

TVA/OGM/CG-81/11

MASTER

TVA COAL-GASIFICATION
COMMERCIAL DEMONSTRATION PLANT PROJECT

VOLUME 4

PLANT BASED ON
BABCOCK & WILCOX GASIFIER

FINAL REPORT
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Foster Wheeler Energy Corporation

110 South Orange Avenue, Livingston, New Jersey

PROCESS PLANTS DIVISION

BY: [Signature] MFW



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SECTION 1.0

INTRODUCTION

FOSTER WHEELER ENERGY CORPORATION



TVA Coal Gasification Study
B&W Gasifier

INTRODUCTION

The baseline design of a coal gasification plant producing medium Btu gas, based upon the Babcock and Wilcox gasification process is documented in this report.

The coal gasification plant consists of four identical modules, each with a capacity of approximately 5,000 tons of coal per day as delivered to the gasifiers. The entire plant (four modules) produces 1205.7 Million Standard Cubic Feet per day of gas with a GHV value of approximately 299 Btu/SCF for a total heating value of about 360 billion Btu/day.

The plant location is the rural site of Murphy Hill, located along the Tennessee River, some 30 miles east of Huntsville, Alabama. Section 1 provides more detailed site information.

The desired product gas is a clean, medium-Btu gas suitable for pipeline distribution. The coal used for processing and for auxiliary boilers is a Kentucky No. 9 coal. The product gas specifications and the coal characteristics are listed in Section 2.

The site is accessible by barge and road, with the plant receiving coal primarily by barge. About 5 percent of plant needs are delivered by truck. The site will not be served by rail. The coal receiving facilities are sized to handle the entire needs of the plant.

Water needed for cooling and for process consumption will be drawn from the Tennessee River and will be treated by the plant water treatment facility. The plant will use closed loop cooling. Electricity will be furnished by TVA at the plant boundary.

The plant will be designed to meet all Federal, State, and local standards and guidelines.

A description of the plant by major sections is included as well as flow diagrams, stream balances and lists of major equipment. A key plot plan is presented in Section 5.

Section 6 presents an estimate of emissions and effluents from the Babcock and Wilcox coal gasification plant.



2.1 Discussion of Choice of Processing Sequence

Evaluations and specific studies completed in Task I and the characteristics of the B & W gasifier influence the process selection for both the plant main units and the support facilities. Studies involved in Task I included:

- o Gas Cleanup
- o Oxygen Purity
- o Coal Washing
- o Sulfur Recovery

Support facilities studies include:

- o Equipment Drives
- o Gas Storage and Spares
- o Gas Delivery Pressure
- o Effects of Scale
- o Effects of Load Change

Process selection depends upon economics, experience with the process application and upon the characteristics of the B & W gasifier. In addition to the selection of the process units, there is also the problem of selection of the process configuration involving the arrangement of units, number of trains, multiple part-capacity equipment items all integrated with the optimum plant capacity. Some configuration limitations are due to the state of development of the gasifier, some to equipment size and scale limitations, as well as product demand variation and high risk, high maintenance items.



2.2 General Description of Flow

Drawing No. 54099--50-27-1 is a block flow diagram illustrating a coal conversion MBG plant using the Babcock and Wilcox gasifier. As shown in the diagram, coal, air, and water are the only raw materials entering the plant. Medium Btu gas is the only product leaving the plant, together with by-products of sulfur, carbon dioxide and slag.

The accompanying Process Block Flow Diagram provides an overview of the main processing units selected for preparing medium Btu gas based on incorporating B & W's gasification reactor. A brief review of the schematic which traces the flow of raw materials into finished product is furnished below, as well as a more detailed description of each individual unit.

Raw coal is received from barges and is transported to coal storage piles. The coal is crushed, screened and dried, and fed to the gasifier, where it is reacted with oxygen from the air separation plant. The gasifier product gas is cooled and scrubbed free of solids, after which the acid gas components, CO₂, H₂S and COS, are removed in the Selexol unit. Slag emanating from the gasifier is removed to a slag disposal area; sour water condensates generated from various processing units is treated by steam stripping. The hydrogen sulfide removed in the acid gas treating step is further processed to recover saleable sulfur, either in molten or prilled form. The resulting clean medium Btu gas is compressed for transmission to the distribution system.

Support facilities common to these various units include: utilities, waste water treating, flare/incineration, and cooling tower.

Air Separation Plant

The B & W gasification system requires approximately 4,200 ST/D of oxidant per module to react with coal. The air separation plant is designed for a capacity of 5% higher than that shown in the material balance. This 5% factor accounts for variations in the coal composition, heating value and carbon content, but does not include any factors associated with licensor's guarantees or with on-stream factors.

Task I evaluation studies indicate a 98% concentration of O₂ is optimum and a low pressure reversing exchanger process is economical.

For B & W gasifiers, a 98% oxygen purity means that the GHV of product gas will be about 296 Btu/SCF.



The B & W Gasifier

The B & W gasifier is based upon the principle of entrained flow, high temperatures and short residence time. Pulverized coal, oxygen and transport gas are fed to the reactor in a multiplicity of feed points or burners, creating a rising stream of hot gas. The "combustion zone" temperature is very high, promoting the melting of the ash which falls by gravity to a central tap hole, then to a quench section. The slag breaks up to a frit in the quench zone and is removed from the gasifier by means of an ash lock hopper. Recycle char from the two stages of cyclones is reinjected into the gasifier, using steam transport. Fine char rises with the hot, high velocity gas. The gas cools due to continued gasification and, also, due to heat transfer to the bare wall evaporator tubes in the upper zone of the gasifier. The gas exits the gasifier together with partially reacted char, the bulk of which is removed in the primary cyclone. Heat is then recovered in the waste heat boiler, which is followed by a secondary cyclone. After heat recovery, the gas is further cleaned of particulates by means of a venturi scrubber.

The gasifier system includes the coal feed lock hoppers, gasifier, ash lock hopper, cyclones, waste heat boiler and scrubber. The gasifier will be designed for 5% increased capacity above the normal material balance to account for coal variations.

Acid Gas Removal

Gas from the scrubbers is sent to a Selexol unit to remove sulfur compounds in the gas. The Selexol system chosen in Task I is a physical absorption acid gas removal system operating at low temperatures of $0^{\circ}\text{F} \pm 20^{\circ}\text{F}$. The Selexol plant will be designed for both 105% of material balance capacity and for 115% of the H_2S and COS concentration to allow for coal variations.

The Selexol system can absorb all sulfur compounds in the gas phase. However, COS solubility in the Selexol solution is lower than that for H_2S . As a result, the solution circulation and utilities are determined by COS. This is evident if the COS concentration is high or if the sulfur specification of the product gas is low. For 200 ppm sulfur, it is economical to hydrolyze COS after the scrubber and then remove H_2S and residual COS in the Selexol unit. The hydrolysis unit is designed for 5% higher capacity and 15% more COS than the normal material balance.



Sulfur Recovery

The most economical method of sulfur recovery from acid gas is by means of the Claus plus tail gas plant, provided the H₂S concentration in the acid gas is above 15 to 20%. For the B & W gasifier, the H₂S concentration will be better than 20% H₂S concentration regardless of the amount of CO₂ removed from the product gas, which has a low CO₂ concentration. A tail gas cleanup is required with a Claus unit, which only converts 90% of the H₂S to elemental sulfur. The Beavon-Stretford type was chosen in Task I to remove sulfur compounds from the Claus tail gas. The H₂S concentration in the acid gas is sufficiently high to allow a "split flow" Claus operation. Reasonable concentrations of H₂S are required in order to sustain combustion in the Claus furnace. The Beavon unit converts all the sulfur compounds from the Claus unit back to H₂S. The concentration of H₂S in the tail gas from the Beavon unit is very low. Consequently, a Stretford unit is used to convert the low concentration, low pressure H₂S to elemental sulfur. The tail gas is then vented.

Task I evaluations and studies conclude that elemental sulfur would be the more desirable product rather than to convert H₂S to sulfuric acid. The least expensive way of handling the elemental sulfur would be as a molten liquid. Sulfur can be produced in either molten or solid form; it was concluded that the prilled solid form would be preferable for the TVA design. The Claus-Beavon-Stretford Sulfur Recovery System will be designed for 115% of material balance to account for variations of sulfur content of the coal.

Support Facilities

Support facilities include utilities, coal and ash handling, wastewater treatment and general facilities.

Steam Production and Distribution

Steam production from the gasifier includes 245,000 lbs/hr of 250 psi and saturated, plus 650,000 lbs/hr of 950 psi steam superheated to 750°F. The low pressure steam will be used to drive turbines. However, steam generation in boilers will be small compared to that required for the Lurgi Dry Ash system. For the capacities required, it is believed that the most economical boiler for the B & W gasifier would be a coal fired fluidized bed boiler. This choice would eliminate the stack gas scrubber and also eliminate sludge disposal problems. There would still be a problem of disposal of solid ash plus calcium sulfit-sulfate, a simpler problem than sludge disposal.



Plant Water Treating and Distribution

Plant water is obtained from the river, with each module requiring about 3000 gpm. The systems to which plant water is distributed include:

- o Fire water
- o Boiler feed water
- o Potable water
- o Cooling tower water makeup
- o Ash quench and sluice makeup

Sufficient spare pump capacity is required to account for pump maintenance while operating and for variation in coal properties.

Fire water is simply river water with coarse screening to remove trash and silt.

Boiler feed water, in addition to the above, will have treatment and demineralization sufficient for the purity required for the steam generating pressure and superheat.

Potable water will be treated for purity required for drinking purposes.

Cooling tower makeup must be treated to remove silt and for chemical addition to prevent corrosion and prevent algae growth. Part of the cooling tower makeup water may come from the treated process waste water.

Ash quench and ash sluice water makeup may come from river water. It may also come from treated process waste water or it may come in part from cooling tower blowdown.



Waste Water Treatment

Waste water treatment is a single train system for each module. Process water before disposal must be reduced in dissolved acid gases by means of a sour water stripper. The gas from the sour water stripper is sent to the Claus unit to recover sulfur and the stripped water is sent to the waste water treatment system. Waste water treating consists of clarification, neutralization, aeration, sludge removal, holding tanks and disposal to outfall. In addition to process waste water, the coal pile runoff is also treated in the same system as the process waste water. Other liquid streams which require treatment are sanitary effluents, spent service water, inside battery limits (ISBL) storm runoff, cooling tower blowdown and neutralization water from ion exchange demineralizers.

All the above streams are held in effluent holding basins to measure pH, turbidity, BOD and priority pollutants before sending the water to the river. Cooling tower blowdown must have a chromium destruct system before allowing that water to flow to the river. Sanitary effluent will be treated by conventional package system and ISBL storm runoff will be treated with the normal process waste water system. However, in order to smooth out a large surge in storm water capacity, a holding basin is provided so that storm water may be worked off gradually.

Coal Handling, Treating and Feeding

Coal receiving, unloading, conveying, stacking and reclaiming are not influenced by the gasification process and are the same for all gasification processes with slight variations in amount of coal for each process. The Babcock and Wilcox gasification process differs from the Lurgi type in that all the coal to the gasifier shall be crushed and pulverized to 70% by weight through 200 mesh. The pulverized coal (PC) shall be dried and pneumatically transported to lock hoppers to raise the coal to operating pressures and then the coal must be injected into the gasifier by means of multiple burners.

Coal is reclaimed from the live or long storage piles, screened and crushed to a size of $1\frac{1}{2}$ x 0. The crushed coal will be further reduced in the pulverizer to 70% through 200 mesh. Hot flue gas enters the pulverizer, drying coal to 2% moisture and lifting the coal to the primary pulverizer cyclone. Hot flue gas is generated in hot air heaters by burning coal.



Pulverized coal is gravity fed from the cyclones and baghouses directly into the coal storage bin. From the storage bin, the coal drops by gravity into lock hoppers where the coal is pressurized and then directed to the feed tank. Coal is transported from the bottom of the feed tank into the gasifier with inert gas.

Slag Handling

Slag is formed when molten ash in the gasifier is quenched with water. The molten slag is broken into small size frit.

A slag slurry from each gasifier lock hopper is gravity fed into a transfer hopper and then sluiced to a sump. The slurry from a number of gasifiers is collected in the sump and pumped to a dewatering bin. Damp ash is conveyed by truck to onsite storage piles together with other solid wastes, such as sludge from stack gas scrubbers or spent limestone (gypsum) from fluidized bed boilers. Water from the dewatering bin is clarified and then returned to the slag lock hoppers for reuse. About 10% by weight of the slag is water remaining after dewatering.

Slag handling equipment is designed at a rate of 25% higher than material balance to account for coal property variations.

Slag Disposal

Slag is trucked from the Slag Handling area dewatering bins, together with spent limestone from the boilers to basins for 20 years of storage. Water is pumped from drainage culverts surrounding the ash piles to a holding pond and then the drainage water is used for slag conveying, quenching and lock hoppers. Excess water is sent to the waste water treating section for disposal. The slag storage area is based upon the material balance with no increased factor for coal variations. Any variation in coal should be smoothed out in 20 years.



2.3 NOMINAL PLANT CAPACITIES

11-28-54099

PLANT BASED ON B&W GASIFIERS
SUMMARY OF CAPACITY OF THE PLANT SECTIONS

2.3

SECTION	SECTION DESCRIPTION	NO. OF PLANTS	CAPACITY 1 MODULE		CAPACITY 4 MODULES		INSTALLED COST MM\$
			NORMAL	DESIGN	NORMAL	DESIGN	
100	COAL PREPARATION CRUSH & SCREEN LIVE COAL STORAGE DEAD PULVERIZE	1	15,744 T/D 76,000 TONS 488,000 TONS PART OF SECTION 300	21,168 T/D 76,000 TONS 488,000 TONS SECTION 300	62,976 T/D 304,000 TONS 1,952,000 TONS	84,672 T/D 304,000 TONS 1,952,000 TONS	
200	AIR SEPARATION O ₂ PLANT LOX STORAGE O ₂ COMPR	8-508	4,200 T/D 1 Motor Driven 1 Turbine "	4,410 T/D 4,500 TONS 11,744 BHP 6.78 lbs.stm/hr-HP 250 TONS 8,400 TONS NONE	16,800 T/D 4 Motor Driven 4 Turbine "	17,640 T/D 18,000 TONS 4x11,744 BHP 6.78 lbs.stm/hr-HP 1,000 TONS 33,600 TONS NONE	
300	LIQ N ₂ STOR GAS O ₂ STOR GAS N ₂ STOR	4	5,418 T/D WET 5,000 T/D DRIED	5,418 T/D WET 5,000 T/D DRIED	21,672 T/D WET 20,000 T/D DRIED	21,672 T/D WET 20,000 T/D DRIED	
400	COAL GASIFICATION ACID GAS REMOVAL COMPRESSION HYDROLYSIS (RAW GAS T=200°F)	4	756,291 lbs/hr MW = 21.085 30,911 lbs/hr total 17,484 lbs/hr H ₂ S	794,106 lbs/hr	3,025,164 lbs/hr	3,176,424 lbs/hr	
500	TRT GAS COMPR	4	1 Turbine Driven	29,469 BHP 6.69 lbs/hr-H.P.	4 Turbine Driven	4x29,469 BHP 6.69 lbs/hr-H.P.	
600	SULFUR RECOVERY CLAUS PLT	5	198 T/D SULFUR IN FEED 50,865 lbs/hr total sulfur 649 lbs/hr	2 PLANTS IN 1ST MODULE 456 T/D SULFUR 116,870 lbs/hr Equiv. 1,492 lbs/hr	990 T/D SULFUR 254,325 lbs/hr 3,245 lbs/hr	1140 T/D SULFUR 292,475 lbs/hr 3,730 lbs/hr	
700	5 BEAVON UNITS: TOTAL TAIL GAS TAIL GAS CLEANUP, SULFUR: SULFUR PRILLING SOUR WATER STRIPPING H ₂ S IN FEED = 22 lbs/hr NH ₃ IN FEED = 31 lbs/hr	4	SWS Bottoms = 279,893 lbs/hr SWS Feed = 297,883 lbs/hr	293,888 lbs/hr 312,777 lbs/hr	119,572 lbs/hr 1,191,532 lbs/hr	1,175,552 lbs/hr 1,251,108 lbs/hr	

PLANT BASED ON B&W GASIFIERS
SUMMARY OF CAPACITY OF THE PLANT SECTIONS

2.3

11-28-54099

SECTION	SECTION DESCRIPTION	NO. OF PLANTS	CAPACITY 1 MODULE		CAPACITY 4 MODULES		INSTALLED COST MMS
			NORMAL	DESIGN	NORMAL	DESIGN	
800	ASH/SLAG HANDLING DEWATERING	4	Feed=413,810 lbs/hr Incl. 360,000 H ₂ O	517,263 lbs/hr Incl. 450,000 H ₂ O	1,655,240 lbs/hr	2,069,052 lbs/hr	
	HANDLING						
1200	UTILITY AREA RAW WATER STORE TRT POTABLE WATER TRT BFW TRT CONDENSATE TRT (1-TURN) STEAM GENERATION 8 Boilers - H.P.STM	1 1 4 4 4	100 GPM 1,900 GPM 56,300 lbs/hr	115 GPM 2,185 GPM 143,000 lbs/hr x2	4,000 GPM 25 GPM 4x100 GPM 4x1,900 GPM 4x56,300 lbs/hr	4,600 GPM 29 GPM 4x115 GPM 4x2,185 GPM 8x143,000 lbs/hr	
	@ 150°F From Puly. Coal Baghouse STACK GAS CL. PLT/INTR AIR-IG N ₂		908,074 lbs/hr MW=28.367 FROM SECTION 200 - AIR SEP. PLANT	1,044,285 lbs/hr x2	4x908,074 lbs/hr	8x1,044,285 lbs/hr	
1300	COOLING WATER SYS COOLING TWR SYS	4	103,800 GPM Circ., Δt=15°F 550 GPM Blowdown	124,560 GPM 660 GPM	415,200 GPM 2,200 GPM	498,240 GPM 2,640 GPM	
1400	FLARE AND INCIN.	4					
1500	SERVICE WATER+C.P. RUNOFF+ STR SOUR WATER- WASTE WATER TRT	4	954 GPM	1,002 GPM	3,816 GPM	4,008 GPM	
2000	GFNL FACILITIES L.T.SOLID WASTE STORAGE BYPROD & CHEM STOR SULFUR 198 T/D Produced Per Plant		6,000 TONS	6,000 TONS	24,000 TONS	24,000 TONS	

PLANT BASED ON B&W GASIFIERS
 SUMMARY OF CAPACITY OF THE PLANT SECTIONS

2.3

11-28-54099

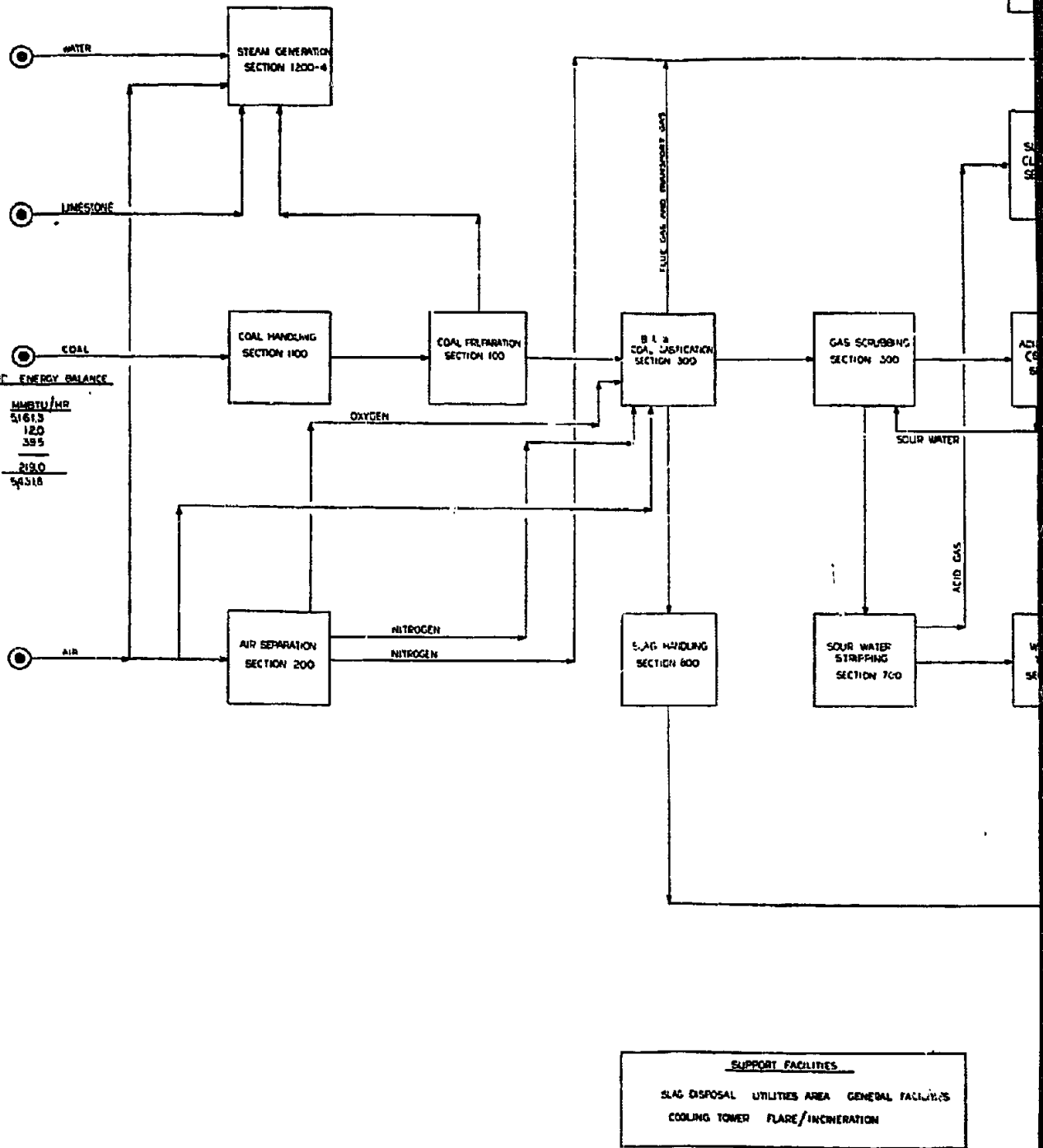
SECTION	SECTION DESCRIPTION	NO. OF PLANTS	CAPACITY 1 MODULE		CAPACITY 4 MODULES		INSTALLED COST MM\$
			NORMAL	DESIGN	NORMAL	DESIGN	
2000	GENL FACILITIES (cont'd) LIMESTONE 4,000 lbs/hr Usage per plant WATER CHEMICALS ELECT PWR DIST SPARE PARTS LIGHT & COMM ROADS AND FENCES FIREWATER SYSTEM SEWAGE PLANT INTERCONN PIPING		56,000 TONS	56,000 TONS	224,000 TONS	224,000 TONS	
2100	BUILDINGS						
2200	DOCK FACILITIES						
	100-1000 SUB TOTAL						
	1100-2200 SUB TOTAL						
	TOTAL						

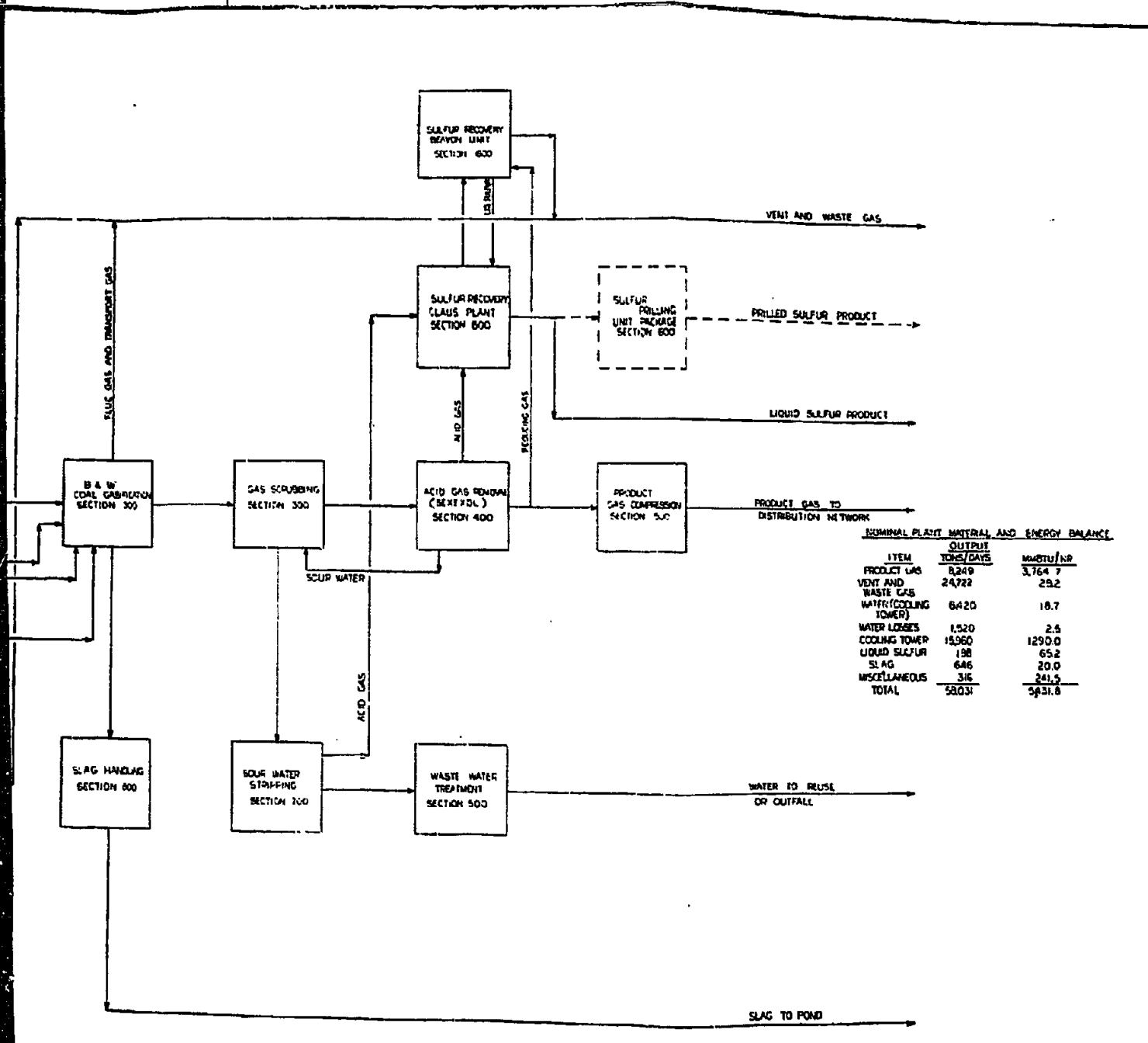


2.4 BLOCK FLOW DIAGRAM

NOMINAL PLANT MATERIAL AND ENERGY BALANCE

ITEM	INPUT TONS/DAYS	MMBTU/HR
COAL	5840	51613
AIR	28818	120
WATER	23,696	385
LIMESTONE	77	
POWER		2190
TOTAL	58,031	54518






NOMINAL PLANT MATERIAL AND ENERGY BALANCE

ITEM	OUTPUT TONS/DAYS	MMBTU/HR
PRODUCT GAS	8,249	3,764.7
VENT AND WASTE GAS	24,722	29.2
WATER (COOLING TOWER)	6,420	18.7
WATER LOSSES	1,520	2.5
COOLING TOWER	15,960	1290.0
LIQUID SULFUR	198	65.2
SLAG	646	20.0
MISCELLANEOUS	316	241.5
TOTAL	58,031	5,831.8

SUPPORT FACILITIES
 SLAG DISPOSAL UTILITIES AREA GENERAL FACILITIES
 COOLING TOWER FLARE/INCINERATION


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BLOCK FLOW DIAGRAM
TVA COAL GASIFICATION STUDY
B & W GASIFIERS-ONE MODULE

DRAWN BY: [] CHECKED BY: [] DATE: []
 PROJECT NO. 11-27-54099 DRAWING NO. DWG-54099-27-150-200



TVA Coal Gasification Study
B&W Gasifier

SECTION DESCRIPTION

3.1

SECTION 100 COAL PREPARATION

A. Reference Material:

- Process Flowsheet FWEC Dwg. No. 54099-27-1-50-1
- Elevation Drawing FWEC Dwg. No. 54099-27-1-01-1
- Equipment List

B. Description of Flow

The unit is designed to receive, store, prepare and transport coal/limestone to the coal gasification units.

Sized coal 3" x 0" (8" maximum) will be delivered to the site via 1500 ton barges. Each barge will be unloaded using a 5600 TPH* free digging barge unloader. The barge unloader (27-UD101) will feed belt conveyor 27-CR102 which will convey the coal to a 600 ton surge bin (27-TK101). Prior to entering the surge bin, tramp iron will be removed by magnetic separator 27-S101. Vibrating feeders 27-FD101 and 27-FD102 located under the surge bin will feed belt conveyors 27-CR103 and 27-CR104 conveying the material to sampling stations 27-SS101 and 27-SS102. Prior to entering the sampling stations an inventory of the material will be made by belt weigh scales 27-WS101 and 27-WS102.

An alternate feed arrangement will be provided using dump trucks. Trucks delivering coal to the site will be weighed, for inventory, using truck scale 27-WS103 located at the unloading site. The trucks will dump the material into a 25 ton receiving hopper 27-TK102. The material will then be removed from the hopper using vibrating feeder 27-FD103 and will be conveyed to the sampling tower. Prior to sampling, tramp iron will be removed using magnetic separator 27-S102.

After sampling the material will be fed to 4 coal breakers (27-SR101 thru 27-SR104) where the coal will be reduced to 1-1/4" x 0" lumps and then fed to 2 collecting conveyors (27-CR108 and 27-CR109) transporting the coal to a transfer tower. Refuse material discharged by the coal breakers will be collected by refuse conveyors 27-CR106 and 27-CR107 which will convey the refuse out of the breaker tower and discharge to grade.

- * Barge unloading at 6 times average coal usage to allow for daylight unloading, five days per week, minor repairs & for pulling the barges into position.



TVA Coal Gasification Study
B&W Gasifier

At the transfer tower the material will either be directed to four 14,500 ton coal storage silos (27-TK103 thru 27-TK106) or to the load out area. Coal discharged to the silos will be weighed for silo inventory by belt scale 27-WS105 and then conveyed by belt conveyor 27-CR114 to a cascaded conveyor system (27-CR111, 27-CR112 and 27-CR113) on top of the silos.

Coal will then be removed from the silos using either 3 to 4 belt feeders per silo (27-FD104A-G thru 27-FD107A-G). They will be feeding belt conveyor 27-CR115 discharging the material to the gasifier and steam generator feed conveyors 27-CR117A/B. Prior to this the material will be weighed on belt scale 27-WS106 and tramp iron will be removed by magnetic separator 27-S104.

Coal directed to the load out area will be weighed for dead storage inventory on belt scale 27-WS104 and then be conveyed on belt conveyor 27-CR110 to a load out dump where scrapers will build the 90 day dead storage pile.

In the event that coal from dead storage is to be used it will be drawn from 2 reclaim hoppers (27-TK107 and 27-TK108) located at the dead storage site. Vibrating pan feeders 27-FD108 and 27-FD109 located under the hoppers will each feed reclaim collecting conveyor 27-CR116 which conveys the material to the gasifier and steam generator feed conveyors 27-CR117A/B.

The gasifier and steam generator feed conveyors will direct the material to either the pulverizer bunker fill conveyors 27-CR118A/B which will fill four 1430 tons storage bunkers (27-TK109 thru 27-TK112 each having a 4 hour storage capacity) or to the steam generator transfer conveyors 27-CR119A/B which convey the material onto the steam generator bunker fill conveyors 27-CR120A/B.

All equipment from the gasifier and steam generator feed conveyors to the storage bunkers are provided with one operating and one spare train.

Limestone Storage

Limestone will be delivered to the plant site by barge, then loaded into trucks. The trucks will be equipped with pneumatic unloaders for unloading into the 980 ton limestone storage silo. Limestone will be removed from the silo using vibrating bin bottom 27-BV101 and will be fed into a pneumatic transport line by 2 rotary feeders 27-FD110A/B, leading the material to the steam generator limestone storage bunkers. The pneumatic transport line will be equipped with silencers before and after pneumatic transport blowers 27-B101A/B for noise suppression.



TVA Coal Gasification Study
B&W Gasifier

Barge Unloading System

A power winch system for barge pulling has been contemplated and included in Item UD-101, of the equipment list for Section 100, Coal Preparation. The barge puller is designed to move a line of coal laden barges, already moved, and eventually, a single barge only during the actual coal unloading operation of that barge.

Considering the scale of the Key Plot Plan, 1 in. = 400 ft., the barge puller is not shown. It does not appear on the Process Flow Diagrams of Section 100, either, as it is an ancillary device which does not serve to clarify the movement and treatment of the product, coal, the principal purpose of the Process Flow Diagrams.

The cost of the barge puller is included as part of the hardware costs of equipment Item UD-101, for each of the coal gasification plants.

The foregoing comments apply as well to the barge cleanout system which consists of a small front end loader and a single bucket crane which loads the residual coal into a barge dedicated to the plant site for cleanout service. When it becomes full, the dedicated barge is moved into the unloading line and is then replaced by another of the empty barges.

Movement of single barges, other than those operated by the power winch, is effected by means of a 750 hp switch boat for which pricing provisions have been made in our estimate of plant costs.



FOSTER WHEELER ENERGY CORPORATION
 CUSTOMER: TVA
 LOCATION: Murbby Hill, Alabama

SECTION NAME: B/W COAL PREPARATION
 REF. DWG.: 54099-27-1-50-1
 CONTRACT NO. 11-27-5-099 REV.: 0

SECTION NO.: 100
 PAGE NO.: 1 of 4
 DATE: 6/30/80

EQUIPMENT SUMMARY

ITEM	DESCRIPTION	DEFINITION	DESIGN * TEMP. (°F)	DESIGN * PRESS. (PSIG)	CONSTRUCTION MATERIAL *
27-B101A/B	Pneumatic Transport Supply Blrs.				
27-BV101	Vibrating Discharger	25 TPH			
27-CR101	Unloader Transfer Conveyor	84" Belt	5,600 TPH		
27-CR102	Surge Bin Feed Conveyor	84" Belt	5,600 TPH		
27-CR103	Sampling Station Feed Conveyor	48" Belt	1,700 TPH		
27-CR104	Sampling Station Feed Conveyor	48" Belt	1,700 TPH		
27-CR105	Truck Receiving Transfer Conveyor	30" Belt	125 TPH		
27-CR106	Breaker Refuse Conveyor	24" Belt			
27-CR107	Breaker Refuse Conveyor	24" Belt			
27-CR108	Breaker Collecting Conveyor	48" Belt	1,762 TPH		
27-CR109	Breaker Collecting Conveyor	48" Belt	1,762 TPH		
27-CR110	Dead Storage Load Out Conveyor	66" Belt	3,525 TPH		
27-CR111	Silo Fill Conveyor	66" Belt	3,525 TPH		
27-CR112	Silo Fill Conveyor	66" Belt	3,525 TPH		
27-CR113	Silo Fill Conveyor	66" Belt	3,525 TPH		
27-CR114	Silo Feed Conveyor	66" Belt	3,525 TPH		
27-CR115	Silo Discharge Collecting Conveyor	48" Belt	1,300 TPH		
27-CR116	Reclaim Collecting Conveyor	48" Belt	1,300 TPH		
27-CR117A/B	Gasifier & Stm. Gen. Feed Conveyor	48" Belt	1,300 TPH		
27-CR118A/B	Pulverizer Bunker Fill Conveyor	48" Belt	1,300 TPH		
27-CR119A/B	Steam Gen. Transfer Conveyor	48" Belt	1,300 TPH		
27-CR120A/B	Steam Gen. Fill Conveyors	48" Belt	1,300 TPH		
27-DC101	Dust Collection System	Includes F-101 thru F-109			
27-DP101	Dust Suppression System				

* SHELL/TUBE WHERE APPLICABLE



FOSTER WHEELER ENERGY CORPORATION
 CUSTOMER: TVA
 LOCATION: Murphy Hill, Alabama

SECTION NAME: B/W COAL PREPARATION
 REF. DWG.: 54099-27-1-50-1
 CONTRACT NO.: 11-27-54099 REV.: 0

SECTION NO.: 100
 PAGE NO.: 2 OF 4
 DATE: 6/30/80

EQUIPMENT SUMMARY

ITEM	DESCRIPTION	DEFINITION	DESIGN * TEMP. (°F)	DESIGN * PRESS. (PSIG)	CONSTRUCTION MATERIAL *
27-F101	Silo Bag House	Part of 27-DC101			
27-F102	Silo Bag House	Part of 27-DC101			
27-F103	Silo Bag House	Part of 27-DC101			
27-F104	Silo Bag House	Part of 27-DC101			
27-F105	Pulverizer Storage Bunker Filter	Part of 27-DC101			
27-F106	Pulverizer Storage Bunker Filter	Part of 27-DC101			
27-F107	Pulverizer Storage Bunker Filter	Part of 27-DC101			
27-F108	Pulverizer Storage Bunker Filter	Part of 27-DC101			
27-F109	Limestone Silo Filter - Separator	Part of 27-DC101			
27-FD101	Unloader Surge Bin Vib. Feeder	1,700 TPH			
27-FD102	Unloader Surge Bin Vib. Feeder	1,700 TPH			
27-FD103	Truck Receiving Vib. Feeder	125 TPH			
27-FD104A-G	Silo Discharge Feeder	4 @ 325 & 3 @ 433 TPH			
27-FD105A-G	Silo Discharge Feeder	4 @ 325 & 3 @ 433 TPH			
27-FD106A-G	Silo Discharge Feeder	4 @ 325 & 3 @ 433 TPH			
27-FD107A-G	Silo Discharge Feeder	4 @ 325 & 3 @ 433 TPH			
27-FD108	Reclaim Hopper Discharge Feeder	650 TPH			
27-FD109	Reclaim Hopper Discharge Feeder	650 TPH			
27-FD110A/B	Rotary Feeders	25 TPH			
27-SL101	Silencer				
27-SL102	Silencer				
27-S101	Unloader Mag. Separator	84" (Suspended Elec. Mag.)			
27-S102	Truck Receiving Mag. Separator	30" (Suspended Elec. Mag.)			
27-S103	Dead Storage Reclaim Mag. Sep.	48" (Suspended Elec. Mag.)			
27-S104	Silo Discharge Mag. Separator	48" (Suspended Elec. Mag.)			

* SHELL/TUBE WHERE APPLICABLE



FOSTER WHEELER ENERGY CORPORATION
 CUSTOMER: TVA
 LOCATION: Murphy Hill, Alabama

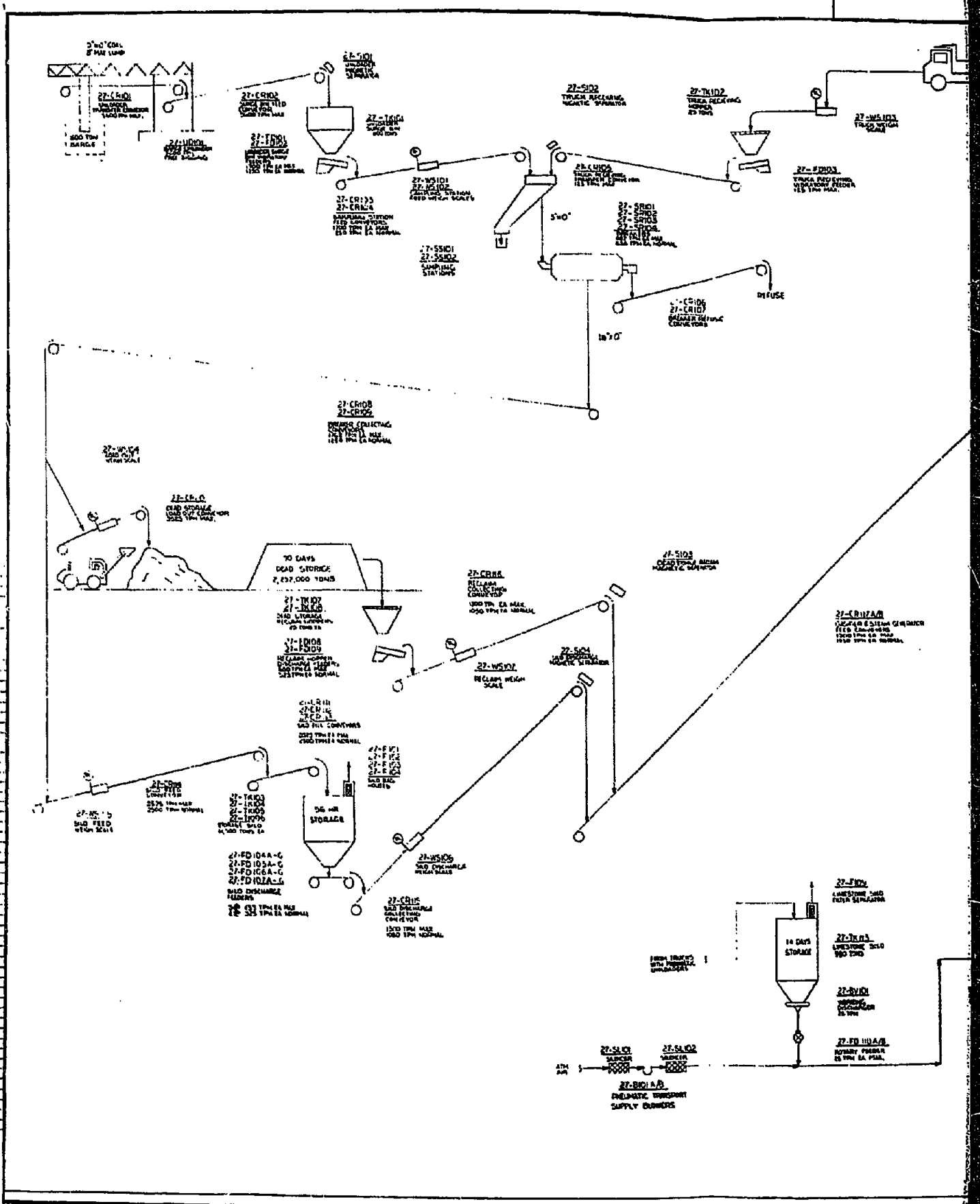
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 REF. DWG.: 54099-27-1-50-1
 CONTRACT NO. 11-27-54099 REV.: 0

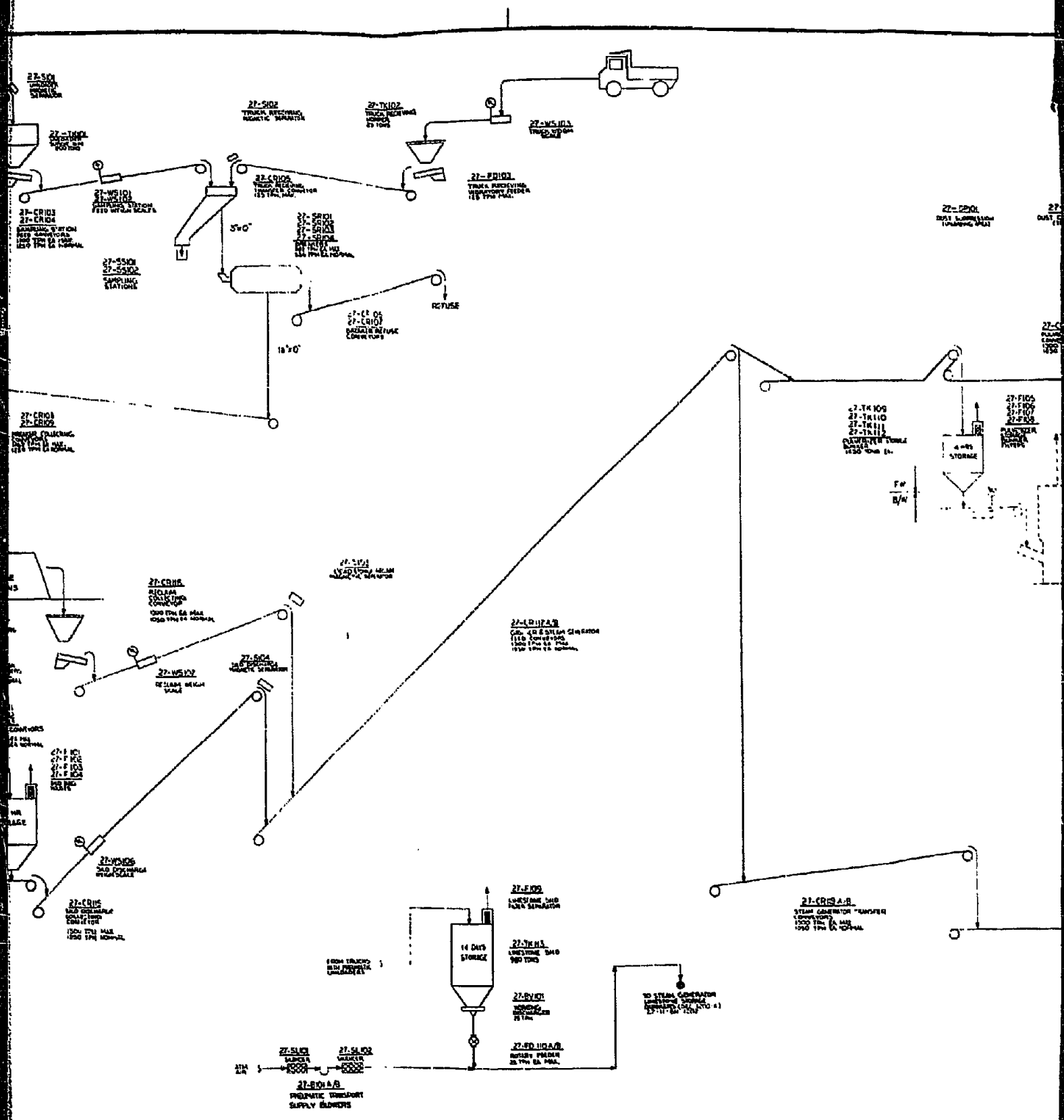
SECTION NO.: 100
 PAGE NO.: 3 of 4
 DATE: 6/30/80

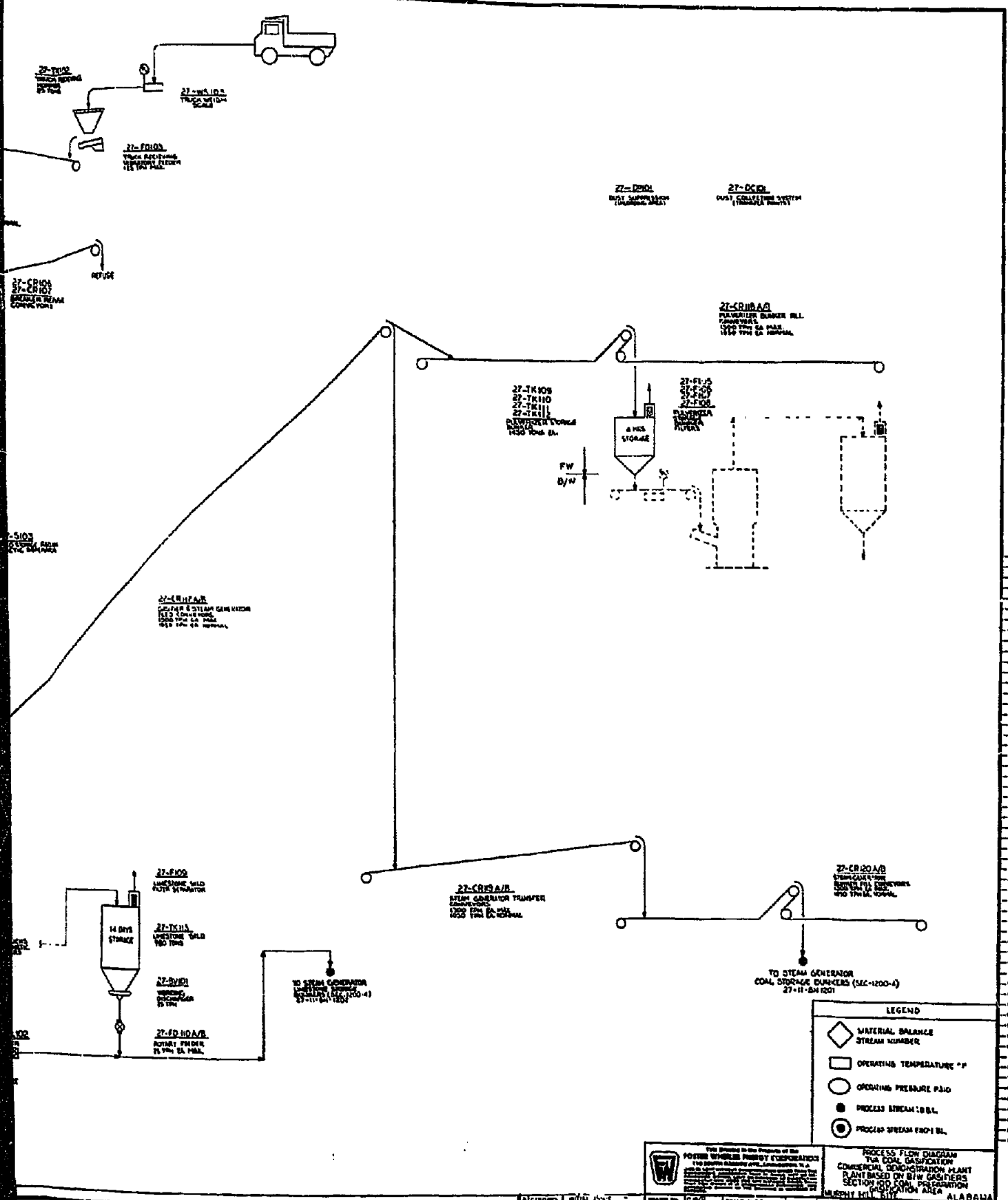
EQUIPMENT SUMMARY

ITEM	DESCRIPTION	DEFINITION	DESIGN * TEMP. (°F)	DESIGN * PRESS. (PSIG)	CONSTRUCTION MATERIAL *
27-SR101	Breaker	882 TPH			
27-SR102	Breaker	882 TPH			
27-SR103	Breaker	882 TPH			
27-SR104	Breaker	882 TPH			
27-SS101	Sampling Station	Two Stage			
27-SS102	Sampling Station	Two Stage			
27-TK101	Unloader Surge Bin	600 Tons			
27-TK102	Truck Receiving Hopper	25 Tons			
27-TK103	Storage Silo	14,500 Tons			
27-TK104	Storage Silo	14,500 Tons			
27-TK105	Storage Silo	14,500 Tons			
27-TK106	Storage Silo	14,500 Tons			
27-TK107	Dead Storage Reclaim Hopper	25 Tons			
27-TK108	Dead Storage Reclaim Hopper	25 Tons			
27-TK109	Pulverizer Storage Bunker	1,430 Tons			
27-TK110	Pulverizer Storage Bunker	1,430 Tons			
27-TK111	Pulverizer Storage Bunker	1,430 Tons			
27-TK112	Pulverizer Storage Bunker	1,430 Tons			
27-TK113	Limestone Silo	980 Tons			
27-UD101	Barge Unloader	5,600 TPH			
27-WS101	Sampling Sta. Feed Weigh Scale	1,700 TPH			
27-WS102	Sampling Sta. Feed Weigh Scale	1,700 TPH			
27-WS103	Truck Weigh Scale	10' x 60'			
27-WS104	Load Out Weigh Scale	3,525 TPH			
27-WS105	Silo Feed Weigh Scale	3,525 TPH			

* SHELL/TUBE WHERE APPLICABLE







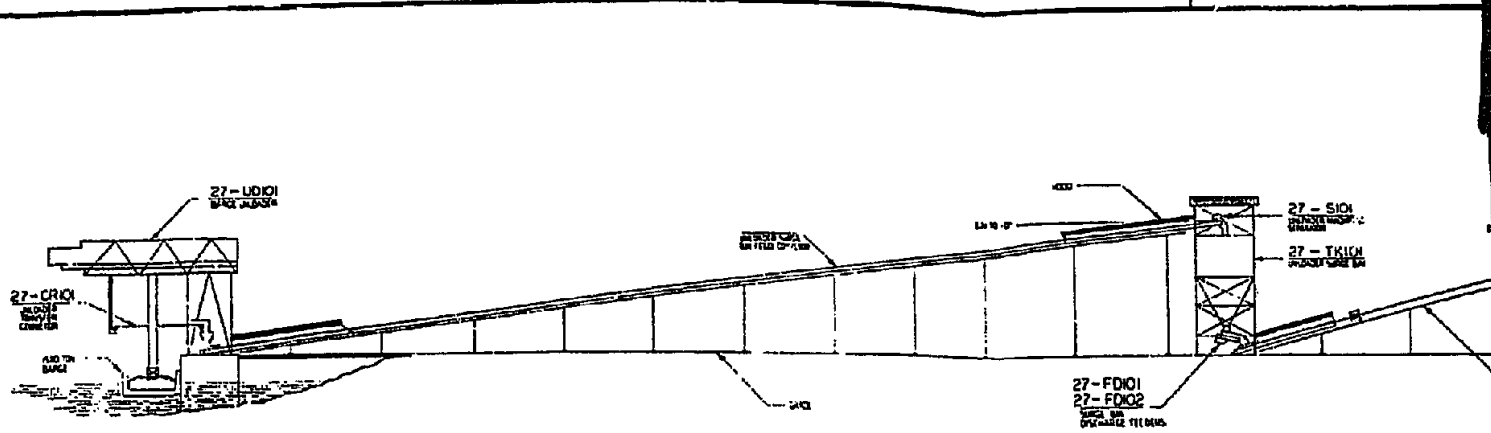
LEGEND

- ◇ MATERIAL BALANCE
- ◇ STREAM NUMBER
- OPERATING TEMPERATURE °F
- OPERATING PRESSURE PSIG
- PROCESS STREAM NO. 1 BL.
- ⊙ PROCESS STREAM NO. 2 BL.

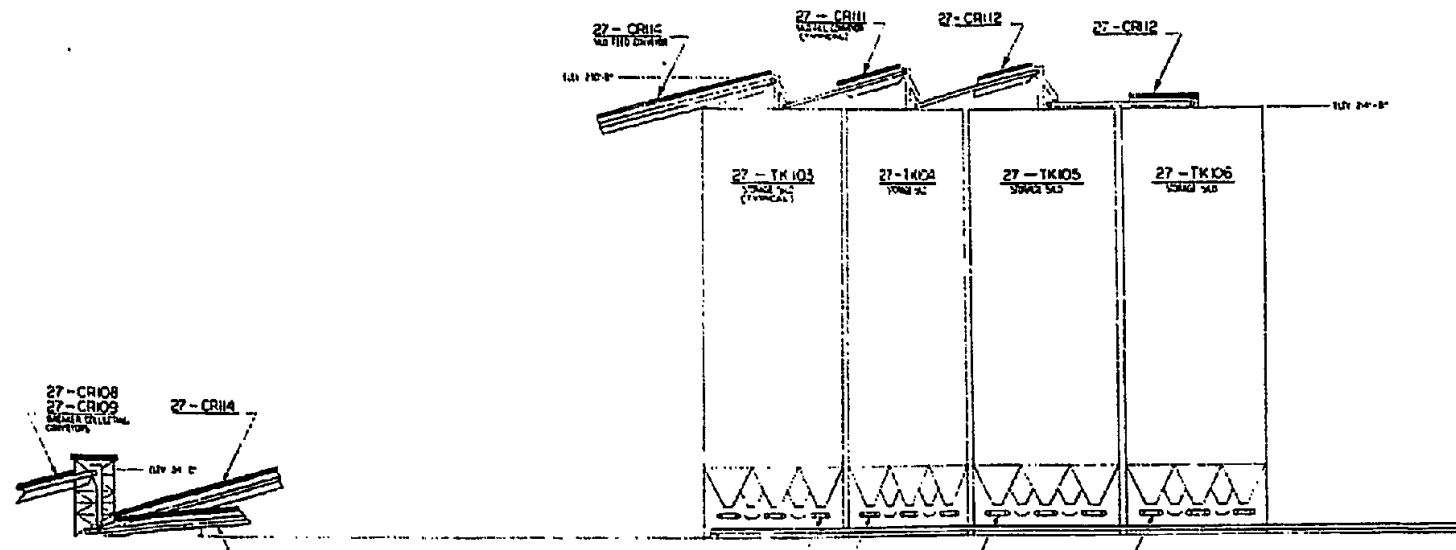
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PROCESS FLOW DIAGRAM
 FOR COAL GASIFICATION
 PLANT BASED ON B/W GASIFIERS
 SECTION FOR COAL PREPARATION
 MURPHY HILL, ALA.

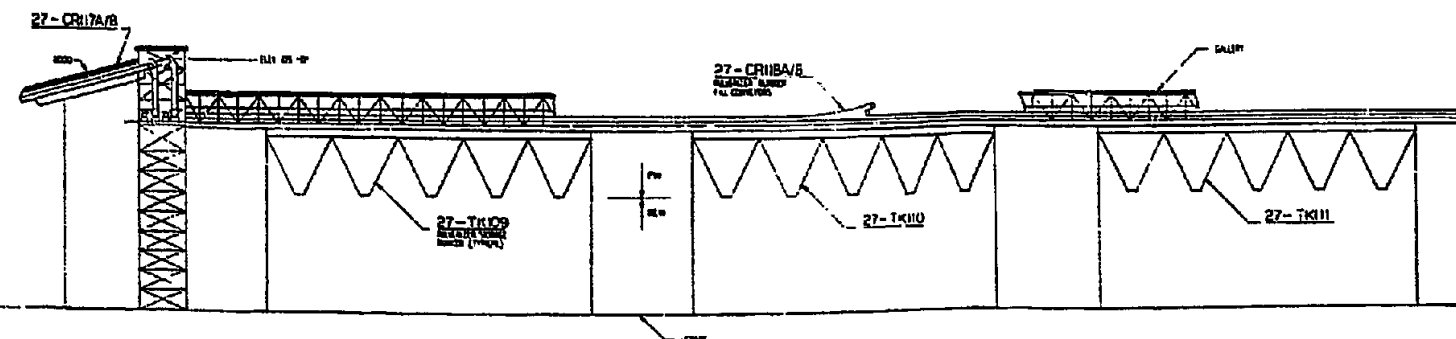
11-27-54039 DWG. NO 54039-27-1-50



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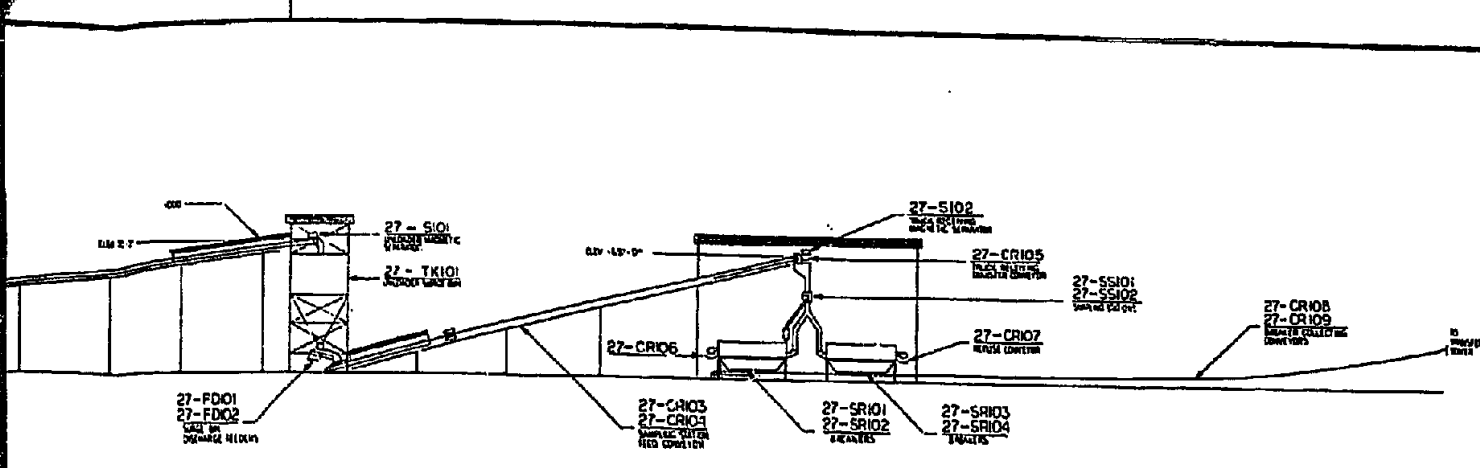


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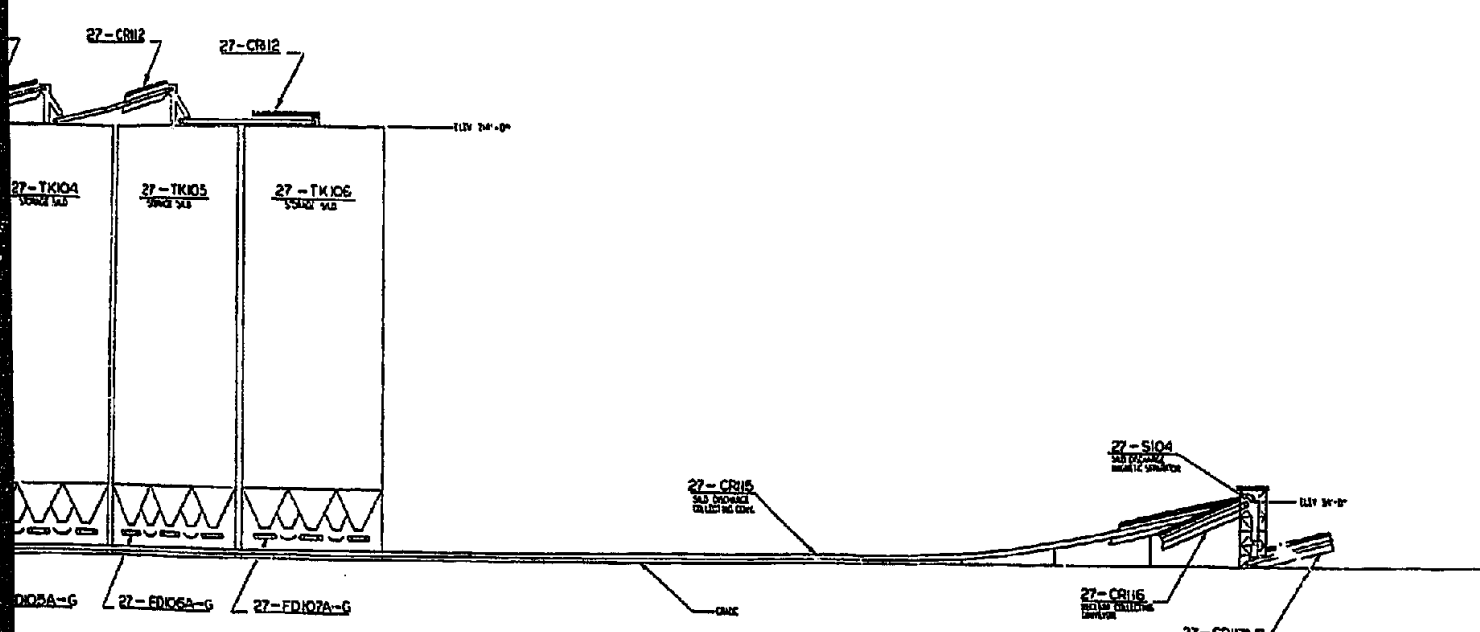


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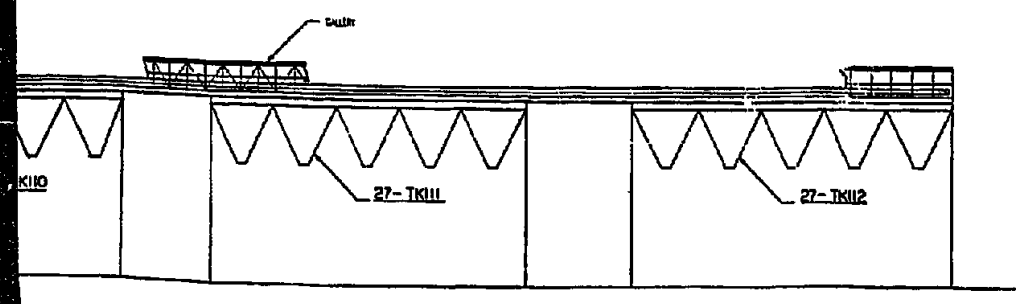




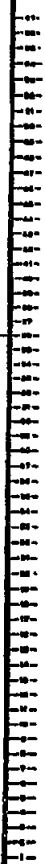
SCALE: 1" = 32'



SCALE: 1" = 32'



SCALE: 1" = 32'



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	DRAWN BY: [blank] CHECKED BY: [blank] DATE: 11-27-94 DESIGNED BY: [blank] DATE: 11-27-94 PROJECT: [blank]	DRAWING NO. 54099-27-1-CR-1 SHEET NO. 11 OF 11

11/27/94 SERIAL ISSUE



TVA Coal Gasification Study
B&W Gasifier

SECTION DESCRIPTION

3.2 SECTION 200 - AIR SEPARATION PLANT

A. Reference Material:

- . Process Flowsheet FWEC Dwg. No. 54099-27-1-50-2
- . Equipment List
- . Material Balance

B. Description of Flow

Filtered air is compressed to approximately 90 PSIG in three stage Air Compressors (27-12-C-201A/B), half turbine/half motor driven. Intercoolers, an aftercooler, and K.O. Drums are provided. Condensate leaving the K.O. Drums flows to the cooling tower.

Some compressed air is fed to the gasifier during startup. Normally compressed air is fed only to the Cold Box Package (27-12-PG-201).

The Cold Box Package produces nitrogen containing about 10 ppmv O₂ and oxygen of about 98 vol % O₂ purity. Waste nitrogen is vented through the Waste Nitrogen Silencer (27-12-SL-201) to atmosphere. Oxygen gas leaving the cold box package is compressed in three stage machines (half turbine driven) to a pressure of about 275 PSIG by the Oxygen Compressor (27-12-C-202). Intercoolers and K.O. drums will be provided by the compressor manufacturer. A portion of the compressed oxygen is recirculated through the Oxygen Comp. Recirc. Cooler (27-12-E-207), to the suction side of the Oxygen Compressor for controllability. A fraction of the compressed oxygen is sent to the Gasifier (27-14-R-301) in Section 300. A smaller fraction is boosted to about 3,000 PSIG by the O₂ Storage Feed Compressor and flows to the Gaseous Oxygen Storage Tanks (27-12-TK-202A/B/C/D). Stored oxygen is required for the Gasifiers in Section 300, approximately ten minutes every two hours, due to a reversal in Cold Box Package operation.

The liquid oxygen product leaving the Cold Box Package (27-12-PG-201) enters the Liquid Oxygen Storage Tank (27-12-TK-201). When required, liquid oxygen is vaporized in the Liquid Oxygen Vaporation Package (27-12-PG-205), then combined with oxygen from the O₂ Storage Feed Compressors in both air plants (two air plants per module). The combined gaseous oxygen stream enters the Gaseous Oxygen Storage Tanks.



Liquid nitrogen leaves the Cold Box Package and enters the Liquid Nitrogen Storage Tank (27-12-TK-003). When required, liquid nitrogen is vaporized in the Nitrogen Vaporization Packages (27-12-PG-204A/B). Vaporized nitrogen from Nitrogen Package PG-204A is sent to the Gasifier in Section 300, while vaporized nitrogen from Nitrogen Vaporization Package PG-204B is used for Plant Instruments.


Gaseous nitrogen from the Cold Box Package, PG-201, enters the Plant Nitrogen Compressor (27-12-C-203A/B), motor driven, with intercoolers, an aftercooler and knockout drums. Compressed nitrogen leaving the Knockout Drum at a pressure of about 585 PSIG is distributed to process users. A fraction of the compressed nitrogen is utilized by plant instruments, the remainder used for purging, blanketing, coal system shutdown, coal treatment and the coal feed system.

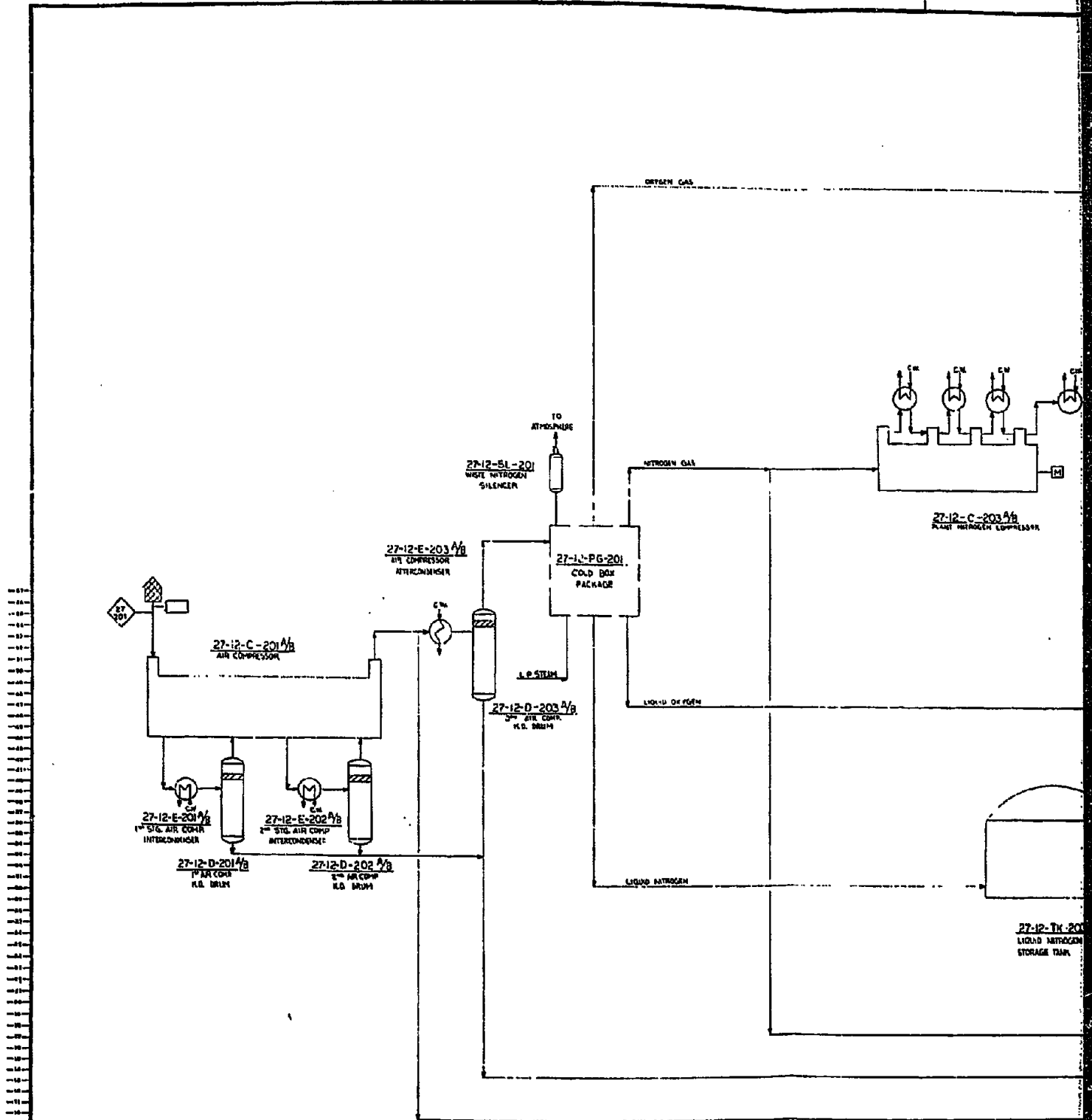
TWO 50% AIR PLANTS (BOTH OPERATING) PER MODULE. FOUR MODULES TOTAL. B & W GASIFIERS
 FORM NO 135-904

FOSTER WHEELER ENERGY CORP. PROCESS PLANTS DIVISION		CONTRACT 11-27-54099		EQUIPMENT LIST				
CLIENT: TVA (COAL GASIFICATION STUDY)		SECTION: 200		AIR SEPARATION PLANT				
LOCATION: ALABAMA				NAME OF UNIT				
CLASS	ITEM NO.	DESCRIPTION	REVISION DATE	1	2	3	4	PAGE OF
COMPRESSORS	Per Plant		No./Module					1 2
27-12-	C-201A/B	AIR COMPRESSOR	4-25%					
-	C-202	OXYGEN COMPRESSOR	2-50%					
-	C-203A/B	PLANT NITROGEN COMPRESSOR	4-25%					
-	C-204	O ₂ STORAGE FEED COMPRESSOR	2-50%					
27-12-	D-201A/B	1st AIR COMPRESSOR K.O. DRUM	4-25%					
-	D-202A/B	2nd AIR COMPRESSOR K.O. DRUM	4-25%					
-	D-203A/B	3rd AIR COMPRESSOR K.O. DRUM (AIR COMPRESSOR AFTER DRUM)	4-25%					
EXCHANGERS								
27-12-	E-201A/B	1st STG AIR COMP. INTERCONDENSER	4-25%					
-	E-202A/B	2nd STG AIR COMP. INTERCONDENSER	4-25%					
-	E-203A/B	AIR COMPRESSOR AFTERCONDENSER	4-25%					
-	E-204	O ₂ COMP 1st STG INTERCOOLER	2-50%					
-	E-205	O ₂ TEMP. 2nd STG INTERCOOLER	2-50%					
-	E-207	OXYGEN COMP. RECIRC COOLER	2-50%					

TWO 50% AIR PLANTS (BOTH OPERATING) PER MODULE. FOUR MODULES TOTAL B & W GASIFIERS

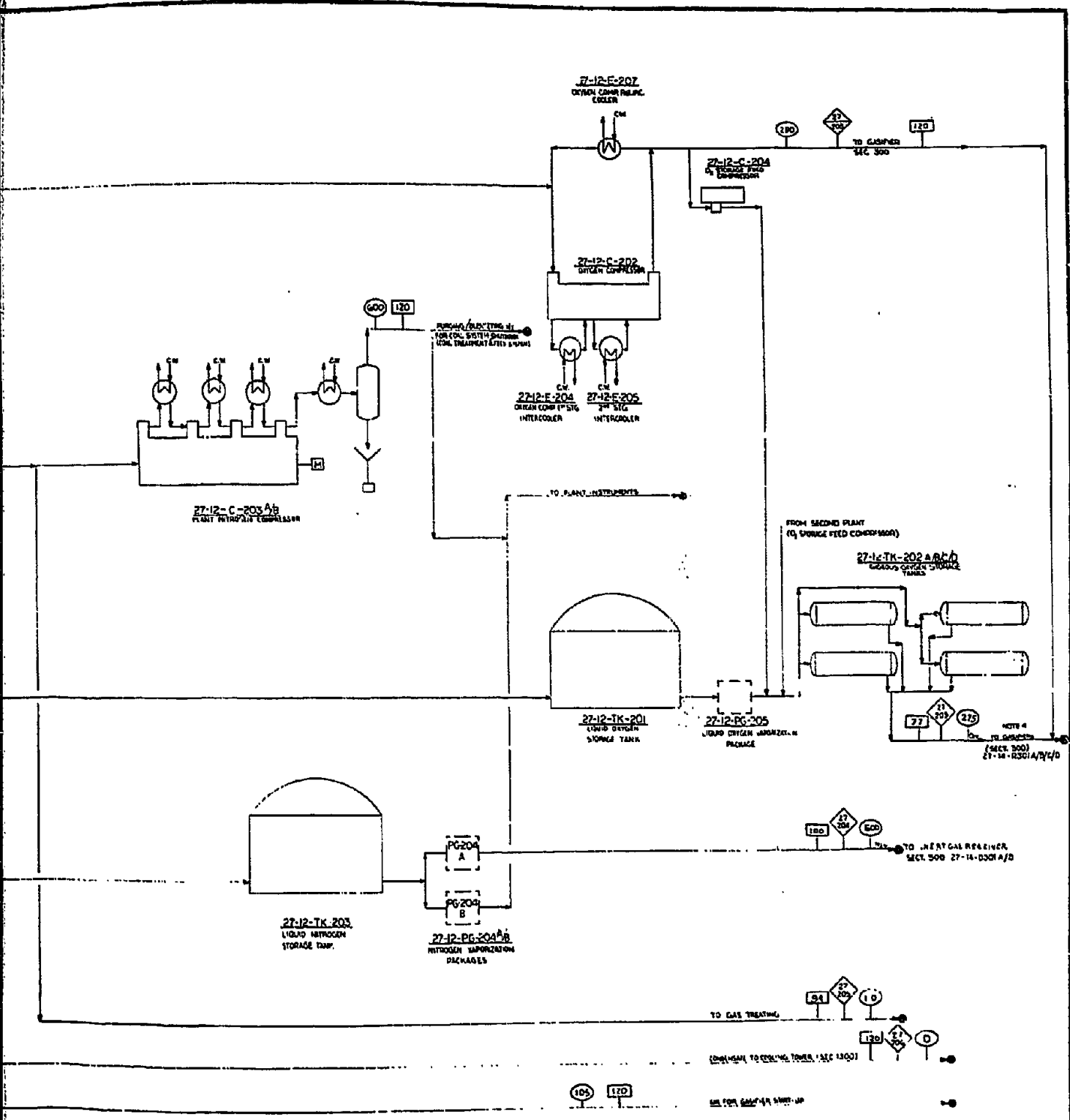
FORM NO. 135-904

 FOSTER WHEELER ENERGY CORP. PROCESS PLANTS DIVISION		CONTRACT 11-27-54099 SECTION: 200		EQUIPMENT LIST					NAME OF UNIT AIR SEPARATION PLANT		PAGE	OF
CLIENT: TVA (COAL GASIFICATION STUDY)	LOCATION: ALABAMA	DESCRIPTION	EFD	REVISION DATE	ORIGINAL	1	2	3	4	2	2	
CLASS	ITEM NO.	DESCRIPTION	EFD	NO./Module							REV.	
PACKAGE ITEMS	Per Plant											
27-12-	PG-201	COLD BOX PACKAGE		2-50%								
-	PG-204A/B	NITROGEN VAPORIZATION PKGS		2-100 Tons/Day Each								
-	PG-205	LIQUID OXYGEN VAPORIZATION PKG.		1-185 Tons/Hr								
TANKS												
27-12-	TK-201	LIQUID OXYGEN STORAGE TANK		1-4,500 Tons								
-	TK-202A/B	GASEOUS OXYGEN STORAGE TANKS		4-50%								
-	TK-203	LIQUID NITROGEN STORAGE TANK		1-250 Tons								
SILENCER												
27-12-	SL-201	WASTE NITROGEN SILENCER		2-50%								



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- NOTE:
1. TWO AIR PLANTS PER MODULE. SHOW AIR PLANTS TOTAL. ONE PLANT EXCEPT FOR O₂ STORAGE WHICH IS ONE.
 2. ONE AIR COMPRESSOR IS MOTOR DRIVEN PER AIR PLANT (A TWO MOTOR SYSTEM IS SHOWN PER MODULE).
 3. ONE OXYGEN COMPRESSOR IS MOTOR DRIVEN PER MODULE.
 4. DEVICES REQUIRED FROM STORAGE TO TRANSMIT EVERY TWO HOURS.
 5. PPA LEGEND SEE Dwg. NO. 84000-



- NOTE:
1. TWO AIR PLANTS PER MODULE. SEVEN AIR PLANTS TOTAL. ONE PLANT SHOWN ABOVE EXCEPT FOR O₂ STORAGE WHICH IS SHOWN FOR ONE MODULE.
 2. ONE AIR COMPRESSOR IS MOTOR DRIVEN AND ONE TURBINE DRIVEN PER AIR PLANT. TWO MOTOR DRIVEN AND TWO TURBINE DRIVEN PER MODULE.
 3. ONE OXYGEN COMPRESSOR IS MOTOR DRIVEN AND ONE TURBINE DRIVEN PER MODULE.
 4. OXYGEN IS QUINNED FROM STORAGE APPROXIMATELY TEN MINUTES EVERY TWO HOURS.
 5. FOR LEGEND SEE D. NO. 34099-27-1-30-1

	THIS DRAWING IS THE PROPERTY OF THE FOSTER WHEELER ENERGY CORPORATION AND IS NOT TO BE REPRODUCED OR TRANSMITTED IN ANY FORM OR BY ANY MEANS, ELECTRONIC OR MECHANICAL, INCLUDING PHOTOCOPYING, RECORDING, OR BY ANY INFORMATION STORAGE AND RETRIEVAL SYSTEM, WITHOUT THE WRITTEN PERMISSION OF FOSTER WHEELER ENERGY CORPORATION.		PHASES FLOW DIAGRAM TVA COAL GASIFICATION STUDY SECT. 200 AIR SEPARATION PLANT B & N GASIFIERS
	DRAWN BY: [Signature] CHECKED BY: [Signature]	SCALE: [Blank] SHEET NO. FW 11-27-54099	



TVA Coal Gasification Study
B&W Gasifier

SECTION DESCRIPTION

3.3 SECTION 300A- B&W GASIFICATION SYSTEM

A. Reference Material:

- . Process Flow Diagram FWEC Dwg. No. 54099-27-1-50-3
- . Equipment List
- . Material Balance

B. Description of Flow

Crushed coal from Coal Preparation (Section 100) is surged in the Crushed Coal Bunker (27-14-BN-301), then flows to the Raw Coal Feeder (27-14-FD-301 A thru J) which conveys the coal (dried basis) at an average rate of 5000 T/D per module into the Coal Pulverizers (27-14-GR-301 A thru J). Coal is pulverized so as to pass through 200 mesh and dried in the Pulverizers with flue gases from the Steam Generators (27-11-SG-1201 A/B). The pulverized coal and flue gas enter the Pulv. Coal Cyclone (27-14-S-301 A-H) where the two are separated, coal flowing through the Coal Cyclone Discharge Feeder (27-14-TK-301 A,B,C,D) to the Pulv. Coal Reservoir Tank (27-14-TK-301 A,B,C,D). The Pulv. Coal Cyclone is vented through the Primary Pulv. Coal Baghouses (27-14-FD-301 A thru H) which removes particulates to a low level before venting the gas to the atmosphere. Coal fines recovered are discharged through the Primary Baghouse Discharge Feeder, D-303 A,B,C,D to the Pulv. Coal Reservoir Tank.

Pulverized coal from the Pulv. Coal Reservoir Tank enters the Pulv. Coal Lock Hoppers (27-14-BN-302 A thru H) where it is pneumatically transported to the Pulv. Coal Feed Tank (27-14-TK-302 A,B,C,D). High pressure nitrogen from the Inert Gas Receiver is fed to the Lock Hoppers and the Feed Tank to pneumatically transport the pulverized coal to the Gasifiers (27-14-R-302 A,B,C,D). Vented gas from the Feed Tank and Lock Hoppers is sent through the Sec. Pulv. Coal Baghouse (27-14-F-302 A,B,C,D), then released to atmosphere. Coal particles are returned to the Pulv. Coal Reservoir Tank by the Sec. Baghouse Discharge Feeder (27-14-FD-304 A,B,C,D). The lock hopper/feed tank arrangement permits continuous feeding of the Gasifiers.

Gaseous oxygen from the Air Plant is injected directly into the gasification zone where it is mixed and combusted with the pulverized coal. The ash in the coal forms a molten slag which drops into the Slag Tank (27-14-TK-303 A,B,C,D) and quenched with sluice water. The slag is transported to the Slag Lock Hopper (27-14-BN-303 A,B,C,D) intermittently and conveyed by the Slag Eductor (27-14-J-301 A,B,C,D) to the slag disposal pond.



Hot gases leaving the gasification zone contain ungasified suspended char particles. Much of the char is removed in the Primary Char Cyclone (27-14-S-302 A,B,C,D) where it is cooled and discharged through the Prim. Char Cyclone Discharge Feeder (27-14-FD-305 A,B,C,D) and combined with char recovered from the Secondary Char Cyclone Discharge Feeder (27-14-FD-306 A,B,C,D). The combined stream is returned to the Gasifier by the Char Eductor (27-14-J-302 A,B,C,D).

Heat is recovered from raw gas indirectly in the upper portion of the Gasifier, producing H.P. Steam in the waterwall. The H.P. steam-condensate mixture flows to the H.P. Steam Drum (27-14-D-303 A,B,C,D). Separated steam flows to the Heat Recovery Boiler (27-14-E-301 A,B,C,D), is superheated, then flows to the H.P. steam header.

Heat is recovered from the hot raw gas leaving the Primary Char Cyclone in the Heat Recovery Boiler, E-301 A,B,C,D, thereby producing additional H.P. superheated steam. The cooled gases at about 450°F flow through the Secondary Char Cyclone to aqueous Gas Scrubbing also in Section 300.

Four gasifiers are provided in each module (sixteen gasifiers in the entire plant), two operating, two on standby, to gasify the normal throughput of 5,000 T/D of coal per module.



FOSTER WHEELER ENERGY CORPORATION
 SECTION NAME: B. & W. GASIFICATION
 SECTION NO.: 300
 CUSTOMER: TVA COAL GASIFICATION
 REF. DWG.: 54099-27-1-50-3
 PAGE NO.: 2
 LOCATION: ALABAMA
 CONTRACT NO.: 1-1-27-54099
 REV.:
 DATE:
 PLANT TYPE: B. & W. GASIFIERS

STREAM NUMBER	27	311	27	317	27	315	27	318	27	319
STREAM DESCRIPTION	Oxidant Into Gasifier	Sluice Water	Char Recycle	Slag To Ash Pond	Gas to Purification					
COMPONENTS (MW)	MOL/HR	MOL/HR	MOL/HR	MOL/HR	MOL/HR	MOL/HR	MOL/HR	MOL/HR	MOL/HR	MOL/HR
HYDROGEN	2.016									10.039
CARBON MONOXIDE	28.011									20.707
CARBON DIOXIDE	44.011									1.557
METHANE	15.043									900
NITROGEN	28.014	1								0
OXYGEN	32.000	10,663								489
HYDROGEN SULFIDE	34.080									33
CARBONYL SULFIDE	60.075									1
AMMONIA	17.031									
HYDROGEN CYANIDE	27.028									15
CHLORIDES	35.453									
SULFUR	32.066									
CARBON DISULFIDE	76.143									
SULFUR DIOXIDE	64.006									217
ARGON	39.944	217								TRACE
MERCAPTANS										
TOTAL DRY GAS		10,881								33,955
WATER	38.016									1,522
TOTAL WET GAS		10,881				1,966				35,480
		LBS/HR				LBS/HR				LBS/HR
TOTAL STREAM LBS/HR		349,905		360,000		35,417		413,810		767,131
SOLIDS LBS/HR										
COAL										
ASH								52,436		12,272
CARBON								1,374		5,599
TOTAL SOLIDS								53,810		17,871
WATER LIQUID				360,000				360,000		
TOTAL STREAM		77		77		100		90		150
TEMPERATURE, °F										

MMSCFD DRY GAS
 LBS/HR

FOUR GASIFIERS PER MODULE

FORM NO. 135-904



FOSTER WHEELER ENERGY CORP.
PROCESS PLANTS DIVISION

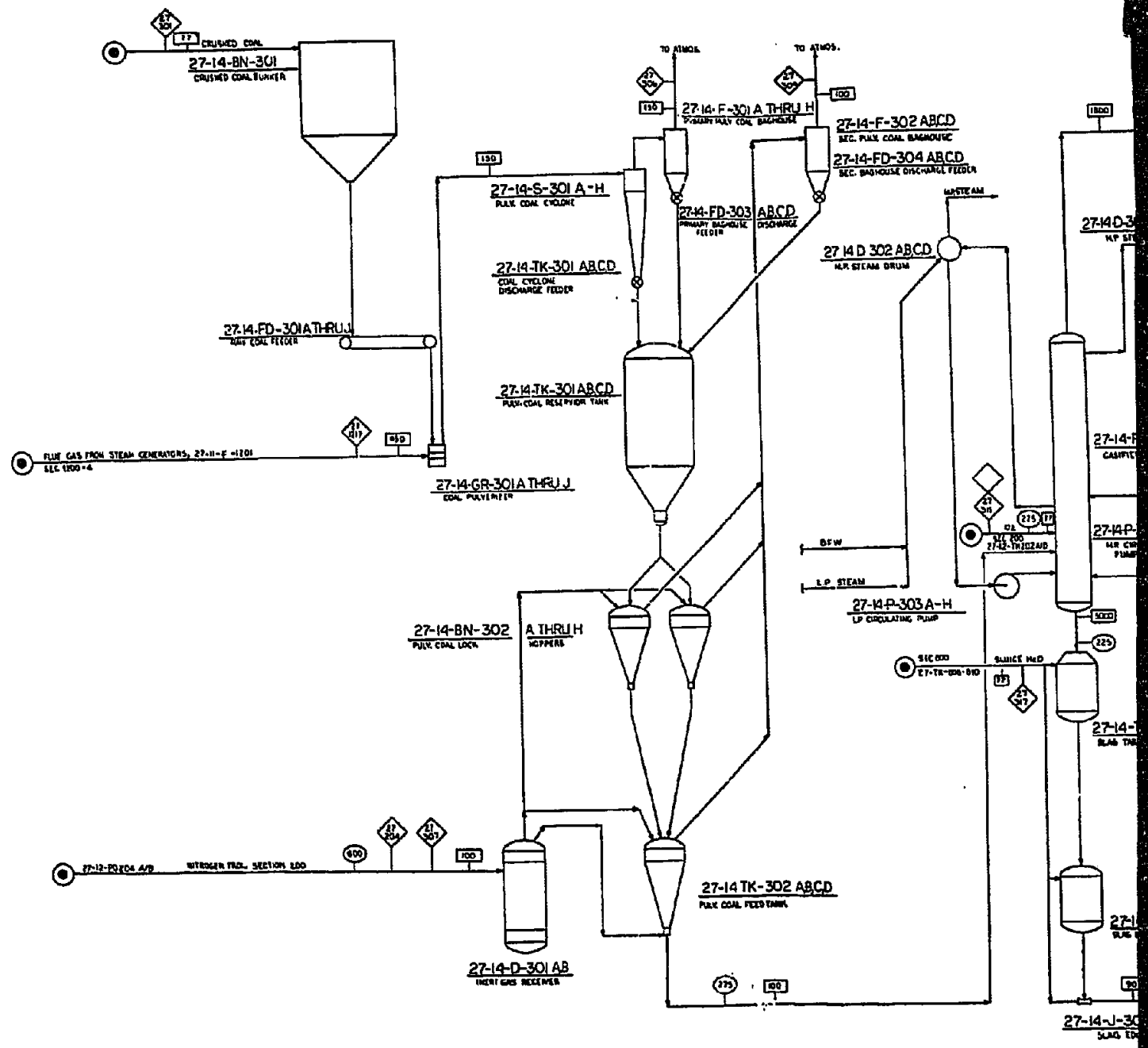
CONTRACT: 11-27-54099
SECTION: 300

EQUIPMENT LIST

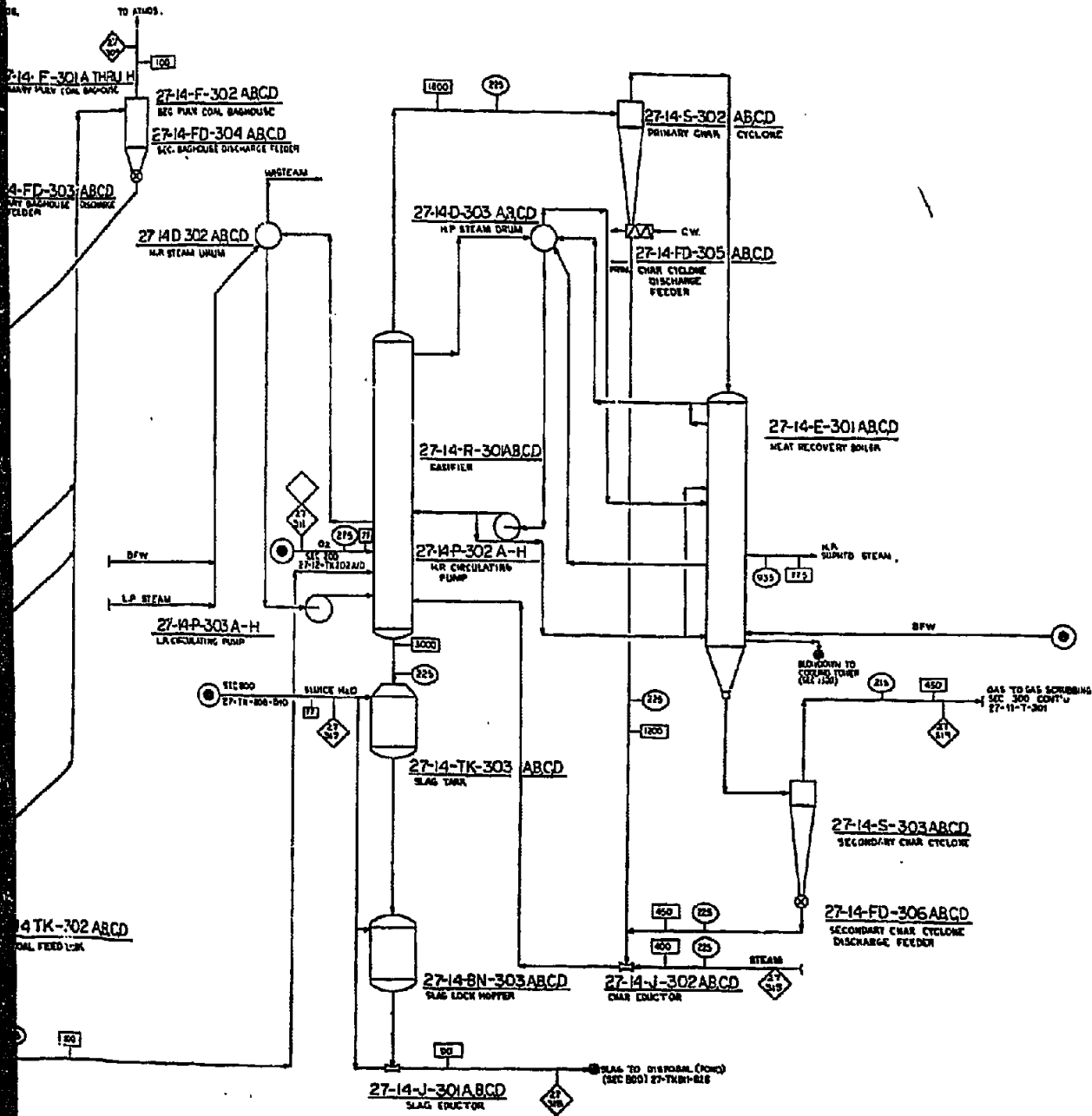
NAME OF UNIT
B & W GASIFICATION


PAGE 3 OF 3

CLASS	ITEM NO.	DESCRIPTION	EFD	REVISION		ORIGINAL	NAME OF UNIT					
				DATE	No./Module		1	2	3	4	5	
SEPARATORS 27-14-	S-301 A-H	PULVERIZED COAL CYCLONE				4-50%						
	S-302 A-D	PRIMARY CHAR CYCLONE				4-50%						
	S-303 A-D	SECONDARY CHAR CYCLONE				4-50%						
TANKS 27-14-	TK-301 A-D	PULVERIZED COAL RESERVOIR TANK				4-50%						
	TK-302 A-D	PULVERIZED COAL FEED TANK				4-50%						
REACTOR 27-14-	TK-303 A-D	SLAG TANK				4-50%						
	R-301 A-D	GASIFIER				4-50%						



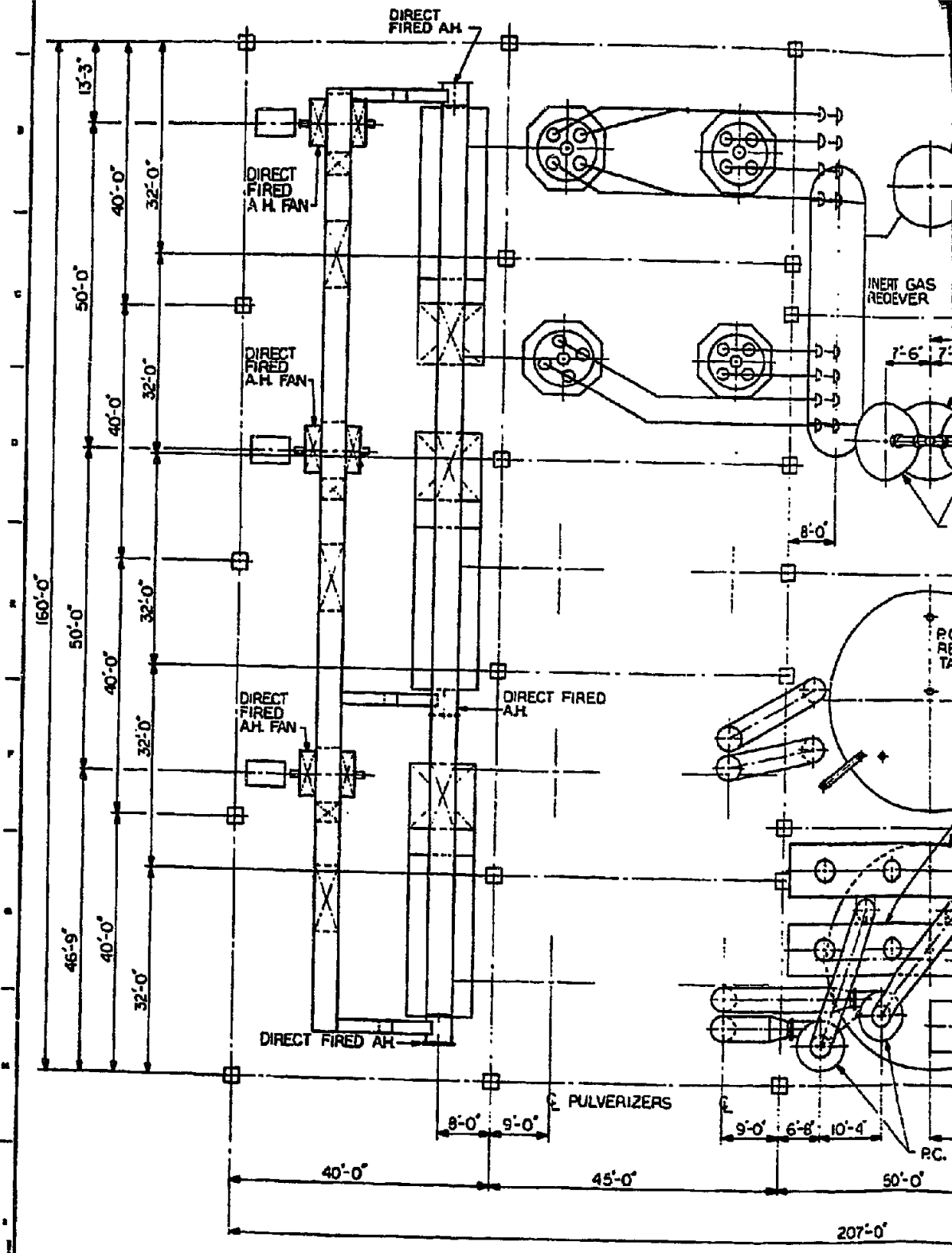
NOTES: EQUIPMENT IS INDICATED FOR ONE MODULE
 THERE ARE FOUR MODULES IN THE PLANT
 SEE EQUIPMENT LIST FOR NUMBER OF ITEMS PER MODULE
 ? FOR LEGEND SEE OLC. NO. 34899-1P-1




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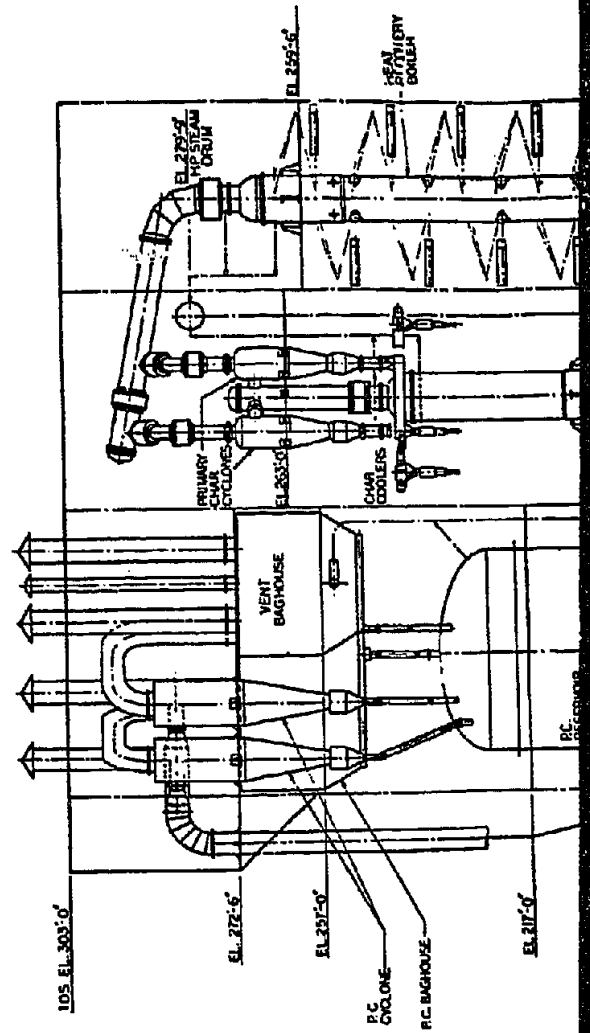
PROCESS FLOW DIAGRAM
 TVA COAL GASIFICATION STUDY
 SECTION 300 BFW GASIFICATION SYSTEM
 P/W: 27-14-1039
 BFW GASIFIERS
 DWG. NO: 27-14-1039-27-14-1039
 THE DRAWING IS THE PROPERTY OF
 THE DRAWING SUPPLIER

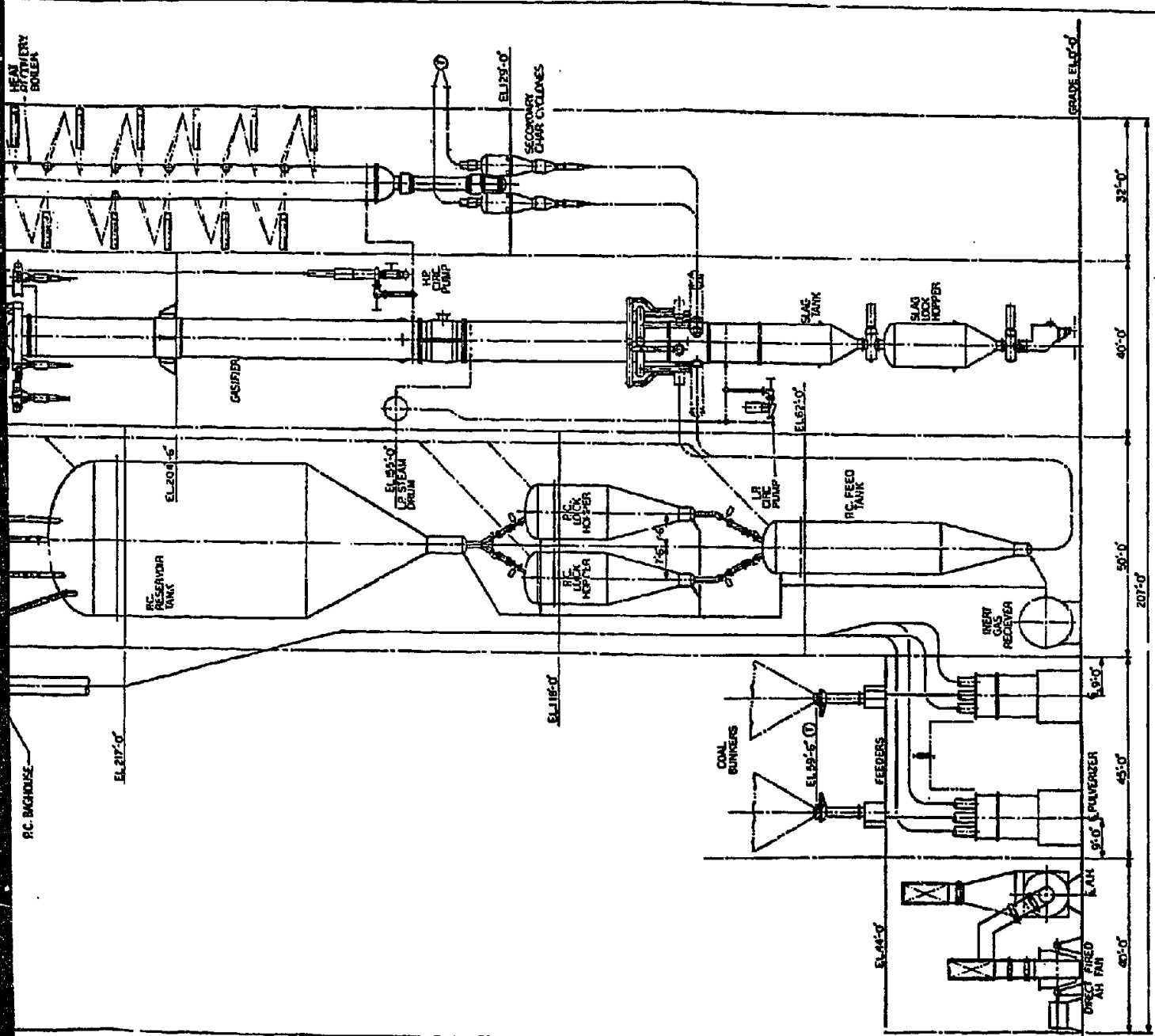
279903E



I I

392239





Babcock & Wilcox
POWER GENERATION GROUP

ARRANGEMENT
OF
2500 TONS/DAY
GASIFICATION M.C. #1E

SHEET NO. 15256 F - 0
 DRAWN BY: [Name]
 CHECKED BY: [Name]
 DATE: [Date]



TVA Coal Gasification Study
E&W Gasifier

Section Description

Section 300B - Gas Scrubbing

A. Reference Material

Process Flowsheet FWEC Drawing No. 54099-27-1-50-4

Equipment Summary List

Material Balance


B. Description of Flow

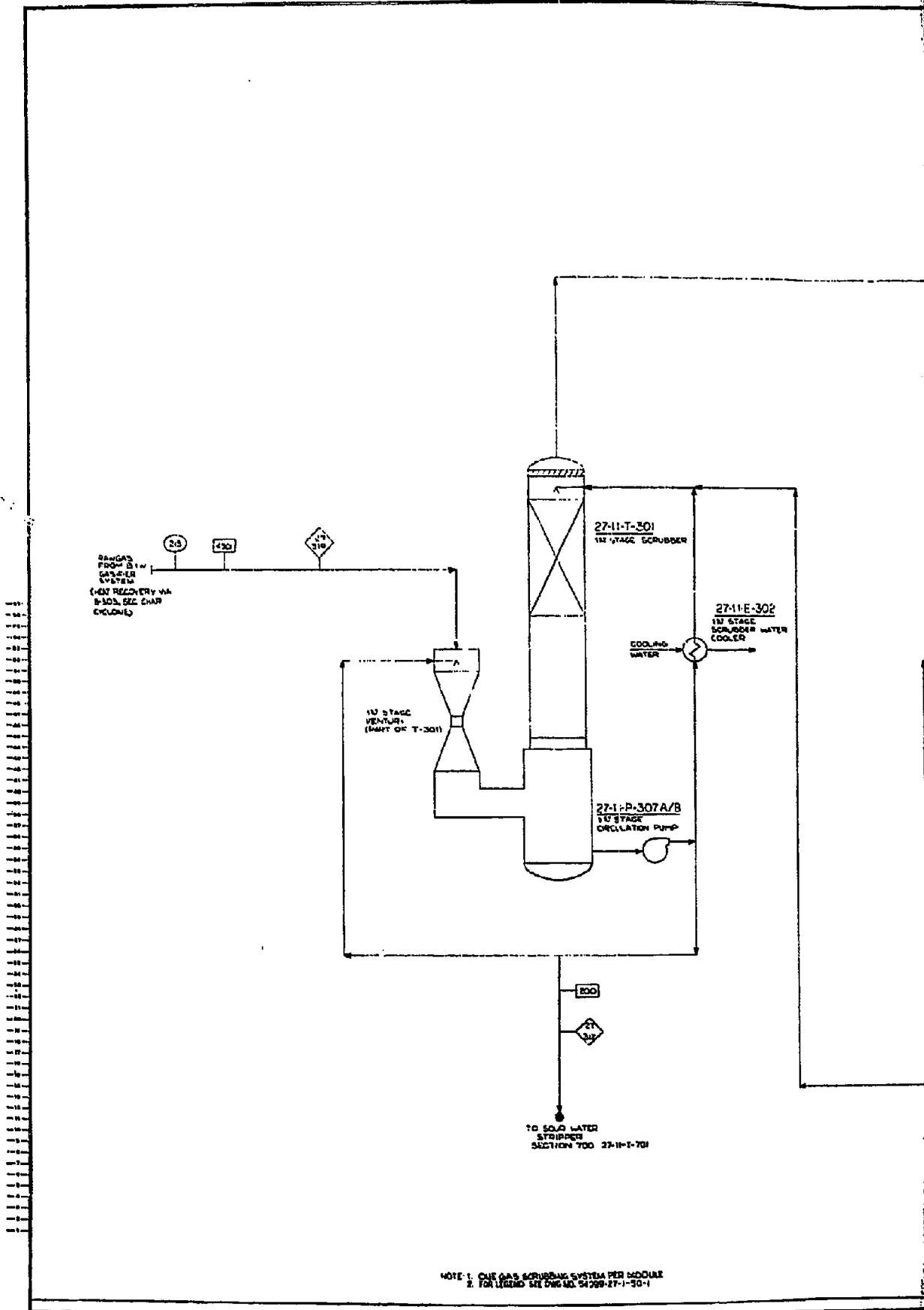
The raw gas is fed to the venturi section of the 1st Stage Scrubber (27-11-T-301) and contacted with a portion of the 1st Stage circulating water from P-307A/B. Purged water from the bottom of the 2nd Stage Scrubber (27-11-T-302) is added as makeup to the 1st Stage water circulation stream. Carbon, ash and small quantities of ammonia and hydrogen sulfide are scrubbed from the raw gas in the two Scrubbers in addition to cooling the raw gas. Recirculating 1st Stage scrubbing water in turn is cooled externally with cooling water in the 1st Stage Scrubber Water Cooler, E-302, before returning to the top of the 1st Stage Scrubber, T-301.

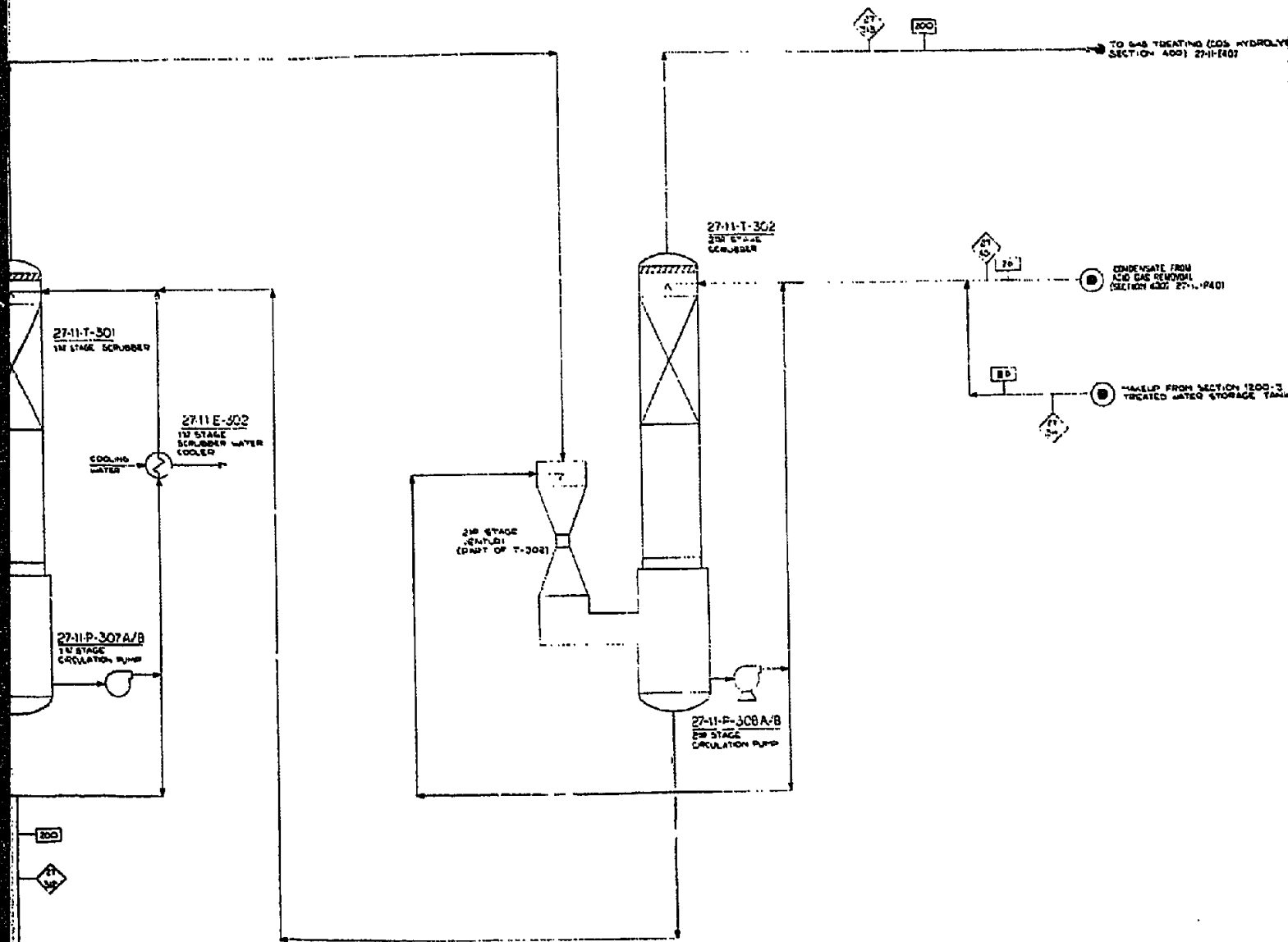
Scrubbing water is purged from the 1st Stage Scrubber at a rate of approximately 560 gpm. Purged water will be pumped to the Sour Water Stripping Unit (Section 700). Partially scrubbed raw gas leaving the 1st stage flows to the 2nd Stage Scrubber venturi where it is contacted in similar fashion to the 1st stage with recirculating water and makeup water from the Treated Water Storage Tank (27-11-TK-1201) (in Section 1200-3) in addition to sour condensate from Acid Gas Removal (Selexol-Section 400). Scrubbing water from the 2nd stage is purged to the 1st Stage Scrubber. The raw gas leaving the 2nd Stage Scrubber flows to G.s Treating (Section 400-Selexol) for further reduction of hydrogen sulfide and ammonia. The hydrogen sulfide concentration in scrubbed gas is about 13,700 ppmv but the ammonia level is relatively low (~ 23 ppmv).

B & W GASIFIERS

FORM NO. 135-304

 FOSTER WHEELER ENERGY CORP. PROCESS PLANTS DIVISION		CONTRACT 11-27-54099 SECTION: 300 cont'd	EQUIPMENT LIST					NAME OF UNIT GAS SCRUBBING (CONTINUATION OF GASIFICATION)	PAGE 1 OF 1
CLIENT: TVA (COAL GASIFICATION STUDY) LOCATION: ALABAMA	ITEM NO.	DESCRIPTION	REVISION DATE	ORIGINAL	1	2	3	4	5
CLASS	EFD No./Module	REV.	REV.	REV.	REV.	REV.	REV.	REV.	REV.
EXCHANGERS 27-11-	E-302	1st STG SCRUBBER WATER COOLER	1-100%						
PUMPS 27-11-	P-307A/B	1st STG CIRCULATION PUMP	2-100%						
	P-308A/B	2nd STG CIRCULATION PUMP	2-100%						
TOWERS 27-11-	T-301	1st STAGE VENTURI SCRUBBER	1-100%						
	T-302	2nd STAGE VENTURI SCRUBBER	1-100%						

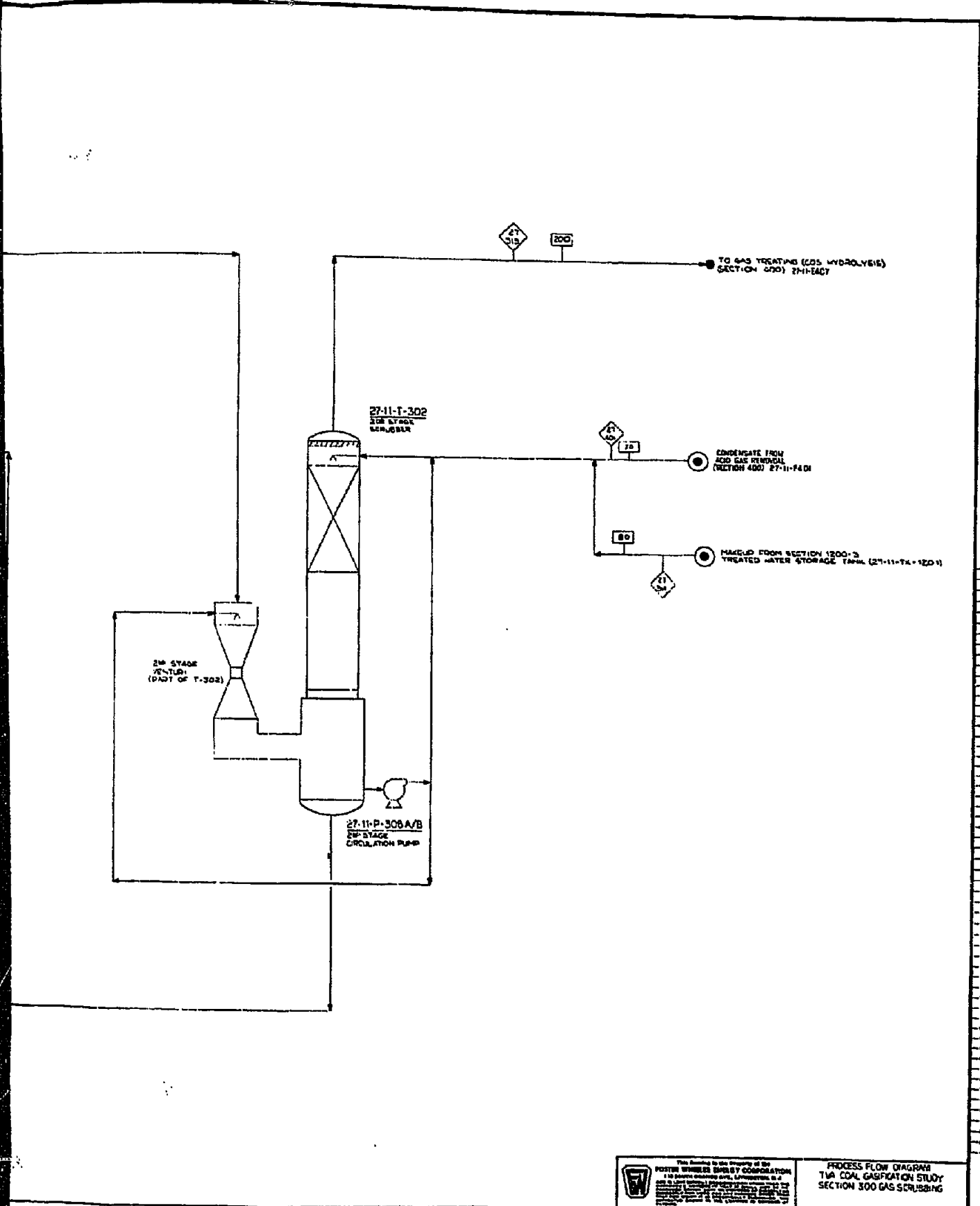





COOLING WATER
SECTION 200 27-11-T-701

WATER SYSTEM PER MODULE
SECTION 200 27-11-T-701

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	DRAWN BY: [] CHECKED BY: [] DATE: []	PROJECT: [] SHEET NO.: []	TOTAL SHEETS: [] SHEET NO.: []	



 <p>This drawing is the property of the FOSTER WHEELER ENERGY CORPORATION It is loaned to the client for use only in the project for which it is prepared. It is not to be used for any other purpose without the written consent of the company. © 1998 Foster Wheeler Energy Corporation</p>	<p>PROCESS FLOW DIAGRAM TVA COAL GASIFICATION STUDY SECTION 300 GAS SCRUBBING</p>	
	<p>DESIGNED BY: JPL SCALE: DRAWN BY: JPL</p>	<p>3/27/98 DWG NO: 400327-30-4</p>



SECTION DESCRIPTION

3.4 SECTION 400 - ACID GAS REMOVALA. Reference Material

Process Flow Diagram: FWEC Dwg. No. 54099-27-1-50-50-5
Equipment List
Material Balance

B. Description of Flow

The purpose of this section is to remove sulfur compounds from the raw gas. Raw gas from Gas Scrubbing (Section 300) flows to the Raw Gas Heater (27-11-E-407). The raw gas is heated to a temperature of 300°F by external heat exchange with 250 PSIG steam. The scrubbed raw gas then flows to the COS Hydrolysis Unit (27-11-PG-401).

The hydrolysis reactor converts the bulk of the COS in the raw gas to H₂S using the Haldor Topsoe CKA catalyst. The conversion of COS to H₂S in the Hydrolysis Unit decreases the utility requirements and size of the Selexol Unit. The raw gas leaving COS Hydrolysis flows to the Sour Gas Condenser, 27-11-E-408, where it is cooled with cooling water. Condensed water in the raw gas is removed in the Condenser K.O. Drum, 27-11-D-405, then combined with additional sour condensate from the H₂S Absorber K.O. Drum, 27-11-D-401, and pumped to Gas Scrubbing (Section 300). Raw gas from the Condenser K.O. Drum is combined with process recycle gas from the Recycle Gas Compressor, 27-11-C-401, and then cooled in the Feed-Product Gas Exchanger, 27-11-E-401, with the product gas. Additional water condensed from the raw gas is separated in the H₂S Absorber K.O. Drum, 27-11-D-401. Raw gas leaving the H₂S Absorber, 27-11-T-401, flows to the H₂S Absorber, 27-11-T-401, where cold lean Selexol solvent physically absorbs H₂S, residual COS and some CO₂. Product gas leaving the top of the H₂S Absorber is cooled in the Feed-Product Gas Exchanger. Most of the product gas flows to Section 500 (Compression) and the remainder to the Beavon Unit, Section 600, to be utilized as a reducing gas. The product gas contains less than 100 ppmv H₂S and less than 30 ppmv COS.

The Selexol solvent leaving the bottom of the H₂S Absorber flows directly to the H₂S Flash Drum, 27-11-D-402. Most of the absorbed CO₂ and sour gases are flashed, then compressed in the Recycle Gas Compressor, 27-11-C-401, and combined with the raw gas feed entering the Feed-Product Gas Exchanger. Make up solvent is added to the H₂S Flash Drum. Fresh solvent is stored in a Solvent Storage Tank, 27-11-TK-401.



Solvent leaving the bottom of the H₂S Flash Drum is pumped to the H₂S Stripper Preheater, 27-11-E-402. The Stripper Preheater is heated with hot lean solvent pumped from the bottom of the H₂S Stripper, 27-11-T-401. Preheated solvent enters the H₂S Stripper for removal of acid gases. Stripper bottoms are reboiled in the H₂S Stripper Reboiler, 27-11-E-404, heated with 60 PSIG steam. Vapors leaving the H₂S Stripper overhead are condensed in the H₂S Stripper Condenser, 27-11-E-405, then enter the Stripper Recycle Drum, D-403. Condensate is totally recycled back to the Stripper, while the Acid Gases flow to the Sulfur Recovery Claus Plant (Section 600). Hot lean solvent is pumped from the bottom of the H₂S Stripper and cooled in the H₂S Stripper Preheater as described earlier. The solvent is chilled in the Lean Solution Refrigerator, 27-11-E-403, then enters the top of the H₂S Absorber. The refrigerant required for E-403 will be provided from a package refrigeration system.

1 SELEXOL UNIT PER MODULE

FORM NO. 125-904

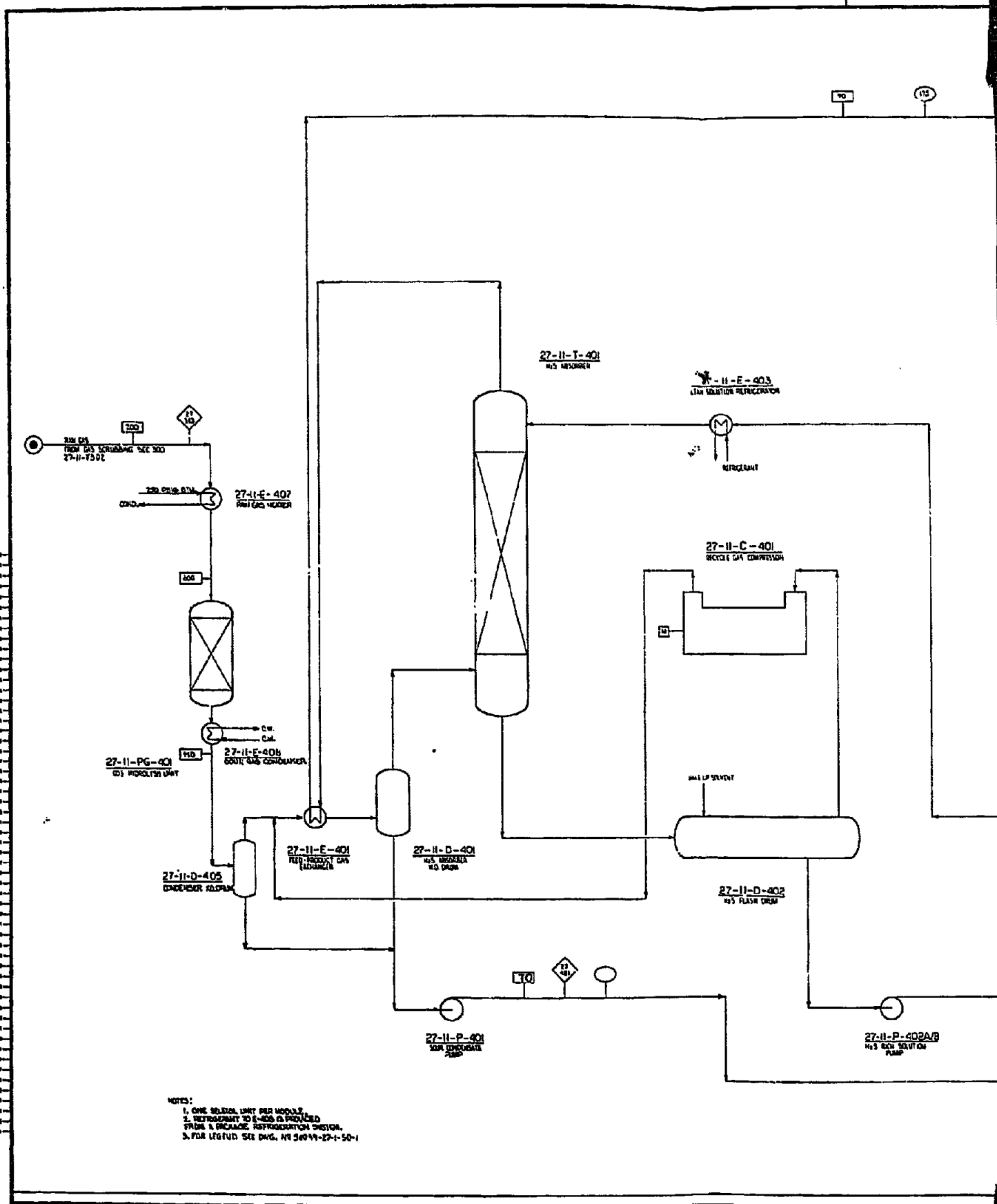
FOSTER WHEELER ENERGY CORP. PROCESS PLANTS DIVISION		CONTRACT 11-27-54099 SECTION 400		EQUIPMENT LIST					NAME OF UNIT			
CLIENT/TVA (COAL GASIFICATION STUDY)				REVISION	ORIGINAL	1	2	3	4	5	ACID GAS REMOVAL (SELEXOL)	
LOCATION: ALABAMA				DATE	NO./Module							
CLASS	ITEM NO.	DESCRIPTION	EPD								PAGE	OF
COMPRESSOR											1	3
27-11-	C-401	RECYCLE GAS COMPRESSOR						1-100%				
DRUMS												
27-11-	D-401	H ₂ S ABSORBER K.O. DRUM						1-100%				
	D-402	H ₂ S FLASH DRUM						1-100%				
	D-403	STRIPPER RECYCLE DRUM						1-100%				
	D-404	RECYCLE COMPRESSOR INTERSTAGE DRUM						1-100%				
	D-405	CONDENSER K.O. DRUM						1-100%				
EXCHANGERS												
27-11-	E-401	FEED-PRODUCT GAS EXCHANGER						1-100%				
	E-402	H ₂ S STRIPPER PREHEATER						1-100%				
	E-403	LEAN SOLUTION REFRIGERATOR						1-100%				
	E-404	H ₂ S STRIPPER REBOILER						1-100%				
	E-405	H ₂ S STRIPPER CONDENSER						1-100%				
	E-406	RECYCLE COMPRESSOR INTERCOOLER						1-100%				

B & W GASIFIERS

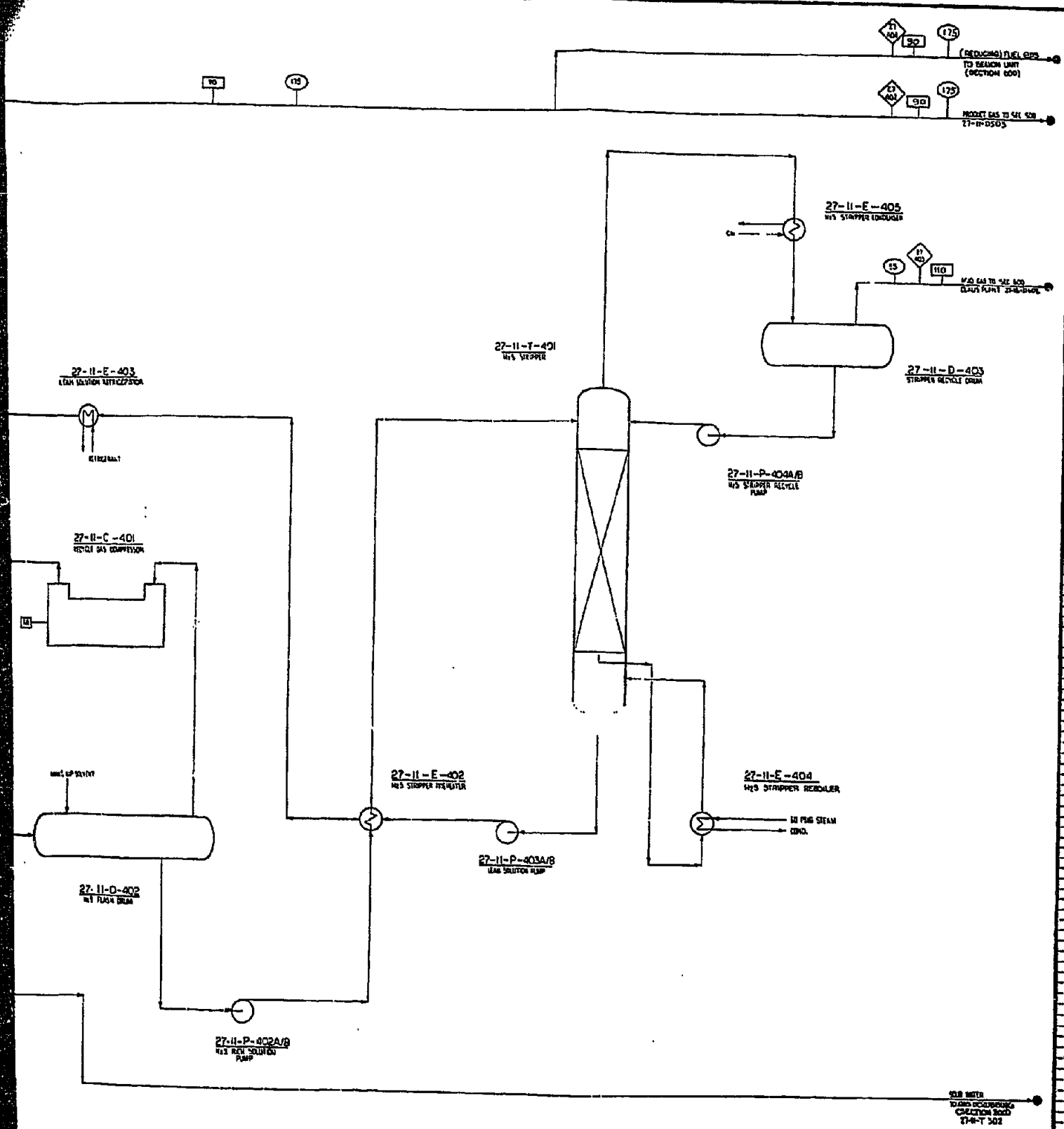
1 SELEXOL UNIT PER MODULE

FORM NO. 115-904

FOSTER WHEELER ENERGY CORP. PROCESS PLANTS DIVISION		CONTRACT 11-27-54099	NAME OF UNIT				
CLIENT: TVA (COAL GASIFICATION STUDY)		SECTION: 400	ACID GAS REMOVAL (SELEXOL)		PAGE	OF	
LOCATION: ALABAMA			1	2	3	4	
CLASS	ITEM NO.	DESCRIPTION	REVISION	DATE	REV.	5	
27-11-	E-407	RAW GAS HEATER					
<u>PUMPS</u>	E-408	SOUR GAS CONDENSER					
27-11-	P-401	SOUR CONDENSATE PUMP					
27-11-	P-402A/B	H ₂ S RICH SOLUTION PUMP	2-100%				
-	P-403A/B	CLEAN SOLUTION PUMP	2-100%				
-	P-404A/B	H ₂ S STRIPPER RECYCLE PUMP	2-100%				
-	P-405A/B	SOLVENT SUMP PUMP	2-100%				
<u>TANK</u>	TK-401	SOLVENT STORAGE TANK	1-100%				
27-11-	F-401	H ₂ S LEAN SOLUTION FILTER	1-100%				
<u>FILTER</u>							
27-11-	PG-401	COS HYDROLYSIS PACKAGE	1-100%				
<u>PACKAGE ITEM</u>							
27-11-	PG-402	SELEXOL REFRIGERATION PACKAGE	1-100%				
-							



NOTES:
 1. ONE SOLID UNIT PER MOBILE.
 2. REFRIGERANT TO E-403 IS PRODUCED FROM A PACKAGE REFRIGERATION SYSTEM.
 3. FOR LEGEND SEE DWG. NO 36099-27-1-50-1



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 170 NORTH BRIDGE AVENUE, PITTSBURGH, PA. 15222
 DRAWING NO. 27-11-400-100-100
 DATE 11/27/80
 DRAWN BY: DTND-016 (DND) CHECKED BY: [Signature] DATE: 12/1/80
 TITLE: PROCESS FLOW DIAGRAM
 TVA COAL GASIFICATION STUDY
 SEC 400 ACID GAS REMOVAL (SELENO)
 SHEET NO. 100 OF 100



TVA Coal Gasification Study
B&W Gasifier

SECTION DESCRIPTION

3.5 SECTION 500 - TREATED GAS COMPRESSION

A. Reference Material:

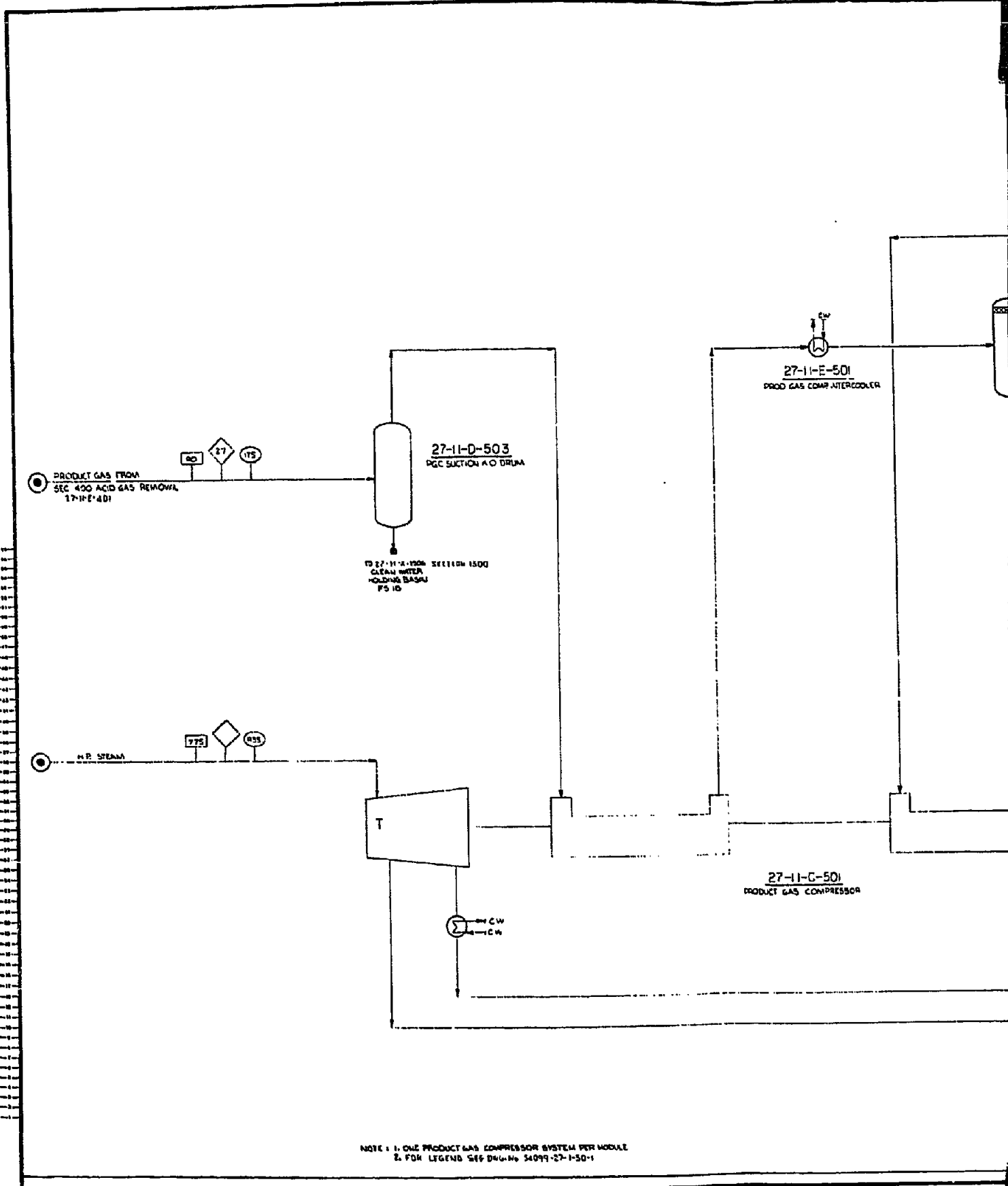
- . Process Flow Diagram FWEC Dwg. No. 54099-27-1-50-6
- . Equipment List

B. Description of Flow

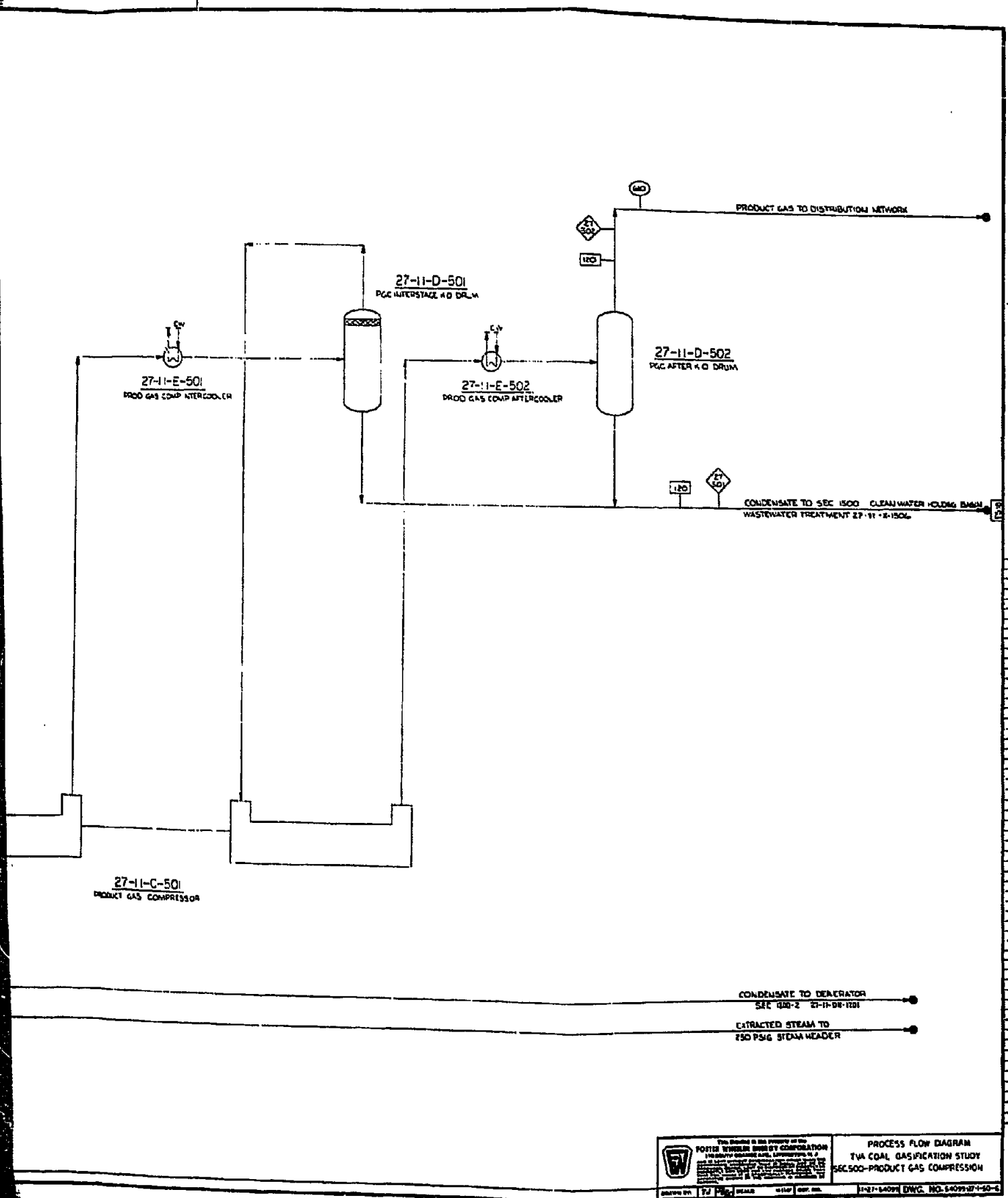
This section compresses the product gas from a pressure of approximately 175 PSIG to about 610 PSIG for subsequent transfer to the distribution network. One product gas compressor is provided per module.

Product gas from Acid Gas Removal (Section 400) enters the PGC Suction K.O. Drum (27-11-D-503) for removal of entrained clean water. This water flows to the Clean Water Holding Basin (X-1506 on FS #18). Product gas leaving the top of the drum enters the turbine driven Product Gas Compressor (27-11-C-501). The turbine utilizes H.P. (935 PSIG superheated) steam and is an extraction type turbine, extracting a required amount of M.P. (250 PSIG) steam, the rest condensed. Extracted steam flows to the 250 PSIG steam header. Condensate from the turbine condenser flows to the Deaerator (27-11-DH-1201).

The compressed product gas enters the water cooled Prod. Gas Comp. Aftercooler (27-11-E-502) which cools the gas to about 120°F. Cooled product gas enters the PGC after K.O. Drum (27-11-D-502), then flows to the gas distribution network.



NOTE 1: ONE PRODUCT GAS COMPRESSOR SYSTEM PER MODULE
2: FOR LEGEND SEE DRAWING 54099-27-1-50-1



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	DRAWN BY: [] CHECKED BY: [] DATE: []	DESIGNED BY: [] DATE: []	



TVA Coal Gasification Study
B&W Gasifier

Section Description

3.6 SECTION 600 - SULFUR RECOVERY PLANT

CLAUS UNIT

A. Reference Material

Process Flowsheet FWEC Drawing No. 54099-27-1-50-7

Equipment List

Material Balance

B. Description of Flow

Acid gas from the Selexol Unit Stripper Recycle Drum, D-403, and a smaller stream of acid gas from the Sour Water Stripper Reflux Drum, D-701, flow through respective K.O. drums and enter the Muffle Furnace, H-601, for destruction of ammonia. Hydrogen sulfide is partially (about one-third) oxidized to sulfur dioxide, utilizing air fed by the Process Air Blower, B-601. High pressure steam is generated in the Waste Heat Boiler, E-601, and is the major source of H.P. steam for process use (refer to 54099-27-1-50-151).

Gases leaving the Waste Heat Boiler flow to a three stage Claus reactor system, consisting of R-601, 602, and 603, where sulfur dioxide reacts catalytically with the remaining hydrogen sulfide, producing elemental sulfur and water. The Claus Unit is about 96% efficient in removal of sulfur compounds from acid gas. Treated tail gas leaving the Claus Unit flows to the Beavon Unit (in series with the Claus Unit) for further reduction of sulfur compounds from the gas and recovery as elemental sulfur. Total normal sulfur production from Claus and Beavon Units combined is about 198 T/D per module.

Gas leaving each Claus Reactor (stage) is cooled below about 300°F to condense sulfur before entering the next stage or flowing to the Beavon Unit. A third Reactor Preheater, E-606, is provided for optimum operation in the third stage.

Liquified (condensed) sulfur flows to a Sulfur Pit, X-601, and may be stored in the Liquid Sulfur Storage Tank, TK-601A/B, for sale as a liquid product or prilled in the Sulfur Prilling Unit, PG-601. At present, it has been decided to normally prill all of the sulfur recovered.

Medium pressure steam is generated during gas cooling to recover sulfur. Boiler blowdown streams will be used as cooling tower makeup as shown on 54099-27-1-50-151.

198 T/D S EACH PLANT 5 TRAINS TOTAL PER PLANT (4 MODULES)
 FORM NO. 135-804

FOSTER WHEELER ENERGY CORP.
 PROCESS PLANTS DIVISION
 CLIENT: TVA (COAL GASIFICATION STUDY)
 LOCATION: ALABAMA

CONTRACT: 11-27-54099
 SECTION: 600

CLASS	ITEM NO.	DESCRIPTION	EFD	REQN. NO./Module	NAME OF UNIT			PAGE	OF
					REVISION	DATE	REV.		
DRUMS 27-15-	D-601	SWS GAS K.O. DRUM			1-100%		1	2	4
	D-602	ACID GAS K.O. DRUM			1-100%		2	3	4
	D-603	BLOWDOWN DRUM			1-100%		3	4	5
HEAT EXCHANGERS 27-15-	E-601	WASTE HEAT BOILER			1-100%				
	E-602	1ST SULFUR CONDENSER			1-100%				
	E-603	SECOND REACTOR FEED HEATER			1-100%				
	E-604	2ND SULFUR CONDENSER			1-100%				
	E-605	3RD SULFUR CONDENSER			1-100%				
	E-606	THIRD REACTOR FEED HEATER			1-100%				
	E-607	FINAL SULFUR CONDENSER			1-100%				
	E-608	SULFUR PIT HEATER			1-100%				
	E-609	SULFUR TANK HEATER			1-100%				
	E-610	AIR PREHEATER			1-100%				
	E-611	ACID GAS PREHEATER			1-100%				
PACKAGE ITEM 27-15-	PG-601	SULFUR PRILLING UNIT PACKAGE			1-100%				

198 T/D SEARCH PLANT (4 MODULES)

5 TRAINS TOTAL PER PLANT

135-904

FOSTER WHEELER ENERGY CORP.
PROCESS PLANTS DIVISION

CONTRACT: 11-27-54099
SECTION: 600

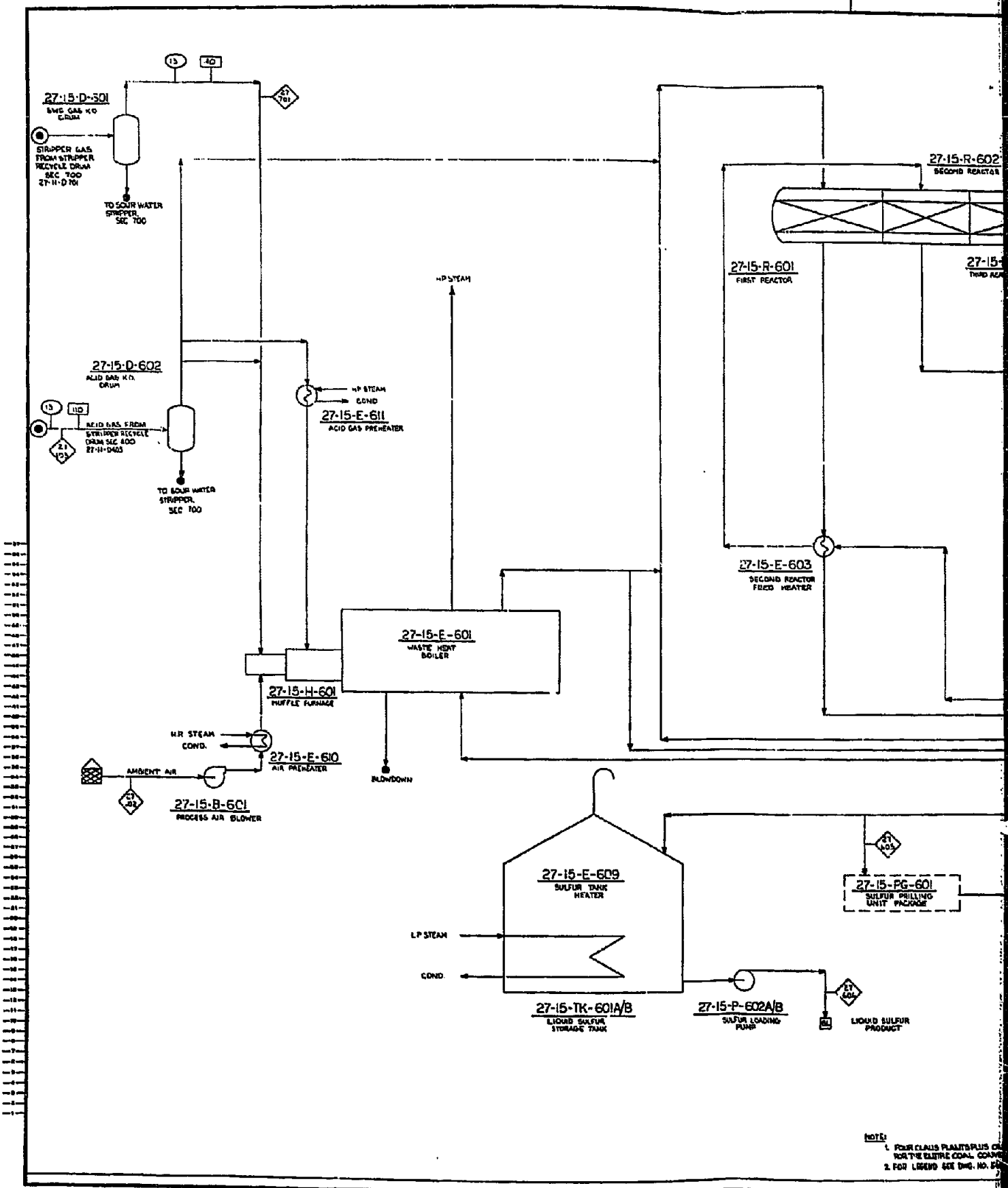
TVA (COAL GASIFICATION STUDY)

ALABAMA

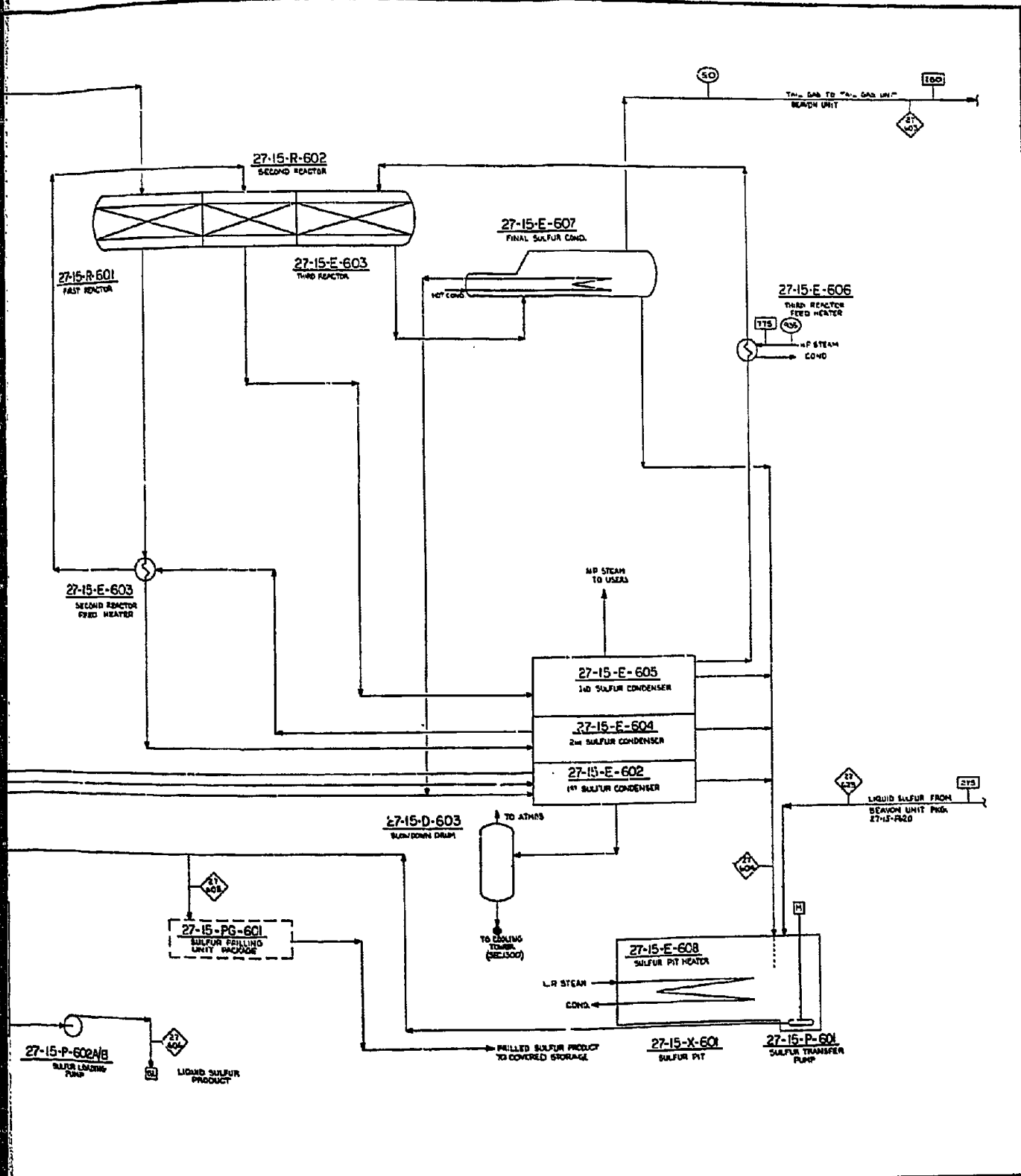
EQUIPMENT LIST

CLASS	ITEM NO.	DESCRIPTION	EFD	REVISION		ORIGINAL	NAME OF UNIT				PAGE	OF	
				DATE	NO./Module		1	2	3	4			2
BLOWER	27-15-												
	B-601	PROCESS AIR BLOWER				1-100%							
FURNACE	H-601	MUFFLE FURNACE				1-100%							
	R-601	FIRST REACTOR				1-100%							
REACTORS	R-602	SECOND REACTOR				1-100%							
	R-603	THIRD REACTOR				1-100%							
PUMPS	P-601	SULFUR TRANSFER PUMP				1-100%							
	P-602A/B	SULFUR LOADING PUMP				2-50%							
TANKS	TK-601A/B	LIQUID SULFUR STORAGE TANK				2-50%							
MISC.	X-601	SULFUR PIT				1-100%							

REV.



NOTE:
 1. FOUR CLAUIS PLANTS PLUS ONE FOR THE ENTIRE COAL COAL
 2. FOR LEGEND SEE DWG. NO. 27-15-100



NOTE:
 1. FOUR CLAUS PLANTS PLUS ONE SPARE UNIT ARE REQUIRED FOR THE ENTIRE COAL CONVERSION PLANT.
 2. FOR LEGEND SEE Dwg. NO. 24099-27-130-1.

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	DRAWING NO. 24099-27-130-1 SHEET NO. 11-27-54099	DWG. NO. 24099-27-50-7 THIS DRAWING ORIGINATED BY THIS DRAWING APPROVED BY