC STORAGE DRUM	16		1-100%					

35-11-PG-1201
DEMINEALIZER PACKAGE



P
P
P
P
P
P
P
P
P
P
P
P

35-11-PG-1201
DEMINERALIZER PACKAGE



NOTE: 4 ONE DEMINERALIZATION UNIT DESIG. PER MODULE
2. SEC. 1200-3 BFW TREATMENT

	This drawing is the property of the FEDERAL BUREAU OF INVESTIGATION FEDERAL BUREAU OF INVESTIGATION, U.S. DEPARTMENT OF JUSTICE	PROCESS FLOW DIAGRAM TWA COIL GASIFICATION STUDY SEC. 1200-3 BFW TREATMENT
	35-11-PG-1201	35-11-E-1202



TVA Coal Gasification Study
Texaco Gasifier

SECTION DESCRIPTION

3.8 SECTION 1200-4 - STEAM GENERATION AND DISTRIBUTION

A. Reference Material

- . Process Flowsheets FWEC Dwg. No. 54099-35-1-50-17
- . Steam Balance Summary FWEC Dwg. No. 54099-35-1-50-151
- . Equipment Summary List

B. Description of Flow

Flow of steam generation and distribution may be followed on the Plant Steam, Condensate and Boiler Feed Water Diagram, Drawing No. 54099-35-1-50-151.

The Steam Header System consists of four steam levels

High Pressure (H.P.)	900 psig, 1000 ^o F
Medium Pressure (M.P.)	150 psig, 365 ^o F
Low Pressure (L.P.)	85 psig, 460 ^o F
Low Pressure (L.P.)	50 psig, 298 ^o F

High pressure saturated steam is generated through waste heat recovery in the Radiant Cooler, E-313 and Convection Cooler, E-314. Most of high pressure steam is condensed or expanded through turbines driving Air Compressor, C-201, and the Oxygen Compressor, C-202. A small amount of H.P. steam is required for preheat in the Clause Sulfur Recovery Plant. Condensate from H.P. steam users is returned to the deaerator.

Medium pressure steam is generated in Clause Plant Section in the Waste Heat Boiler, E-601. Medium pressure steam is utilized principally in the Gasification Section 300.

85 psig steam is extracted from the oxygen compressor turbine. It is utilized principally in the H₂S Stripper Reboiler, E-403, in Acid Gas Removal Section 400. Other consumers of 85 psig steam are the H.P. Condensate Heater, E-1205, and Deaerator, DH-1201. Also the Beavon Tail Gas Treating Unit, steam tracing and miscellaneous items utilize 85 psig steam.



50 psig steam is generated by flashing medium and high pressure steam condensate into Condensate Flash Drum, D-1203. Waste Heat Boiler, SG-1203, upstream of the Fluid Bed Boiler Superheater, SG-1202, also generates 50 psig steam by recovering heat from flue gas. Consumers of the 50 psig steam are: Deaerator, DH-1201, the Flash Drum, D-701, and Ammonia Stripper, T-701 in Section 700, Tail Gas Treating Unit and Sulfur Prilling Unit. Blowdown from various steam generating equipment is directed to the cooling tower as cooling tower makeup. L.P. condensate flows to the Condensate Storage Tank, TK-1203 and flashes to 15 psig steam. Final Sulfur Condenser, E-607, also generates 15 psig steam. Deaerator, DH-1201, utilizes all of the 15 psig steam generated within the plant. The condensate from the storage tank is pumped to the deaerator for subsequent use as boiler feed water. A BFW Booster Pump, P-1213, is provided in series with the M.P. BFW Pump, P-1205, to pump a portion of the deaerated condensate to the H.P. level.

Process flowsheet 54099-35-1-17 shows the Steam Generator, SG-1201, and the Fluid Bed Boiler Superheater, SG-1202. The Steam Generator is used during the plant startup. The Fluid Bed Boiler Superheater superheats the 900 psig saturated steam produced in the Gasifier. Limestone is injected into both the Steam Generator and Fluid Bed Boiler to reduce the sulfur emission. Approximately 90% of the sulfur in the coal is converted to calcium sulfite, recovered as ash and discharged to the slag pond.

1 TRAIN PER MODULE

FOSTER WHEELER ENERGY CORP. PROCESS PLANTS DIVISION CLIENT "VA (COAL GASIFICATION STUDY) LOCATION ALABAMA	CONTRACT NO. 11-35-54099		EQUIPMENT LIST				SECTION 1200-4	TYPE OF UNIT				PAGE OF
	ITEM NO	DESCRIPTION	REVISION	ORIGINAL	2	3		4	5			
CLASS	FD*	DATE	REQ'D NO.	NO./MODULE					REV			
BLOWERS 35-11	B-1201	BOILER AIR BLOWER	17		ONE FOR ENTIRE PLANT							
	B-1202	SUPERHEATER AIR BLOWER	17	1-100%								
BUNKERS 35-11	BN-1201	COAL BUNKER	17	1-100%								
	BN-1202	LIMESTONE BUNKER	17	1-100%								
	BN-1203	ASH BUNKER	17	1-100%								
DRUMS 35-11	L-1206	CONTINUOUS BLOWDOWN DRUM	17		ONE FOR ENTIRE PLANT							
	D-1207	INTERMITTENT BLOWDOWN DRUM	17		ONE FOR THE ENTIRE PLANT							

1 TRAIN PER MODULE

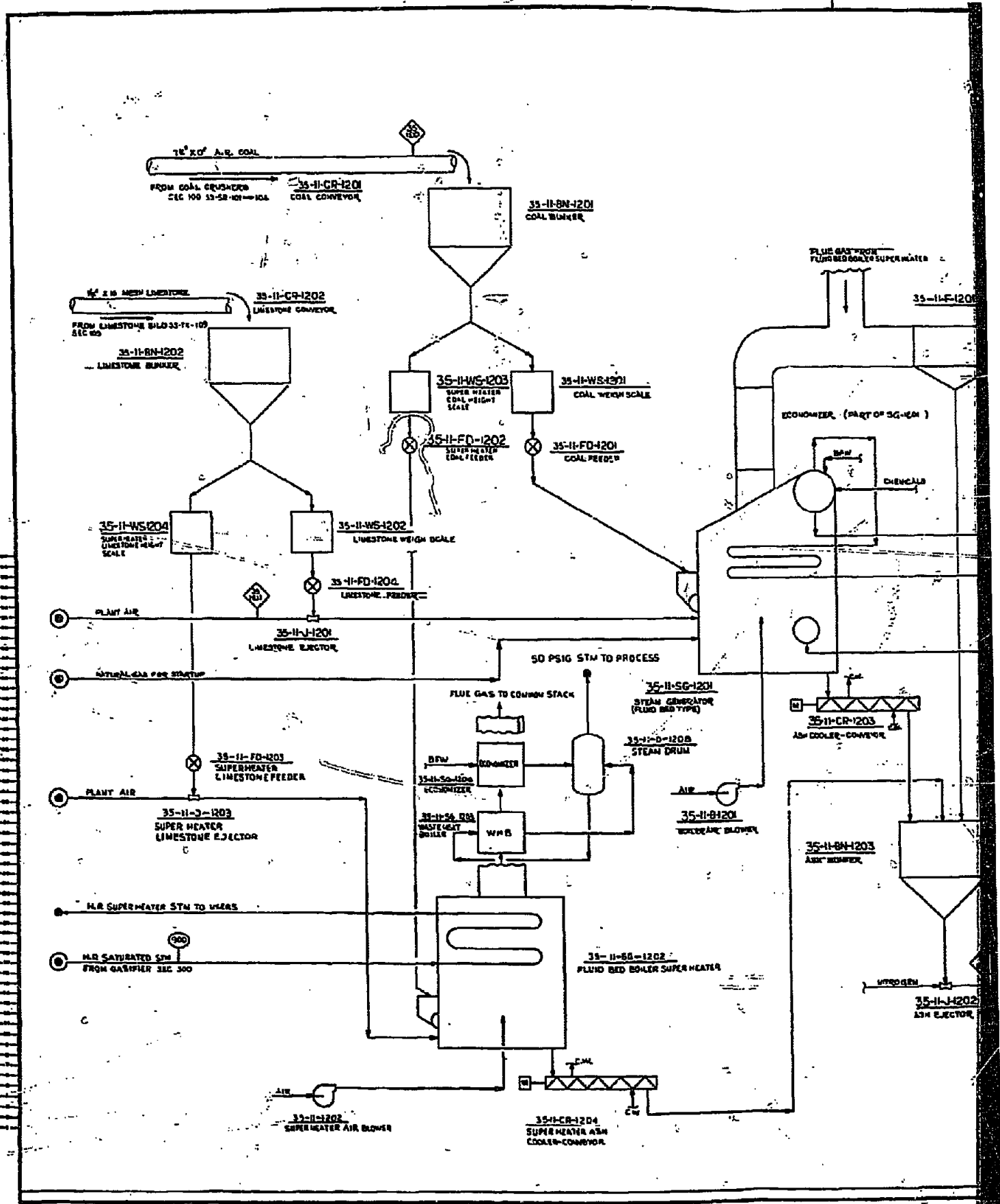
FOSTER WHEELER ENERGY CORP. PROCESS PLANTS DIVISION		CONTRACT NO. 11-35-54099		EQUIPMENT LIST		SECTION 1200-4		TYPE OF UNIT STREAM GENERATION				
CLIENT TVA (COAL GASIFICATION STUDY)				REVISION	ORIGINAL	1	2	3	4	5	6	7
LOCATION	ITEM NO	DESCRIPTION	REV#	DATE	REV#	NO./MODULE	ONE FOR THE ENTIRE PLANT	ONE FOR THE ENTIRE PLANT	ONE FOR THE ENTIRE PLANT	ONE FOR THE ENTIRE PLANT	ONE FOR THE ENTIRE PLANT	REV
CONVEYORS 35-11-	CR-1201	COAL CONVEYOR	17		1-100%							
	CR-1202	LIMESTONE CONVEYOR	17		1-100%							
	CR-1203	ASH COOLER-CONVEYOR	17				ONE FOR THE ENTIRE PLANT					
	CR-1204	SUPERHEATER ASH COOLER CONVEYOR	17		1-100%							
EJECTORS 35-11-	J-1201	LIMESTONE EJECTOR	17				ONE FOR THE ENTIRE PLANT					
	J-1202	ASH EJECTOR	17				ONE FOR THE ENTIRE PLANT					
	J-1203	SUPERHEATER LIMESTONE EJECTOR	17		1-100%							

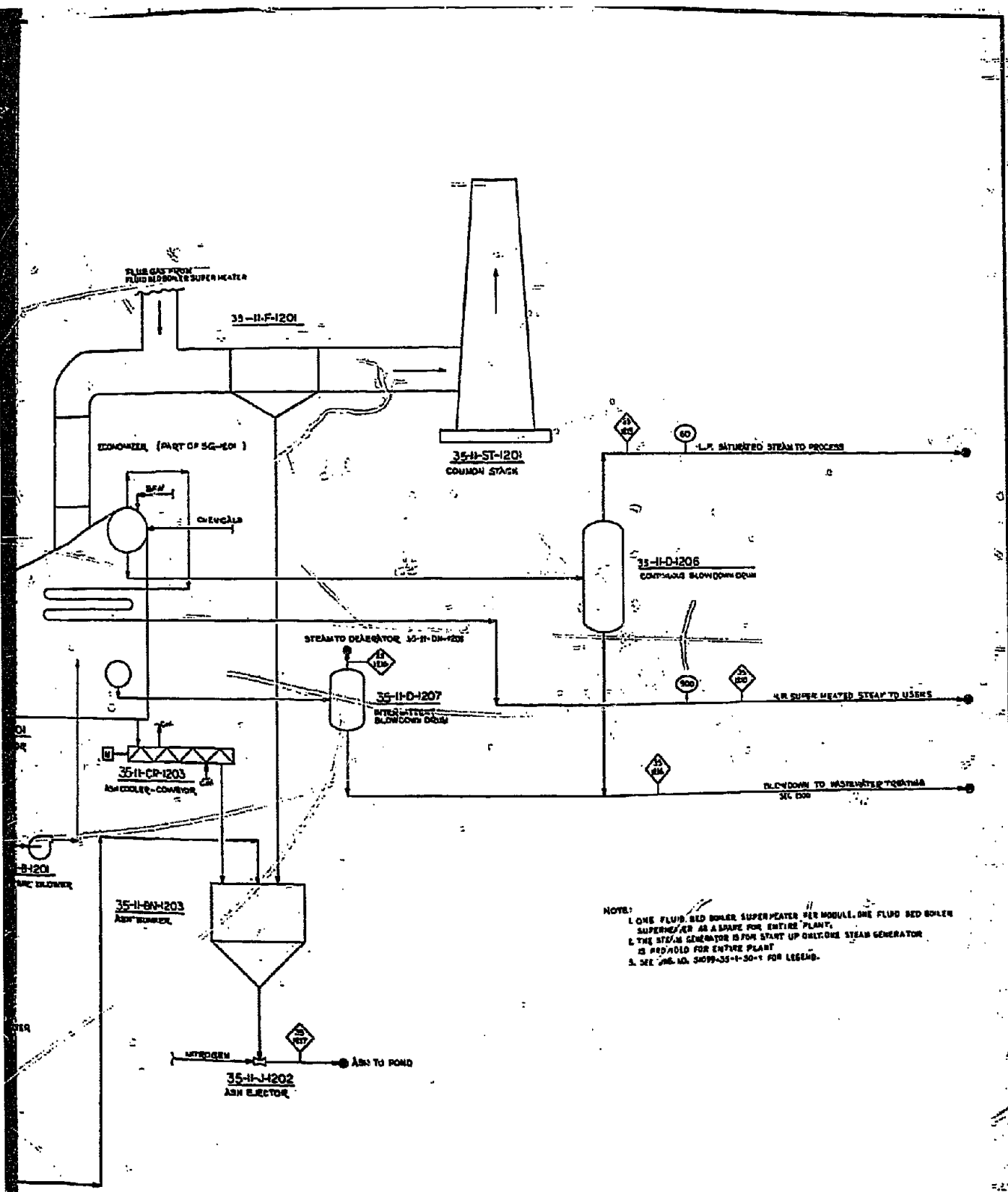
1 TRAIN PER MODULE
EQUIPMENT LIST

CLASS	ITEM NO	DESCRIPTION	FOF	REVISION	DATE	REQ'N. NO. /Module	TYPE OF UNIT			PAGE OF
				ORIGINAL	2		3	4	5	
FEEDERS 35-11-	ED-1201	COAL FEEDER	17			ONE FOR ENTIRE PLANT				
	ED-1202	SUPERHEADER COALEFEEDER	17			1-100A				
	ED-1203	SUPERHEADER LIMESTONE FEEDER	17			1-100A				
	ED-1204	LIMESTONE FEEDER	17			ONE FOR ENTIRE PLANT				


1 TRAIN PER MODULE

FOSTER WHEELER ENERGY CORP. PROCESS PLANTS DIVISION		CONTRACT NO. 11-35-54099		EQUIPMENT LIST				SECTION: 1200-4		TYPE OF UNIT STEAM GENERATION			PAGE OF 4 4	
CLIENT TVA (COAL GASIFICATION) ALABAMA	LOCATION	ITEM NO	DESCRIPTION	REV DATE	REV DATE	REQ'D NO./Module	ORIGINAL	1	2	3	4	5	REV	
35-11-	STREAM GENERATORS	SG-1201	STEAM GENERATOR	17										
35-11-		SG-1202	FLUID BED BOILER SUPERHEATER	17		1-100%								
		SG-1203	ECONOMIZER	17		1-100%								
	STACK	SG-1204	WASTE HEAT BOILER	17		1-100%								
35-11-		ST-1201	COMMON STACK	17		1-100%								
	FILTER (Pbtr)													
35-11-		F-1201	ELECTROSTATIC PRECIPITATOR	17		1-100%								
	WEIGH SCALES													
35-11-		WS-1201	COAL WEIGH SCALE	17										
		WS-1202	LIMESTONE WEIGH SCALE	17										
		WS-1203	SUPERHEATER COAL WEIGH SCALE	17		1-100%								
		WS-1204	SUPERHEATER LIMESTONE WEIGH SCALE	17		1-100%								





NOTE:
 1. ONE FLUID BED BOILER SUPERHEATER PER MODULE, ONE FLUID BED BOILER SUPERHEATER AS A SPARE FOR ENTIRE PLANT.
 2. THE STEAM GENERATOR IS FOR START UP ONLY, ONE STEAM GENERATOR IS REQUIRED FOR ENTIRE PLANT.
 3. SEE SHE. NO. 3409-35-1-30-1 FOR LEGEND.


 U.S. ENVIRONMENTAL PROTECTION AGENCY
 OFFICE OF RESEARCH AND DEVELOPMENT
 WASHINGTON, D.C. 20460

PROCESS FLOW DIAGRAM
 FOR THE COAL GASIFICATION STUDY
 SECTION 4 - STEAM GENERATION
 FLUIDIZED BED BOILER

SHEET NO. 3409-35-1-30-1
 DRAWING NO. 3409-35-1-30-1



TVA Coal Gasification Study
Texaco Gasifiers

SECTION DESCRIPTION

3.9 SECTION 1300 - COOLING WATER SYSTEM

A. Reference Material:

. Process Flowsheet: 54099-35-1-50-18
54099-35-1-50-161

. Equipment Summary List:

B. Description of Flow

The cooling water system consists of a mechanical draft cooling tower, cooling water circulation pumps, chemical addition, blowdown pumps, chromate recovery (if economical), chromate destruct, and settler/thickener packages.

Cooling water at 88°F is pumped by Cooling Water Circulating Pumps, P-1301, A/B/C from Cooling Tower, CT-1301 to the supply header. From the supply header it flows through the distribution system to users and then, into the return header at an average temperature of 103°F. From the return header, it flows back into Cooling Tower, CT-1301, thus completing a closed-loop cycle.

Chemical feeding equipment associated with the cooling water system includes facilities for the addition of chlorine, corrosion inhibitor, dispersant and sulfuric acid. A cooling water monitoring system provides for automatic and continuous sensing of circulating water quality and sends resulting output signals to chemical additives pumps, provided as part of the cooling tower package, and a cooling bleed valve for maintaining non-scaling, minimum corrosion conditions. Gaseous chlorine from cylinders is fed directly into the cooling tower basin by means of an eductor, with water supplied by a tap off the circulating pumps discharge as motive fluid.

To control pH and total dissolved solids content of the cooling water, a bleed stream is pumped by the Cooling Tower Blowdown Pump, P-1302 A/B, to Chromate Recovery, X-1504, then to Chromate Destruct Package, X-1505, located in the Wastewater Treatment Section. The effluent stream from Chromate Destruct is fed to a Settler/Thickener Package, part of




X-1505, from which clarified overflow is sent to a Treated C. T. Effluent Tank, TK-1503, then discharged to the outfall. Thickened underflow sludge is pumped to an offsite area for eventual landfill.

The primary source of make-up cooling water is treated river water from the Treated Water Storage Tank, TK-1201, in Section 1200-3. Makeup is also available as intermittently flowing streams from Wastewater Treatment, Sec 1500, and other sections (Sec 200, etc.)

Cooling water users are shown on dwg. no. 54099-35-1-50-161.

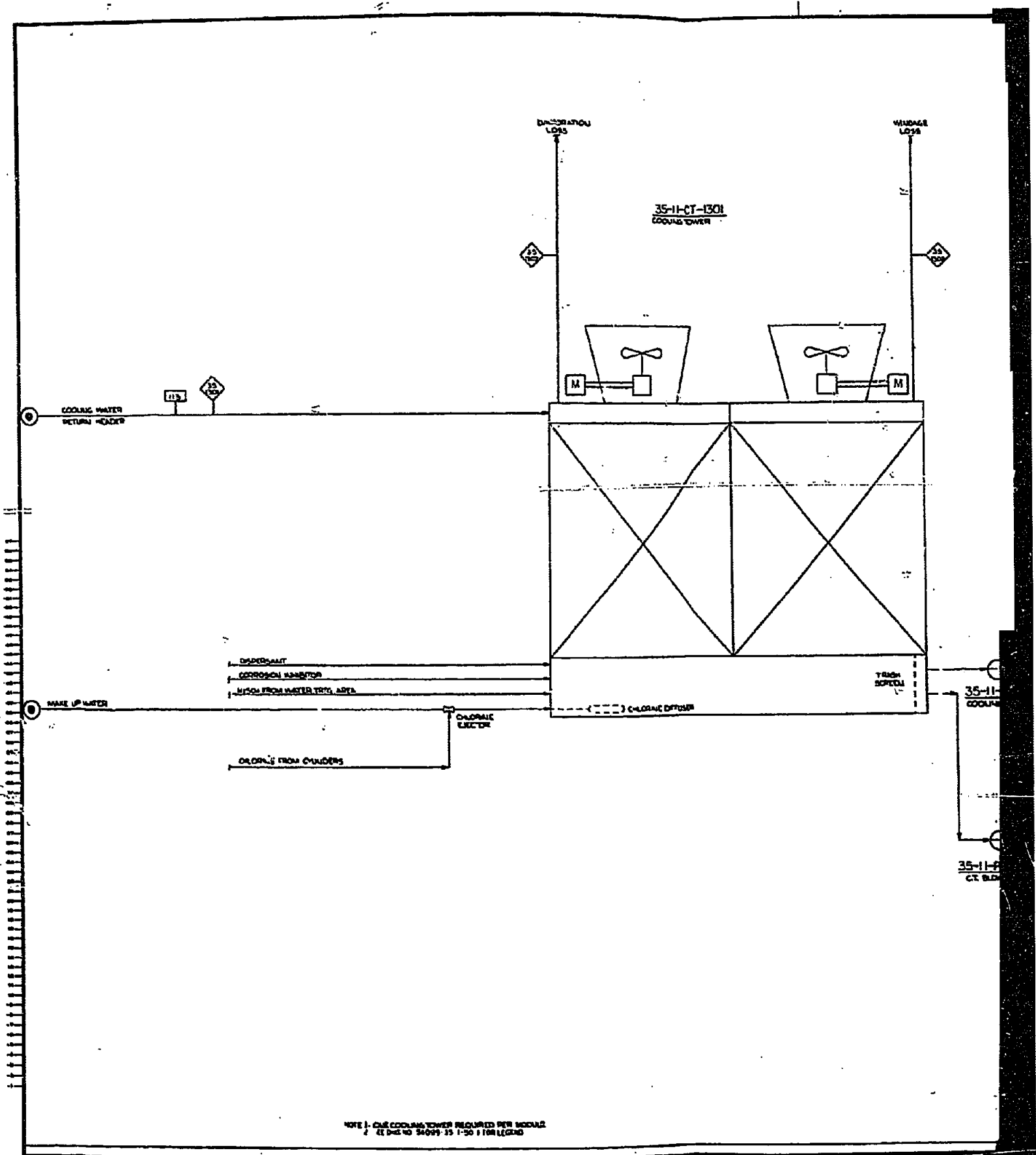
1 TRAIN PER MODULE

 FOSTER WHEELER ENERGY CORP. PROCESS PLANTS DIVISION	CONTRACT NO.	EQUIPMENT LIST		TYPE OF UNIT		PAGE OF	
	11-35-54099	SECTION 1300	COOLING WATER SYSTEM		1 1		1 5
CLIENT TVA (COAL GASIFICATION STUDY)	REVISION		DATE				
LOCATION ALABAMA							

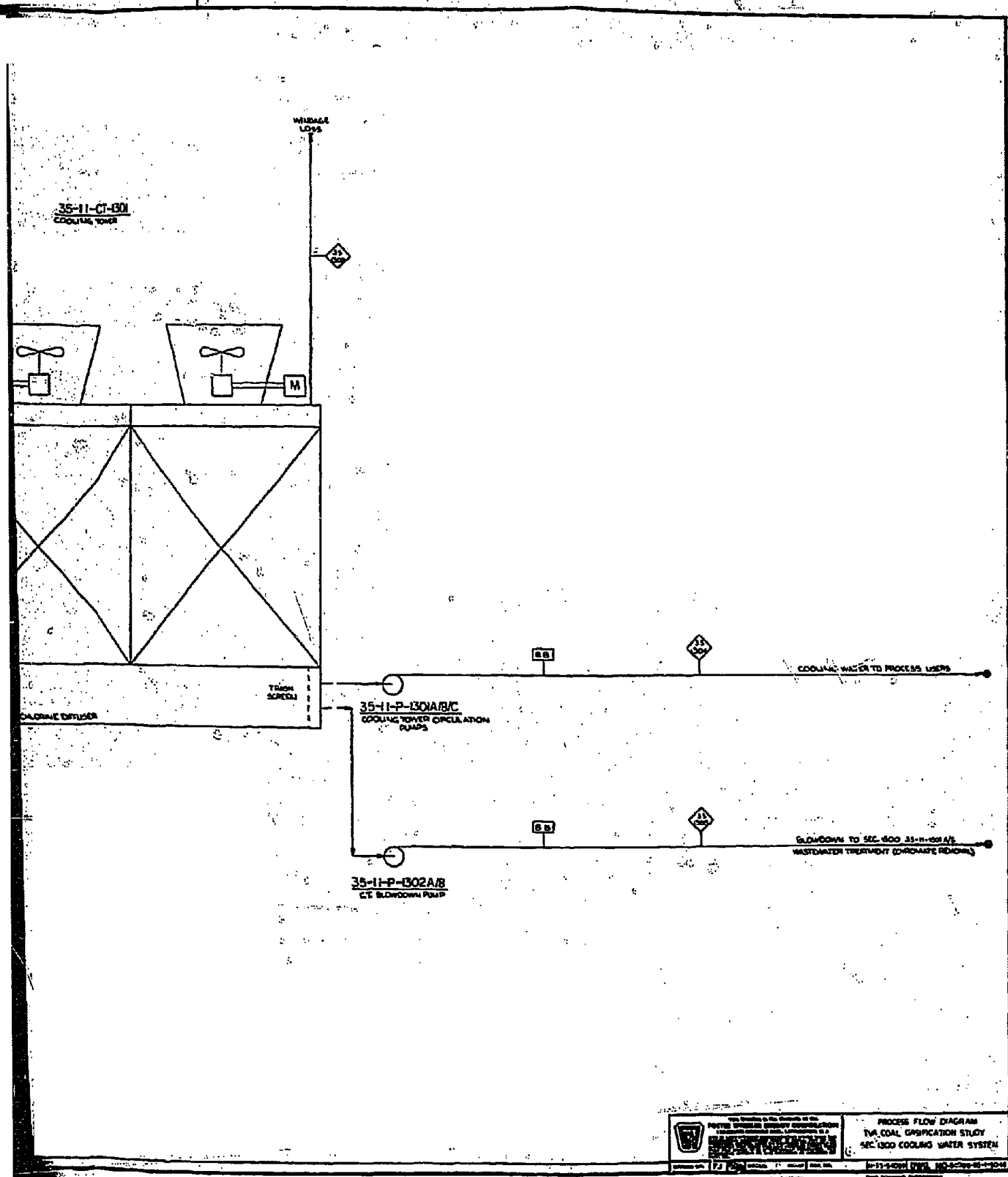
CLASS	ITEM NO	DESCRIPTION	FD	REQ'N. NO./MODULES	REV
COOLING TOWER					
35-11-	CT-1301	COOLING TOWER PACKAGE	18	1-1000	
PUMPS					
35-11-	P-1301	COOLING TOWER CIRCULATION PUMPS	18	3-500	
	A/B/C				
35-11-	P-1302	COOLING TOWER BLOWDOWN PUMP	18	2-1000	
	A/B				

FORM NO. 135-660

p



NOTE 1 - ONE COOLING TOWER REQUIRED PER MODULAR
 2 - SEE DIS NO 34009-35 1-30 1 FOR LEGEND



	PROCESS FLOW DIAGRAM TVA COAL GASIFICATION STUDY SEC 1300 COOLING WATER SYSTEM
	35-11-001 PFD, NO. 3299-01-0048



TVA Coal Gasification Study
 Texaco Gasifiers

SECTION DESCRIPTION

3.10 SECTION 1400 - FLARE SYSTEM

A. Reference Material:

- . Process Flowsheet: FWEC Dwg. No. 54099-35-1-50-19
- . Equipment Summary List:

B. Description of Flow

The function of the flare system is to provide for safe burning of combustible vapors released from process equipment during plant startup, shutdown or during operating upsets.

Flare (K.O.) Seal Drum, D-1401, receives the discharge from vents and safety valves in the various process units connected to a single main flare header. Water collected in the Flare Seal Drum, D-1401, is drained intermittently to Waste Water Treating, Section 1500. Vapors from the Flare (K.O.) Seal Drum are burned in Elevated Flare, FL-1401. The Flare Seal Drum is provided with a steam coil to prevent water freezing in cold weather. Elevated Flare, FL-1401, includes the following features:

- . Facilities for smokeless burning of hydrocarbons.
- . An air seal, located underneath the flare tip to prevent oxygen back-diffusion into the system.
- . A flame front generator for igniting pilots.
- . Facilities are provided for automatic nitrogen injection into the flare knockout drum to compensate for the system "contraction" after a hot blow.

As part of the flare package, a Pilot Gas K.O. Drum is provided in the pilot gas line to separate all liquid droplets from the gas. Similarly, a Steam Separator removes entrained mist and bulk condensate from the steam line.

An incinerator or ground flare, H-1401, is provided to combust raw gas during startup. Incinerator air is blown by B-1401 A/B,

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one operating blower and one 100% spare, through the air Pre-heater, E-1401, and into the incinerator combustion chamber. Flue gases are vented to a stack provided by the incinerator vendor.

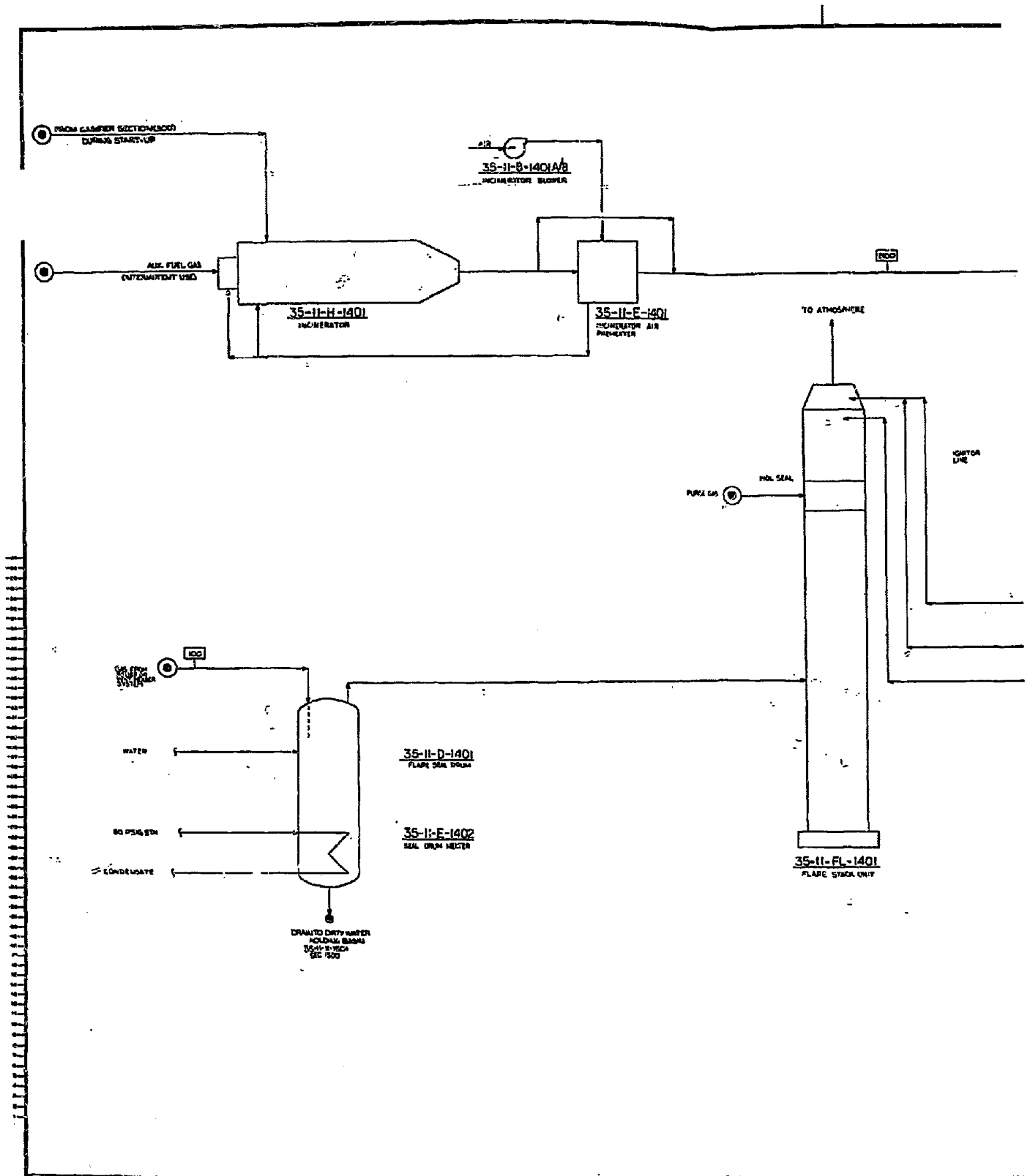
Form No. 130-171

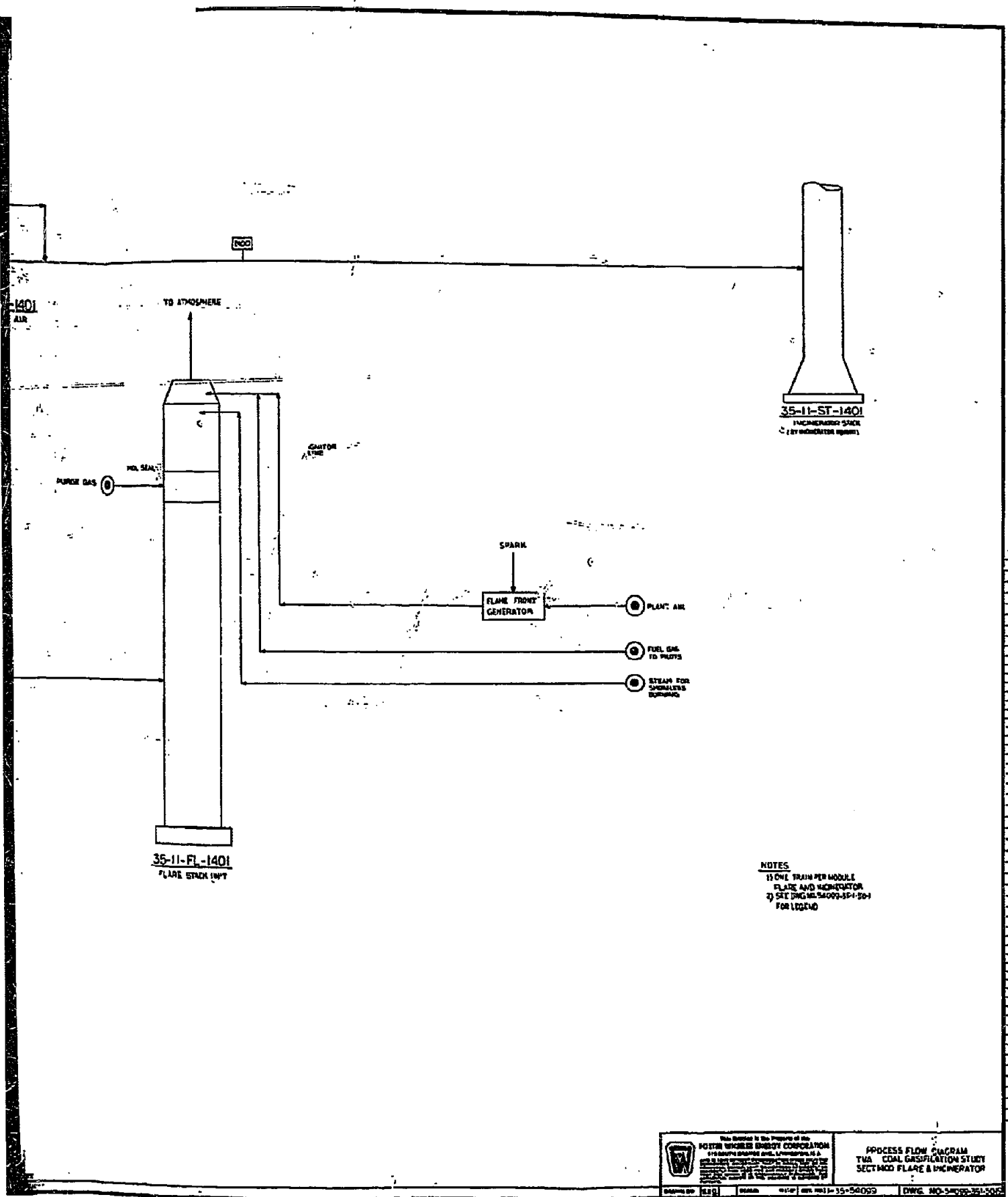
1 TRAIN PER MODULE

FOSTER WHEELER ENERGY CORP. PROCESS PLANTS DIVISION		CONTRACT NO. 11-35-54099	EQUIPMENT LIST			PAGE OF	
CLIENT TVA (COAL GASIFICATION STUDY)			SECTION 1400	TYPE OF UNIT FLARE & INCINERATOR	1	2	
LOCATION ALABAMA	ITEM NO	DESCRIPTION	FD#	REVISION DATE	ORIGIAL		
CLASS				REQ'N. NO. /Module			REV
<u>DRUM</u>							
35-11-	D-1401	FLARE SEAL DRUM	19		1-1008		5
<u>FLARE</u>							
35-11-	FL-1401	FLARE STACK UNIT	19		1-1008		
<u>EXCHANGER</u>							
35-11-	E-1401	INCINERATOR AIR PREHEATER	19		1-1008		
	E-1402	SEAL DRUM HEATER	19		1-1008		
<u>FURNACE</u>							
35-11-	F-1401	INCINERATOR	19		1-1008		

1 TRAIN PER MODULE

CLIENT	LOCATION	CLASS	ITEM NO	DESCRIPTION	FDR	REVISION		SECTION	TYPE OF UNIT			PAGE	OF
						DATE	NO.		1	2	3		
FOSTER WHEELER ENERGY CORP. PROCESS PLANTS DIVISION	TVA (COAL GASIFICATION STUDY)	ALABAMA							1400	ETABE & INCINERATOR	2	2	
CONTRACT NO. 11-35-54099								ORIGINAL			4	5	
EQUIPMENT LIST													
INCINERATOR STACK													
35-11-	ST-1401			INCINERATOR STACK	19				1-100#				
BLOWER													
35-11-	B-1401	A/B		INCINERATOR BLOWER	19				2-100#				





	This Drawing is the Property of the POLAR WHEELS ENERGY CORPORATION 215 SOUTH BRADLEY AVE., FORT WORTH, TEXAS 76102		PROCESS FLOW DIAGRAM TMA COAL GASIFICATION STUDY SECTION 1400 FLARE & INCINERATOR
	DRAWING NO. 35-11-101	SHEET NO. 1401	

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TVA Coal Gasification Study
Texaco Gasifier Alternate

SECTION DESCRIPTION

3.11 SECTION 1500 - WASTE WATER TREATMENT

A. Reference Material:

. Process Flowsheet: FWEC Dwg. No. 54099-35-1-50-20

. Equipment Summary List:

B. Description of Flow

Wastewaters will be generated from several sources in the plant. The type and degree of treatment and the ultimate disposal of these wastewaters will depend on the source of the wastewater and on the type and concentration of pollutants in the water. The wastewaters and their sources are:

1. Stormwater falling on, and drained from the area inside the limits of processing units (ISBL);
2. Ash Pile Leachate from stormwater falling on piles of ash;
3. Rinse and Neutralization Water from regeneration of the Demineralizer in Sec. 1200-3;
4. Spent service water (deck washings, flushing, etc.)
5. Stormwater falling on, and drained from the coal piles; Coal Pile Runoff
6. Cooling tower blowdown;
7. Sanitary wastewater generated by plant personnel.

The treatment and disposal of these wastewater streams are described below:

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Clean Water Streams - ISBL Stormwater,
Ash Pile Leachate and Rinse
and Neutralization Waters

The above clean water streams are collected in the Clean Water Holding Basin, 35-11-X-1506 for analyses before pumping these waters to the cooling tower (as makeup) or discharging to the outfall depending upon dissolved solids level.

ISBL stormwater is collected from process units and may require lifting to the holding basin depending on the plant terrain. Ash pile leachate is an intermittent stream which drains from piles of ash during a rainfall. Rinse and neutralization waters are obtained during regeneration of the Demineralizer. The latter unit reduces the dissolved solids level to permit the use of water as BFW makeup to the H.P. Steam Generators.

Dirty Water Streams - Coal Pile Runoff,
Service Water

The above streams are described in the Preliminary Report on Emissions and Effluents. They are relatively low in organics (BOD, COD) but do contain a significant amount of dissolved solids. Cyanides may be present in the stripped sour water stream, although analyses or estimated cyanide level have not been determined. If cyanides are present, these will be destroyed rather easily by the relatively inexpensive ozonation-UV system.

Coal pile leachate (runoff), spent service water from deck washings, etc. are collected in the Dirty Water Holding Basin, 35-11-X-1501. A continuous discharge is pumped to the Neutralization Basin, TK-1501, into which hydrated lime is fed by gravity from a large storage bin mounted above the basin. The lime adjusts the PH to approximately 8.5. The wastewater then flows by gravity to an Aerating Basin, X-1502, where fixed aerators aerate and mix the incoming stream oxidizing inorganic ionic materials, thereby causing them to form insoluble hydroxides. The aerated stream flows by gravity to the rectangular clarifier with traveling arm siphon sludge removal, CL-1501, where the insoluble precipitate settles from the water.

The 20 wt.% solids precipitate slurry is pumped to a disposal pond. Decant from the pond is returned by gravity to the clarifier. Sludge is removed periodically from the pond for disposal to landfill.

It may be necessary to recarbonate the clarified stream to remove excess lime. This could be accomplished using the CO₂ rich gas stream emitted



from the Beavon Unit absorber. The clarified-recarbonated stream then would enter an ozonation-UV package system for destruction of cyanides. Since oxygen is available from the Air Separation Plant, Sec. 200, ozone could be generated simply by providing an ozone generator. Ozone would contact the aqueous stream in an Ozone Contactor.

Treated wastewater is pumped to the Treated Wastewater Basin, X-1503, for analyses, then pumped to the Cooling Tower as makeup or discharged to the outfall.

Cooling Tower Blowdown.

Cooling Tower blowdown contains chromium and zinc which must be reduced to very low levels before this aqueous stream, high in dissolved solids, can be discharged.

A chrome recovery system, X-1504, is shown on drwg. 54099-35-1-50-20, preceded by a sandfilter to remove suspended solids and prevent fouling of ion-exchange resins in the recovery system. A moving bed ion exchange system could reduce chromium and zinc levels to less than 1 ppm each. The recovery system would be followed by a Chrome Destruct Unit, X-1505, which would precipitate residual chromium and zinc as insoluble hydroxides, thereby reducing these metals to undetectable levels.

The cost effectiveness of a recovery system must be studied i.e. whether the value of recovered materials would pay out the capital cost in a reasonable period of time. If not cost effective, the recovery system will be omitted and all the chrome and zinc in the C.T. blowdown destroyed.

Treated cooling tower blowdown is held in a day tank, TK-1503, for analyses before being pumped to the outfall.

Sanitary Wastewater


Sanitary wastewater from toilets, showers and wash basins will be sent to a package biological unit to reduce BOD and destroy microorganisms. The treated wastewater will be discharged.

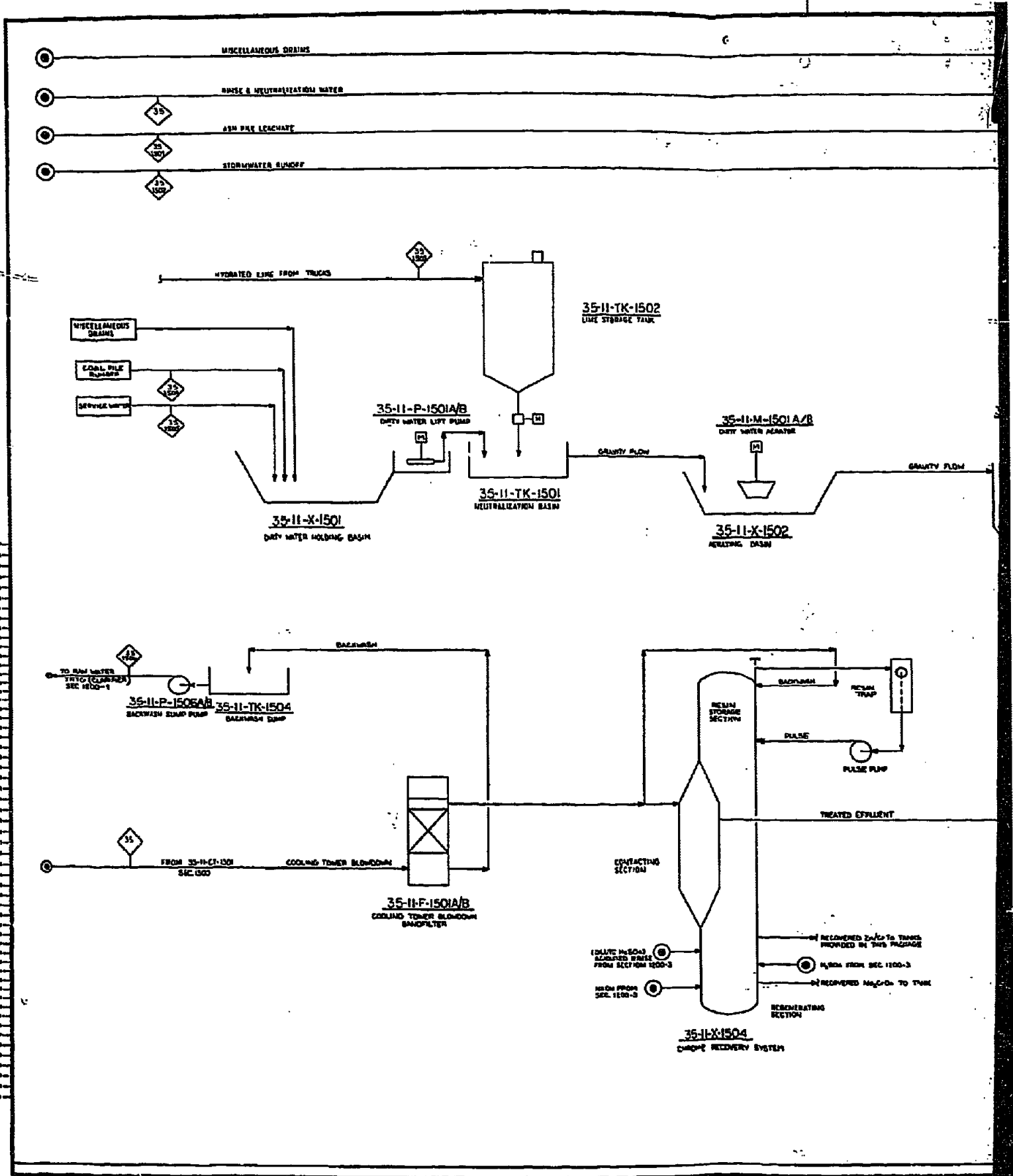
FOSTER WHEELER ENERGY CORP. PROCESS PLANTS DIVISION		CONTRACT NO. 11-35-54099		EQUIPMENT LIST		SECTION 1500		TYPE OF UNIT WASTEWATER TREATMENT		PAGE 1 OF 3	
CLIENT TVA (COAL GASIFICATION STUDY)	LOCATION ALABAMA	REVISION	DATE	REQ'N. NO.	NO./MODULE	ORIGINAL	2	3	4	5	REV
CLASS	ITEM NO	DESCRIPTION	QTY								
FILTER											
35-11-	F-1501	COOLING TOWER BLOWDOWN SANDFILTER	20			2-100%					
	A/B										
TANKS											
35-11-	TK-1501	NEUTRALIZATION BASIN	20			1-100%					
-	TK-1502	LIME STORAGE TANK	20			1-100%					
-	TK-1503										
-	TK-1504	BACKWASH SUMP	20			1-100%					
CLARIFIER											
35-11-	CL-1501	LIME TREATMENT CLARIFIER	20			1-100%					

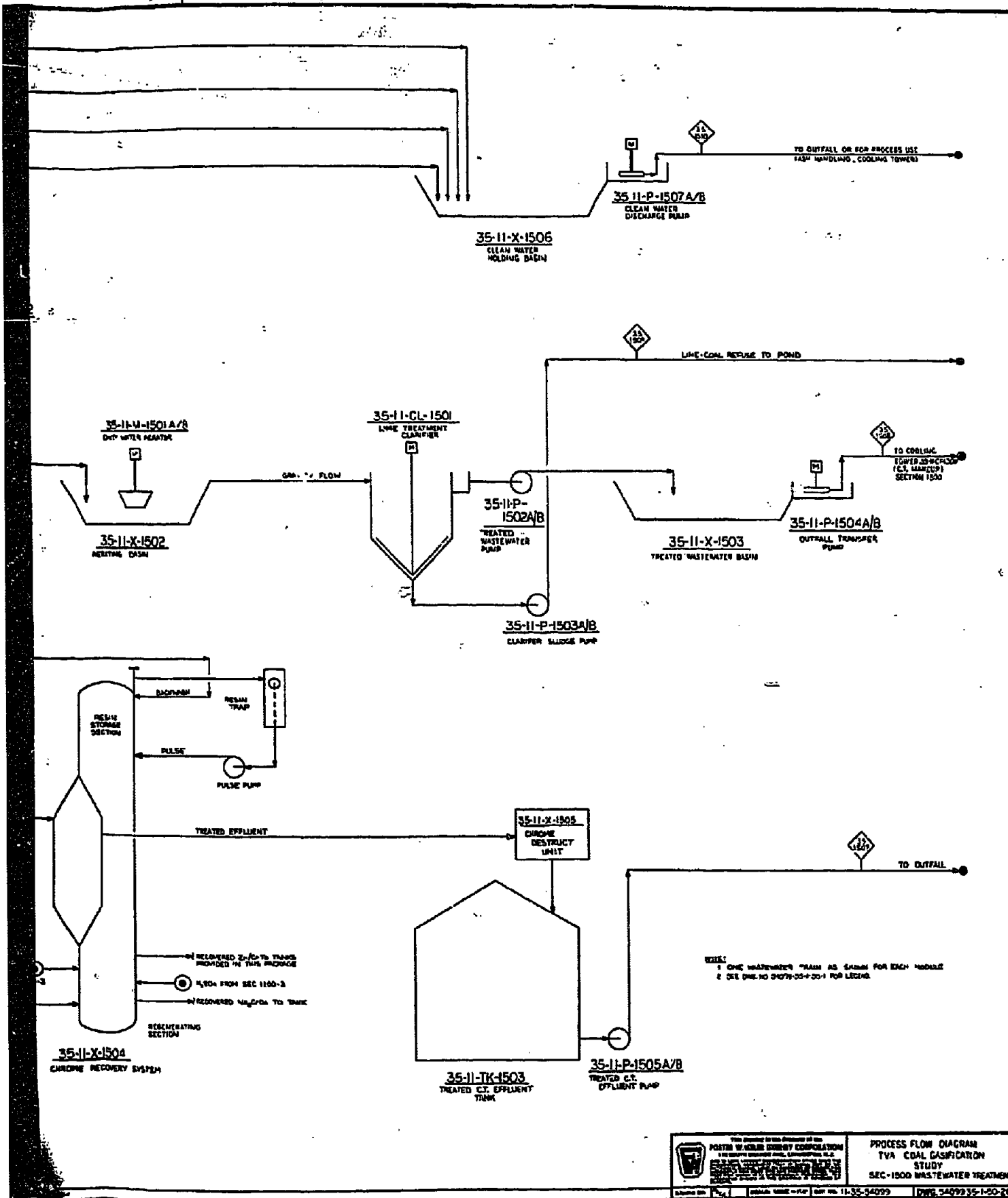
1 TRAIN FOR EACH MODULE

FOSTER WHEELER ENERGY CORP. PROCESS PLANTS DIVISION		CONTRACT NO. 11-35-54099		EQUIPMENT LIST				PAGE OF	
CLIENT TVA (COAL GASIFICATION STUDY)				SECTION		TYPE OF UNIT			
LOCATION ALABAMA				1500 ORIGINAL		WASTEWATER TREATMENT		2 3	
CLASS	ITEM NO	DESCRIPTION	REV. NO.	DATE	REQ'D NO.	NO. / Module	REV		
AERATOR									
35-11-	N-1501	DIRTY WATER AERATOR	20			2-100%			
	A/B								
PUMPS									
35-11-	1501A/B	DIRTY WATER LIFT PUMP	20			2-100%			
	1502A/B	TREATED WASTEWATER PUMP	20			2-100%			
	1503A/B	CLARIFIER SLUDGE PUMP	20			2-100%			
	1504A/B	OUTFALL TRANSFER PUMP	20			2-100%			
	1505A/B	TREATED C.T. EFFLUENT PUMP	20			2-100%			
	1506A/B	BACKWASH SUMP PUMP	20			2-100%			
	1507A/B	CLEAN WATER DISCHARGE PUMP	20			2-100%			

1 TRAIN FOR EACH MODULE

 FOSTER WHEELER ENERGY CORP. PROCESS PLANTS DIVISION TVA (COAL GASIFICATION STUDY) ALABAMA		CONTRACT NO.	EQUIPMENT LIST				PAGE OF	
CLIENT	LOCATION	CLASS	ITEM NO	DESCRIPTION	REV. NO.	DATE	TYPE OF UNIT	REV
11-35-54099	ALABAMA							
							1	3
							2	4
							3	5
MISCELLANEOUS								
35- 11-			X-1501	DIRTY WATER HOLDING	20		1-100%	
-			X-1502	AERATING BASIN	20		1-100%	
-			X-1503	TREATED WASTEWATER BASIN	20		1-100%	
-			X-1504	CHROME RECOVERY SYSTEM	20		1-100%	
-			X-1505	CHROME DESTRUCT UNIT	20		1-100%	
-			X-1506	CLEAN WATER HOLDING BASIN	20		1-100%	







TVA Coal Gasification Study
Texaco Gasifiers

SECTION DESCRIPTION

3.12 SECTION 2000 - GENERAL FACILITIES

This section describes long-term ash and slag storage, by-products and chemicals storage, firewater system, sewage plant, power, lighting and communications.

Ash and Slag Storage

An irregular area, generally N.E. of the operating plant facilities, is to be cleared and rough graded for deposition of ash and other spent solids related to the combustion processes. The perimeter of the ash pile is designed with a vertical to horizontal slope 1:3 to provide for a reasonable margin of design for stability. Should it be required, an additional margin of stability of the perimeter embankment can be provided by employing earth and rock fill material from the site.

Slag from the Texaco gasifiers and flyash and spent bed materials from auxiliary fluidized bed superheaters, are expected to have a chemical composition and resulting physical properties resembling irregularly shaped glass beads. The foregoing may render the slag pozzolanic when reacted with lime in the presence of moisture. In any event, either the slag in its natural state, or with the addition of lime, would be hospitable to supporting root systems for plant growth. Ultimately, such vegetation would be an effective means for stabilizing both the surface of the slag pile as well as the perimeter.

The Design Criteria (Section 4.3) of TVA, for base-case design, stipulates no lining under ash, sludge, and water containment ponds. The present design, which is dry storage, does not include any lining. The reader should be alerted to the possibility of leachate from the slag and ash pile finding its way into Guntersville Reservoir. A relatively high iron oxide content in the ash/slag would indicate an acidic leachate. In any event, none of the chemical constituents of the ash indicated in the Design Criteria appear as toxic materials which could leach into water ultimately destined for consumption by humans, fish or animals. Elsewhere, it has been reported, however, that flyash normally contains a variety of toxic elements in trace amounts which could leach into the soil and, ultimately, into Guntersville Reservoir.

None of the foregoing comments are to be construed as definitive statements of fact and should, therefore, be verified by suitable testing immediately following startup of the plant to verify the chemical and physical behavior of the ash. The presence of toxic elements and the possible attenuating properties of the soil from the proposed plant site of Murphy Hill should be determined.



By-products and Chemicals Storage

A 14-day supply of limestone for the fluidized bed steam superheaters is provided.

Sulfur is converted into a solid form in a prilling operation at the sulfur recovery unit serving each module of the gasification plant. The solid prills are then transported to a storage bin of 30 days production capacity prior to removal from the plant site.

A variety of solvents, catalysts and other chemicals are stored either as a periodic replacement charge or as a continuing, expendable requirement. Such solvents, catalysts and chemicals are indicated in the succeeding section 2. Plant Requirements.

Firewater System

A 10-inch underground looped piping network will be provided to supply firewater to all areas of the plant. Hydrants are located at approximately 300-foot intervals. In the Process Area, 25 percent of the hydrants will be provided with monitor nozzles capable of directing water coverage on equipment in minimal response time.

The source of firewater is an allowance in the Raw Water Storage Tank. Three (3) 2000 gpm pumps -- one diesel-driven and two motor-driven -- supply water to the piping grid. A fourth 300 gpm capacity jockey pump provides pressurization of the system at all times. Should loss of pressure occur due to fire, the main pump(s) are sequentially started automatically. Pump discharge pressure is 150 psig. This assures firewater supply demands to remote hydrants at 80 to 100 psig.

Sewage System

Several sewer systems will be provided. These include a clean rain runoff system, an oily water system to handle rain runoff from areas of oily contamination, systems to handle rain runoff from coal pile and ash storage areas and sanitary sewer collecting wastes from all building sanitary facilities. All these systems direct flow to the waste treatment facilities for treatment.

Power, Lighting and Communications

1. General

The electrical facilities for the Coal Gasification Complex will be a complete installation, including power supply from a TVA power substation, lighting, communications, fire alarm and aircraft warning systems.



2. Standards, Codes and Regulations

The design, materials, equipment and installation of the electrical facilities will be in accordance with Foster Wheeler's Engineering Standard 70A1, the latest edition of the codes and regulations contained therein, and including the following:

- Section 1.4.3 Electrical Design Considerations (TVA Design Criteria)
- U.S. Bureau of Mines
- FAA Regulations
- FCC Regulations

3. Area Classification

All areas within limits are classified in accordance with the National Electrical Code, Article 500.

4. Power Distribution

A 30 MVA, 138/13.8 KV intertie with the TVA power grid will be provided to supply power.

The overall design basis for the proposed electrical system is one of high reliability to minimize interruption of operation. Key features of the design are as follows:

- Dual feeders from the TVA power system.
- Secondary-selective double-ended substation load centers are provided as required to supply medium and low voltage process loads.
- Double radial feeders are run to each load center.
- Outdoor/indoor bus duct is furnished from the outdoor transformers to the indoor 5 KV or 480 KV switchgears.
- All switchgear and Motor Control Centers are indoors.
- Electric power is distributed to power consumers on the following basis:

Motors 250 HP to 5,000 HP; 416 V, 3 phase, 3 wire

Motors ½ to 200 HP; 460 V, 3 phase, 3 wire

Motors below ½ HP; single phase, 2 wire

Lighting & Instrument branch circuit; 120 V, single phase.



5. Electrical Equipment

In general, electrical equipment and wiring materials are furnished as required by Article 500 of the National Electrical Code and Section 1.4.3 Electrical Design Considerations (TVA Design Criteria), and to conform to the following standards, where applicable:

- National Electrical Manufacturer's Association (NEMA)
- American National Standards Institute (ANSI)
- Underwriter Laboratories (UL)

In non-hazardous locations, equipment enclosures are dictated by dust and moisture or corrosive conditions of the location. The minimum enclosure for electrical apparatus is NEMA, Type 1.

6. Motor Control Equipment

The 4000 V motors up to 2000 HP are magnetic contactor-type control with current limiting fuses. Two-high units are furnished. Motors greater than 2000 HP are controlled by switchgear-type circuit breakers. The 460 V motors are controlled by a combination circuit breaker and magnetic contactor.

7. Wiring Method

Both 13.8 KV and 416 V distribution will be in underground conduits. Within process unit limits where overhead pipe racks or supports are available, wiring for 480 V and less will be in overhead conduit. All rigid conduit will be hot-dipped galvanized steel or PVC (polyvinyl chloride).

8. Lighting

Lighting for process areas is provided in accordance with FW Engineering Standard 70A1 and all applicable standards referred to in Section 1.4.3 Electrical Design Considerations (TVA Design Criteria).

Aviation obstruction lighting will be provided in accordance with the FAA requirements for the site.

Road and fence lighting will be provided, using mercury vapor lighting fixtures mounted on poles and incandescent fixtures for fence lighting whenever road/fence layout does not allow the use of a combined lighting system.

9. Communications

Telephone Company System: An empty conduit system will be provided for the local telephone company to furnish and install telephone service to the plant.

Two-way Communication: A two-way FM radio communication system will be provided for plant operation.



10. Fire Alarm System

The fire alarm system design is based on utilization of the telephone system for fire alert throughout the plant. Telephone-type relays will be provided to actuate fire signal devices in areas required for personal safety.

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TVA Coal Gasification Study
Texaco Gasifiers

SECTION DESCRIPTION

3.13 SECTION 2100 - BUILDINGS

Buildings for the Coal Gasification Complex will be provided in accordance with the building list tabulated below. This indicates the nominal building dimensions and designates the basic materials of construction. The buildings will be in accord with standard industry design. The envisioned scope of supply includes necessary foundations, structural framing, sheathing, roofing, insulation, plumbing, heating and ventilating, along with electrical power and lighting circuitry. All design and construction will be completely in accordance with applicable local and state codes.

Allowance is provided for building furnishings. This includes office furnishings for the administration building and other office areas for personnel, tools and shop equipment to sufficiently outfit the various craft shops in the maintenance building to conduct normal maintenance of plant equipment, laboratory equipment for sampling and analyzing process streams, change house lockers and facilities for personnel convenience.

<u>Service</u>	<u>Dimensions (ft)</u>	<u>Area (ft²)</u>	<u>Construction Material</u>
Administration		25,600	Masonry
Maintenance			
Shop	75 x 280	21,000	Pre-fab Metal
Offices	48 x 100	4,800	Masonry
Warehouse	200 x 240	48,000	Pre-fab Metal
Laboratory	50 x 100	5,000	Masonry
Firehouse/First Aid	50 x 90	4,500	Pre-fab Metal
Gate/Change House	80 x 125	10,000	Pre-fab Metal
Process Control	60 x 100	6,000	Masonry
Water Treatment	100 x 200	20,000	Pre-fab Metal
Electrical Substations (size varies 10 required)			Masonry

Form No. 130-171