

Appendix C

Case 3: Natural gas only

CASE 3

The following report gives a brief description of each of the units in the block flow diagram. All capital cost data in this report, except where otherwise specified, have been estimated from similar installations described in the Houston Area Medium-BTU Coal Gasification Project Final Report, published in June 1982 by Union Carbide [1] (All references to material in this report will be referred to as Houston, and all scaling exponents from the Houston report are 0.65). The plant consumes 1.2 billion standard cubic meters of natural gas per year and produces 0.50 million metric tons of mixed alcohols per year.

SYNGAS PRODUCTION FROM NATURAL GAS

Compressed natural gas (stream 14) and steam (stream 15) are reacted in the Steam Reformation Block. The cooled output gas (stream 17) goes to the Rectisol Block. The cost for this unit was estimated from data found for a hydrogen production facility, with a scaling exponent of 0.8 [2]. The fuel gas usage for this block is estimated to be 30% of the natural gas feed.

RECTISOL

The cooled gas stream (stream 17), nitrogen gas (stream 19) for methanol regeneration, and methanol make-up (stream 20) for vapor loss all enter the Rectisol Block. CO₂ levels are reduced to the ppm range. The clean syngas (stream 22) is sent to the alcohol synthesis loop. A CO₂-N₂ mixture (stream 24) and a CO₂ rich stream (stream 23) are produced as byproducts. Condensed water is also removed (stream 17A). This block is the same as Houston Plant 05. The cost for this plant was estimated by using exponential scaling.

PRESSURE SWING ADSORPTION

The clean syngas (stream 22) is sent to PSA for selective hydrogen removal and purification. The adjusted syngas (stream 22AA), which leaves the PSA unit at 200 kPa, is compressed and then sent on to the reactor. The purified excess hydrogen is then split into two streams. One stream (27A) sent to the plant battery limits for sale, if possible.

MoS₂ ALCOHOL SYNTHESIS LOOP

Clean syngas (stream 26) at 140 atmospheres enters the catalytic reactor along with the syngas recycle (stream 56B). The products (stream 26A) are taken to the separations block where the unreacted syngas is removed (stream 59). Part of this stream (stream 27) is sent to power generation while the rest (stream 56) is sent to CO₂ removal. The cost of this block was estimated from the cost of a methanol synthesis loop, with a scaling exponent of 0.565 [3].

CO₂ REMOVAL

This block is very similar to the Rectisol Block. Recycled gas from the alcohol separation block (stream 56) is the only feed. CO₂ free syngas (stream 56A) is then recompressed and sent back to the reactor. CO₂ is taken off as a product (stream 57). The cost of this block is calculated the same way as in the Rectisol block. The power requirement for this unit is included in the Rectisol block.

COMBUSTION GAS TURBINE

The light hydrocarbons extracted from the reactor recycle (stream 27) in the Alcohol Synthesis Loop are sent to a combustion gas turbine with hot gas heat recovery. The power from the combustion gas turbines is assumed to be 35% of the HHV of the fuel in stream 27. This is consistent with recent studies on IGCC plants using medium BTU synthesis gas [5]. The cost for this block was estimated from data taken from an EPRI report, where each train can produce up to 200 MW with a scaling exponent of 0.67 [6].

EXHAUST GAS HEAT RECOVERY

The hot exhaust gas stream from the Gas Turbine Block (stream 70) at 590°C and 101 kPa enters the Exhaust Gas Heat Recovery Block and is cooled against process boiler feed water at 25°C (stream 73). The exhaust gas stream exits at 200°C (stream 75), and the boiler feed exits as steam at 10,000 kPa and 535°C (stream 74). The cost for this block was estimated from data taken from an EPRI report, where each train can generate up to 425 tons of steam per hour with a scaling exponent of 0.67 [6]. This block also supplies the reheat between the high pressure and intermediate pressure steam turbines.

POWER GENERATION

The steam from the Exhaust Gas Heat Recovery Block is let down in the steam turbines for power production. The cost for this block was estimated from data taken from an EPRI report, where each train can produce up to 500 MW with a scaling exponent of 0.67 [6]. This is a 3-stage steam turbine system. The high pressure stage

inlet is 535°C, 10,000 kPa steam. The exhaust at 3,000 kPa is reheated to 535°C before entering the intermediate pressure stage. The final stage exhausts to a surface condenser at 7.4 kPa. Each turbine has an assumed efficiency of 75%.

TOTAL ESTIMATED CAPITAL INVESTMENT (MM\$)

| | |
|---------------------------|--------------|
| Pressure Swing Adsorption | 15.1 |
| Syngas Reforming | 90.3 |
| Rectisol | 25.8 |
| Gas Turbines | 45.0 |
| Steam Turbines | 9.9 |
| Exhaust Gas Heat Recovery | 11.1 |
| CO2 Removal | 26.9 |
| Other Compressors | 57.5 |
| Alcohol Synthesis Loop | 47.2 |
| TOTAL | 328.8 |

(sum of individual block costs does not exactly equal the total due to round-off)

OVERALL ECONOMIC EVALUATION

The following table gives the totals and breakdowns for the yearly operating costs as well as the total installed cost for the plant, for Case 3A.

| | | |
|--|-------|-------|
| TOTAL ESTIMATED INSTALLED CAPITAL COST (MM\$) | | 335.9 |
| TOTAL ESTIMATED OPERATING COSTS (MM\$/YR) | | 223.3 |
| Natural Gas (\$106/1000 cubic meters) | 164.1 | |
| Other Expenses | 59.2 | |
| TOTAL ESTIMATED CREDITS (EXCLUDING ALCOHOLS) (MM\$/YR) | | 112.4 |
| Hydrogen (\$35.31/1000 cubic meters) | 95.7 | |
| | H-5 | |
| <hr/> | | |
| Power (\$0.05/kWh) | 16.7 | |

The following table gives the totals and breakdowns for the yearly operating costs as well as the total installed cost for the plant, for Case 3B.

| | | |
|--|------|-------|
| TOTAL ESTIMATED INSTALLED CAPITAL COST (MM\$) | | 328.8 |
| TOTAL ESTIMATED OPERATING COSTS (MM\$/YR) | | 153.6 |
| Natural Gas (\$61.8/1000 cubic meters) | 95.7 | |
| Other Expenses | 57.9 | |
| TOTAL ESTIMATED CREDITS (EXCLUDING ALCOHOLS) (MM\$/YR) | | 72.5 |
| Hydrogen (\$20.6/1000 cubic meters) | 55.8 | |
| Power (\$0.05/kWh) | 16.7 | |

Credits for nitrogen, argon, and other rare gases have not been included because prices were not available and potential markets have not yet been identified.

STAND ALONE COMPRESSORS AND POWER SUMMARY

There are 2 compressors that are not included in any of the blocks. Their inlet, outlet, pressure change, power rating, and installed capital cost are listed below. Following that is a summary of the total plant power output/input (4). An efficiency of 70% is assumed for all compressors, with a maximum pressure ratio of 5 for a single stage of compression. Multiple compression stages with intercooling are used for services with pressure ratios greater than 5.

| FUNCTION | INLET STREAM | P (kPa) | OUTLET STREAM | P (kPa) | POWER (MW) | COST (MM\$) |
|---|-----------------|------------|------------------|------------|---------------|----------------|
| Rxtr Prep | 22AA | 200 | 26 | 14000 | -60.1 | 53.8 |
| Recy Comp | 56A | 12666 | 56B | 14000 | -3.6 | 3.6 |
| Total compressor needs | | | | | -63.6 | |
| Other in plant needs | | | | | -1.4 | |
| Total produced in steam and gas turbines | | | | | 106.8 | |
| Net power output | | | | | 41.7 | |
| Total installed compressor costs (1992 dollars) | | | | | | 57.5 |

REFERENCES

1. *Final Report on the Houston Area Medium-BTU Coal Gasification Project, Volumes 2 and 3*. Prepared by the Linde Division of Union Carbide Corporation, June 1982.
2. Baasel, William D., *Preliminary Chemical Engineering Plant Design, 2nd edition*. (Van Nostrand Reinhold, New York 1990), pp. 268-269.
3. Frank, "Methanol: Emerging Uses, New Syntheses," *Chemtech*, June 1982, pp. 358-362.
4. Baasel, pp. 529-530.
5. Report TR-101789, Houston Lighting and Power Company's Evaluation of Coal Gasification Coproduction Energy Facilities, EPRI Project 3226-04, 1992.
6. EPRI Report TR-100319, *Evaluation of a 510-MWe Destec GCC Power Plant Fueled With Illinois No. 6 Coal*, Prepared by Fluor Daniel, Inc., EPRI Project 2733-12, 1992.

Figure C.1 : Block Flow Diagram for Case 3

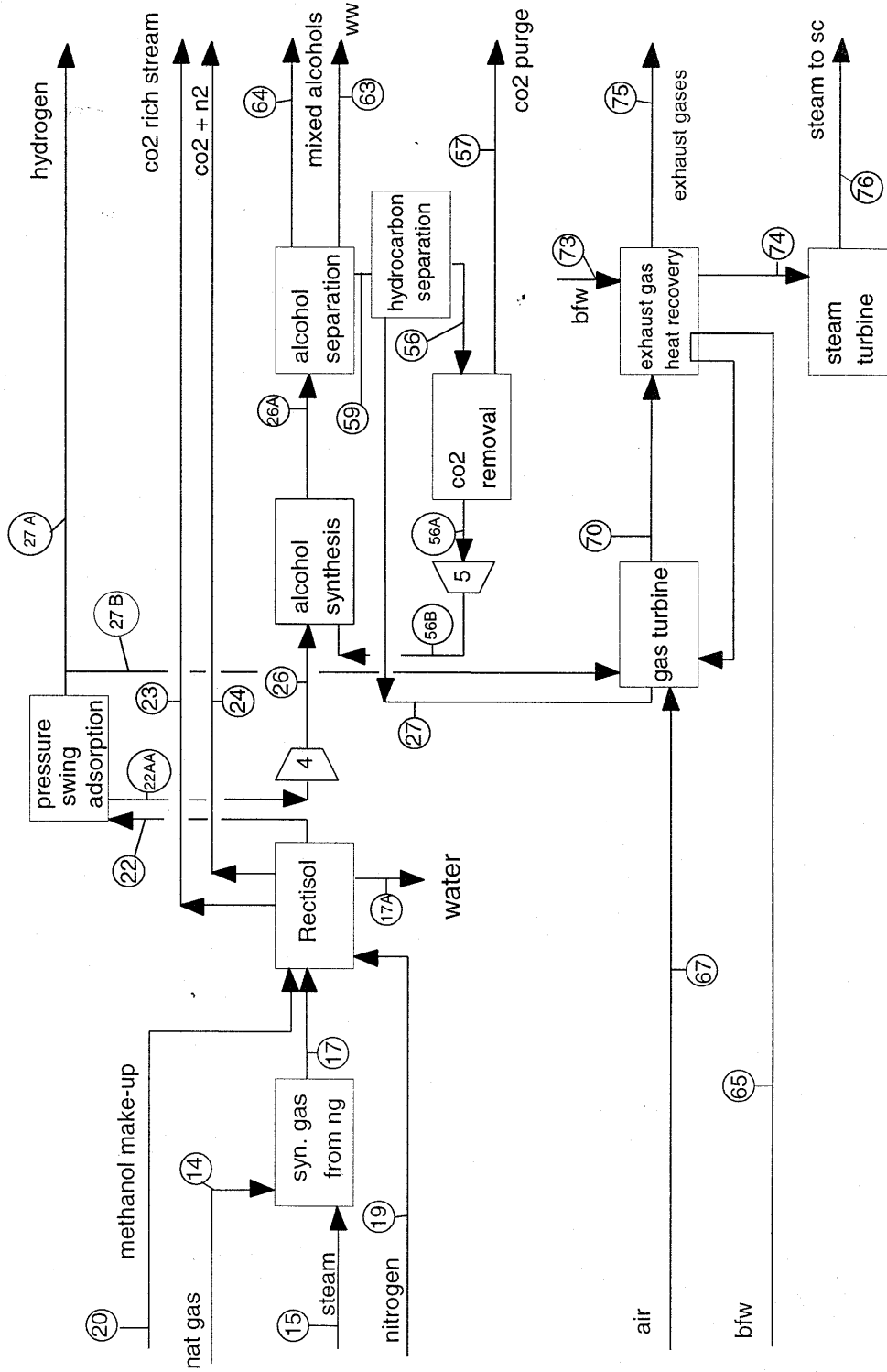


Table C.1 Case 3 Flow Table

| | 014 | 015 | 017 | 017A | 019 | 020 | 022 | 022A | 023 |
|--------------|----------|----------|----------|----------|--------|-------|----------|----------|---------|
| Air | | | | | | | | | |
| C | | | | | | 0.6 | | | |
| CH3OH | | | | | | | | | |
| C2H5OH | | | | | | | | | |
| C3H7OH | | | | | | | | | |
| C4H9OH | | | | | | | | | |
| C5H11OH | | | | | | | | | |
| CO | | | 5382.1 | | | | 5382.1 | 5382.1 | 755.5 |
| CO2 | | | 1259.2 | | | | | | |
| COS | | | | | | | | | |
| CsCO3 | | | | | | | | | |
| H2 | | | 21183.2 | | | | 21183.2 | 6057.1 | |
| H2O | | 15708.1 | 7807.6 | 7807.6 | | | | | |
| H2S | | | | | | | | | |
| N2 | | | | | 150.1 | | | | |
| NH3 | | | | | | | | | |
| O2 | | | | | | | | | |
| S | | | | | | | | | |
| A12O3 | | | | | | | | | |
| C3H6O2 | | | | | | | | | |
| C4H8O2 | | | | | | | | | |
| CH4 | 6646.5 | | 5.2 | | | | 5.2 | 5.2 | |
| C2H6 | | | | | | | | | |
| kmol/hr | 6646.5 | 15708.1 | 35637.3 | 7807.6 | 150.1 | 0.6 | 26570.5 | 11444.4 | 755.5 |
| kg/hr | 106344.5 | 282745.6 | 389090.1 | 140536.0 | 4202.6 | 18.4 | 193148.7 | 162896.6 | 33243.2 |
| Temp. (C) | 25.0 | 100.0 | 25.0 | 25.0 | 25.0 | 25.0 | 25.0 | 25.0 | 25.0 |
| Press. (kPa) | 1480.0 | 1480.0 | 1400.0 | 1400.0 | 1400.0 | 101.3 | 1400.0 | 200.0 | 1400.0 |

Table C.1 Case 3 Flow Table (cont'd)

| | 024 | 026 | 026A | 027 | 27A | 27B | 056 | 056A | 056B |
|--------------|---------|----------|----------|---------|---------|--------|----------|----------|----------|
| Ar | | | | | | | | | |
| C | | | | | | | | | |
| CH3OH | | | 628.3 | | | | | | |
| C2H5OH | | | 655.4 | | | | | | |
| C3H7OH | | | 145.0 | | | | | | |
| C4H9OH | | | 36.5 | | | | | | |
| C5H11OH | | | 15.2 | | | | | | |
| CO | | 5382.1 | 7001.9 | 714.2 | | | 6287.7 | 6287.7 | 6287.7 |
| CO2 | 503.7 | | 1493.7 | 152.4 | | | 1341.4 | | |
| COS | | | | | | | | | |
| CaCO3 | | | | | | | | | |
| H2 | | 6057.1 | 7880.0 | 803.8 | 15126.1 | | 7076.3 | 7076.3 | 7076.3 |
| H2O | | | 140.1 | | | | | | |
| H2S | | | | | | | | | |
| N2 | 150.1 | | | | | | | | |
| NH3 | | | | | | | | | |
| O2 | | | | | | | | | |
| S | | | | | | | | | |
| Al2O3 | | | | | | | | | |
| C3H6O2 | | | 18.0 | | | | | | |
| C4H8O2 | | | 11.9 | | | | | | |
| CH4 | | 5.2 | 4375.8 | 446.3 | | | 3929.5 | 3929.5 | 3929.5 |
| C2H6 | | | 171.6 | 17.5 | | | 154.1 | 154.1 | 154.1 |
| kmol/hr | 653.8 | 11444.4 | 22573.5 | 2134.1 | 15126.1 | | 18788.9 | 17447.5 | 17447.5 |
| kg/hr | 26364.7 | 162896.6 | 420598.8 | 35975.2 | 30252.1 | | 316722.5 | 257702.2 | 257702.2 |
| Temp. (C) | 25.0 | 240.0 | 310.0 | 25.0 | 25.0 | 25.0 | 25.0 | 25.0 | 45.0 |
| Press. (kPa) | 1400.0 | 14000.0 | 12666.0 | 12666.0 | 1400.0 | 1400.0 | 12666.0 | 12666.0 | 14000.0 |

Table C.1 Case 3 Flow Table (cont'd)

| | 057 | 059 | 063 | 064 | 065 | 067 | 070 | 073 | 074 |
|--------------|---------|----------|---------|---------|---------|----------|----------|---------|---------|
| Ar | | | | | | | | | |
| C | | | | | | | | | |
| CH3OH | | | | 628.3 | | | | | |
| C2H5OH | | | | 658.4 | | | | | |
| C3H7OH | | | | 145.0 | | | | | |
| C4H9OH | | | | 36.5 | | | | | |
| C5H11OH | | | | 15.2 | | | | | |
| CO | | 7001.9 | | | | | | | |
| CO2 | 1341.4 | 1493.7 | | | | | 1347.9 | | |
| COS | | | | | | | | | |
| CaCO3 | | | | | | | | | |
| H2 | | 7860.0 | | | | | | | |
| H2O | | | 140.1 | | 955.8 | | 2704.7 | 4298.2 | 4298.2 |
| H2S | | | | | | | | | |
| N2 | | | | | | | | | |
| NH3 | | | | | | | 20181.9 | | |
| O2 | | | | | | | | | |
| S | | | | | | | | | |
| Al2O3 | | | | | | | | | |
| C3H6O2 | | | 18.0 | | | | | | |
| C4H8O2 | | | 11.9 | | | | | | |
| CH4 | | 4375.8 | | | | | | | |
| C2H6 | | 171.6 | | | | | | | |
| kmol/hr | 1341.4 | 20923.0 | 170.1 | 1480.4 | 955.8 | 25546.7 | 27886.4 | 4298.2 | 4298.2 |
| kg/hr | 59020.4 | 352697.7 | 4805.1 | 62996.0 | 17204.2 | 736757.3 | 789946.7 | 77367.5 | 77367.5 |
| Temp. (C) | 25.0 | 25.0 | 25.0 | 25.0 | 25.0 | 25.0 | 50.0 | 25.0 | 50.0 |
| Press. (kPa) | 12666.0 | 12666.0 | 12666.0 | 12666.0 | 10000.0 | 101.3 | 101.3 | 10000.0 | 10000.0 |

Table C.1 Case 3 Flow Table (cont'd)

| | 075 | 076 | 077 | 078 |
|--------------|----------|---------|---------|---------|
| Ar | | | | |
| C | | | | |
| CH3OH | | | | |
| C2H5OH | | | | |
| C3H7OH | | | | |
| C4H9OH | | | | |
| C5H11OH | | | | |
| CO | | | | |
| CO2 | 1347.9 | | | |
| CO3 | | | | |
| CaCO3 | | | | |
| H2 | | | | |
| H2O | 2704.7 | 4298.2 | 4298.2 | 4298.2 |
| H2S | | | | |
| N2 | 20181.9 | | | |
| NH3 | | | | |
| O2 | 3651.9 | | | |
| S | | | | |
| Al2O3 | | | | |
| C3H6O2 | | | | |
| C4H8O2 | | | | |
| CH4 | | | | |
| C2H6 | | | | |
| kmol/hr | 27896.4 | 4298.2 | 4298.2 | 4298.2 |
| kg/hr | 789946.7 | 77367.5 | 77367.5 | 77367.5 |
| Temp. (C) | 200.0 | 40.0 | 380.0 | 535.0 |
| Press. (kPa) | 101.3 | 7.4 | 3000.0 | 3000.0 |

Table C.2 Case 3 Energy Analysis

| ELECTRICITY | | |
|----------------|-----------------------|---------------------------|
| Plant | Electricity Used (MW) | Electricity Produced (MW) |
| Rectisol Plant | 1.4 | 0 |
| Gas Turbine | 0 | 80.7 |
| Steam Turbine | 0 | 26.1 |
| Compressor 4 | 60.1 | 0 |
| Compressor 5 | 3.6 | 0 |
| Total | 65.1 | 106.8 |