

**APPENDIX C**  
**SOURCE FORTRAN CODE OF MFREK**  
**AND A SAMPLE INPUT DATA**

## C.1 MFREK.F

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C-----+
C      MULTIPHASE
C      FLOW SIMULATOR WITH
C      REACTIONS,
C      ENERGY EQUATIONS AND
C      KINETIC THEORY.
C
C      MODIFIED BY
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PROGRAM MFREK
INCLUDE 'mfrek.com'
CHARACTER*10 RESTART
CHARACTER*80 NAME
READ(5,'(A)')RESTART
OPEN(9,FILE=RESTART,FORM='UNFORMATTED',TYPE='UNKNOWN')
READ(5,'(A)')NAME
WRITE(6,'(A)') SIMULATION - ',NAME
READ(5,*)(DR(I),I=1,IB2)
READ(5,*)(DZ(J),J=1,JB2)
WRITE(6,210)ITC,IB2,JB2,DR(1),DZ(1)
WRITE(6,215)(DR(I),I=1,IB2)
WRITE(6,216)(DZ(J),J=1,JB2)
READ(5,*)(NSL(M),M=1,4)
WRITE(6,220)(NSL(M),M=1,4)
WRITE(6,230)NIN,NOUT,NFL,NOBS
WRITE(6,240)
DO 5 N=1,NT
READ(5,*)NSO(N),ITHMF(N),(IOB(M,N),M=1,4)
WRITE(6,245)NSO(N),(IOB(M,N),M=1,4)
IF(ITHMF(N).EQ.1)THEN
READ(5,*)QQ(N),TOBB(N),COEK(N)
ENDIF
5 CONTINUE
READ(5,*)(DK(K),K=1,NPHASE)
READ(5,*)(PHI(K),K=1,NPHASE)
READ(5,*)(RL(K),K=1,NPHASE)
READ(5,*)(CL(K),K=1,NPHASE)
READ(5,*)(VISS(K),K=1,NPHASE)
READ(5,*)(KIN(K),RLKMIN(K),K=1,NPHASE)

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WRITE(6,250)
WRITE(6,255)(DK(K),RL(K),CL(K),PHI(K),K=1,NPHASE)
READ(5,*)UIO(1),VIO(1),PIO(1),THIO(1),TEMIO(1)
READ(5,*)(UPIO(K,1),VPIO(K,1),THPIO(K,1),TEMPIO(K,1)
1,TSKIO(K,1),K=1,NPHASE)
WRITE(6,260)
WRITE(6,265)UIO(1),VIO(1),PIO(1),THIO(1),TEMIO(1)
WRITE(6,270)
WRITE(6,275)(K,UPIO(K,1),VPIO(K,1),THPIO(K,1),TEMPIO(K,1),K=1
1,NPHASE)
WRITE(6,280)
DO 10 N=2,NO
READ(5,*)UIO(N),VIO(N),PIO(N),THIO(N),TEMIO(N)
READ(5,*)(UPIO(K,N),VPIO(K,N),THPIO(K,N),TEMPIO(K,N),
1TSKIO(K,N),K=1,NPHASE)
10 WRITE(6,285)UIO(N),VIO(N),PIO(N),THIO(N),TEMIO(N)
WRITE(6,290)
DO 15 N=2,NO
15 WRITE(6,295)(K,UPIO(K,N),VPIO(K,N),THPIO(K,N),TEMPIO(K,N),
1K=1,NPHASE)
READ(5,*)IHEAT,IRXN
IF(IRXN.EQ.1)THEN
READ(5,*)(WM(JX),JX=1,JXN)
WRITE(6,*)
WRITE(6,*)'MOLECULAR WEIGHT'
WRITE(6,*)' CO CO2 H2 CH4 CH3OH N2'
WRITE(6,*)'WM=',(WM(JX),JX=1,JXN)
WRITE(6,*)
WRITE(6,*)'REACTION HEAT & STOICHIOMETRIC COEFF.'
DO 16 K=1,NPHASE+1
WRITE(6,*)
READ(5,*)IHO(K),IHE(K)
WRITE(6,*)'PHASE',K-1,', # OF HOMO-REACTIONS=',IHO(K),
1', # OF HETERO-REACTIONS=',IHE(K)
IF(IHO(K).NE.0)THEN
WRITE(6,*)' HOMO-REACTIONS'
DO 17 IX=1,IHO(K)
READ(5,*)HHO(K,IX),(AHO(K,IX,JX),JX=1,JXN)
17 WRITE(6,*)' REACTION',IX,' COEF.',(AHO(K,IX,JX),JX=1,JXN)
ENDIF
IF(IHE(K).NE.0)THEN
WRITE(6,*)' HETERO-REACTIONS'
DO 21 IX=1,IHE(K)
READ(5,*)HHE(K,IX),(AHE(K,IX,JX),JX=1,JXN)
21 WRITE(6,*)' REACTION',IX,' COEF.',(AHE(K,IX,JX),JX=1,JXN)

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        ENDIF
16    CONTINUE
        WRITE(6,*)
        WRITE(6,*)'COMPOSITIONS'
        WRITE(6,*)
        DO 19 N=1,NO
        DO 19 K=1,NPHASE+1
        READ(5,*)(YIO(K,JX,N),JX=1,JXN)
19    WRITE(6,519)N,K-1,(YIO(K,JX,N),JX=1,JXN)
519  FORMAT(' BLOCK',I2,', PHASE ',I1,',',6G11.4)
        ENDIF
        READ(5,*)ITD
        READ(5,*)TIME,TSTOP,DT
        READ(5,*)TPR,TDUMP
        WRITE(6,300)ITD,TIME,TSTOP,DT,TPR,TDUMP
        READ(5,*)GRAVX,GRAVY
        WRITE(6,310)GRAVY,GRAVX
        WRITE(6,*)
        DO 30 J=1,JB2
        DO 30 I=1,IB2
        IJ=I+(J-1)*IB2
        TOB(IJ)=0.0
        COE(IJ)=0.0
30    QF(IJ)=0.0
        DO 22 N=1,NT
        IF(ITHMF(N).NE.1)GOTO 22
        DO 23 J=IOB(3,N),IOB(4,N)
        DO 23 I=IOB(1,N),IOB(2,N)
        IJ=I+(J-1)*IB2
        TOB(IJ)=TOBB(N)
        COE(IJ)=COEK(N)
23    QF(IJ)=QQ(N)
22    CONTINUE
        DO 27 N=1,NT
        IF(ITHMF(N).NE.1) GOTO 27
C    WRITE(6,*)'HEAT SOURCE/SINK (T-OBSTACLE/FLUX)'
        DO 24 J=1,JB2
        DO 24 I=1,IB2
        IJ=I+(J-1)*IB2
24    Q(IJ)=QF(IJ)+TOB(IJ)
C    DO 26 IJ=IB2JB2,IB2,-IB2
C26  WRITE(6,25)(Q(IL),IL=IJ-IB1,IJ)
25    FORMAT(6(1X,G12.4))
        GOTO 29
27    CONTINUE

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29  CONTINUE
C
    REWIND(9)
    DO 500 K=1,NPHASE
    VISSD(K)=VISS(K)
    DO 500 IJ=1,IB2JB2
500  VISBL(K,IJ)=0.0
    TTIM=0.0
    IF (ITD.EQ.2) CALL TAPERD
    DO 20 K=1,NPHASE
20   ARL(K)=1./RL(K)
    CALL FLIC
    CALL SETUP
    CALL PROG
    STOP
210  FORMAT(/' 1. GEOMETRY/' A. COORDINATES
    1(CART=0, CYLIND=1, SPHER=2)
    1='I3/' B. MESH SIZE, IB2='I3,6X,'JB2='I3/'
    1C. CELL SIZE'
    2,', DR='1PE12.4,' DZ='1PE12.4)
215  FORMAT(7X,'DR='8(2X,F6.3))
216  FORMAT(7X,'DZ='8(2X,F6.3))
220  FORMAT(/' 2. CELL FLAGS/' A. BOUNDARIES (FREE-SLIP=2
    1NO-SLIP=3)'
    1/7X,'BOTTOM='I3,' LEFT='I3,' TOP='I3,' RIGHT='I3)
230  FORMAT(' B. INLETS ='I3,' OUTLETS ='I3,' FLUIDS =' I3,
    1' OBSTACLES ='I3)
240  FORMAT(' SLIP',10X,'-----COORDINATES-----')
245  FORMAT(5X,I3,4(4X,I5))
250  FORMAT(/' 3. PARTICULATE PHASE DATA/7X,'DIAMETER',4X,
    1'MACROSCOPIC',
    1' DENSITY',4X,' HEAT CAPACITY',4X,'SPHERICITY')
255  FORMAT((2(6X,G10.3),13X,G10.3,7X,G10.3))
260  FORMAT(/' 4. INITIAL AND BOUNDARY DATA/' A. INITIAL DATA',
    1'(FLUID)/11X,'UO',13X,'VO',13X,'PO',12X,'THO',11X,'TEMGO')
265  FORMAT((2X,5(4X,1PE11.4)))
270  FORMAT(' B. INITIAL DATA (SOLID)/8X,'PHASE',9X,
    1'UKO',11X,'VKO',10X,'THKO',9X,'TEMKO')
275  FORMAT((8X,I3,3X,4(3X,1PE11.4)))
280  FORMAT(' C. INFLOW - OUTFLOW DATA (FLUID)/10X,'UIO',12X,
    1'VIO',12X,'PIO',12X,'THIO',11X,'TEMIO')
285  FORMAT((2X,5(4X,1PE11.4)))
290  FORMAT(' D. INFLOW - OUTFLOW DATA (SOLID)/8X,'PHASE',9X,
    1'UPIO',11X,'VPIO',10X,'THPIO',9X,'TEMPIO')
295  FORMAT((8X,I3,3X,4(4X,1PE11.4)))

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300  FORMAT(/ 5. CONTROL/ 3X,'A. DUMP AND RESTART, ITD='
      1,I3/3X,
      1'B. TIME TSTART=',1PE11.4,' TSTOP=',1PE11.4,' DT=',
      11PE11.4/
      1' C. PRINTING AND PLOTTING, TPR=',1PE11.4,' TDUMP=',
      11PE11.4)
310  FORMAT(/ 6. GRAVITY/' A. GRAVY=',1PE15.7,' GRAVX='
      1,1PE15.7)
      END

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C -----BDRY

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SUBROUTINE BDRY
INCLUDE 'mfrek.com'

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DO 200 J=2,JB1
DO 200 I=2,IB1
IJ=I+(J-1)*IB2
IF(IFL(IJ).EQ.1) THEN
RGNP(IJ)=RGP(IJ)
THN(IJ)=TH(IJ)
SIEGN(IJ)=SIEG(IJ)
TG(IJ)=C1+SIEG(IJ)/CG
IF(IHEAT.EQ.0)TG(IJ)=TEMIO(1)
CALL ROGY(IJ)
AKG(IJ)=8.67D5*(TG(IJ)/1400.0)**1.786
DO 9 K=1,NPHASE
SIELN(K,IJ)=SIEL(K,IJ)
IF (RLK(K,IJ).EQ.0.0) THEN
  TL(K,IJ)=0.0
ELSE
  TL(K,IJ)=C2+SIEL(K,IJ)/CL(K)
ENDIF
IF(IHEAT.EQ.0)TL(K,IJ)=TEMPIO(K,1)
CALL THRCON
TSKN(K,IJ)=TSK(K,IJ)
9  RLKN(K,IJ)=RLK(K,IJ)
IPJ=IJ+1
IJP=IJ+IB2
IMJ=IJ-1
IJM=IJ-IB2
IPJP=IJP+1
IMJP=IJP-1
IPJM=IJM+1
NFLR=IFL(IPJ)
NFLTR=IFL(IPJP)
NFLT=IFL(IJP)

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IF(NFLR.EQ.4.OR.NFLR.GE.7) THEN
N1=IJ
N2=IPJ
IF(NFLR.EQ.4.OR.UG(N1).GT.0.)THEN
RGFR(N2)=RGFR(N1)
RGP(N2)=RGP(N1)
RUG(N2)=RUG(N1)
TH(N2)=TH(N1)
TG(N2)=TG(N1)
DO 14 JX=1,JXN
14 YN(1,JX,N2)=YN(1,JX,N1)
Y(1,JX,N2)=Y(1,JX,N1)
DO 15 K=1,NPHASE
RLFRK(K,N2)=RLFRK(K,N1)
RLK(K,N2)=RLK(K,N1)
TSK(K,N2)=TSK(K,N1)
TSKN(K,N2)=TSK(K,N1)
RUK(K,N2)=RUK(K,N1)
DO 13 JX=1,JXN
13 YN(K+1,JX,N2)=YN(K+1,JX,N1)
Y(K+1,JX,N2)=Y(K+1,JX,N1)
15 TL(K,N2)=TL(K,N1)
IF(NFLR.GE.7)THEN
IJ=N2
CALL CNVERT
IJ=N1
ELSE
P(N2)=P(N1)
ENDIF
ENDIF
IF(NFLTR.GE.4)THEN
VG(N2)=VG(N1)
DO 17 K=1,NPHASE
17 VK(K,N2)=VK(K,N1)
ENDIF
DO 18 K=1,NPHASE
18 UK(K,N2)=UK(K,N1)
UG(N2)=UG(N1)
IF (NFLR.EQ.8)THEN
DO 20 K=1,NPHASE
20 UK(K,N2)=0.0
VK(K,N2)=0.0
ENDIF
ENDIF
IF(NFLT.EQ.4.OR.NFLT.GE.7) THEN

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N1=IJ
N2=IJP
IF(NFLT.EQ.4.OR.VG(N1).GT.0.)THEN
RGFT(N2)=RGFT(N1)
RGP(N2)=RGP(N1)
RVG(N2)=RVG(N1)
TH(N2)=TH(N1)
TG(N2)=TG(N1)
DO 24 JX=1,JXN
YN(1,JX,N2)=YN(1,JX,N1)
24 Y(1,JX,N2)=Y(1,JX,N1)
DO 25 K=1,NPHASE
RLFTK(K,N2)=RLFTK(K,N1)
TSK(K,N2)=TSK(K,N1)
TSKN(K,N2)=TSK(K,N1)
RLK(K,N2)=RLK(K,N1)
RVK(K,N2)=RVK(K,N1)
DO 23 JX=1,JXN
YN(K+1,JX,N2)=YN(K+1,JX,N1)
23 Y(K+1,JX,N2)=Y(K+1,JX,N1)
25 TL(K,N2)=TL(K,N1)
IF(NFLT.GE.7)THEN
IJ=N2
CALL CNVERT
IJ=N1
ELSE
P(N2)=P(N1)
ENDIF
ENDIF
IF(NFLTR.GE.4) THEN
UG(N2)=0.0
DO 27 K=1,NPHASE
27 UK(K,N2)=0.0
ENDIF
RGP(N2)=RGP(N1)
VG(N2)=VG(N1)
C VG(N2)=RGP(N1)*VG(N1)/RGP(N2)
DO 28 K=1,NPHASE
28 VK(K,N2)=VK(K,N1)
IF (NFLT.EQ.8)THEN
DO 30 K=1,NPHASE
UK(K,N2)=0.0
30 VK(K,N2)=0.0
ENDIF
ENDIF

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## C OBSTACLES

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      IF(IFL(IJ).EQ.1)THEN
      IF (NFLR .EQ. 2) THEN
      VG(IPJ)=VG(IJ)
      DO 91 K=1,NPHASE
91    VK(K,IPJ)=VK(K,IJ)
      ELSEIF (NFLR .EQ. 3 ) THEN
      VG(IPJ)=0.0
      DO 92 K=1,NPHASE
92    VK(K,IPJ)=0.0
      ENDIF
      IF (NFLT .EQ. 2) THEN
      UG(IJP)=UG(IJ)
      DO 93 K=1,NPHASE
93    UK(K,IJP)=UK(K,IJ)
      ELSEIF (NFLT .EQ. 3) THEN
      UG(IJP)=0.0
      DO 94 K=1,NPHASE
94    UK(K,IJP)=0.0
      ENDIF
      NFLL=IFL(IMJ)
      NFLTL=IFL(IMJP)
      IF (NFLL .EQ. 2) THEN
      VG(IMJ)=VG(IJ)
      DO 95 K=1,NPHASE
95    VK(K,IMJ)=VK(K,IJ)
      ELSEIF (NFLL .EQ. 3) THEN
      VG(IMJ)=0.0
      DO 96 K=1,NPHASE
96    VK(K,IMJ)=0.0
      ENDIF
      NFLB=IFL(IJM)
      NFLBR=IFL(IPJM)
      IF (NFLB .EQ. 2) THEN
      UG(IJM)=UG(IJ)
      DO 97 K=1,NPHASE
97    UK(K,IJM)=UK(K,IJ)
      ELSEIF (NFLB .EQ. 3) THEN
      UG(IJM)=0.0
      DO 98 K=1,NPHASE
98    UK(K,IJM)=0.0
      ENDIF
      ENDIF
      ENDIF
200  CONTINUE

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RETURN
END

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C -----BETAS

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SUBROUTINE BETAS
INCLUDE 'mfrek.com'

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PARAMETER (EPSG=1.0D-4)
DO 10 J=2,JB1
DO 10 I=2,IB1
IJ=I+(J-1)*IB2
IF(IFL(IJ).NE.1) GOTO 10
CALL INDXA
IF(IFL(IPJ).EQ.1.OR.IFL(IPJ).EQ.4.OR.IFL(IPJ).GE.7)THEN
RIG=RB(I)*(AR(I)*TH(IJ)+BR(I)*TH(IJR))
ELSE
RIG=0.
ENDIF
IF(IFL(IMJ).NE.2.AND.IFL(IMJ).NE.3.AND.IFL(IMJ).NE.5)THEN
EFL=RB(I-1)*(BR(I-1)*TH(IJ)+AR(I-1)*TH(IJL))
ELSE
EFL=0.
ENDIF
IF(IFL(IJP).EQ.1.OR.IFL(IJP).EQ.4.OR.IFL(IJP).GE.7)THEN
TOP=AZ(J)*TH(IJ)+BZ(J)*TH(IJT)
ELSE
TOP=0.
ENDIF
IF(IFL(IJM).EQ.1.OR.IFL(IJM).EQ.4.OR.IFL(IJM).EQ.6)THEN
BOT=BZ(J-1)*TH(IJ)+AZ(J-1)*TH(IJB)
ELSE
BOT=0.
ENDIF
CONV(IJ)=EPSG*RGP(IJ)
RBETA=TH(IJ)*ROG(IJ)/P(IJ)+DTODZ(J)*DTODZ(J)*(TOP+BOT)+
1DTODR(I)*DTODR(I)*(RIG+EFL)
ABETA(IJ)=1./RBETA
10 CONTINUE
RETURN
END

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C -----CNVERT

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SUBROUTINE CNVERT
INCLUDE 'mfrek.com'

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CALL ROGY(IJ)

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RGP(IJ)=ROG(IJ)*TH(IJ)
RGN(IJ)=RGP(IJ)
SIEG(IJ)=(TG(IJ)-C1)*CG
SIEGN(IJ)=SIEG(IJ)
AKG(IJ)=8.67D5*(TG(IJ)/1400.0)**1.786
DO 10 K=1,NPHASE
TSKN(K,IJ)=TSK(K,IJ)
RLKN(K,IJ)=RLK(K,IJ)
SIEL(K,IJ)=(TL(K,IJ)-C2)*CL(K)
SIELN(K,IJ)=SIEL(K,IJ)
10 CONTINUE
RETURN
END

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C -----COMPOS

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SUBROUTINE COMPOS
C SOLVE THE COMPOSITION FOR EACH PHASE
INCLUDE 'mfrek.com'
IF(IRXN.EQ.0)RETURN
DO 2 J=2,JB1
DO 2 I=2,IB1
IJ=I+(J-1)*IB2
IF(IFL(IJ).NE.1)GOTO 2
CALL INDXA
DO 10 K=1,LT
K1=K-1
IF(K.EQ.1)GOTO 6
IF(RLK(K1,IJ).GT.0.0)GOTO 6
DO 5 JX=1,JXN
5 Y(K,JX,IJ)=0.0
GOTO 10
6 CALL RRATE
IF(K.EQ.1)THEN
C CALL MASFGY
IF(UG(IMJ).GE.0.)THEN
RGFRY(IMJ)=UG(IMJ)*RGP(IJ)*RB(I-1)
KEY(2)=IJL
ELSE
RGFRY(IMJ)=UG(IMJ)*RGP(IJ)*RB(I-1)
KEY(2)=IJ
ENDIF
IF(VG(IJM).GE.0.)THEN
RGFTY(IJM)=VG(IJM)*RGP(IJB)
KEY(4)=IJB
ELSE

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RGFTY(IJM)=VG(IJM)*RGP(IJ)
KEY(4)=IJ
ENDIF
C  ENTRY MASFGAY
   IF(UG(IJ).GE.0.)THEN
     RGFRY(IJ)=UG(IJ)*RGP(IJ)*RB(I)
     KEY(1)=IJ
   ELSE
     RGFRY(IJ)=UG(IJ)*RGP(IJR)*RB(I)
     KEY(1)=IJR
   ENDIF
   IF(VG(IJ).GE.0.)THEN
     RGFTY(IJ)=VG(IJ)*RGP(IJ)
     KEY(3)=IJ
   ELSE
     RGFTY(IJ)=VG(IJ)*RGP(IJT)
     KEY(3)=IJT
   ENDIF
   ELSE
C  CALL MASFKY
   IF(UK(K1,IMJ).GE.0.)THEN
     RLFRKY(K1,IMJ)=UK(K1,IMJ)*RLK(K1,IJL)*RB(I-1)
     KEY(2)=IJL
   ELSE
     RLFRKY(K1,IMJ)=UK(K1,IMJ)*RLK(K1,IJ)*RB(I-1)
     KEY(2)=IJ
   ENDIF
   IF(VK(K1,IJM).GE.0.)THEN
     RLFTKY(K1,IJM)=VK(K1,IJM)*RLK(K1,IJB)
     KEY(4)=IJB
   ELSE
     RLFTKY(K1,IJM)=VK(K1,IJM)*RLK(K1,IJ)
     KEY(4)=IJ
   ENDIF
C
C  ENTRY MASFKAY
   IF(UK(K1,IJ).GE.0.)THEN
     RLFRKY(K1,IJ)=UK(K1,IJ)*RLK(K1,IJ)
     KEY(1)=IJ
   ELSE
     RLFRKY(K1,IJ)=UK(K1,IJ)*RLK(K1,IJR)
     KEY(1)=IJR
   ENDIF
   IF(VK(K1,IJ).GE.0.)THEN
     RLFTKY(K1,IJ)=VK(K1,IJ)*RLK(K1,IJ)

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KEY(3)=IJ
ELSE
RLFTKY(K1,IJ)=VK(K1,IJ)*RLK(K1,IJT)
KEY(3)=IJT
ENDIF
ENDIF
THY=0.0
DO 25 JX=1,JXN
DOTMJ(K,JX)=0.0
DO 30 IX=1,IHO(K)
30 DOTMJ(K,JX)=DOTMJ(K,JX)+RHO(K,IX)*AHO(K,IX,JX)
DO 27 IX=1,IHE(K)
27 DOTMJ(K,JX)=DOTMJ(K,JX)+RHE(K2,IX)*AHE(K2,IX,JX)
IF(K.EQ.1)THEN
SUMN=WM(JX)*DOTMJ(1,JX)*DT+RGPN(IJ)*YN(1,JX,IJ)
1+DGG(IJ)*YN(1,JX,IJ)
SUMD=TH(IJ)*ROG(IJ)
IF(KEY(1).EQ.IJ)THEN
SUMD=SUMD+DTORDR(I)*RGFRY(IJ)
ELSE
SUMN=SUMN-DTORDR(I)*RGFRY(IJ)*YN(1,JX,IJR)
ENDIF
IF(KEY(2).EQ.IJ)THEN
SUMD=SUMD-DTORDR(I)*RGFRY(IMJ)
ELSE
SUMN=SUMN+DTORDR(I)*RGFRY(IMJ)*YN(1,JX,IJL)
ENDIF
IF(KEY(3).EQ.IJ)THEN
SUMD=SUMD+DTODZ(J)*RGFTY(IJ)
ELSE
SUMN=SUMN-DTODZ(J)*RGFTY(IJ)*YN(1,JX,IJT)
ENDIF
IF(KEY(4).EQ.IJ)THEN
SUMD=SUMD-DTODZ(J)*RGFTY(IJM)
ELSE
SUMN=SUMN+DTODZ(J)*RGFTY(IJM)*YN(1,JX,IJB)
ENDIF
Y(1,JX,IJ)=SUMN/SUMD
ELSE
SUMN=WM(JX)*DOTMJ(K,JX)*DT+RLKN(K1,IJ)*YN(K,JX,IJ)
SUMD=RLK(K1,IJ)
IF(KEY(1).EQ.IJ)THEN
SUMD=SUMD+DTORDR(I)*RLFRKY(K1,IJ)
ELSE
SUMN=SUMN-DTORDR(I)*RLFRKY(K1,IJ)*YN(K,JX,IJR)

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ENDIF
IF(KEY(2).EQ.IJ)THEN
SUMD=SUMD-DTORDR(I)*RLFRKY(K1,IMJ)
ELSE
SUMN=SUMN+DTORDR(I)*RLFRKY(K1,IMJ)*YN(K,JX,IJL)
ENDIF
IF(KEY(3).EQ.IJ)THEN
SUMD=SUMD+DTODZ(J)*RLFTKY(K1,IJ)
ELSE
SUMN=SUMN-DTODZ(J)*RLFTKY(K1,IJ)*YN(K,JX,IJT)
ENDIF
IF(KEY(4).EQ.IJ)THEN
SUMD=SUMD-DTODZ(J)*RLFTKY(K1,IJM)
ELSE
SUMN=SUMN+DTODZ(J)*RLFTKY(K1,IJM)*YN(K,JX,IJB)
ENDIF
Y(K,JX,IJ)=SUMN/SUMD
ENDIF

C
IF(Y(K,JX,IJ).LE.1D-10)Y(K,JX,IJ)=0.0
THY=THY+Y(K,JX,IJ)
25 CONTINUE
IF(ABS(THY-1.0).LE.1D-10)GOTO 10
C NORMALIZE THE COMPOSITION,
C PUT THE ERROR TO A MAJOR COMPONENT SUCH AS #6
IF(K.EQ.1)THEN
Y(K,6,IJ)=1.0-(THY-Y(K,6,IJ))
ELSE
Y(K,6,IJ)=1.0-(THY-Y(K,6,IJ))
ENDIF
10 CONTINUE
2 CONTINUE
3 DO 9 IJ=1,IB2JB2
IF(IFL(IJ).NE.1)GOTO 9
DO 8 K=1,LT
DO 8 JX=1,JXN
YN(K,JX,IJ)=Y(K,JX,IJ)
8 CONTINUE
9 CONTINUE
RETURN
END

C -----FEFLUX
SUBROUTINE FEFLUX
INCLUDE 'mfrek.com'

```

```

C
C CALCULATE FLUCTUATING ENERGY FLUXES OF KINETIC THEORY
C
  TSKCB(K)=(TSKN(K,IJ)-TSKN(K,IJB))
  1*(BZ(J-1)*GCON(K,IJ)+AZ(J-1)*GCON(K,IJB))*RDZP(J-1)
  TSKFB(K,I)=1.5*TSKFB(K,I)-TSKCB(K)
C
  ENTRY FEFLUXA
  IF(IFL(IMJ).NE.1)THEN
  TSKCL(K)=(TSKN(K,IJ)-TSKN(K,IJL))*RB(I-1)
  1*(BR(I-1)*GCON(K,IJ)+AR(I-1)*GCON(K,IJL))*RDRP(I-1)
  TSKFL(K)=1.5*TSKFL(K)-TSKCL(K)
  ENDIF
C
  ENTRY FEFLUXB
  TSKCR(K)=(TSKN(K,IJR)-TSKN(K,IJ))*RB(I)
  1*(BR(I)*GCON(K,IJR)+AR(I)*GCON(K,IJ))*RDRP(I)
  TSKFR(K)=1.5*TSKFR(K)-TSKCR(K)
C
  TSKCT(K)=(TSKN(K,IJT)-TSKN(K,IJ))
  1*(BZ(J)*GCON(K,IJT)+AZ(J)*GCON(K,IJ))*RDZP(J)
  TSKFT(K)=1.5*TSKFT(K)-TSKCT(K)
  RETURN
  END
C -----FLIC
  SUBROUTINE FLIC
  INCLUDE 'mfrek.com'
  IJ=0
  DO 150 J=1,JB2
  DO 150 I=1,IB2
  IJ=IJ+1
  IFL(IJ)=1
  IF (J.EQ.JB2) THEN
  IFL(IJ)=NSL(3)
  ELSEIF (J.EQ.1) THEN
  IFL(IJ)=NSL(1)
  ENDIF
  IF (I.EQ.1) THEN
  IFL(IJ)=NSL(2)
  ELSEIF (I.EQ.IB2) THEN
  IFL(IJ)=NSL(4)
  ENDIF
150 CONTINUE
  DO 300 N=1,NT
  DO 300 I=IOB(1,N),IOB(2,N)

```

```

DO 300 J=IOB(3,N),IOB(4,N)
IJ=I+(J-1)*IB2
IFL(IJ)=NSO(N)
300 CONTINUE
IF(IFL(IB1JB2).EQ.4.AND.IFL(IB2JB1).EQ.4)IFL(IB2JB2)=4
IF(IFL(IB1JB2).EQ.7.AND.IFL(IB2JB1).EQ.7)IFL(IB2JB2)=7
RETURN
END

```

C -----GRNVIS

SUBROUTINE GRNVIS

INCLUDE 'mfrek.com'

C

C CALCULATE NEW GRANULAR TEMPERATURES

C AND SOLIDS PROPERTIES

C USING KINETIC THEORY OF GRANULAR SOLIDS

C

CALL VWORKL

DO 10 J=2,JB1

DO 10 I=2,IB1

IJ=I+(J-1)\*IB2

IF(IFL(IJ).EQ.1)THEN

IMJ=INDS(IJ,2)

IIM=INDS(IJ,4)

DO 5 K=1,NPHASE

IF(KIN(K).NE.1)GOTO 5

C GRANULAR KINETIC THEORY IS APPLIED

C ONLY IF (EF-EF,MIN) > 1.E-10

CWW IF(RLK(K,IJ).GT.RLKMIN(K).AND.

CWW 1(TH(IJ)-THMIN).GT.1.E-10)THEN

IF(RLK(K,IJ).GT.RLKMIN(K))THEN

C

THL(K,IJ)=ARL(K)\*RLK(K,IJ)

TSKS=TSK(K,IJ)\*\*0.5

C CALCULATE RADIAL DISTRIBUTION FUNCTION & OTHER PARAMETERS

G0=1.0/(1.0-(THL(K,IJ)/(1.0-THMIN))\*\*(1./3.))

CS1=(1.0+CRES)\*THL(K,IJ)\*G0

CS2=3.0\*(1.0-CRES)\*RLK(K,IJ)\*CS1

C CS3=RLK(K,IJ)/(RLK(K,IJ)+DMFP(K))

CS4=2.\*VISDIL(K)/((1.+CRES)\*G0)

RSQRTPI=1.0/SQRT(PI)

GAMMA(K,IJ)=CS2\*(4.0\*RSQRTPI/DK(K)\*TSKS-SILM(K,IJ))

PS(K,IJ)=RLK(K,IJ)\*(1.0+2.0\*CS1)

C

VISCD=CS4\*(1.+8\*CS1)\*\*2



```
VISBL(K,IJ)=(4./3.)*RLK(K,IJ)*DK(K)*CS1/PI**0.5
VISCL(K,IJ)=VISCD+0.6*VISBL(K,IJ)
```

C

C GRANULAR CONDUCTIVITY

```
GCON(K,IJ)=3.75*CS4*(1.+1.2*CS1)**2*TSKS
1+1.5*VISBL(K,IJ)*TSKS
```

ELSE

GCON(K,IJ)=0.0

ENDIF

5

CONTINUE

ENDIF

10

CONTINUE

C

C FINAL SOLUTION OF GRANULAR TEMPERATURE

DO 100 J=2,JB1

DO 100 I=2,IB1

IJ=I+(J-1)\*IB2

IF(IFL(IJ).EQ.1)THEN

CALL INDX

C

DO 20 K=1,NPHASE

IF(KIN(K).NE.1)GOTO 20

CALL GRTEMP

CW IF(RLK(K,IJ).GT.RLKMIN(K).AND.

CW 1(TH(IJ)-THMIN).GT.1.E-10)THEN

IF(RLK(K,IJ).GT.RLKMIN(K))THEN

AP0=(-1.5\*RLK(K,IJ)\*TSK(K,IJ)-DTODZ(J)\*(TSKFT(K)

1-TSKFB(K,I))-DTORDR(I)\*(TSKFR(K)-TSKFL(K)))

AP1=-(VISCL(K,IJ)\*VWLS(K,IJ)+(VISBL(K,IJ)

1-(2./3.)\*VISCL(K,IJ))\*VWLM(K,IJ))

CWW D.G. INDICATES THE DRAG IN THE KINETIC EQS

C MUST BE ELIMINATED

AP2=(1.5\*RLK(K,IJ)+DT\*(3.0\*RKPG(K,IJ)\*0.00001

1+PS(K,IJ)\*SILM(K,IJ)+GAMMA(K,IJ)))

C

CALL QESOL(AP0,AP1,AP2,TSKS)

IF(TSKS.LT.0.0)TSKS=0.0

IF(TSKS.GT.1000.0)TSKS=1000.0

TSK(K,IJ)=TSKS\*TSKS

C

C SOLID PHASE BULK AND SHEAR VISCOSITIES

VISBL(K,IJ)=VISBL(K,IJ)\*TSKS

VISCL(K,IJ)=VISCL(K,IJ)\*TSKS

C

C SOLIDS PHASE PRESSURE

```

PS(K,IJ)=PS(K,IJ)*TSK(K,IJ)
ELSE
TSK(K,IJ)=0.0
VISBL(K,IJ)=0.0
VISCL(K,IJ)=0.0
PS(K,IJ)=0.0
ENDIF
TSKFL(K)=TSKFR(K)
TSKFB(K,I)=TSKFT(K)
20 CONTINUE
C
ENDIF
100 CONTINUE
RETURN
END

C -----GRPROP
SUBROUTINE GRPROP
INCLUDE 'mfrek.com'
C
C INITIALIZE SOLIDS PROPERTIES USING GRANULAR KINETIC THEORY
C
C GRANULAR KINETIC THEORY IS APPLIED
C ONLY IF (EF-EF,MIN) > 1.E-10
CWW IF(RLK(K,IJ).GT.RLKMIN(K).AND.
CWW 1(TH(IJ)-THMIN).GT.1.E-10)THEN
IF(RLK(K,IJ).GT.RLKMIN(K))THEN
THL(K,IJ)=ARL(K)*RLK(K,IJ)
TSKS=TSK(K,IJ)**0.5
GO=1.0/(1.0-(THL(K,IJ)/(1.0-THMIN))**(1./3.))
CS1=(1.0+CRES)*THL(K,IJ)*GO
CS2=3.0*(1.0-CRES)*RLK(K,IJ)*CS1
C CS3=RLK(K,IJ)/(RLK(K,IJ)+DMFP(K))
CS4=2.*VISEDIL(K)/((1.+CRES)*GO)
VISCD=CS4*(1.+8*CS1)**2
VISBL(K,IJ)=(4./3.)*RLK(K,IJ)*DK(K)*CS1*TSKS/PI**0.5
VISCL(K,IJ)=VISCD*TSKS+0.6*VISBL(K,IJ)
PS(K,IJ)=RLK(K,IJ)*(1.0+2.0*CS1)*TSK(K,IJ)
GCON(K,IJ)=3.75*CS4*(1.+1.2*CS1)**2*TSKS
1+1.5*VISBL(K,IJ)
ELSE
VISBL(K,IJ)=0.0
VISCL(K,IJ)=0.0
PS(K,IJ)=0.0
GCON(K,IJ)=0.0

```

```

ENDIF
RETURN
END

```

```

C -----GRTEMF

```

```

SUBROUTINE GRTEMF
INCLUDE 'mfrek.com'

```

```

C
C CALCULATES GRANULAR TEMPERATURE FLUXES OF KINETIC THEORY
C

```

```

IF(UK(K,IJ).GE.0.)THEN
TSKFR(K)=RLFRK(K,IJ)*TSKN(K,IJ)
ELSE
TSKFR(K)=RLFRK(K,IJ)*TSKN(K,IJR)
ENDIF
IF(VK(K,IJ).GE.0.)THEN
TSKFT(K)=RLFTK(K,IJ)*TSKN(K,IJ)
ELSE
TSKFT(K)=RLFTK(K,IJ)*TSKN(K,IJT)
ENDIF
IF(IFL(IMJ).NE.1)GOTO 1
IF(IFL(IJM).NE.1)GOTO 2
CALL FEFLUXB
RETURN

```

```

C
1 IF(UK(K,IMJ).GE.0.)THEN
TSKFL(K)=RLFRK(K,IMJ)*TSKN(K,IJL)
ELSE
TSKFL(K)=RLFRK(K,IMJ)*TSKN(K,IJ)
ENDIF
IF(IFL(IJM).NE.1)GOTO 2
CALL FEFLUXA
RETURN

```

```

C
2 IF(VK(K,IJM).GE.0.)THEN
TSKFB(K,I)=RLFTK(K,IJM)*TSKN(K,IJB)
ELSE
TSKFB(K,I)=RLFTK(K,IJM)*TSKN(K,IJ)
ENDIF
CALL FEFLUX
RETURN
END

```

```

C -----HEATCG

```

```

SUBROUTINE HEATCG

```

```
INCLUDE 'mfrek.com'
```

```
C
```

```
C CALCULATES THE HEAT FLUXES FROM GAS CONDUCTIVITY
```

```
C
```

```
HFGB=(BZ(J-1)*AKG(IJ)+AZ(J-1)*AKG(IJB))*
1*(BZ(J-1)*TH(IJ)+AZ(J-1)*TH(IJB))*
1*(TG(IJ)-TG(IJB))*RDZP(J-1)
ENTRY HEATGA
HFGL=RB(I-1)*(BR(I-1)*AKG(IJ)+AR(I-1)*AKG(IJL))
1*(BR(I-1)*TH(IJ)+AR(I-1)*TH(IJL))*
1*(TG(IJ)-TG(IJL))*RDRP(I-1)
ENTRY HEATGB
HFGR=RB(I)*(AR(I)*AKG(IJ)+BR(I)*AKG(IJR))
1*(AR(I)*TH(IJ)+BR(I)*TH(IJR))*
1*(TG(IJR)-TG(IJ))*RDRP(I)
HFGT=(AZ(J)*AKG(IJ)+BZ(J)*AKG(IJT))
1*(AZ(J)*TH(IJ)+BZ(J)*TH(IJT))*
1*(TG(IJT)-TG(IJ))*RDZP(J)
RETURN
END
```

```
C
```

```
-----HEATCL
```

```
SUBROUTINE HEATCL
INCLUDE 'mfrek.com'
```

```
C
```

```
C CALCULATES THE HEAT FLUXES FROM SOLIDS CONDUCTIVITY
```

```
C
```

```
HFLB(K,I)=(BZ(J-1)*AKL(K,IJ)+AZ(J-1)*AKL(K,IJB))
1*(BZ(J-1)*RLK(K,IJ)+AZ(J-1)*RLK(K,IJB))*
1*(TL(K,IJ)-TL(K,IJB))*ARL(K)*RDZP(J-1)
ENTRY HEATLA
HFLL(K)=RB(I-1)*(BR(I-1)*AKL(K,IJ)+AR(I-1)*AKL(K,IJL))*
1*(BR(I-1)*RLK(K,IJ)+AR(I-1)*RLK(K,IJL))
1*(TL(K,IJ)-TL(K,IJL))*ARL(K)*RDRP(I-1)
ENTRY HEATLB
HFLR(K)=RB(I)*(AR(I)*AKL(K,IJ)+BR(I)*AKL(K,IJR))*
1*(AR(I)*RLK(K,IJ)+BR(I)*RLK(K,IJR))
1*(TL(K,IJR)-TL(K,IJ))*ARL(K)*RDRP(I)
HFILT(K)=(AZ(J)*AKL(K,IJ)+BZ(J)*AKL(K,IJT))*
1*(AZ(J)*RLK(K,IJ)+BZ(J)*RLK(K,IJT))
1*(TL(K,IJT)-TL(K,IJ))*ARL(K)*RDZP(J)
RETURN
END
```

```
C
```

```
-----ICONV
```

```
SUBROUTINE ICONV
```

```

INCLUDE 'mfrek.com'
DIMENSION AI(NP,NP),BI(NP)
C
C FINAL UPDATING OF THE SPECIFIC ENERGIES ( ENTHALPIES )
C
IF(IHEAT.EQ.0)RETURN
DO 100 J=2,JB1
DO 100 I=2,IB1
IJ=I+(J-1)*IB2
IF(IFL(IJ).EQ.1) THEN
CALL INDXA
CALL SIEGF
CALL QRXN
CALL QFLUX
AI(1,1)=RGP(IJ)
BI(1)=RGP(IJ)*SIEG(IJ)-SIEGN(IJ)*(RGP(IJ)-RGPN(IJ))-
IDTODZ(J)*(EGFT-EGFB(I))-DTORDR(I)*(EGFR-EGFL)
C FOR INTERNAL ENERGY (MODEL B) <<
CWU THE WORK DONE BY THE FLUID HAS CONSIDERABLE EFFECT
C ON ENERGY EQUATION. HERE REDUCE IT TO ITS 10%.
1-0.1*P(IJ)*(DTODZ(J)*(VG(IJ)-VG(IJM))
1+DTORDR(I)*(RB(I)*UG(IJ)-RB(I-1)*UG(IMJ)))
BI(1)=BI(1)+DT*(QGEN(1)+QFLOW(1))
C >>
C FOR ENTHALPY (MODEL B) <<
C 1+((P(IJ)-PN(IJ))+0.5*DTODZ(J)*(VG(IJ)+VG(IJM))
C 1*((AZ(J)-BZ(J-1))*P(IJ)+BZ(J)*P(IJT)-AZ(J-1)*P(IJB))
C 1+0.5*DTORDR(I)*(UG(IJ)+UG(IMJ))*(RB(I)
C 1*(BR(I)*P(IJR)+AR(I)*P(IJ))
C 1-RB(I-1)*(BR(I-1)*P(IJ)+AR(I-1)*P(IJL))))
C >>
DO 10 K=1,NPHASE
CALL SIELF
KP=K+1
RHT=-0.5*DT*RHEAT(K,IJ)
AI(1,KP)=RHT/CL(K)
AI(KP,1)=RHT/CG
AI(1,1)=AI(1,1)-AI(KP,1)
AI(KP,KP)=RLK(K,IJ)-AI(1,KP)
RIT=(SIEG(IJ)/CG-SIEL(K,IJ)/CL(K)+TL(K,IJ)-TG(IJ))*RHT
BI(1)=BI(1)-RIT
BI(KP)=RLK(K,IJ)*SIEL(K,IJ)-SIELN(K,IJ)*(RLK(K,IJ)-
IRLKN(K,IJ))+
1RIT-DTODZ(J)*(ELFT(K)-ELFB(K,I))-DTORDR(I)*(ELFR(K)
1-ELFL(K))

```

```

      BI(KP)=BI(KP)+DT*(QGEN(KP)+QFLOW(KP))
10  CONTINUE
      CALL IINV(NPHS1,AI,BI)
      SIEG(IJ)=BI(1)
      DO 20 K=1,NPHASE
      SIEL(K,IJ)=BI(K+1)
      ELFL(K)=ELFR(K)
20  ELFB(K,I)=ELFT(K)
      EGFB(I)=EGFT
      EGFL=EGFR
      ENDIF
100 CONTINUE
      RETURN
      END

```

C -----IGIL

```

SUBROUTINE IGIL
INCLUDE 'mfrek.com'
DIMENSION AI(NP,NP),BI(NP)
IF(IHEAT.EQ.0)RETURN
CALL QRXN
CALL QFLUX
AI(1,1)=RGP(IJ)
BI(1)=RGP(IJ)*SIEGN(IJ)
BI(1)=BI(1)+DT*(QGEN(1)+QFLOW(1))
DO 10 K=1,NPHASE
  KP=K+1
  RHT=-0.5*DT*RHEAT(K,IJ)
  AI(1,KP)=RHT/CL(K)
  AI(KP,1)=RHT/CG
  AI(1,1)=AI(1,1)-AI(KP,1)
  AI(KP,KP)=RLK(K,IJ)-AI(1,KP)
  RIT=(SIEGN(IJ)/CG-SIELN(K,IJ)/CL(K)+TLN(K,IJ)-TGN(IJ))*RHT
  BI(1)=BI(1)-RIT
  BI(KP)=RLK(K,IJ)*SIELN(K,IJ)+RIT
10  BI(KP)=BI(KP)+DT*(QGEN(KP)+QFLOW(KP))
      CALL IINV(NPHS1,AI,BI)
      SIEG(IJ)=BI(1)
      DO 100 K=1,NPHASE
100  SIEL(K,IJ)=BI(K+1)
      RETURN
      END

```

C -----IINV

```

SUBROUTINE IINV(NP,A,B)
IMPLICIT REAL*8(A-H,O-Z)
DIMENSION A(NP,NP),B(NP)

```

C INVERSE OF MATRIX WITH NON-ZERO FIRST COLUMN,  
 C FIRST ROW & DIAGONAL COLUMN

```

    DO 10 K=NP,2,-1
      IF (ABS(A(K,K)) .LE. 1.D-6) THEN
        A(1,K)=0.0
        A(K,1)=0.0
        B(K)=0.0
      ELSE
        DIV=1./A(K,K)
        A(K,1)=A(K,1)*DIV
        B(K)=B(K)*DIV
        B(1)=B(1)-A(1,K)*B(K)
        A(1,1)=A(1,1)-A(1,K)*A(K,1)
      ENDIF
10  CONTINUE
    B(1)=B(1)/A(1,1)
    DO 20 K=2, NP
20  B(K)=B(K)-A(K,1)*B(1)
    RETURN
  END

```

C -----INDX

```

  SUBROUTINE INDX
  INCLUDE 'mfrek.com'

```

```

C
  IMJP=IJ-1+IB2
  IJTL=IMJP
  IF((IFL(IMJP).EQ.2).OR.(IFL(IMJP).EQ.3)) IJTL=IJ+IB2
  IPJM=IJ+1-IB2
  IJBR=IPJM
  IF((IFL(IPJM).EQ.2).OR.(IFL(IPJM).EQ.3)) IJBR=IJ+1
  IJRR=IJ+2
  IF (I.EQ.IB1) IJRR=IJ+1
  IF((IFL(IJRR).EQ.2).OR.(IFL(IJRR).EQ.3)) IJRR=IJ+1
  IJTT=IJ+IB2+IB2
  IF (J.EQ.IB1) IJTT=IJ+IB2
  IF((IFL(IJTT).EQ.2).OR.(IFL(IJTT).EQ.3)) IJTT=IJ+IB2
  ENTRY INDXA
  IPJ=IJ+1
  IJP=IJ+IB2
  IMJ=IJ-1
  IJM=IJ-IB2
  IPJP=IJP+1
  IJR=INDS(IJ,1)
  IJL=INDS(IJ,2)
  IJT=INDS(IJ,3)

```

```

IJB=INDS(IJ,4)
IJTR=INDS(IJ,5)
RETURN
END

```

```

C -----ITER
SUBROUTINE ITER
INCLUDE 'mfrek.com'
C
LOGICAL MUSTIT
PARAMETER (LMAX=5,OMEGA=1.05)
DO 5 IJ=1,IB2JB2
PN(IJ)=P(IJ)
TGN(IJ)=C1+SIEGN(IJ)/CG
DO 5 K=1,NPHASE
IF (RLK(K,IJ).EQ.0.0) THEN
TLN(K,IJ)=0.0
ELSE
TLN(K,IJ)=C2+SIELN(K,IJ)/CL(K)
ENDIF
5 CONTINUE
MUSTIT=.FALSE.
DO 200 NIT=1,200
DO 100 J=2,JB1
DO 100 I=2,IB1
IJ=I+(J-1)*IB2
IF (IFL(IJ).NE.1) GOTO 100
LOOP=0
KROS=-1
CALL INDXA
CALL RXN
DG=RGF(IJ)-RGPN(IJ)+DTORDR(I)*(RGFR(IJ)-RGFR(IMJ))
1+DTODZ(J)*
1(RGFT(IJ)-RGFT(IJM))
DG=DG-DT*DOTM(1)
ADG=ABS(DG)
DGORIG=ADG
IF(ADG.LE.CONV(IJ)) GOTO 78
MUSTIT=.FALSE.
D3=DG
P3=P(IJ)
IF(NIT.EQ.1)GOTO55
10 IF(D3.GT.0.0)GOTO11
D2=D3
P2=P3
IF(KROS.EQ.-1)KROS=1

```



```

IF(KROS.EQ.0)KROS=2
GOTO12
11  D1=D3
    P1=P3
    IF(KROS.EQ.-1)KROS=0
    IF(KROS.EQ.1)KROS=2
12  IF(KROS.EQ.3)GOTO54
    IF(KROS.EQ.2)GOTO13
    DSN=SIGN(1.,D3)
    DP=-D3*ABETA(IJ)
    IF(-DP*DSN.GT.0.25*P3) DP=-0.25*DSN*P3
    P(IJ)=P(IJ)+DP
    GOTO54
13  P(IJ)=(D1*P2-D2*P1)/(D1-D2)
    ABETA(IJ)=(P1-P2)/(D1-D2)
    KROS=3
54  P3=P(IJ)
55  CONTINUE
    CALL IGIL
    TG(IJ)=C1+SIEG(IJ)/CG
    IF(IHEAT.EQ.0)TG(IJ)=TEMIO(1)
    CALL ROGY(IJ)
    DO 83 K=1,NPHASE
    IF (RLK(K,IJ).EQ.0.0) THEN
    TL(K,IJ)=0.0
    ELSE
    TL(K,IJ)=C2+SIEL(K,IJ)/CL(K)
    ENDIF
    IF(IHEAT.EQ.0)TL(K,IJ)=TEMPIO(K,1)
83  CONTINUE
    RGP(IJ)=TH(IJ)*ROG(IJ)
    CALL MATS
    CALL VELSK
    CALL MASFK
    CALL RXN
78  THX=0.0
    DO 79 K=1,NPHASE
    RLK(K,IJ)=RLKN(K,IJ)-DTORDR(I)*(RLFRK(K,IJ)-RLFRK(K,IMJ))
    1-DTODZ(J)*(RLFTK(K,IJ)-RLFTK(K,IJM))
    RLK(K,IJ)=RLK(K,IJ)+DT*DOTM(K+1)
    IF(RLK(K,IJ).LT.1.D-27)RLK(K,IJ)=0.0
79  THX=THX+RLK(K,IJ)*ARL(K)
    TH(IJ)=1.-THX
    RGP(IJ)=ROG(IJ)*TH(IJ)
    IF(ADG.LE.CONV(IJ))GOTO99

```

```

CALL MASFG
CALL RXN
DG=RGP(IJ)-RGPN(IJ)+DTORDR(I)*(RGFR(IJ)-RGFR(IMJ))+DTODZ(J)*
1(RGFT(IJ)-RGFT(IJM))
DG=DG-DT*DOTM(1)
ADG=ABS(DG)
IF((ADG.LE.CONV(IJ)).AND.(ADG.LT.DGORIG)) GOTO 99
IF((NIT.EQ.1).AND.(LOOP.EQ.0)) DGORIG=ADG
D3=DG
LOOP=LOOP+1
IF((KROS.LT.2).AND.(LOOP.EQ.LMAX)) ABETA(IJ)=.5
1*LMAX*ABETA(IJ)
IF(LOOP.EQ.LMAX) GOTO 99
IF(KROS.EQ.3)CALL NEWP
GOTO10
99 DGG(IJ)=DG
100 CONTINUE
IF(MUSTIT) RETURN
MUSTIT=.TRUE.
IF (NIT.EQ.200) WRITE(6,*)'MAX ITERATION AT TIME = ',TIME
200 CONTINUE
RETURN
END

```

C -----KDRAGG

```

SUBROUTINE KDRAGG(DRAG,VREL)
INCLUDE 'mfrek.com'

```

C

```

DRCOE=0.44
REYN=TH(IJ)*ROG(IJ)*DK(K)*VREL*PHI(K)/VISF
IF(REYN.LT.0.001)REYN=0.001
IF(REYN.LE.1000.0) DRCOE=(24.0/REYN)*(1.0+0.15*REYN**0.687)
DRDVTH=DRCOE*VREL/TH(IJ)**2.65
IF(DRDVTH.LE.1.0D30) THEN
DRAG=0.75*RLK(K,IJ)*DRDVTH*ROG(IJ)*ARL(K)/(DK(K)*PHI(K))
ELSE
DRAG=1.0D30
ENDIF
RETURN
END

```

C -----KDRAGS

```

SUBROUTINE KDRAGS
INCLUDE 'mfrek.com'

```

C

```

DO 130 K=1,NPHASE
DV=(VG(IJ)-VK(K,IJ)+VG(IJM)-VK(K,IJM))*0.5
DU=(UG(IJ)-UK(K,IJ)+UG(IMJ)-UK(K,IMJ))*0.5
VREL=(DU*DU+DV*DV)**0.5
IF(TH(IJ).GE.0.8) THEN
CALL KDRAGG(DRAG,VREL)
ELSE
DENOM=DK(K)*PHI(K)*TH(IJ)
DRAG=(150.0*(1.0-TH(IJ))*VISF/DENOM+1.75*ROG(IJ)*VREL)
1*RLK(K,IJ)/(RL(K)*DENOM)
ENDIF
RKPG(K,IJ)=DRAG*RL(K)/(RL(K)-ROG(IJ))
130 CONTINUE
RETURN
END

```

C -----MASFG

```

SUBROUTINE MASFG
INCLUDE 'mfrek.com'
C
IF(UG(IMJ).GE.0.)THEN
RGFR(IMJ)=UG(IMJ)*RGP(IJL)*RB(I-1)
ELSE
RGFR(IMJ)=UG(IMJ)*RGP(IJ)*RB(I-1)
ENDIF
IF(VG(IJM).GE.0.)THEN
RGFT(IJM)=VG(IJM)*RGP(IJB)
ELSE
RGFT(IJM)=VG(IJM)*RGP(IJ)
ENDIF
ENTRY MASFGA
IF(UG(IJ).GE.0.)THEN
RGFR(IJ)=UG(IJ)*RGP(IJ)*RB(I)
ELSE
RGFR(IJ)=UG(IJ)*RGP(IJR)*RB(I)
ENDIF
IF(VG(IJ).GE.0.)THEN
RGFT(IJ)=VG(IJ)*RGP(IJ)
ELSE
RGFT(IJ)=VG(IJ)*RGP(IJT)
ENDIF
RETURN
END

```

C -----MASFK

```

SUBROUTINE MASFK
INCLUDE 'mfrek.com'
C
DO 10 K=1,NPHASE
IF(UK(K,IMJ).GE.0.)THEN
RLFRK(K,IMJ)=UK(K,IMJ)*RLK(K,IJL)*RB(I-1)
ELSE
RLFRK(K,IMJ)=UK(K,IMJ)*RLK(K,IJ)*RB(I-1)
ENDIF
IF(VK(K,IJM).GE.0.)THEN
RLFTK(K,IJM)=VK(K,IJM)*RLK(K,IJB)
ELSE
RLFTK(K,IJM)=VK(K,IJM)*RLK(K,IJ)
ENDIF
10 CONTINUE
C
ENTRY MASFKA
DO 20 K=1,NPHASE
IF(UK(K,IJ).GE.0.)THEN
RLFRK(K,IJ)=UK(K,IJ)*RLK(K,IJ)*RB(I)
ELSE
RLFRK(K,IJ)=UK(K,IJ)*RLK(K,IJR)*RB(I)
ENDIF
IF(VK(K,IJ).GE.0.)THEN
RLFTK(K,IJ)=VK(K,IJ)*RLK(K,IJ)
ELSE
RLFTK(K,IJ)=VK(K,IJ)*RLK(K,IJT)
ENDIF
20 CONTINUE
RETURN
END
C -----MATS
SUBROUTINE MATS
INCLUDE 'mfrek.com'
CALL RXN
BU1(1)=RUG(IMJ)-DTODRP(I-1)*(P(IJ)-P(IJL))
BV1(1)=RVG(IJM)-DTODZP(J-1)*(P(IJ)-P(IJB))
AU1(1,1)=AR(I-1)*(APP(1,IJL)+RGP(IJL))
1+BR(I-1)*(APP(1,IJ)+RGP(IJ))
AV1(1,1)=AZ(J-1)*(APP(1,IJB)+RGP(IJB))
1+BZ(J-1)*(APP(1,IJ)+RGP(IJ))
AU1(1,1)=AU1(1,1)-DT*DOTM(1)
AV1(1,1)=AV1(1,1)-DT*DOTM(1)
DO 130 K=2,NPHS1
KM1=K-1

```

```

BU1(K)=RUK(KM1,IMJ)
BV1(K)=RVK(KM1,IJM)
DO 110 KK=1,KM1
KS=K*KM1/2+KK
AU1(K,KK)=AR(I-1)*APP(KS,IJL)+BR(I-1)*APP(KS,IJ)
AU1(KK,K)=AU1(K,KK)
AV1(K,KK)=AZ(J-1)*APP(KS,IJB)+BZ(J-1)*APP(KS,IJ)
AV1(KK,K)=AV1(K,KK)
110 CONTINUE
KS=K*(K+1)/2
AU1(K,K)=AR(I-1)*(APP(KS,IJL)+RLK(KM1,IJL))
1+BR(I-1)*(APP(KS,IJ)+RLK(KM1,IJ))
AV1(K,K)=AZ(J-1)*(APP(KS,IJB)+RLK(KM1,IJB))
1+BZ(J-1)*(APP(KS,IJ)+RLK(KM1,IJ))
AU1(K,K)=AU1(K,K)-DT*DOTM(K)
AV1(K,K)=AV1(K,K)-DT*DOTM(K)
130 CONTINUE
ENTRY MATSA
CALL RXN
BU(1)=RUG(IJ)-DTODRP(I)*(P(IJR)-P(IJ))
BV(1)=RVG(IJ)-DTODZP(J)*(P(IJT)-P(IJ))
AU(1,1)=AR(I)*(APP(1,IJ)+RGP(IJ))+BR(I)*(APP(1,IJR)+RGP(IJR))
AV(1,1)=AZ(J)*(APP(1,IJ)+RGP(IJ))+BZ(J)*(APP(1,IJT)+RGP(IJT))
AU(1,1)=AU(1,1)-DT*DOTM(1)
AV(1,1)=AV(1,1)-DT*DOTM(1)
DO 230 K=2,NPHS1
KM1=K-1
BU(K)=RUK(KM1,IJ)
BV(K)=RVK(KM1,IJ)
DO 210 KK=1,KM1
KS=K*KM1/2+KK
AU(K,KK)=AR(I)*APP(KS,IJ)+BR(I)*APP(KS,IJR)
AU(KK,K)=AU(K,KK)
AV(K,KK)=AZ(J)*APP(KS,IJ)+BZ(J)*APP(KS,IJT)
AV(KK,K)=AV(K,KK)
210 CONTINUE
KS=K*(K+1)/2
AU(K,K)=AR(I)*(APP(KS,IJ)+RLK(KM1,IJ))
1+BR(I)*(APP(KS,IJR)+RLK(KM1,IJR))
AV(K,K)=AZ(J)*(APP(KS,IJ)+RLK(KM1,IJ))
1+BZ(J)*(APP(KS,IJT)+RLK(KM1,IJT))
AU(K,K)=AU(K,K)-DT*DOTM(K)
AV(K,K)=AV(K,K)-DT*DOTM(K)
230 CONTINUE
C

```

```

RETURN
END
C -----MULTI
  SUBROUTINE MULTI
  INCLUDE 'mfrek.com'
  KS=1
  DO 100 K=1,NPHASE
C  CALCULATE PARTICLE TO PARTICLE INTERACTION
  KS=KS+1
  APP(KS,IJ)=-RKPG(K,IJ)*DT
  DO 98 KK=1,K-1
  KS=KS+1
  DV=(VK(K,IJ)-VK(KK,IJ)+VK(K,IMJ)-VK(KK,IMJ))*0.5
  DU=(UK(K,IJ)-UK(KK,IJ)+UK(K,IMJ)-UK(KK,IMJ))*0.5
  VREL=(DU*DU+DV*DV)**0.5
98  APP(KS,IJ)=-RLK(K,IJ)*RLK(KK,IJ)*DKF(K,KK)*VREL
100  KS=KS+1
  DO 105 K=1,NPHS1
  SUM=0.0
  DO 101 KK=1,K-1
  KS=K*(K-1)/2+KK
101  SUM=SUM+APP(KS,IJ)
  DO 102 KK=K+1,NPHS1
  KS=KK*(KK-1)/2+K
102  SUM=SUM+APP(KS,IJ)
  KS=K*(K+1)/2
105  APP(KS,IJ)=-SUM
  RETURN
  END
C -----NEWP
  SUBROUTINE NEWP
  INCLUDE 'mfrek.com'
C
  IF(D1.NE.D3) THEN
  PA=(D1*P3-D3*P1)/(D1-D3)
  ELSE
  PA=0.5*(P2+P3)
  ENDIF
  IF(D2.NE.D3) THEN
  PB=(D2*P3-D3*P2)/(D2-D3)
  ELSE
  PB=0.5*(P1+P3)
  ENDIF
  IF(D1*D3.GT.0.) THEN
  IF(PA.LT.P2.OR.PA.GT.P3)PA=0.5*(P2+P3)

```

```

ELSE
IF(PB.LT.P3.OR.PB.GT.P1)PB=0.5*(P1+P3)
ENDIF
P(IJ)=0.5*(PA+PB)
RETURN
END

```

C -----PROD

```

SUBROUTINE PROD
INCLUDE 'mfrek.com'
TMASSG=0.0
TMASSS=0.0
DO 10 J=1,JB2
KI=0
DO 9 JX=1,JXN
AYM(JX,J)=0.0
9 AYMOL(JX,J)=0.0
FLUX(J)=0.0

DO 20 I=2,IB2-1
IJ=I+(J-1)*IB2
IF(IFL(IJ).EQ.3)GOTO 20

CALL ROGY(IJ)
WMO=0.0
DO 7 JX=1,JXN
7 WMO=WMO+Y(1,JX,IJ)/WM(JX)
DO 8 JX1=1,JXN
AYM(JX1,J)=AYM(JX1,J)+TH(IJ)*ROG(IJ)*VG(IJ)
1*Y(1,JX1,IJ)*DR(I)*THICK
YMOL(JX1,IJ)=Y(1,JX1,IJ)/WM(JX1)/WMO
8 AYMOL(JX1,J)=AYMOL(JX1,J)+YMOL(JX1,IJ)
KI=KI+1
FLUX(J)=FLUX(J)+TH(IJ)*ROG(IJ)*VG(IJ)*DR(I)*THICK
IF(J.EQ.1.OR.J.EQ.JB2)GOTO 20
TMASSG=TMASSG+TH(IJ)*ROG(IJ)*DR(I)*DZ(J)*THICK
TMASSS=TMASSS+RLK(1,IJ)*DR(I)*DZ(J)*THICK
20 CONTINUE
DO 11 JX=1,JXN
AYM(JX,J)=AYM(JX,J)/KI
11 AYMOL(JX,J)=AYMOL(JX,J)/KI
WMO=0.0
DO 12 JX=1,JXN
12 WMO=WMO+AYM(JX,J)/WM(JX)
DO 13 JX=1,JXN
IF(WMO.EQ.0.0)THEN

```

```

    AYMOL1(JX,J)=AYMOL(JX,J)
    ELSE
    AYMOL1(JX,J)=AYM(JX,J)/WM(JX)/WMO
    ENDIF
13  CONTINUE
10  CONTINUE

    AMIX(1)=TMASSG
    AMIX(2)=TMASSS
    AMIX(3)=FLUX(1)
    AMIX(4)=FLUX(JB2)
    DO 15 JX=1,JXN
15  AMIX(4+JX)=AYMOL(JX,JB2)
    DO 16 JX=1,JXN
16  AMIX(10+JX)=AYMOL1(JX,JB2)
    AMIX(17)=TIME
    RETURN
    END
C -----PROG
    SUBROUTINE PROG
    INCLUDE 'mfrek.com'
C
    TDUMP1=TIME
    TPRI=TIME
C SPECIAL APPLICATION
    VJET=4.012
C END
1  CONTINUE
    CALL BDRY
C SPECIAL APPLICATION
    CALL PROD
C END
    TPDT=TIME+0.1*DT
    IF(TPDT.GE.TPRI) THEN
    TPRI=TPRI+TPR
    IF(TIME.GE.0.0)THEN
    WRITE(6,547)TIME
    DO 600 K=1,NPHASE
    IF(KIN(K).EQ.1)THEN
    WRITE(6,*)
    WRITE(6,*)'VISCOSITY',K
    WRITE(6,*)
    DO 323 IJ=IB2JB2,IB2,-IB2
323 WRITE(6,550)(VISCL(1,IL),IL=IJ-IB1,IJ)
    WRITE(6,*)

```



```

WRITE(6,*)'P-SOLID',K
WRITE(6,*)
DO 322 IJ=IB2JB2,IB2,-IB2
322 WRITE(6,550)(PS(1,IL),IL=IJ-IB1,IJ)
WRITE(6,*)
WRITE(6,*)'GRANULAR TEMPERATURE',K
WRITE(6,*)
DO 324 IJ=IB2JB2,IB2,-IB2
324 WRITE(6,550)(TSK(1,IL),IL=IJ-IB1,IJ)
ENDIF
600 CONTINUE
WRITE(6,548)
DO 325 IJ=IB2JB2,IB2,-IB2
325 WRITE(6,550)(P(IL),IL=IJ-IB1,IJ)
DO 328 K=1,NPHASE
WRITE(6,549)K
DO 328 IJ=IB2JB2,IB2,-IB2
328 WRITE(6,550)(RLK(K,IL)*ARL(K),IL=IJ-IB1,IJ)
WRITE(6,551)
DO 331 IJ=IB2JB2,IB2,-IB2
331 WRITE(6,550)(TH(IL),IL=IJ-IB1,IJ)
WRITE(6,552)
DO 332 IJ=IB2JB2,IB2,-IB2
332 WRITE(6,550)(VG(IL),IL=IJ-IB1,IJ)
WRITE(6,553)
DO 333 IJ=IB2JB2,IB2,-IB2
333 WRITE(6,550)(UG(IL),IL=IJ-IB1,IJ)
DO 337 K=1,NPHASE
WRITE(6,556)K
DO 336 IJ=IB2JB2,IB2,-IB2
336 WRITE(6,550)(VK(K,IL),IL=IJ-IB1,IJ)
WRITE(6,557)K
DO 337 IJ=IB2JB2,IB2,-IB2
337 WRITE(6,550)(UK(K,IL),IL=IJ-IB1,IJ)
IF(IHEAT.EQ.1)THEN
WRITE(6,554)
DO 338 IJ=IB2JB2,IB2,-IB2
338 WRITE(6,550)(TG(IL),IL=IJ-IB1,IJ)
DO 339 K=1,NPHASE
WRITE(6,555)K
DO 339 IJ=IB2JB2,IB2,-IB2
339 WRITE(6,550)(TL(K,IL),IL=IJ-IB1,IJ)
ENDIF
C SPECIAL APPLICATION
C OUTPUT COMPOSITIONS (AIR PRODUCTS CASE) (OPTIONAL)

```

```

C   WRITE(6,*)'CO'
C   DO 335 IJ=IB2JB2,IB2,-IB2
C335 WRITE(6,550)(YMOL(1,IL),IL=IJ-IB1,IJ)
C   WRITE(6,*)'CO2'
C   DO 400 IJ=IB2JB2,IB2,-IB2
C400 WRITE(6,550)(YMOL(2,IL),IL=IJ-IB1,IJ)
C   WRITE(6,*)'H2'
C   DO 401 IJ=IB2JB2,IB2,-IB2
C401 WRITE(6,550)(YMOL(3,IL),IL=IJ-IB1,IJ)
C   WRITE(6,*)'N2'
C   DO 402 IJ=IB2JB2,IB2,-IB2
C402 WRITE(6,550)(YMOL(6,IL),IL=IJ-IB1,IJ)
C   WRITE(6,*)'CH3OH'
C   DO 403 IJ=IB2JB2,IB2,-IB2
C403 WRITE(6,550)(YMOL(5,IL),IL=IJ-IB1,IJ)
C   WRITE(6,*)'CH3OH IN LIQUID PHASE (KMOLE/M3)'
C   DO 404 IJ=IB2JB2,IB2,-IB2
C404 WRITE(6,550)(Y(3,5,IL)*1000.0*.70025/WM(5),IL=IJ-IB1,IJ)
C   WRITE(6,*)'H2O IN LIQUID PHASE'
C   DO 405 IJ=IB2JB2,IB2,-IB2
C405 WRITE(6,550)(Y(3,6,IL),IL=IJ-IB1,IJ)
C END
      ENDIF
      ENDIF
      IF(TPDT.GT.TSTOP.OR.TPDT.GT.TDUMP1) THEN
        CALL TAPEWR
        REWIND(9)
C SPECIAL APPLICATION
C GRADULLY INCREASE THE JET VELOCITIES
      IF(ITD.NE.2)THEN
        VJET=VJET+VJET
        IF(VJET.GE.80.24)VJET=80.24
        VG(3)=VJET
        VG(8)=VJET
        VG(13)=VJET
      ENDIF
      WRITE(6,100)AMIX(17),(AMIX(J),J=1,4),AMIX(17)
100  FORMAT(6(G11.5))
C END
      TDUMP1=TDUMP1+TDUMP
      ENDIF
      IF(TPDT.LT.TSTOP) THEN
        TIME=TIME+DT
        CALL TILDE
        CALL BETAS

```

```

CALL ITER
DO 11 KNN=1,NPHASE
IF(KIN(KNN).EQ.1)CALL GRNVIS
11 CONTINUE
CALL ICONV
IF(IRXN.EQ.1)CALL COMPOS
GOTO 1
ENDIF
RETURN
547 FORMAT(1X,/,1X,'@ TIME =',G10.3)
548 FORMAT(1X/,1X,'P',/)
549 FORMAT(1X/,1X,'TH',I1,/)
550 FORMAT(6(1X,G11.4))
551 FORMAT(1X/,1X,'THETA',/)
552 FORMAT(1X/,1X,'VG',/)
553 FORMAT(1X/,1X,'UG',/)
554 FORMAT(1X/,1X,'TG',/)
555 FORMAT(1X/,1X,'T',I1,/)
556 FORMAT(1X/,1X,'V',I1,/)
557 FORMAT(1X/,1X,'U',I1,/)
END

```

```

C -----QESOL
SUBROUTINE QESOL(AP0,AP1,AP2,XSOL)
IMPLICIT REAL*8(A-H,O-Z)
C
C SOLVE QUADRATIC EQUATION
C
C SCALING OF COEFFICIENTS
AAP0=ABS(AP0)
AAP1=ABS(AP1)
AAP2=ABS(AP2)
APMAX=AAP2
IF(APMAX.LT.AAP1)APMAX=AAP1
IF(APMAX.LT.AAP0)APMAX=AAP0
AP0=AP0/APMAX
AP1=AP1/APMAX
AP2=AP2/APMAX
C
ENTRY QESOL1(AP0,AP1,AP2,XSOL)
IF(AP0.EQ.0.0)THEN
IF(AP2.EQ.0.0)THEN
XSOL=0.0
ELSE
XSOL=-AP1/AP2

```

```

IF(XSOL.LT.0.0)XSOL=0.0
ENDIF
ELSE
IF(AP1.EQ.0.0)THEN
IF(AP2.EQ.0.0)THEN
XSOL=0.0
ELSE
DISC=-AP0/AP2
IF(DISC.LE.0.0)THEN
XSOL=0.0
ELSE
XSOL=DISC**0.5
ENDIF
ENDIF
ELSE
IF(AP2.EQ.0.0)THEN
XSOL=-AP0/AP1
IF(XSOL.LT.0.0)XSOL=0.0
ELSE
GOTO 10
ENDIF
ENDIF
ENDIF
RETURN

```

```

C
10 ENTRY QESOL2(AP0,AP1,AP2,XSOL)
CONTINUE
SAP1=AP1*AP1
DISC=SAP1-4.0*AP0*AP2
IF(DISC.LT.-1.E-4*SAP1)THEN
XSOL=0.0
ELSE
IF(DISC.LT.0.0)DISC=0.0
IF(AP1.LT.0.0)THEN
XSOL=(-AP1+DISC**0.5)/(2.0*AP2)
ELSE
XSOL=-2.0*AP0/(AP1+DISC**0.5)
ENDIF
ENDIF
RETURN
END

```

```

C -----QFLUX
SUBROUTINE QFLUX
INCLUDE 'mfrek.com'

```

```

DO 5 K=1,LT
5  QFLOW(K)=0.0
   IF(IHEAT.EQ.0)RETURN
   QFL=QF(IJM)+QF(IMJ)+QF(IPJ)+QF(IJP)
   IF(TOB(IJM).NE.0.0)QFLOW(1)=(QFL-(COE(IJM)*(TG(IJ)-TOB(IJM))
   1/DZ(J)))*TH(IJ)
   IF(TOB(IMJ).NE.0.0)QFLOW(1)=(QFL-(COE(IMJ)*(TG(IJ)-TOB(IMJ))
   1/DR(I)))*TH(IJ)
   IF(TOB(IPJ).NE.0.0)QFLOW(1)=(QFL-(COE(IPJ)*(TG(IJ)-TOB(IPJ))
   1/DR(I)))*TH(IJ)
   IF(TOB(IJP).NE.0.0)QFLOW(1)=(QFL-(COE(IJP)*(TG(IJ)-TOB(IJP))
   1/DZ(J)))*TH(IJ)
   DO 10 K=2,LT
   IF(TOB(IJM).NE.0.0)QFLOW(K)=(QFL-(COE(IJM)*(TL(K-1,IJ)-TOB(IJM))
   1/DZ(J))*RLK(K-1,IJ)*ARL(K-1)
   IF(TOB(IMJ).NE.0.0)QFLOW(K)=(QFL-(COE(IMJ)*(TL(K-1,IJ)-TOB(IMJ))
   1/DR(I))*RLK(K-1,IJ)*ARL(K-1)
   IF(TOB(IPJ).NE.0.0)QFLOW(K)=(QFL-(COE(IPJ)*(TL(K-1,IJ)-TOB(IPJ))
   1/DR(I))*RLK(K-1,IJ)*ARL(K-1)
   IF(TOB(IJP).NE.0.0)QFLOW(K)=(QFL-(COE(IJP)*(TL(K-1,IJ)-TOB(IJP))
   1/DZ(J))*RLK(K-1,IJ)*ARL(K-1)
10  CONTINUE
20  RETURN
   END

```

C -----QRXN

```

   SUBROUTINE QRXN
C  CALCULATE THE HEAT GENERATION DUE TO REACTIONS
   INCLUDE 'mfrek.com'
   IF(IRXN.EQ.0)RETURN
   CALL RRATE
   DO 10 K=1,LT
   QGEN(K)=0.0
   DO 15 IX=1,IHO(K)
15  QGEN(K)=QGEN(K)+RHO(K,IX)*HHO(K,IX)
   IF(K.NE.1)THEN
   DO 20 IX=1,IHE(K)
20  QGEN(K)=QGEN(K)+RHE(K,IX)*HHE(K,IX)
   ENDIF
10  CONTINUE
   RETURN
   END

```

C -----RHEATS

```

   SUBROUTINE RHEATS
   INCLUDE 'mfrek.com'

```

```

C
C INTERPASE HEAT TRANSFER COEFFICIENT
C
DO 10 K=1,NPHASE
SP=RLK(K,IJ)*(6./DK(K))*ARL(K)
DV=(VG(IJ)-VK(K,IJ)+VG(IJM)-VK(K,IJM))*0.5
DU=(UG(IJ)-UK(K,IJ)+UG(IMJ)-UK(K,IMJ))*0.5
VREL=SQRT(DU*DU+DV*DV)
REYN=DK(K)*VREL*ROG(IJ)/VISF
PR=CG*VISF/AKG(IJ)
C GUNN MODEL
CRPR=PR**(1./3.)
IF (TH(IJ) .GE. 0.8) THEN
IF(REYN.LE.200.)THEN
PNU=(2.+1.1*REYN**.6*CRPR)*SP
ELSEIF(REYN.LE.2000.)THEN
PNU=.123*(4.*REYN/DK(K))**.83*SP**.17
ELSE
PNU=.61*REYN**.67*SP
ENDIF
ELSE
IF(REYN.LE.200.)THEN
PNU=(2.+0.16*REYN**0.67)*SP
ELSEIF(REYN.LE.1000.)THEN
PNU=8.2*REYN**0.6*SP
ELSE
PNU=1.06*REYN**0.457*SP
ENDIF
ENDIF
RHEAT(K,IJ)=PNU*AKG(IJ)/DK(K)
10 CONTINUE
RETURN
END
C -----ROGY
SUBROUTINE ROGY(MIJ)
C CALCULATE GAS DENSITY
INCLUDE 'mfrek.com'
IF(IRXN.EQ.1)THEN
WMY=0.0
DO 10 JX=1,JXN
10 WMY=WMY+Y(1,JX,MIJ)/WM(JX)
WMY=1.0/WMY
ELSE
WMY=WMYGAS
ENDIF

```

```

ROG(MIJ)=P(MIJ)*WMY/(C17*TG(MIJ)+C18*P(MIJ))
RETURN
END

```

C

C

C

-----RRATE

SUBROUTINE RRATE

C DEFINE THE RATE OF REACTIONS AND HEAT OF REACTIONS

```

INCLUDE 'mfrek.com'
IF(IRXN.EQ.0)RETURN
DO 20 MK=1,LT
DO 10 IX=1,IHO(MK)
10 RHO(MK,IX)=0.0
DO 20 IX=1,IHE(MK)
20 RHE(MK,IX)=0.0
TMO=0.0
DO 30 JX=1,JXN
30 TMO=TMO+YN(1,JX,IJ)/WM(JX)
PATM=P(IJ)*1D-6
PH2=PATM*YN(1,3,IJ)/WM(3)/TMO
PCO=PATM*YN(1,1,IJ)/WM(1)/TMO
PME=PATM*YN(1,5,IJ)/WM(5)/TMO
T=TG(IJ)
IF(T.LE.430.)T=430.0
IF(T.GE.630.)T=630.0
IF(PH2.EQ.0.0.OR.PCO.EQ.0.0)THEN
RHO(1,1)=0.0
ELSE
RK0=8.93D-8*RLK(1,IJ)

```

C TE CHANG'S KEQ MODEL CORRECTED BY THE DATA FROM DME REPORT

```

C RKEQ=1420.8*EXP(21.225+9143.6/T-7.492*LOG(T))
C 1+4.076D-3 *T-7.161D-8*T*T)
RKEQ=6.249/PATM**2
RHO(1,1)=RK0*PCO**(1.0/3.0)*PH2**(2.0/3.0)
1*(1-PME/PCO/PH2**2.0/RKEQ)
DTO=RGPN(IJ)*TMO
CCO=RGPN(IJ)*YN(1,1,IJ)/WM(1)
CH2=RGPN(IJ)*YN(1,3,IJ)/WM(3)
CME=RGPN(IJ)*YN(1,5,IJ)/WM(5)
C CALL SOLUTION(RKEQ,DTO,CCO,CH2,CME,RHOX)
C RHOX=RHOX/DT
IF(RHO(1,1)*DT.GE.MIN(CCO,2*CH2))
1RHO(1,1)=0.1*MIN(CCO,2*CH2)/DT

```

```

C   RHO(1,1)=1.98D7*EXP(-RT1)*(PH2**0.4)*(PCO**0.13)
C   1-2.15D10*EXP(-RT2)*(PME**0.13)
C   RHO(1,1)=RHO(1,1)*RLK(1,IJ)/3.6D6
C   CLM=YN(3,5,IJ)*0.70025/WM(5)
C   HME=1.49D6*EXP(-17235.0/8.314/TG(IJ))
C   CLGM=10.0*PME/HME
C   RHE(3,1)=1.2*(CLGM-CLM)*RLK(2,IJ)/0.70025
C   IF(RHE(3,1).LE.0.0)RHE(3,1)=0.0
C   IF(RHO(1,1).LE.0.0)RHO(1,1)=0.0

```

```

ENDIF

```

```

HHO(1,1)=-8.314D8*T*T*(-9143.6/T/T-7.492/T
1+4.076D-3-7.161D-8*T*2)

```

```

RETURN

```

```

END

```

```

C -----RXN

```

```

SUBROUTINE RXN

```

```

C CALCULATE PHASE CHANGES

```

```

INCLUDE 'mfrek.com'

```

```

IF(IRXN.EQ.0)RETURN

```

```

CALL RRATE

```

```

DOTM(1)=0.0

```

```

DO 10 K=2,LT

```

```

DOTM(K)=0.0

```

```

DO 20 JX=1,JXN

```

```

DO 20 IX=1,IHE(K)

```

```

20 DOTM(K)=DOTM(K)+RHE(K,IX)*WM(JX)*AHE(K,IX,JX)

```

```

DOTM(1)=DOTM(1)-DOTM(K)

```

```

10 CONTINUE

```

```

RETURN

```

```

END

```

```

C -----SETUP

```

```

SUBROUTINE SETUP

```

```

INCLUDE 'mfrek.com'

```

```

C

```

```

WRITE(6,660)

```

```

DO 1 I=1,IB1

```

```

DRP(I)=0.5*(DR(I)+DR(I+1))

```

```

RDR(I)=1.0/DR(I)

```

```

RDRP(I)=2.0/(DR(I)+DR(I+1))

```

```

AR(I)=0.5*DR(I+1)*RDRP(I)

```

```

1 BR(I)=1.0-AR(I)

```

```

DRP(IB2)=DR(IB2)

```

```

RDR(IB2)=1.0/DR(IB2)

```

```

RDRP(IB2)=RDR(IB2)

```



```

AR(IB2)=0.5
BR(IB2)=0.5
DO 2 J=1,JB1
DZP(J)=0.5*(DZ(J)+DZ(J+1))
RDZ(J)=1.0/DZ(J)
RDZP(J)=2.0/(DZ(J)+DZ(J+1))
AZ(J)=0.5*DZ(J+1)*RDZP(J)
2  BZ(J)=1.0-AZ(J)
DZP(JB2)=DZ(JB2)
RDZ(JB2)=1.0/DZ(JB2)
RDZP(JB2)=RDZ(JB2)
AZ(JB2)=0.5
BZ(JB2)=0.5
IF(ITC.EQ.0) GO TO 5
RTC=RST-0.5*DR(1)
RTB=RST
R(1)=RTC**ITC
RB(1)=RTB**ITC
IF((RTC.LE.0.).AND.(ITC.EQ.2))R(1)=-R(1)
IF (RB(1).LT.1.D-8) THEN
RRB(1)=0.0
ELSE
RRB(1)=1.0/RB(1)
ENDIF
DO 3 I=2,IB2
RTC=RTB+0.5*DR(I)
RTB=RTB+DR(I)
R(I)=RTC**ITC
RB(I)=RTB**ITC
RRB(I)=1./RB(I)
3  CONTINUE
GOTO 10
5  CONTINUE
DO 8 I=1,IB2
R(I)=1.
RB(I)=1.
RRB(I)=1.
8  CONTINUE
10 CONTINUE
DO 11 I=1,IB2
RRIDR(I)=RDR(I)/R(I)
RRIDRP(I)=RRB(I)*RDRP(I)
DTODR(I)=DT*RDR(I)
DTODRP(I)=DT*RDRP(I)
DTORDR(I)=DT*RRIDR(I)

```

```

      DTOBDR(I)=DT*RRIDRP(I)
11  CONTINUE
      DO 12 J=1,JB2
      DTODZ(J)=DT*RDZ(J)
12  DTODZP(J)=DT*RDZP(J)
      DO 15 IJ2=IB2JB2,IB2,-IB2
      IJ1=IJ2-IB1
15  WRITE(6,650)(IFL(IKPR),IKPR=IJ1,IJ2)
C
      WRITE(6,660)
C  INITIALIZE SOLID PRESSURE AND COHESIVE STRENGTH
      DO 20 I=0,1000
      THX=I/1000.
      COHF(I)=10.**(-10.6*THX+5.5)
C  COHF(I)=0.0
C20  GTH(I)=10.**(-8.76*THX+8.49)
20  GTH(I)=10.**(-10.466*THX+8.577)
C  INITIALIZE 'INDS'
      DO 30 J=2,JB1
      DO 30 I=2,IB1
      IJ=I+(J-1)*IB2
      IPJ=IJ+1
      IJR=IPJ
      IJP=IJ+IB2
      IJT=IJP
      IMJ=IJ-1
      IJL=IMJ
      IJM=IJ-IB2
      IJB=IJM
      IPJP=IJP+1
      IJTR=IPJP
      IF((IFL(IPJ).EQ.2).OR.(IFL(IPJ).EQ.3)) IJR=IJ
      IF((IFL(IMJ).EQ.2).OR.(IFL(IMJ).EQ.3)) IJL=IJ
      IF((IFL(IJP).EQ.2).OR.(IFL(IJP).EQ.3)) IJT=IJ
      IF((IFL(IJM).EQ.2).OR.(IFL(IJM).EQ.3)) IJB=IJ
      IF(IJ.EQ.(IB2JB1-1))IJTR=IJ
21  GOTO (29,21,21,29,29,29,29),IFL(IPJP)
22  GOTO (22,24,24,22,22,22,22),IFL(IJP)
23  GOTO (25,26,26,25,25,25,25),IFL(IPJ)
24  GOTO (28,25,25,28,28,28,28),IFL(IPJ)
25  IJTR=IJ
      GOTO 29
26  IJTR=IJP
      GOTO 29
28  IJTR=IPJ

```

```

29  CONTINUE
    INDS(IJ,1)=IJR
    INDS(IJ,2)=IJL
    INDS(IJ,3)=IJT
    INDS(IJ,4)=IJB
    INDS(IJ,5)=IJTR
30  CONTINUE
    DO 40 K=1,NPHASE
    DO 40 KK=1,K-1
40  DKF(K,KK)=FAC*DT*(DK(K)+DK(KK))**2/(RL(K)*
    1DK(K)**3+RL(KK)*DK(KK)**3)
    IF(ITD.NE.2)THEN
    DO 60 N=1,NO
    DO 60 J=IOB(3,N),IOB(4,N)
    JJ=(J-1)*IB2
    DO 60 I=IOB(1,N),IOB(2,N)
    IJ=I+JJ
    IF((IFL(IJ).EQ.2).OR.(IFL(IJ).EQ.3))GOTO 60
    P(IJ)=PIO(N)
    TG(IJ)=TEMIO(N)
    TH(IJ)=THIO(N)
    THN(IJ)=TH(IJ)
    UG(IJ)=UIO(N)
    VG(IJ)=VIO(N)
    DO 56 K=1,NPHASE
    IF(KIN(K).EQ.1)TSK(K,IJ)=FSKIO(K,N)
    TL(K,IJ)=TEMPIO(K,N)
    UK(K,IJ)=UPIO(K,N)
    VK(K,IJ)=VPIO(K,N)
    RLK(K,IJ)=RL(K)*THPIO(K,N)
56  RLKN(K,IJ)=RLK(K,IJ)
    DO 55 K=1,LT
    DO 55 JX=1,JXN
    YN(K,JX,IJ)=YIO(K,JX,N)
55  Y(K,JX,IJ)=YIO(K,JX,N)
    CALL ROGY(IJ)
    RGP(IJ)=ROG(IJ)*TH(IJ)
60  CONTINUE
    ENDIF
    DO 65 J=2,JB1
    DO 65 I=2,IB1
    IJ=I+(J-1)*IB2
    IF((IFL(IJ).EQ.2).OR.(IFL(IJ).EQ.3))GOTO 65
    CALL INDXA

```

C INITIAL BED PRESSURE

```

IF(ITD.NE.2)THEN
IF(IPRE.NE.0)THEN
IF(IJ.EQ.IJB)THEN
IF(IJ.NE.IJL)THEN
CALL ROGY(IJL)
CC=ROG(IJL)
RLXSUM=TH(IJL)*CC
DO 61 K=1,NPHASE
61  RLXSUM=RLXSUM+RLK(K,IJL)
P(IJ)=P(IJL)+GRAVX*DR(I)*RLXSUM
ENDIF
ELSE
CALL ROGY(IJB)
CC=ROG(IJB)
RLXSUM=TH(IJB)*CC
DO 62 K=1,NPHASE
62  RLXSUM=RLXSUM+RLK(K,IJB)
P(IJ)=P(IJB)+GRAVY*DZ(J)*RLXSUM
ENDIF
ENDIF
ENDIF

C
CALL CNVERT
CALL MASFGA
CALL MASFKA
THN(IJ)=TH(IJ)
TG(IJ)=C1+SIEG(IJ)/CG
IF(IHEAT.EQ.0)TG(IJ)=TEMIO(1)
CALL ROGY(IJ)
DO 63 K=1,NPHASE
IF (RLK(K,IJ).EQ.0.0) THEN
TL(K,IJ)=0.0
ELSE
TL(K,IJ)=C2+SIEL(K,IJ)/CL(K)
ENDIF
IF(IHEAT.EQ.0)TL(K,IJ)=TEMPIO(K,1)
CALL THRCON
TSKN(K,IJ)=TSK(K,IJ)
IF(KIN(K).EQ.1)CALL GRPROP
63  RLKN(K,IJ)=RLK(K,IJ)
CALL KDRAGS
CALL MULTI
CALL RHEATS
65  CONTINUE
650  FORMAT(1X,78I1)

```

C -----SIELF

SUBROUTINE SIELF  
INCLUDE 'mfrek.com'

C  
C CALCULATES FLUXES OF SPECIFIC INTERNAL  
C ENERGY DENSITY OF THE LIQ.  
C

IF(UK(K,IJ).GE.0.)THEN  
ELFR(K)=RLK(K,IJ)\*SIELN(K,IJ)\*UK(K,IJ)\*RB(I)  
ELSE  
ELFR(K)=RLK(K,IJR)\*SIELN(K,IJR)\*UK(K,IJ)\*RB(I)  
ENDIF

IF(VK(K,IJ).GE.0.)THEN  
ELFT(K)=RLK(K,IJ)\*SIELN(K,IJ)\*VK(K,IJ)  
ELSE  
ELFT(K)=RLK(K,IJT)\*SIELN(K,IJT)\*VK(K,IJ)  
ENDIF

IF(IFL(IMJ).NE.1)GOTO 1  
IF(IFL(IJM).NE.1)GOTO 2  
CALL HEATLB  
GOTO 4

1 IF(UK(K,IMJ).GE.0.)THEN  
ELFL(K)=RLK(K,IJL)\*SIELN(K,IJL)\*UK(K,IMJ)\*RB(I-1)  
ELSE  
ELFL(K)=RLK(K,IJ)\*SIELN(K,IJ)\*UK(K,IMJ)\*RB(I-1)  
ENDIF

IF(IFL(IJM).NE.1)GOTO 2  
CALL HEATLA  
GOTO 3

2 IF(VK(K,IJM).GE.0.)THEN  
ELFB(K,I)=RLK(K,IJB)\*SIELN(K,IJB)\*VK(K,IJM)  
ELSE  
ELFB(K,I)=RLK(K,IJ)\*SIELN(K,IJ)\*VK(K,IJM)  
ENDIF

CALL HEATCL  
ELFB(K,I)=ELFB(K,I)-HFLB(K,I)  
IF(IFL(IMJ).EQ.1)GOTO 4

3 ELFL(K)=ELFL(K)-HFL(L,K)

4 ELFT(K)=ELFT(K)-HFLT(K)  
ELFR(K)=ELFR(K)-HFLR(K)

RETURN  
END

C -----SOLUTION

C NOT IN USE

SUBROUTINE SOLUTION(DK,DTO,C1,C2,C3,X)

```

A=C1
IF(C1.GE.2*C2)A=C2/2.0
B=-C3
C UNDERFLOW
COEM=1.0/(C3+A)
FA=COEM*DK*(C1-A)*(C2-2*A)*(C2-2*A)-
1COEM*(C3+A)*(DIO-2*A)*(DIO-2*A)
FB=COEM*DK*(C1-B)*(C2-2*B)*(C2-2*B)-
1COEM*(C3+B)*(DIO-2*B)*(DIO-2*B)
1 X=(A+B)/2.0
FX=COEM*DK*(C1-X)*(C2-2*X)*(C2-2*X)-
1COEM*(C3+X)*(DIO-2*X)*(DIO-2*X)
IF(ABS(FX/COEM).LE.1D-20)GOTO 10
IF(FX.LT.0.0)THEN
A=X
ELSE
B=X
ENDIF
GOTO 1
10 RETURN
END
C -----TAPERD
SUBROUTINE TAPERD
INCLUDE 'mfrek.com'
C
READ(9)TIME,TTIM
READ(9) (P(IJ),TH(IJ),UG(IJ),VG(IJ),TG(IJ),IJ=1,IB2JB2)
READ(9)((RLK(K,IJ),UK(K,IJ),VK(K,IJ),TL(K,IJ),
1TSK(K,IJ),TSKN(K,IJ),K=1,NPHASE),IJ=1,IB2JB2)
READ(9)((Y(K,JX,IJ),K=1,LT),JX=1,JXN),IJ=1,IB2JB2)
READ(9)((YN(K,JX,IJ),K=1,LT),JX=1,JXN),IJ=1,IB2JB2)
RETURN
END
C -----TAPEWR
SUBROUTINE TAPEWR
INCLUDE 'mfrek.com'
REWIND(9)
C
WRITE(9)TIME,TTIM
WRITE(9) (P(IJ),TH(IJ),UG(IJ),VG(IJ),TG(IJ),IJ=1,IB2JB2)
WRITE(9)((RLK(K,IJ),UK(K,IJ),VK(K,IJ),TL(K,IJ),
1TSK(K,IJ),TSKN(K,IJ),K=1,NPHASE),IJ=1,IB2JB2)
WRITE(9)((Y(K,JX,IJ),K=1,LT),JX=1,JXN),IJ=1,IB2JB2)
WRITE(9)((YN(K,JX,IJ),K=1,LT),JX=1,JXN),IJ=1,IB2JB2)
C WRITE(6,*)'TIME=',TIME

```

RETURN  
END

C -----THRCON

SUBROUTINE THRCON  
INCLUDE 'mfrek.com'  
PARAMETER (PIC=7.26D-3,RKP=0.3289,RKG=0.0269)  
PARAMETER (APIC=1.-PIC,RF=RKP/RKG)

C

C DAMKOHLER'S EQUIVALENT THERMAL CONDUCTIVITY

C

IF (TH(IJ).LT.0.99) THEN  
BB=1.25\*((1.0-TH(IJ))/TH(IJ))\*\*(10./9.)  
CC=1.0-BB/RF  
RKO=(2./CC)\*(BB\*(RF-1.)/(CC\*CC\*RF)\*DLOG(RF/BB)-(BB-1.)/CC  
1-(BB+1.)/2.)  
A3=SQRT(1.0-TH(IJ))  
AKL(K,IJ)=(1.-A3)+A3\*(PIC\*RF+APIC\*RKO)\*AKG(IJ)  
ELSEIF (TH(IJ).EQ.1.0) THEN  
AKL(K,IJ)=0.0  
ELSE  
AKL(K,IJ)=AKG(IJ)  
ENDIF  
RETURN  
END

C -----TILDE

SUBROUTINE TILDE  
INCLUDE 'mfrek.com'

C

DO 10 J=2,JB1  
DO 10 I=2,IB1  
IJ=I+(J-1)\*IB2  
IF (IFL(IJ).NE.1) GOTO 10  
CALL INDX  
CALL UGMOMF  
IGKU=(AR(I)\*TH(IJ)+BR(I)\*TH(IJR))\*1000  
IGKV=(AZ(J)\*TH(IJ)+BZ(J)\*TH(IJT))\*1000  
IGJ=TH(IJ)\*1000  
IGT=TH(IJT)\*1000  
IGR=TH(IJR)\*1000  
RUG(IJ)=(AR(I)\*RGP(IJ)+BR(I)\*RGP(IJR))\*(UG(IJ)+GRAVX\*DT)  
1-DTOBDR(I)\*(UGFR-UGFL)-DTODZ(J)\*(UGFT-UGFB(I))-DT\*SUGC\*ITC  
UGFL=UGFR  
UGFB(I)=UGFT  
CALL VGMOMF  
RVG(IJ)=(AZ(J)\*RGP(IJ)+BZ(J)\*RGP(IJT))\*(VG(IJ)+GRAVY\*DT)

```

DO 20 I=2,IB1
  IJ=I+(J-1)*IB2
  IF(IFL(IJ).NE.1) GOTO 20
  CALL INDXA
  CALL MATSA
  CALL VELSK2
  CALL MASFGA
  CALL MASFKA
20  CONTINUE
  RETURN
  END
C -----UGMOMF
  SUBROUTINE UGMOMF
  INCLUDE 'mfrek.com'
C
  CS=0.5*(UG(IJ)+UG(IPJ))
  IF (CS.GE.0.) THEN
    UGFR=(AR(I)*RGP(IJ)+BR(I)*RGP(IJR))*UG(IJ)*CS*R(I+1)
  ELSE
    UGFR=(AR(I+1)*RGP(IJR)+BR(I+1)*RGP(IJRR))*UG(IPJ)*CS*R(I+1)
  ENDIF
  CS=AR(I)*VG(IJ)+BR(I)*VG(IPJ)
  IF (CS.GE.0.) THEN
    UGFT=(AR(I)*RGP(IJ)+BR(I)*RGP(IJR))*UG(IJ)*CS
  ELSE
    UGFT=(AR(I)*RGP(IJT)+BR(I)*RGP(IJTR))*UG(IPJ)*CS
  ENDIF
  IF(IFL(IMJ).NE.1) GOTO 1
  IF(IFL(IJM).NE.1) GOTO 2
  CALL UGVSB
  GOTO 4
1  CS=0.5*(UG(IJ)+UG(IMJ))
  IF (CS.GE.0.) THEN
    UGFL=(BR(I-1)*RGP(IJ)+AR(I-1)*RGP(IJL))*UG(IMJ)*CS*R(I)
  ELSE
    UGFL=(AR(I)*RGP(IJ)+BR(I)*RGP(IJR))*UG(IJ)*CS*R(I)
  ENDIF
  IF(IFL(IJM).NE.1) GOTO 2
  CALL UGVSA
  GOTO 3
2  CS=(AR(I)*VG(IJM)+BR(I)*VG(IPJM))
  IF (CS.GE.0.) THEN
    UGFB(I)=(AR(I)*RGP(IJB)+BR(I)*RGP(IJBR))*UG(IJM)*CS
  ELSE
    UGFB(I)=(AR(I)*RGP(IJ)+BR(I)*RGP(IJR))*UG(IJ)*CS

```



```

ENDIF
CALL UGVS
UGFB(I)=UGFB(I)-SUGB
IF(IFL(IMJ).EQ.1)GOTO 4
3  UGFL=UGFL-SUGL
4  UGFT=UGFT-SUGT
   UGFR=UGFR-SUGR
   RETURN
   END
C -----UGVS
   SUBROUTINE UGVS
   INCLUDE 'mfrek.com'
C
   SUGB=VISF*((VG(IPJM)-VG(IJM))*RDRP(I)+(UG(IJ)-UG(IJM))
1*RDZP(J-1))*
1(BZ(J-1)*(AR(I)*TH(IJ)+BR(I)*TH(IJR))
1+AZ(J-1)*(AR(I)*TH(IJB)+BR(I)*TH(IJBR)))
C
   ENTRY UGVSA
   SUGL=VISF*(2.*(UG(IJ)-UG(IMJ))*RDR(I)-(2./3.)
1*(RRIDR(I)*RB(I)*
1UG(IJ)-RB(I-1)*UG(IMJ))+VG(IJ)-VG(IJM))
1*RDZ(J))*TH(IJ)*R(I)
C
   ENTRY UGVSB
   SUGT=VISF*((VG(IPJ)-VG(IJ))*RDRP(I)+(UG(IPJ)-
1UG(IJ))*RDZP(J))*
1(AZ(J)*(AR(I)*TH(IJ)+BR(I)*TH(IJR))
1+BZ(J)*(AR(I)*TH(IJT)+BR(I)*TH(IJTR)))
   SUGR=VISF*(2.*(UG(IPJ)-UG(IJ))*RDR(I+1)-(2./3.)*(RRIDR(I+1)
1*(RB(I+1)*
1UG(IPJ)-RB(I)*UG(IJ))+VG(IPJ)-VG(IPJM))*RDZ(J)))
1*TH(IJR)*R(I+1)
   SUGC=VISF*(2.*RRB(I)*UG(IJ)-(2./3.)*(0.5*RRIDRP(I)*
1(RB(I+1)*UG(IPJ)-RB(I-1)*UG(IMJ))+
1(AR(I)*(VG(IJ)-VG(IJM))
1+BR(I)*(VG(IPJ)-VG(IPJM))*RDZ(J))*RRB(I)
1*(AR(I)*TH(IJ)+BR(I)*TH(IJR))
   RETURN
   END
C -----ULMOMF
   SUBROUTINE ULMOMF
   INCLUDE 'mfrek.com'
C
   CS=0.5*(UK(K,IJ)+UK(K,IPJ))

```

```

IF (CS.GE.0.) THEN
  ULFR(K)=(AR(I)*RLK(K,IJ)+BR(I)*RLK(K,IJR))
  1*UK(K,IJ)*CS*R(I+1)
ELSE
  ULFR(K)=(AR(I+1)*RLK(K,IJR)+BR(I+1)*RLK(K,IJRR))
  1*UK(K,IPJ)*CS*R(I+1)
ENDIF
CS=AR(I)*VK(K,IJ)+BR(I)*VK(K,IPJ)
IF (CS.GE.0.) THEN
  ULFT(K)=(AR(I)*RLK(K,IJ)+BR(I)*RLK(K,IJR))*UK(K,IJ)*CS
ELSE
  ULFT(K)=(AR(I)*RLK(K,IJT)+BR(I)*RLK(K,IJTR))*UK(K,IJP)*CS
ENDIF
IF(IFL(IMJ).NE.1) GOTO 1
IF(IFL(IJM).NE.1) GOTO 2
CALL ULVSB
GOTO 4
1  CS=0.5*(UK(K,IJ)+UK(K,IMJ))
   IF (CS.GE.0.) THEN
     ULFL(K)=(BR(I-1)*RLK(K,IJ)+AR(I-1)*RLK(K,IJL))
     1*UK(K,IMJ)*CS*R(I)
   ELSE
     ULFL(K)=(AR(I)*RLK(K,IJ)+BR(I)*RLK(K,IJR))*UK(K,IJ)*CS*R(I)
   ENDIF
   IF(IFL(IJM).NE.1)GOTO2
   CALL ULVSA
   GOTO 3
2  CS=AR(I)*VK(K,IJM)+BR(I)*VK(K,IPJM)
   IF (CS.GE.0.) THEN
     ULFB(K,I)=(AR(I)*RLK(K,IJB)+BR(I)*RLK(K,IJBR))*UK(K,IJM)*CS
   ELSE
     ULFB(K,I)=(AR(I)*RLK(K,IJ)+BR(I)*RLK(K,IJR))*UK(K,IJ)*CS
   ENDIF
   CALL ULVS
   ULFB(K,I)=ULFB(K,I)-SULB(K)
   IF(IFL(IMJ).EQ.1)GOTO 4
3  ULFL(K)=ULFL(K)-SULL(K)
4  ULFT(K)=ULFT(K)-SULT(K)
   ULFR(K)=ULFR(K)-SULR(K)
   RETURN
   END
C -----ULVS
  SUBROUTINE ULVS
  INCLUDE 'mfrek.com'
C

```

```

SULB(K)=((VK(K,IPJM)-VK(K,IJM))*RDRP(I)+(UK(K,IJ)-UK(K,IJM))
1*RDZP(J-1))*((BZ(J-1)*(AR(I)*RLK(K,IJ)+BR(I)*RLK(K,IJR))
1+AZ(J-1)*(AR(I)*RLK(K,IJB)+BR(I)*RLK(K,IJBR)))
1*ARL(K)*(VISSD(K)))

```

C

```

ENTRY ULVSA
SULL(K)=2.*(UK(K,IJ)-UK(K,IMJ))*RDR(I)*R(I)*RLK(K,IJ)*ARL(K)
1*VISSD(K)+(RRIDR(I)*(RB(I)
1*UK(K,IJ)-RB(I-1)*UK(K,IMJ))+(VK(K,IJ)-VK(K,IJM))
1*RDZ(J))*R(I)
1*(VISBL(K,IJ)-RLK(K,IJ)*ARL(K)*(2./3.)*VISSD(K))

```

C

```

ENTRY ULVSB
SULT(K)=((VK(K,IPJ)-VK(K,IJ))*RDRP(I)+(UK(K,IJP)-UK(K,IJ))
1*RDZP(J))
1*((AZ(J)*(AR(I)*RLK(K,IJ)+BR(I)*RLK(K,IJR))
1+BZ(J)*(AR(I)*RLK(K,IJT)+BR(I)*RLK(K,IJTR)))*ARL(K)*(
1VISSD(K)))
SULR(K)=2.*(UK(K,IPJ)-UK(K,IJ))*RDR(I+1)*R(I+1)*
1*RLK(K,IJR)*ARL(K)*(VISSD(K))+((RRIDR(I+1)
1*(RB(I+1)*UK(K,IPJ)-RB(I)*UK(K,IJ))+(VK(K,IPJ)-VK(K,IPJM))
1*RDZ(J))*R(I+1)*(VISBL(K,IJR)-(2./3.)*RLK(K,IJR)*ARL(K)
1*(VISSD(K)))
SULC(K)=(2.*RRB(I)*UK(K,IJ)*(AR(I)*RLK(K,IJ)+BR(I)*RLK(K,IJR))
1*ARL(K)*(VISSD(K)))+(0.5*RRIDRP(I)
1*(RB(I+1)*UK(K,IPJ)-RB(I-1)*UK(K,IMJ))
1+(AR(I)*(VK(K,IJ)-VK(K,IJM))
1+BR(I)*(VK(K,IPJ)-VK(K,IPJM)))*RDZ(J))*RRB(I)*
1(VISBL(K,IJ)-(2./3.)*(AR(I)*RLK(K,IJ)+BR(I)*RLK(K,IJR))
1*ARL(K)*(VISSD(K)))
RETURN
END

```

C

-----VELINV

```

SUBROUTINE VELINV(NH,NP,A,B)
IMPLICIT REAL*8(A-H,O-Z)
DIMENSION A(NP,NP),B(NP)

```

C

```

C USE GAUSS-DOLITTLE METHOD FOR SYMMETRIC MATRIX INVERSION
DO 136 K=2,NP
IF(ABS(A(K,K)).GE.1.D-6)GOTO 136
DO 135 KK=1,NP
A(K,KK)=0.0
135 A(KK,K)=0.0
B(K)=0.0
136 CONTINUE

```

```

C
  DO 160 K=1,NP
  IF(A(K,K).EQ.0.0)GOTO 160
  KP1=K+1
  DIV=1./A(K,K)
  DO 140 KJ=KP1,NP
  A(K,KJ)=A(K,KJ)*DIV
140  CONTINUE
  B(K)=B(K)*DIV
  DO 150 KI=KP1,NP
  AMUL=A(KI,K)
  DO 145 KJ=KP1,NP
145  A(KI,KJ)=A(KI,KJ)-AMUL*A(K,KJ)
150  B(KI)=B(KI)-AMUL*B(K)
160  CONTINUE
  DO 170 K=NH,1,-1
  KP1=K+1
  DO 170 KI=KP1,NP
170  B(K)=B(K)-B(KI)*A(K,KI)
  RETURN
  END

```

C -----VELSK

```

SUBROUTINE VELSK
INCLUDE 'mfrek.com'

```

```

C
  IFLL=IFL(IMJ)
  IF((IFLL.EQ.2).OR.(IFLL.EQ.3).OR.(IFLL.EQ.5))GOTO 200
  CALL VELINV(NPHASE,NPHS1,AU1,BU1)
  UG(IMJ)=BU1(1)
  DO 165 K=2,NPHS1
165  UK(K-1,IMJ)=BU1(K)
200  CONTINUE
  IFLB=IFL(IJM)
  IF((IFLB.EQ.2).OR.(IFLB.EQ.3).OR.(IFLB.EQ.5))GOTO 300

```

```

C
  CALL VELINV(NPHASE,NPHS1,AV1,BV1)
  VG(IJM)=BV1(1)
  DO 265 K=2,NPHS1
265  VK(K-1,IJM)=BV1(K)

```

```

C
  ENTRY VELSK2
300  CONTINUE
  IFLR=IFL(IPJ)
  IF((IFLR.EQ.2).OR.(IFLR.EQ.3).OR.(IFLR.EQ.5))GOTO 400
  CALL VELINV(NPHASE,NPHS1,AU,BU)

```

```

      UG(IJ)=BU(1)
      DO 365 K=2,NPHS1
365   UK(K-1,IJ)=BU(K)
400   CONTINUE
      IFLT=IFL(IJP)
      IF((IFLT.EQ.2).OR.(IFLT.EQ.3).OR.(IFLT.EQ.5))RETURN
      CALL VELINV(NPHASE,NPHS1,AV,BV)
      VG(IJ)=BV(1)
      DO 465 K=2,NPHS1
465   VK(K-1,IJ)=BV(K)
      RETURN
      END

```

C -----VGMOMF

```

      SUBROUTINE VGMOMF
      INCLUDE 'mfrek.com'
C
      CS=0.5*(VG(IJ)+VG(IJP))
      IF (CS.GE.0.) THEN
      VGFT=(AZ(J)*RGP(IJ)+BZ(J)*RGP(IJT))*VG(IJ)*CS
      ELSE
      VGFT=(AZ(J+1)*RGP(IJT)+BZ(J+1)*RGP(IJTT))*VG(IJP)*CS
      ENDIF
      CS=AZ(J)*UG(IJ)+BZ(J)*UG(IJP)
      IF (CS.GE.0.) THEN
      VGFR=(AZ(J)*RGP(IJ)+BZ(J)*RGP(IJT))*VG(IJ)*CS*RB(I)
      ELSE
      VGFR=(AZ(J)*RGP(IJR)+BZ(J)*RGP(IJTR))*VG(IPJ)*CS*RB(I)
      ENDIF
      IF(IFL(IMJ).NE.1) GOTO 1
      IF(IFL(IJM).NE.1) GOTO 2
      CALL VGVSB
      GOTO 4
1     CS=AZ(J)*UG(IMJ)+BZ(J)*UG(IMJP)
      IF (CS.GE.0.) THEN
      VGFL=(AZ(J)*RGP(IJL)+BZ(J)*RGP(IJTL))*VG(IMJ)*CS*RB(I-1)
      ELSE
      VGFL=(AZ(J)*RGP(IJ)+BZ(J)*RGP(IJT))*VG(IJ)*CS*RB(I-1)
      ENDIF
      IF(IFL(IJM).NE.1)GOTO2
      CALL VGVSA
      GOTO 3
2     CS=0.5*(VG(IJM)+VG(IJ))
      IF (CS.GE.0.) THEN
      VGFB(I)=(BZ(J-1)*RGP(IJ)+AZ(J-1)*RGP(IJB))*VG(IJM)*CS
      ELSE

```

```

VGFB(I)=(AZ(J)*RGP(IJ)+BZ(J)*RGP(IJT))*VG(IJ)*CS
ENDIF
CALL VGVS
VGFB(I)=VGFB(I)-SVGB
IF(IFL(IMJ).EQ.1)GOTO 4
3  VGFL=VGFL-SVGL
4  VGFT=VGFT-SVGT
   VGFR=VGFR-SVGR
   RETURN
   END
C -----VGVS
   SUBROUTINE VGVS
   INCLUDE 'mfrek.com'
C
   SVGB=VISF*(2./3.)*(2.*(VG(IJ)-VG(IJM))*RDZ(J)
1-RRIDR(I)*(RB(I)*
1UG(IJ)-RB(I-1)*UG(IMJ)))*TH(IJ)
C
   ENTRY VGVSA
   SVGL=VISF*((VG(IJ)-VG(IMJ))*RDRP(I-1)+(UG(IMJP)-UG(IMJ)
1*RDZP(J))*
1RB(I-1)*(AZ(J)*(BR(I-1)*TH(IJ)+AR(I-1)*TH(IJL))
1+BZ(J)*(BR(I-1)*TH(IJT)+AR(I-1)*TH(IJTL)))
C
   ENTRY VGVSB
   SVGT=VISF*(2./3.)*(2.*(VG(IJP)-VG(IJ))*RDZ(J+1)-RRIDR(I)
1*(RB(I)*
1UG(IJP)-RB(I-1)*UG(IMJP)))*TH(IJT)
   SVGR=VISF*((VG(IPJ)-VG(IJ))*RDRP(I)+(UG(IJP)-UG(IJ)
1*RDZP(J))*
1RB(I)*(AZ(J)*(AR(I)*TH(IJ)+BR(I)*TH(IJR))
1+BZ(J)*(AR(I)*TH(IJT)+BR(I)*TH(IJTR)))
   RETURN
   END
C -----VLMOMF
   SUBROUTINE VLMOMF
   INCLUDE 'mfrek.com'
C
   CS=0.5*(VK(K,IJ)+VK(K,IJP))
   IF (CS.GE.0.) THEN
   VLFT(K)=(AZ(J)*RLK(K,IJ)+BZ(J)*RLK(K,IJT))*VK(K,IJ)*CS
   ELSE
   VLFT(K)=(AZ(J+1)*RLK(K,IJT)+BZ(J+1)*RLK(K,IJTT))
1*VK(K,IJP)*CS
   ENDIF

```

```

CS=AZ(J)*UK(K,IJ)+BZ(J)*UK(K,IJP)
IF (CS.GE.0.) THEN
VLFR(K)=(AZ(J)*RLK(K,IJ)+BZ(J)*RLK(K,IJT))*VK(K,IJ)*CS*RB(I)
ELSE
VLFR(K)=(AZ(J)*RLK(K,IJR)+BZ(J)*RLK(K,IJTR))
1*VK(K,IJ)*CS*RB(I)
ENDIF
IF(IFL(IMJ).NE.1) GOTO 1
IF(IFL(IJM).NE.1) GOTO 2
CALL VLVS
GOTO 4
1 CS=AZ(J)*UK(K,IMJ)+BZ(J)*UK(K,IMJP)
IF (CS.GE.0.) THEN
VLFL(K)=(AZ(J)*RLK(K,IJL)+BZ(J)*RLK(K,IJTL))
1*VK(K,IMJ)*CS*RB(I-1)
ELSE
VLFL(K)=(AZ(J)*RLK(K,IJ)+BZ(J)*RLK(K,IJT))
1*VK(K,IJ)*CS*RB(I-1)
ENDIF
IF(IFL(IJM).NE.1)GOTO2
CALL VLVS
GOTO 3
2 CS=0.5*(VK(K,IJM)+VK(K,IJ))
IF (CS.GE.0.) THEN
VLFB(K,I)=(BZ(J-1)*RLK(K,IJ)+AZ(J-1)*RLK(K,IJB))
1*VK(K,IJM)*CS
ELSE
VLFB(K,I)=(AZ(J)*RLK(K,IJ)+BZ(J)*RLK(K,IJT))*VK(K,IJ)*CS
ENDIF
CALL VLVS
VLFB(K,I)=VLFB(K,I)-SVLB(K)
IF(IFL(IMJ).EQ.1)GOTO 4
3 VLFL(K)=VLFL(K)-SVLL(K)
4 VLFT(K)=VLFT(K)-SVLT(K)
VLFR(K)=VLFR(K)-SVLR(K)
RETURN
END
C -----VLVS
SUBROUTINE VLVS
INCLUDE 'mfrek.com'
C
SVLB(K)=(2./3.)*(2.*(VK(K,IJ)-VK(K,IJM))*RDZ(J)-RRIDR(I)
1*(RB(I)*UK(K,IJ)-RB(I-1)*UK(K,IMJ)))
1*(RLK(K,IJ)*ARL(K)*(VISSD(K)))
1+VISBL(K,IJ)*RRIDR(I)*(RB(I)*UK(K,IJ)-RB(I-1)*UK(K,IMJ))

```

C

```

ENTRY VL VSA
SVLL(K)=((VK(K,IJ)-VK(K,IMJ))*RDRP(I-1)
1+(UK(K,IMJP)-UK(K,IMJ))
1*RDZP(J))*RB(I-1)*((AZ(J)*(BR(I-1)*RLK(K,IJ)+AR(I-1)
1*RLK(K,IJL))
1+BZ(J)*(BR(I-1)*RLK(K,IJT)+AR(I-1)*RLK(K,IJTL)))
1*ARL(K)*(VISSD(K)))
ENTRY VL VSB
SVLT(K)=(2./3.)*(2.*(VK(K,IJP)-VK(K,IJ))*RDZ(J+1)-RRIDR(I)
1*(RB(I)*UK(K,IJP)-RB(I-1)*UK(K,IMJP)))
1*(RLK(K,IJT)*ARL(K)*(VISSD(K)))
1+VISBL(K,IJT)*RRIDR(I)*(RB(I)*UK(K,IJP)-RB(I-1)*UK(K,IMJP))
SVLR(K)=((VK(K,IPJ)-VK(K,IJ))*RDRP(I)+(UK(K,IJP)-UK(K,IJ))
1*RDZP(J))*RB(I)*((AZ(J)*(AR(I)*RLK(K,IJ)+BR(I)*RLK(K,IJR))
1+BZ(J)*(AR(I)*RLK(K,IJT)+BR(I)*RLK(K,IJTR)))
1*ARL(K)*(VISSD(K)))
RETURN
END

```

C -----VWORKL

```

SUBROUTINE VWORKL
INCLUDE 'mfrek.com'

```

C

```

C CALCULATE VISCOUS STRESSES FOR THE WORK TERM IN THE PHASES
C ENERGY EQUATION (NOTE: VISCOSITY IS MULTIPLIED LATER)

```

C

```

DO 100 J=2,JB1
DO 100 I=2,IB1
IJ=I+(J-1)*IB2
IF(IFL(IJ).EQ.1)THEN
CALL INDX
C
CALL OBSTACLE
DO 10 K=1,NPHASE
IF(KIN(K).NE.1)GOTO 10
IF(IFL(IPJM).EQ.3)VK(K,IPJM)=0.0
IF(IFL(IMJM).EQ.3)VK(K,IMJM)=0.0
IF(IFL(IMJP).EQ.3)UK(K,IMJP)=0.0
IF(IFL(IMJM).EQ.3)UK(K,IMJM)=0.0
CS1=0.5*((VK(K,IPJ)+VK(K,IPJM)-VK(K,IMJ)-VK(K,IMJM))
1/(DRP(I)+DRP(I-1)))+(RB(I)*(UK(K,IJP)-UK(K,IJM))
1+RB(I-1)*(UK(K,IMJP)-UK(K,IMJM)))
1/(R(I)*(DZP(J)+DZP(J-1))))
CS2=RDZ(J)*(VK(K,IJ)-VK(K,IJM))
CS3=RDR(I)*(UK(K,IJ)-UK(K,IMJ))
CS4=0.5*(RB(I)*UK(K,IJ)+RB(I-1)*UK(K,IMJ))/(R(I)*R(I))

```



```

C
  SILM(K,IJ)=RRIDR(I)*(RB(I)*UK(K,IJ)
  1-RB(I-1)*UK(K,IMJ))+CS2
  SILRZ=CS1
  SILZZ=2.0*CS2
  SILRR=2.0*CS3
  SILPP=2.0*CS4

C
C CALCULATE VISCOUS WORK FOR THE PHASES
  VWLS(K,IJ)=DT*(SILRZ*CS1+SILZZ*CS2+SILRR*CS3
  1+SILPP*CS4*ITC)
  VWLM(K,IJ)=DT*SILM(K,IJ)*SILM(K,IJ)
10  CONTINUE
    ENDIF
100  CONTINUE
    RETURN
    END

```

**C.2 MFREK.COM.** The followings are common file for "mfrek.f" and its name must be "mfrek.com" and in same subdirectory as that "mfrek.f" is.

```

IMPLICIT DOUBLE PRECISION(A-H,O-Z)
PARAMETER (IB2=18,JB2=60,NPHASE=2,NPHS1=NPHASE+1,LT=NPHS1)
PARAMETER (NIN=1,NOUT=1,NFL=3,NOBS=6,JXN=6,THICK=44.8564)
PARAMETER (ITC=0,WMYGAS=28.5,THMIN=0.36,CRES=0.99999)
PARAMETER (CG=1.80041D7,VISF=1.82D-4)
PARAMETER (RST=0.,IPRE=0)
PARAMETER (C17=8.314D7,C18=0.0 )
PARAMETER (IB=IB2-2,IB1=IB2-1,JB=JB2-2,JB1=JB2-1)
PARAMETER (IB3=IB2+1,IB4=IB2+2,IB2JB2=IB2*JB2)
PARAMETER (IB2JB1=IB2JB2-IB2,IB1JB2=IB2JB2-1,
1IB2JB0=JB*IB2+1)
PARAMETER (NO=NIN+NOUT+NFL,NT=NO+NOBS)
PARAMETER (NH=NPHASE,NC=IB2JB2,NI=IB2,NJ=JB2,
1 NP=NPHS1,NF=NP*(NP+1)/2)
PARAMETER (PI=3.14159265359)

C SETC
  PARAMETER (C1=300.,C2=300)

C COMMON BLOCKS
  COMMON / PARAM1 / DT,KIN(NH),IRXN,IHEAT,VISS(NH),
  1 DG, D1, D2, D3, P1, P2, P3, GRAVX,GRAVY,NIT,
  1 TIME, TDUMP, TPR, TSTOP, TARRAY(2), TTIM
  COMMON / PARAM2 /ITHMF(NT), QF(NC),
  1 AYM(JXN,JB2),AYMOL(JXN,JB2),AYMOL1(JXN,JB2),YMOL(JXN,NC),
  1 FLUX(JB2),AMIX(20),

```

1 TG(NC), TL(NH,NC), TGN(NC), TLN(NH,NC),  
 1 SIEG(NC), SIEGN(NC), AKG(NC),  
 1 SIEL(NH,NC), SIELN(NH,NC), AKL(NH,NC),  
 1 CL(NH), RHEAT(NH,NC),  
 1 UGFL, UGFR, UGFT, UGFB(NI),  
 1 ULFL(NH), ULFR(NH), ULFT(NH), ULFB(NH,NI),  
 1 VGFL, VGFR, VGFT, VGFB(NI),  
 1 VLFL(NH), VLFR(NH), VLFT(NH), VLFB(NH,NI),  
 1 THFL, THFR, THFT, THFB(NI),  
 1 EGFL, EGFR, EGFT, EGFB(NI),  
 1 HFGL, HFGR, HFGT, HFGB,  
 1 ELFL(NH), ELFR(NH), ELFT(NH), ELFB(NH,NI),  
 1 HFL(NH), HFLR(NH), HFLT(NH), HFLB(NH,NI),  
 1 OMTFL(NH), OMTFR(NH), OMTFT(NH), OMTFB(NH,NI),  
 1 SUGL, SUGR, SUGT, SUGB, SUGC,  
 1 SULL(NH), SULR(NH),SULT(NH), SULB(NH), SULC(NH),  
 1 SVGL, SVGR, SVGT, SVGB,  
 1 SVLL(NH), SVLR(NH),SVLT(NH), SVLB(NH)  
 COMMON / PARAM3 /  
 1 IOB(4,NT), ARL(NH), DK(NH), GTH(0:1000), DKF(NH,NH),  
 1 C(16), RL(NH), VISSD(NH),IFL(NC),INDS(NC,5), PHI(NH),  
 1 CPHI(NH), PHILIM(NH,NH), EPSL(NH,NH), EPSU(NH,NH),  
 1 R(NI), RB(NI), RRB(NI),COHF(0:1000),  
 1 DR(NI), DZ(NJ), DRP(NI), DZP(NJ),  
 1 RDR(NI), RDZ(NJ), RDRP(NI), RDZP(NJ),  
 1 AR(NI), BR(NI), AZ(NJ), BZ(NJ),  
 1 DTODR(NI), DTODZ(NJ), DTODRP(NI), DTODZP(NJ),  
 1 RRIDR(NI), RRIDRP(NI), DTOBDR(NI), DTORDR(NI)  
 COMMON / PARAMI /  
 1 I, IJ, IJB, IJBR, IJL, IJM, IJP, IJR,IMJM,  
 1 IJRR, IJT, IJTL, IJTR, IJTT, IMJ, IMJP, IPJ,  
 1 IPJM, IPJP, ITD, J, K, NSL(4), NSO(NT)  
 COMMON/AREA1/  
 1 ABETA(NC), CONV(NC), P(NC), PN(NC), TH(NC), THN(NC),  
 1 RGFR(NC), RGFT(NC), RGP(NC),RGPN(NC), ROG(NC),  
 1 RGFY(NC),RGFTY(NC),  
 1 APP(NF,NC), RUG(NC), RVG(NC),  
 1 AU1(NP,NP), AV1(NP,NP), AU(NP,NP), AV(NP,NP),  
 1 BU1(NP), BV1(NP), BU(NP), BV(NP)  
 COMMON/AREA2/  
 1 RLFRK(NH,NC), RLFTK(NH,NC), RKPG(NH,NC),  
 1 RLFRKY(NH,NC),RLFTKY(NH,NC),  
 1 RUK(NH,NC), RVK(NH,NC), RLK(NH,NC), RLKN(NH,NC),  
 1 UG(NC), VG(NC), UK(NH,NC), VK(NH,NC)  
 COMMON/INPUT/

1 UIO(NO), VIO(NO), PIO(NO), THIO(NO), TEMIO(NO),  
 1 UPIO(NH,NO), VPIO(NH,NO), THPIO(NH,NO), TEMPPIO(NH,NO),  
 1 WM(JXN),Q(NC),DOTM(LT),DOTMJ(LT,JXN),YIO(LT,JXN,NO),  
 1 QGEN(LT),QFLOW(LT),IHO(LT),IHE(LT),HHO(LT,5),  
 1 HHE(LT,5),AHO(LT,5,JXN),AHE(LT,5,JXN),Y(LT,JXN,NC),  
 1 RHO(LT,5),RHE(LT,5),TOB(NC),YN(LT,JXN,NC),  
 1 KEY(4),AHK(LT,5,JXN),DGG(NC),QQ(NT),TOBB(NT),COEK(NT),  
 1 COE(NC),  
 1 RLKMIN(NH),TSKIO(NH,NO),TSK(NH,NC),VISBL(NH,NC),  
 1 VISCL(NH,NC),VISDIL(NH),PS(NH,NC),TSKN(NH,NC),  
 1 SILM(NH,NC),VWLM(NH,NC),VWLS(NH,NC),GCON(NH,NC),  
 1 GAMMA(NH,NC),TSKCB(NH),TSKFB(NH,NI),THL(NH,NC),  
 1 TSKCL(NH),TSKCT(NH),TSKCR(NH),  
 1 TSKFL(NH),TSKFT(NH),TSKFR(NH)

**C.3 MFREK.D.** The followings are a sample input data file named "mfrek.d".

mfrek.r

SAMPLE INPUT DATA

18\*1.786

60\*13.31

5	2	3	3		
1	0	2	17	2	13
1	0	2	17	14	31
1	0	2	17	32	59
5	0	2	17	1	1
7	0	2	17	60	60
3	1	12	13	40	42
0	273.15		2.0D6		
3	1	12	13	34	36
0	273.15		2.0D6		
3	1	12	13	28	30
0	273.15		2.0D6		
3	1	12	13	22	24
0	273.15		2.0D6		
3	1	12	13	16	18
0	273.15		2.0D6		
3	1	12	13	10	12
0	273.15		2.0D6		
0.005	0.1				
1.0	1.0				
3.011	0.70025				
4.9D7	3.0D7				
5.0	0.089				
1	0.1	0	0.1		

0	4.80	5.3129D7	0.050	523.15		
0	0		0.524	523.15	1.0	
0	0		0.426	523.15	1.0	
0	4.80	5.2944D7	0.050	523.15		
0	0		0	0	1.0	
0	0		0.950	523.15	1.0	
0	0.24	5.2944D7	1.000	523.15		
0	0		0	0	1.0	
0	0		0	0	1.0	
0	0.24	5.3349D7	1.000	523.15		
0	0		0	0	1.0	
0	0		0	0	1.0	
0	0.24	5.2944D7	1.000	523.15		
0	0		0	0	1.0	
0	0		0	0	1.0	
1	1					
28	44	2	16	32	28	
1	0					
0	-1	0	-2	0	1	0
0	0					
0	0					
0.6806		0.2726	0.0334	0.0000	0.0000	0.0134
0		0	0	0	0	0
0		0	0	0	0	0
0.6806		0.2726	0.0334	0.0000	0.0000	0.0134
0		0	0	0	0	0
0		0	0	0	0	0
0.6806		0.2726	0.0334	0.0000	0.0000	0.0134
0		0	0	0	0	0
0		0	0	0	0	0
0.6806		0.2726	0.0334	0.0000	0.0000	0.0134
0		0	0	0	0	0
0		0	0	0	0	0
0		0	0	0	0	0
0		0	0	0	0	0
0	30	1D-4				
0.05	0.005					
0	-980.62					