Commercial-Scale Demonstration of the Liquid Phase Methanol (LPMEOTH $^{\text{TM}}$) Process

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Abstract

The Liquid Phase Methanol (LPMEOH™) Demonstration Project at Kingsport, Tennessee, is a \$213.7 million cooperative agreement between the U.S. Department of Energy (DOE) and Air Products Liquid Phase Conversion Company, L.P. (the Partnership) to produce methanol from coal-derived synthesis gas (syngas). Air Products and Chemicals, Inc. (Air Products) and Eastman Chemical Company (Eastman) formed the Partnership to execute the Demonstration Project. The LPMEOH™ Process Demonstration Unit was built at a site located at the Eastman coal-to-chemicals complex in Kingsport.

During this quarter, initial planning and procurement work continued on the seven project sites which have been accepted for participation in the off-site, product-use test program. Approximately 12,000 gallons of fuel-grade methanol (98+ wt% methanol, <1 wt% water) produced during operation on carbon monoxide (CO)-rich syngas at the LPMEOHTM Demonstration Unit was loaded into trailers and shipped off-site for future product-use testing. At one of the projects, three buses have been tested on chemical-grade methanol and on fuel-grade methanol from the LPMEOHTM Demonstration Project.

During the reporting period, planning for a proof-of-concept test run of the Liquid Phase Dimethyl Ether (LPDMETM) Process at the Alternative Fuels Development Unit (AFDU) in LaPorte, TX continued. The commercial catalyst manufacturer (Calsicat) has prepared the first batch of dehydration catalyst in large-scale equipment. Air Products will test a sample of this material in the laboratory autoclave.

Catalyst activity, as defined by the ratio of the rate constant at any point in time to the rate constant for freshly reduced catalyst (as determined in the laboratory autoclave), was monitored for the initial extended operation at the lower initial reactor operating temperature of 235°C. At this condition, the decrease in catalyst activity with time from the period 20 December 1997 through 27 January 1998 occurred at a rate of 1.0% per day, which represented a significant improvement over the 3.4% per day decline measured during the initial six weeks of operation in April and May of 1997. The deactivation rate also improved from the longer-term rate of 1.6% per day calculated throughout the summer and autumn of 1997.

Based on this improvement, DOE accepted a recommendation by Air Products and Eastman to further reduce the reactor temperature to 225°C. The initial operation at this temperature (from 31 January through 18 February 1998) showed a modest improvement in the deactivation rate to 0.7% per day. However, most of the activity decline occurred during a test period on CO-rich feed gas and immediately after an interruption in the Balanced Gas supply at the end of that test case. During two additional stable operating periods between 19 February and 31 March 1998, deactivation rates of 0.27% and 0.36% per day were measured. A discontinuity occurred in the data on 15 March 1998, again coincidental with an excursion in the Balanced Gas supply. If the current results prove to be correct, the current baseline activity decline of about 0.4% per day matches the original target from the 4-month proof-of concept run on a natural-gas derived syngas at the LaPorte

AFDU. Additional operating time is necessary to further quantify the catalyst deactivation rate and the effects of operating conditions and syngas supply excursions.

The weight of catalyst in the LPMEOHTM Reactor has reached 67% of the design value, and the slurry concentration approached 40 wt%. Catalyst slurry samples from the LPMEOHTM Reactor have been taken on a regular basis to correlate any change in plant performance with changes in the physical properties of the catalyst. So far, samples from mid-February and mid-March of 1998 have shown an increase in arsenic loading, although not nearly to the levels measured in the summer of 1997. Copper crystallite size measurements are still pending, as are analyses from more recent samples which will help complete the picture.

The performance of the alternative gas sparger, which was designed by Air Products and installed into the LPMEOHTM Reactor prior to the restart of the LPMEOHTM Demonstration Unit in December of 1997, was monitored throughout the reporting period. Pressure drop through the gas sparger was stabilized using a continuous flush of condensed oil and entrained slurry which were gravity-drained from downstream process equipment. As with the original gas sparger design, the return of the internal oil and slurry streams via the flush connection was required to stabilize the pressure drop after extended interruptions of the flush fluid. When compared to the original gas sparger, the alternative gas sparger may have greater flexibility in maintaining stable pressure drop after interruptions of the syngas supply; this may also be a result of greater attention to achieving a proper standby condition during shutdowns. The most recent results provide an initial confirmation of the encouraging data reported for the first two weeks of operation at the end of the prior reporting period.

The Alternative Fuels Field Test Unit (AFFTU), a transportable laboratory equipped with an autoclave and analytical equipment, was shipped from the Air Products' Iron Run laboratory in Allentown, PA to Kingsport to perform additional testing on the reactor feed gas at the site. Performance results from the 31-day campaign on coal-derived syngas at Kingsport were generally consistent with other laboratory experiments on poison-free syngas. A postmortem analysis on the catalyst revealed no unusual levels of catalyst poisons or significant changes in catalyst physical properties. The AFFTU test concluded on 20 January 1998, and the equipment was returned to the Air Products' Iron Run laboratory.

During the reporting period, a total of 5,762,047 gallons of methanol was produced at the LPMEOHTM Demonstration Unit. Apart from 12,000 gallons shipped off-site for productuse testing, Eastman accepted all of this methanol for use in the production of methyl acetate, and ultimately cellulose acetate and acetic acid. During a portion of the operating period on CO-rich syngas, approximately 181,800 gallons (600 tons) of stabilized methanol (99.3 wt% methanol, 0.3 wt% water) was utilized directly from the LPMEOHTM Demonstration Unit in Eastman's methyl acetate plant, bypassing the normal route through the distillation equipment which is designed to remove water, higher alcohols, and process oil. This provides another indication of the flexibility of the LPMEOHTM Process. No safety or environmental incidents were reported during this quarter. Availability exceeded 99%, as the demonstration unit continued to operate through the longest continuous campaign to date (45 days) as of 31 March 1998.

Ninety-nine percent (99%) of the \$38 million of funds forecast for the Kingsport portion of the LPMEOHTM Process Demonstration Project for the Phase 1 and Phase 2 tasks have been expended (as invoiced), as of 31 March 1998. Nineteen percent (19%) of the \$158 million of funds for the Phase 3 tasks have been expended (as invoiced), as of 31 March 1998.

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ACRONYMS AND DEFINITIONS

Acurex - Acurex Environmental Corporation
Air Products - Air Products and Chemicals, Inc.

AFDU - Alternative Fuels Development Unit - The "LaPorte PDU"

AFFTU - Alternative Fuels Field Trailer Unit

Balanced Gas - A syngas with a composition of hydrogen (H₂), carbon monoxide (CO), and

carbon dioxide (CO₂) in stoichiometric balance for the production of methanol

Carbon Monoxide Gas - A syngas containing primarily carbon monoxide (CO); also called CO Gas

Catalyst Age (η - eta) - the ratio of the rate constant at any point in time to the rate constant for a freshly reduced

catalyst (as determined in the laboratory autoclave)

Catalyst Concentration - Synonym for Slurry Concentration
Catalyst Loading - Synonym for Slurry Concentration

CO Conversion - the percentage of CO consumed across the reactor

Crude Grade Methanol - Underflow from rectifier column (29C-20), defined as 80 wt% minimum purity;

requires further distillation in existing Eastman equipment prior to use

DME - dimethyl ether

DOE - United States Department of Energy

DOE-FETC - The DOE's Federal Energy Technology Center (Project Team)

DOE-HQ - The DOE's Headquarters - Coal Fuels and Industrial Systems (Project Team)

DTP - Demonstration Test Plan - The four-year Operating Plan for Phase 3, Task 2 Operation

DVT - Design Verification Testing
Eastman - Eastman Chemical Company
EIV - Environmental Information Volume
EMP - Environmental Monitoring Plan
EPRI - Electric Power Research Institute

FFV - flexible fuel vehicle

Fresh Feed - sum of Balanced Gas, H₂ Gas, and CO Gas

Gas Holdup - the percentage of reactor volume up to the Gassed Slurry Height which is gas

Gassed Slurry

Height - height of gassed slurry in the reactor

HAPs - Hazardous Air Pollutants

Hydrogen Gas - A syngas containing an excess of hydrogen (H₂) over the stoichiometric balance for

the production of methanol; also called H2 Gas

IGCC - Integrated Gasification Combined Cycle, a type of electric power generation plant
IGCC/OTM - An IGCC plant with a "Once-Thru Methanol" plant (the LPMEOH™ Process) added-on

Inlet Superficial

Velocity - the ratio of the actual cubic feet of gas at the reactor inlet (calculated at the reactor

temperature and pressure) to the reactor cross-sectional area (excluding the area contribution

by the internal heat exchanger); typical units are feet per second

K - Sparger resistance coefficient (term used in calculation of pressure drop)

KSCFH - Thousand Standard Cubic Feet per Hour

LaPorte PDU - The DOE-owned experimental unit (PDU) located adjacent to Air Products' industrial

gas facility at LaPorte, Texas, where the LPMEOH™ process was successfully piloted

LPDMETM - Liquid Phase DME process, for the production of DME as a mixed coproduct with

methanol

LPMEOH™ - Liquid Phase Methanol (the technology to be demonstrated)

M85 - a fuel blend of 85 volume percent methanol and 15 volume percent unleaded gasoline

MeOH - methanol

Methanol Productivity - the gram-moles of methanol produced per hour per kilogram catalyst (on an oxide basis)

MTBE - methyl tertiary butyl ether

MW - molecular weight, pound per pound mole
NEPA - National Environmental Policy Act

OSHA - Occupational Safety and Health Administration

ρ - density, pounds per cubic foot

ACRONYMS AND DEFINITIONS (cont'd)

Partnership - Air Products Liquid Phase Conversion Company, L.P.

PDU - Process Development Unit
PFD - Process Flow Diagram(s)
ppbv - parts per billion (volume basis)
ppmw - parts per million (weight basis)

Project - Production of Methanol/DME Using the LPMEOH™ Process at an

Integrated Coal Gasification Facility

psi - Pounds per Square Inch

psia - Pounds per Square Inch (Absolute)
psig - Pounds per Square Inch (gauge)
P&ID - Piping and Instrumentation Diagram(s)

Raw Methanol - sum of Refined Grade Methanol and Crude Grade Methanol; represents total methanol

which is produced after stabilization

Reactor Feed - sun of Fresh Feed and Recycle Gas

Reactor O-T-M

Conversion - percentage of energy (on a lower heating value basis) in the Reactor Feed converted to

methanol (Once-Through-Methanol basis)

Reactor Volumetric

Productivity - the quantity of Raw Methanol produced (tons per day) per cubic foot of reactor volume

up to the Gassed Slurry Level

Recycle Gas - the portion of unreacted syngas effluent from the reactor "recycled" as a feed gas

Refined Grade Methanol - Distilled methanol, defined as 99.8 wt% minimum purity; used directly in downstream

Eastman processes

SCFH - Standard Cubic Feet per Hour

Slurry Concentration - percentage of weight of slurry (solid plus liquid) which is catalyst (on an oxide basis)

Sl/hr-kg - Standard Liter(s) per Hour per Kilogram of Catalyst

Syngas - Abbreviation for Synthesis Gas

Syngas Utilization - defined as the number of standard cubic feet of Balanced Gas plus CO Gas to the

LPMEOH™ Demonstration Unit required to produce one pound of Raw Methanol

Synthesis Gas - A gas containing primarily hydrogen (H₂) and carbon monoxide (CO), or mixtures of

H₂ and CO; intended for "synthesis" in a reactor to form methanol and/or other hydrocarbons (synthesis gas may also contain CO₂, water, and other gases)

Tie-in(s) - the interconnection(s) between the LPMEOH™ Process Demonstration

Facility and the Eastman Facility

TPD - Ton(s) per Day

volumetric flowrate, thousand standard cubic feet per hour

VOC - volatile organic compound
WBS - Work Breakdown Structure

wt - weight

Executive Summary

The Liquid Phase Methanol (LPMEOH™) Demonstration Project at Kingsport, Tennessee, is a \$213.7 million cooperative agreement between the U.S. Department of Energy (DOE) and Air Products Liquid Phase Conversion Company, L.P. (the Partnership) to produce methanol from coal-derived synthesis gas (syngas). Air Products and Chemicals, Inc. (Air Products) and Eastman Chemical Company (Eastman) formed the Partnership to execute the Demonstration Project. The LPMEOH™ Process Demonstration Unit was designed, constructed, and is in operation at a site located at the Eastman coal-to-chemicals complex in Kingsport.

On 04 October 1994, Air Products and Eastman signed the agreements that would form the Partnership, secure the demonstration site, and provide the financial commitment and overall project management for the project. These partnership agreements became effective on 15 March 1995, when DOE authorized the commencement of Budget Period No. 2 (Modification No. A008 to the Cooperative Agreement). The Partnership has subcontracted with Air Products to provide the overall management of the project, and to act as the primary interface with DOE. As subcontractor to the Partnership, Air Products provided the engineering design, procurement, construction, and commissioning of the LPMEOHTM Process Demonstration Unit, and is providing the technical and engineering supervision needed to conduct the operational testing program required as part of the project. As subcontractor to Air Products, Eastman is responsible for operation of the LPMEOHTM Process Demonstration Unit, and for the interconnection and supply of syngas, utilities, product storage, and other needed services.

The project involves the operation of an 80,000 gallons per day (260 tons per day (TPD)) methanol unit utilizing coal-derived syngas from Eastman's integrated coal gasification facility. The new equipment consists of syngas feed preparation and compression facilities, the liquid phase reactor and auxiliaries, product distillation facilities, and utilities.

The technology to be demonstrated is the product of a cooperative development effort by Air Products and DOE in a program that started in 1981. Developed to enhance electric power generation using integrated gasification combined cycle (IGCC) technology, the LPMEOH™ process is ideally suited for directly processing gases produced by modern day coal gasifiers. Originally tested at a small, DOE-owned experimental unit in LaPorte, Texas, the technology provides several improvements essential for the economic coproduction of methanol and electricity directly from gasified coal. This liquid phase process suspends fine catalyst particles in an inert liquid, forming a slurry. The slurry dissipates the heat of the chemical reaction away from the catalyst surface, protecting the catalyst and allowing the methanol synthesis reaction to proceed at higher rates.

At the Eastman complex, the technology is integrated with existing coal gasifiers. A carefully developed test plan will allow operations at Eastman to simulate electricity demand load-following in coal-based IGCC facilities. The operations will also demonstrate the enhanced stability and heat dissipation of the conversion process, its reliable on/off

operation, and its ability to produce methanol as a clean liquid fuel without additional upgrading. An off-site, product-use test program will be conducted to demonstrate the suitability of the methanol product as a transportation fuel and as a fuel for stationary applications for small modular electric power generators for distributed power.

The four-year operating test phase and off-site product-use test program will demonstrate the commercial viability of the LPMEOH™ process and allow utilities to evaluate the application of this technology in the coproduction of methanol with electricity. A typical commercial-scale IGCC coproduction facility, for example, could be expected to generate 200 to 350 MW of electricity, and to also manufacture 45,000 to 300,000 gallons per day of methanol (150 to 1,000 TPD). A successful demonstration at Kingsport will show the ability of a local resource (coal) to be converted in a reliable (storable) and environmentally preferable way to provide the clean energy needs of local communities for electric power and transportation.

This project may also demonstrate the production of dimethyl ether (DME) as a mixed coproduct with methanol if laboratory- and pilot-scale research and market verification studies show promising results. If implemented, the DME would be produced during the last six months of the four-year demonstration period. DME has several commercial uses. In a storable blend with methanol, the mixture can be used as a peaking fuel in gasification-based electric power generating facilities, or as a diesel engine fuel. Blends of methanol and DME can be used as chemical feedstocks for synthesizing chemicals, including new oxygenated fuel additives.

The project was reinitiated in October of 1993, when DOE approved a site change to the Kingsport location. DOE conditionally approved the Continuation Application to Budget Period No. 2 (Design and Construction) in March of 1995 and formally approved it on 01 June 1995 (Modification No. M009). After approval, the project initiated Phase 1 - Design - activities. Phase 2 - Construction - activities were initiated in October of 1995. The project required review under the National Environmental Policy Act (NEPA) to move to the construction phase. DOE prepared an Environmental Assessment (DOE/EA-1029), and subsequently a Finding of No Significant Impact (FONSI) was issued on 30 June 1995. The Cooperative Agreement was modified (Modification No. A011) on 08 October 1996, authorizing the transition from Budget Period No. 2 (Design and Construction) to the final Budget Period (Commissioning, Start-up, and Operation). This modification provides the full \$213,700,000 of authorized funding, with 56.7% participant cost share and 43.3% DOE cost share.

During this quarter, initial planning and procurement work continued on the seven project sites which have been accepted for participation in the off-site, product-use test program. Approximately 12,000 gallons of fuel-grade methanol (98+ wt% methanol, <1 wt% water) produced during operation on carbon monoxide (CO)-rich syngas at the LPMEOHTM Demonstration Unit was loaded into trailers and shipped off-site for future product-use testing. At one of the projects, three buses have been tested on chemical-grade methanol and on fuel-grade methanol from the LPMEOHTM Demonstration Project. At two other project sites (a flexible fuel vehicle and a fuel cell application), testing on fuel-grade methanol from

the LPMEOH™ Demonstration Project is scheduled for the second quarter of calendar year 1998.

During the reporting period, planning for a proof-of-concept test run of the Liquid Phase Dimethyl Ether (LPDMETM) Process at the Alternative Fuels Development Unit (AFDU) in LaPorte, TX continued. The commercial catalyst manufacturer (Calsicat) has prepared the first batch of dehydration catalyst in large-scale equipment. Air Products will test a sample of this material in the laboratory autoclave.

Catalyst activity, as defined by the ratio of the rate constant at any point in time to the rate constant for freshly reduced catalyst (as determined in the laboratory autoclave), was monitored for the initial extended operation at the lower initial reactor operating temperature of 235°C. At this condition, the decrease in catalyst activity with time from the period 20 December 1997 through 27 January 1998 occurred at a rate of 1.0% per day, which represented a significant improvement over the 3.4% per day decline measured during the initial six weeks of operation in April and May of 1997. The deactivation rate also improved from the longer-term rate of 1.6% per day calculated throughout the summer and autumn of 1997.

Based on this improvement, DOE accepted a recommendation by Air Products and Eastman to further reduce the reactor temperature to 225°C. The initial operation at this temperature (from 31 January through 18 February 1998) showed a modest improvement in the deactivation rate to 0.7% per day. However, most of the activity decline occurred during a test period on CO-rich feed gas and immediately after an interruption in the Balanced Gas supply at the end of that test case. This observation more likely indicated a real change in catalyst activity, and this type of behavior seems to have occurred after other excursions in the Balanced Gas supply. During two additional stable operating periods between 19 February and 31 March 1998, deactivation rates of 0.27% and 0.36% per day were measured. A discontinuity occurred in the data on 15 March 1998, again coincidental with an excursion in the Balanced Gas supply. If the current results prove to be correct, the current baseline activity decline of about 0.4% per day is a measurable improvement over the 1% per day rate seen at 235°C in January of 1998 and matches the original target from the 4-month proof-of concept run on a natural-gas derived syngas at the LaPorte AFDU. Additional operating time is necessary to further quantify the catalyst deactivation rate and the effects of operating conditions and syngas supply excursions.

The weight of catalyst in the LPMEOHTM Reactor has reached 67% of the design value, and the slurry concentration approached 40 wt%. Catalyst slurry samples from the LPMEOHTM Reactor have been taken on a regular basis to correlate any change in plant performance with changes in the physical properties of the catalyst. So far, samples from mid-February and mid-March of 1998 have shown an increase in arsenic loading, although not nearly to the levels measured in the summer of 1997. Copper crystallite size measurements are still pending, as are analyses from more recent samples which will help complete the picture.

The performance of the alternative gas sparger, which was designed by Air Products and installed into the LPMEOHTM Reactor prior to the restart of the LPMEOHTM Demonstration Unit in December of 1997, was monitored throughout the reporting period. Pressure drop through the gas sparger of the LPMEOHTM Reactor was stabilized using a continuous flush

of condensed oil and entrained slurry which were gravity-drained from the 29C-05 secondary oil knock-out drum and 29C-06 cyclone. As with the original gas sparger design, the return of the internal oil and slurry streams via the flush connection was required to stabilize the pressure drop after extended interruptions of the flush fluid. When compared to the original gas sparger, the alternative gas sparger may have greater flexibility in maintaining stable pressure drop after interruptions of the syngas supply; this may also be a result of greater attention to achieving a proper standby condition during shutdowns. The most recent results provide an initial confirmation of the encouraging data reported for the first two weeks of operation at the end of the prior reporting period. This parameter will continue to be closely monitored for any change in flow resistance.

The Alternative Fuels Field Test Unit (AFFTU), a transportable laboratory equipped with an autoclave and analytical equipment, was shipped from the Air Products' Iron Run laboratory in Allentown, PA to Kingsport to perform additional testing on the reactor feed gas at the site. Analytical results from the AFFTU showed less than 10 ppbv concentrations of metal carbonyls and hydrogen sulfide within the reactor loop. Carbonyl sulfide was typically less than 10 ppbv in the loop, but occasionally drifted higher; these excursions could not be correlated with any changes in the feed gas cleanup operations upstream of the LPMEOHTM facility. Performance results from the 31-day campaign on coal-derived syngas at Kingsport were generally consistent with other laboratory experiments on poison-free syngas. A postmortem analysis on the catalyst revealed no unusual levels of catalyst poisons or significant changes in catalyst physical properties. The AFFTU test concluded on 20 January 1998, and the equipment was returned to the Air Products' Iron Run laboratory.

During the reporting period, a total of 5,762,047 gallons of methanol was produced at the LPMEOHTM Demonstration Unit. Apart from 12,000 gallons shipped off-site for productuse testing, Eastman accepted all of this methanol for use in the production of methyl acetate, and ultimately cellulose acetate and acetic acid. During a portion of the operating period on CO-rich syngas, approximately 181,800 gallons (600 tons) of stabilized methanol (99.3 wt% methanol, 0.3 wt% water) was pumped directly from the LPMEOHTM Demonstration Unit to Eastman's methyl acetate plant, bypassing the normal route through the distillation equipment designed to remove water, higher alcohols, and process oil. This test was the first attempt to feed a stabilized methanol stream with low water content directly into one of Eastman's downstream chemical processes, providing another indication of the flexibility of the LPMEOHTM Process. No safety or environmental incidents were reported during this quarter. Availability exceeded 99%, as the demonstration unit continued to operate through the longest continuous campaign to date (45 days) as of 31 March 1998.

Ninety-nine percent (99%) of the \$38 million of funds forecast for the Kingsport portion of the LPMEOHTM Process Demonstration Project for the Phase 1 and Phase 2 tasks have been expended (as invoiced), as of 31 March 1998. Nineteen percent (19%) of the \$158 million of funds for the Phase 3 tasks have been expended (as invoiced), as of 31 March 1998.

A. Introduction

The Liquid Phase Methanol (LPMEOHTM) demonstration project at Kingsport, Tennessee, is a \$213.7 million cooperative agreement between the U.S. Department of Energy (DOE) and Air Products Liquid Phase Conversion Company, L. P. (the Partnership). Air Products and Chemicals, Inc. (Air Products) and Eastman Chemical Company (Eastman) formed the Partnership to execute the Demonstration Project. A demonstration unit producing 80,000 gallons per day (260 TPD) of methanol was designed, constructed, and is operating at a site located at the Eastman complex in Kingsport. The Partnership will own and operate the facility for the four-year demonstration period.

This project is sponsored under the DOE's Clean Coal Technology Program, and its primary objective is to "demonstrate the production of methanol using the LPMEOHTM Process in conjunction with an integrated coal gasification facility." The project will also demonstrate the suitability of the methanol produced for use as a chemical feedstock or as a low-sulfur dioxide, low-nitrogen oxides alternative fuel in stationary and transportation applications. The project may also demonstrate the production of dimethyl ether (DME) as a mixed coproduct with methanol, if laboratory- and pilot-scale research and market verification studies show promising results. If implemented, the DME would be produced during the last six months of the four-year demonstration period.

The LPMEOH™ process is the product of a cooperative development effort by Air Products and the DOE in a program that started in 1981. It was successfully piloted at a 10-TPD rate in the DOE-owned experimental unit at Air Products' LaPorte, Texas, site. This demonstration project is the culmination of that extensive cooperative development effort.

B. Project Description

The demonstration unit, which occupies an area of 0.6 acre, is integrated into the existing 4,000-acre Eastman complex located in Kingsport, Tennessee. The Eastman complex employs approximately 12,000 people. In 1983, Eastman constructed a coal gasification facility utilizing Texaco technology. The synthesis gas (syngas) generated by this gasification facility is used to produce carbon monoxide and methanol. Both of these products are used to produce methyl acetate and ultimately cellulose acetate and acetic acid. The availability of this highly reliable coal gasification facility was the major factor in selecting this location for the LPMEOHTM Process Demonstration. Three different feed gas streams (hydrogen gas, carbon monoxide gas, and balanced gas) will be diverted from existing operations to the LPMEOHTM Demonstration Unit, thus providing the range of coalderived syngas ratios (hydrogen to carbon monoxide) needed to meet the technical objectives of the demonstration project.

For descriptive purposes and for design and construction scheduling, the project has been divided into four major process areas with their associated equipment:

- Reaction Area Syngas preparation and methanol synthesis reaction equipment.
- Purification Area Product separation and purification equipment.

- Catalyst Preparation Area Catalyst and slurry preparation and disposal equipment.
- Storage/Utility Area Methanol product, slurry, and oil storage equipment.

The physical appearance of this facility closely resembles the adjacent Eastman process plants, including process equipment in steel structures.

• Reaction Area

The reaction area includes feed gas compressors, catalyst guard beds, the reactor, a steam drum, separators, heat exchangers, and pumps. The equipment is supported by a matrix of structural steel. The most salient feature is the reactor, since with supports, it is approximately 84-feet tall.

• Purification Area

The purification area features two distillation columns with supports; one is approximately 82-feet tall, and the other 97-feet tall. These vessels resemble the columns of the surrounding process areas. In addition to the columns, this area includes the associated reboilers, condensers, air coolers, separators, and pumps.

• Catalyst Preparation Area

The catalyst preparation area consists of a building with a roof and partial walls, in which the catalyst preparation vessels, slurry handling equipment, and spent slurry disposal equipment are housed. In addition, a hot oil utility system is included in the area.

Storage/Utility Area

The storage/utility area includes two diked lot-tanks for methanol, two tanks for oil storage, a slurry holdup tank, a trailer loading/unloading area, and an underground oil/water separator. A vent stack for safety relief devices is located in this area.

C. Process Description

The LPMEOH™ Demonstration Unit is integrated with Eastman's coal gasification facility. A simplified process flow diagram is included in Appendix A. Syngas is introduced into the slurry reactor, which contains a slurry of liquid mineral oil with suspended solid particles of catalyst. The syngas dissolves through the mineral oil, contacts the catalyst, and reacts to form methanol. The heat of reaction is absorbed by the slurry and is removed from the slurry by steam coils. The methanol vapor leaves the reactor, is condensed to a liquid, sent to the distillation columns for removal of higher alcohols, water, and other impurities, and is then stored in the day tanks for sampling before being sent to Eastman's methanol storage. Most of the unreacted syngas is recycled back to the reactor with the syngas recycle compressor, improving cycle efficiency. The methanol will be used for downstream feedstocks and in off-site, product-use testing to determine its suitability as a transportation fuel and as a fuel for stationary applications in the power industry.

D. Results and Discussion

The project status is reported by task, covering those areas in which activity took place during the reporting period. Major accomplishments during this period are as follows:

D.1 Off-Site Testing (Product-Use Demonstration)

Discussion

The product-use test program, developed in 1992 to support the demonstration at the original Cool Water Gasification Facility site, became outdated due in large part to changes within the power and chemical industries. This original product test program under-represented new utility dispersed electric power developments, and possibly new mobile transport engine developments. The updated product-use test program attempts for broader market applications and for commercial fuels comparisons. The objective of the product-use test program is to demonstrate commercial market applications for the "as produced" methanol as a replacement fuel and as a fuel supplement. Fuel economics will be evaluated for the "as produced" methanol for use in municipal, industrial, and utility applications and as fuel supplements for gasoline, diesel, and natural gas. These fuel evaluations will be based on the U.S. energy market needs projected during the 1998 to 2018 time period when the LPMEOHTM technology is expected to be commercialized.

The product-use test program has been developed to enhance the early commercial acceptance of central clean coal technology processing facilities, coproducing electricity and methanol to meet the needs of the local community. One of the advantages of the LPMEOHTM Process for coproduction from coal-derived syngas is that the as-produced, stabilized (degassed) methanol product is of unusually high quality (e.g. less than 1 wt% water) which may be suitable for the premium fuel applications. When compared to conventional methanol synthesis processes, cost savings (10 to 15%) of several cents per gallon of methanol can be achieved in coproduction facilities, if the suitability of the stabilized product as a fuel can be demonstrated. The applications (for example, as a hydrogen source for fuel cells, and as a clean transportable, storable fuel for dispersed power) will require testing of the product to confirm its suitability. Chemical feedstock applications will also be tested as warranted.

A limited quantity (up to 400,000 gallons) of the methanol product as produced from the demonstration unit will be made available for product-use tests. Product-use tests were targeted for an approximate 18 to 30-month period, and commenced during the first year of demonstration operations. An initial inventory of approximately 12,000 gallons of stabilized methanol was produced at LPMEOHTM Demonstration Unit in February of 1998 to supply the needs of the product-use test program; due to the pre-1998 timing for certain tests, methanol was shipped from the inventory held at the Alternative Fuels Development Unit (AFDU) in LaPorte, TX. Air Products, ARCADIS, Geraghty & Miller (formerly Acurex

Environmental Corporation), and the DOE have worked together to select the projects to be included in the off-site, product-use test program.

Activity during this quarter

Eight sites involving a variety of product-use tests have been selected to participate in this task. The sites and project titles are listed in Appendix B-1. In a letter to the DOE dated 31 July 1997, Air Products formally recommended that seven of the eight projects had been defined in sufficient detail so that final planning and implementation should begin. DOE accepted Air Products' recommendation to proceed with the seven projects in August of 1997. The eighth project, involving the testing of a water/naphtha/methanol emulsion as a transportation fuel, is awaiting final project definition.

All of the remaining product-use test projects have begun planning and equipment procurement. Methanol produced from carbon monoxide (CO)-rich syngas at the LaPorte AFDU has been shipped to three of the project sites. Appendix B-2 through B-8 contain summary reports from the approved projects. Highlights from these reports include:

Acurex Flexible Fuel Vehicle (FFV) - The first drum of M85 fuel using methanol supplied from the inventory at the LaPorte AFDU was prepared. Operation is scheduled for May of 1998.

Stationary Turbine for Volatile Organic Carbon (VOC) Control - ARCADIS, Geraghty & Miller is continuing to work on selecting a host site for the project. Allied Signal is the leading candidate using their existing 525 kilowatt gas turbine.

West Virginia University (WVU) Stationary Gas Turbine - The gas turbine has been run successfully on jet fuel. Work is focusing on overcoming a flame-out when the turbine is switched from jet fuel to methanol fuel at idle speed. Methanol from inventory at the LaPorte AFDU is being used in this program.

<u>Aircraft Ground Equipment Emulsion</u> - Tyndall Air Force Base will begin scoping tests in May of 1998 to determine the best emulsion composition.

<u>University of Florida Fuel Cell</u> - Testing is scheduled to begin in June of 1998 pending results of the analysis of the fuel-grade methanol from the LPMEOHTM Demonstration Project and an assessment of the impact (if any) of impurities on the fuel cell system.

West Virginia University Tri-Boro Bus - Three buses have been tested on chemical-grade methanol and on fuel-grade methanol from the inventory at the LaPorte AFDU. Data reduction is underway, and a full report is expected in July of 1998.

Florida Institute of Technology Bus & Light Vehicle - Both vehicles remain operational, and fuel-grade methanol from the LPMEOH™ Demonstration Project has been received. Emissions data will be collected and processed during the next reporting period

D.2 Commercialization Studies

Discussion

Several areas have been identified for development to support specific commercial design studies. These include: a) product purification options; b) front-end impurity removal options; c) catalyst addition/withdrawal options; and d) plant design configuration options. Plant sizes in the range of 300 TPD to 1,800 TPD and plant design configurations for the range from 20% up to 70% syngas conversion will be considered. The Kingsport demonstration unit design and costs will be the basis for value engineering work to focus on specific cost reduction targets in developing the initial commercial plant designs.

The Process Economics Study - Outline has been prepared to provide guidance for the overall study work. The four part outline is included in Appendix C. This Outline addresses several needs for this Task 1.5.2 Commercialization Study:

- a) to provide process design guidance for commercial plant designs.
- b) to meet the Cooperative Agreement's technical objectives requirement for comparison with gas phase methanol technology. This preliminary assessment will help set demonstration operating goals, and identify the important market opportunities for the liquid phase technology.
- c) to provide input to the Demonstration Test Plan (Task 2.3).
- d) to provide input to the Off-Site Testing (Task 1.4) product-use test program.

Recent Activities

- Part One of the Outline "Coproduction of Methanol" has been written for release as a Topical Report. Comments from DOE on the 31 March 1997 draft of the Topical Report "Economic Analysis LPMEOHTM Process as an Add-on to IGCC for Coproduction" are the current basis for discussion. As part of reviewing this report, Air Products has submitted a recommendation that the cost breakdown by plant area matches the format to be used in the Final Report Volume 1 Public Design. The Topical Report on the Economic Analysis of LPMEOHTM will be updated and sent to DOE for further comment.
- Part Two of the Outline "Baseload Power and Methanol Coproduction", has been incorporated into the paper, "Fuel and Power Coproduction - The Liquid Phase Methanol (LPMEOHTM) Process Demonstration at Kingsport ", that was presented at the DOE's Fifth Annual Clean Coal Technology Conference in January of 1997.
- Part Four of the Outline "Methanol Fuel Applications", was used as the basis to update the product-use test program (Task 1.4).

D.3 DME Design Verification Testing

Discussion

The first decision milestone, on whether to continue with dimethyl ether (DME) Design Verification Testing (DVT), was targeted for 01 December 1996. This milestone was relaxed to July of 1997 to allow time for further development of the Liquid Phase Dimethyl Ether (LPDMETM) catalyst system. DVT is required to provide additional data for engineering design and demonstration decision-making. The essential steps required for decision-making are: a) confirm catalyst activity and stability in the laboratory, b) develop engineering data in the laboratory, and c) confirm market(s), including fuels and chemical feedstocks. The DME Milestone Plan, showing the DVT work and the decision and implementation timing, is included in Appendix D.

Prior work in this task included a recommendation to continue with DME DVT and Market Economic Studies. Ongoing activity is focusing on Laboratory R&D.

DME DVT Recommendation

DOE issued a letter dated 31 July 1997 accepting Air Products' recommendation to continue with the design verification testing to coproduce DME with methanol, and to proceed with planning a proof-of-concept test run at the DOE's AFDU in LaPorte, Texas. A copy of the recommendation (dated 30 June 1997) is included in Appendix D. The recommendation was based on the results of the Market Economic Studies and on the LPDMETM catalyst system R&D work, and is summarized in the following.

The Market Economic Studies show that the LPDMETM Process should have a significant economic advantage for the coproduction of DME with methanol for local markets. The studies show that the market applications for DME are large. DME is an ultra clean diesel fuel; and an 80% DME mixture with methanol and water is now being developed and tested by others. DME is a key intermediate in a commercial syngas-to-gasoline process, and is being developed as an intermediate for other chemicals and fuels. An LPDMETM catalyst system with reasonable long-term activity and stability has been developed from the laboratory R&D work.

Based upon the potential size of the markets and the promise of the LPDME™ catalyst system, proof-of-concept planning for the LaPorte AFDU was recommended. A summary of the DME DVT recommendation is:

• Planning for a DME test run at the LaPorte AFDU, in conjunction with other DOE Liquid Fuels Programs, should be initiated. Test plans, budgets, and a schedule for these LaPorte AFDU tests should now be developed. Up to \$875,000 of Clean Coal Technology Program budget support from the LPMEOHTM Project budget could be made available to support a suitable LPDMETM test run at LaPorte.

• An implementation decision, made mutually by the DOE's Clean Coal Technology Program (DE-FC22-92PC90543) LPMEOH™ project participants, and by the DOE's Liquid Fuels Program (DE-FC22-95PC93052) project participants, will be made in time to meet the schedule for testing at LaPorte.

LPDMETM is not applicable to hydrogen (H₂)-rich syngas; and it is unlikely that a substantive LPDMETM demonstration will be recommended for Kingsport. Therefore, a convincing case that the test-run on CO-rich syngas at LaPorte will lead to successful commercialization must be made, prior to approving the final test-run plan. The strategy for commercialization must present the technical logic to combine the results of the following two areas:

- 1) catalyst performance (productivity, selectivity, and life) for the LPDME™ catalyst system under CO-rich syngas from the proof-of-concept testing at the LaPorte AFDU; and
- 2) reactor performance (methanol catalyst activity and life, hydrodynamics, and heat transfer) from the LPMEOHTM Process Demonstration Unit at Kingsport.

The DME DVT recommendation summarizes the catalyst targets, experimental results, and the corresponding economics for a commercially successful LPDMETM catalyst.

Market Economic Studies

Work on the feasibility study for the coproduction of DME and methanol with electric power continued. The product DME would be used as a domestic liquid cooking fuel, to replace imported Liquid Petroleum Gas, for China and the Pacific Rim regions. The results to date, are included in the DME recommendation in Appendix D.

Laboratory R&D

Initially, synthesis of DME concurrently with methanol in the same reactor was viewed as a way of overcoming the syngas conversion limitations imposed by equilibrium in the LPMEOH™ Process. Higher syngas conversion would provide improved design flexibility for the coproduction of power and liquid fuels from an IGCC facility. The LPDME™ Process concept seemed ideally suited for the slurry-based liquid phase technology, since the second reaction (methanol to DME) could be accomplished by adding a second catalyst with dehydration activity to the methanol-producing reactor. Initial research work determined that two catalysts, a methanol catalyst and an alumina-based dehydration catalyst, could be physically mixed in different proportions to control the yield of DME and of methanol in the mixed product. Previously, proof-of-concept runs, in the laboratory and at the Alternative Fuels Development Unit (AFDU), confirmed that a higher syngas conversion could be obtained when a mixture of DME and methanol is produced in the liquid phase reactor.

Subsequent catalyst activity-maintenance experiments have shown the catalyst system utilized in the proof-of-concept runs experienced relatively fast deactivation compared to the LPMEOHTM process catalyst system. Further studies of the LPDMETM catalyst deactivation phenomenon, initially undertaken under the DOE's Liquid Fuels Program (Contract No. DE-FC22-95PC93052), was continued under this Task 1.5.3 through Fiscal Year 1996, and is now again being continued under the DOE Liquid Fuels Program. This LPDMETM catalyst deactivation research has determined that an interaction between the methanol catalyst and the dehydration catalyst is the cause of the loss of activity. Parallel research efforts--a) to determine the nature of the interaction; and b) to test new dehydration catalysts--was undertaken. In late 1995, the stability of the LPDMETM catalyst system was greatly improved, to near that of an LPMEOHTM catalyst system, when a new aluminum-based (AB) dehydration catalyst was developed. This new AB catalyst development showed that modification of the LPDMETM catalyst system could lead to long life. During this quarter, laboratory work continued on developing an LPDMETM catalyst system based on the AB series of catalysts.

Summary of Laboratory Activity and Results

- A manufacturer for the dehydration catalyst (Calsicat) was selected by the Liquid Fuels Program. The initial schedule (contained in the DME Milestone Plan in Appendix D) showed a catalyst delivery date to the LaPorte AFDU of 01 March 1998. This date could be met assuming that the dehydration catalyst would be produced in a series of campaigns in a pilot plant. The Liquid Fuels Program has determined that it is important to complete the scale-up of the dehydration catalyst as part of the proposed LaPorte run. This will increase the time requirement, as a production test in the pilot plant is still required before operating the commercial catalyst production unit. The new estimated delivery date of dehydration catalyst to LaPorte is 01 June 1998. The DME DVT Recommendation will be updated to reflect the change in schedule and the impact (if any) on the implementation of the coproduction of DME with methanol at the LPMEOHTM Demonstration Unit.
- Recent activities have focused on the scale-up of the manufacturing technique for the
 dehydration catalyst. The commercial catalyst manufacturer (Calsicat) has prepared the
 first batch of dehydration catalyst in large-scale equipment. Air Products will test a
 sample of this material in the laboratory autoclave.

D.4 LPMEOH™ Process Demonstration Facility - Methanol Operation

Table D.4-1 contains the summary table of performance data for the LPMEOH™ Demonstration Unit during the reporting period. These data represent daily averages, typically from a 24-hour material balance period, and those days with less than 12 hours of stable operation are omitted. Appendix E contains samples of the detailed material balance reports which are representative of the operation of the LPMEOH™ Demonstration Unit during the reporting period.

TABLE D.4-1

DATA SUMMARY FOR LPMEOHTM DEMONSTRATION UNIT

| Spamer | | Kesistance | E | 476 | 4 58 | 88. | 4.73 | 4.77 | 4,72 | 4.65 | 4,60 | 4.77 | 4.85 | 4.89 | 4.83 | 4.85 | 20,0 | 9.50 | 5.29 | 534 | 5.38 | 5.27 | 5.34 | 5.29 | 4.96 | 68.9 | 8. t | 4.93 | 4.78 | 4.79 | 4.92 | 4.78 | 48.4 | 4. n | 5.58 4.78 | 4.78 | 4.93 | 5.25 F. AF | 6.16 | 5.42 | 5.23 | 5.27 | 5.42 | 5. 5. 5. 5. | 5.44 | 5.42 | 5.47 | 5.47 | 5,34 A.A.B | 5.39 | 5.41 |
|------------|--------------|------------------|------------|------------|------------|----------|----------|----------|----------|----------|----------|-----------|------------|------------|-------------|--------------|-------------|------------|-----------|-----------|--------------|-----------|------------|-----------|-------------|-----------------|--------------|------------|----------|-------------|----------------|------------|----------------------------|----------|--------------|----------|--|----------------|------------|--------------|-----------|----------------|------------|----------------|-----------|--------------|-----------|----------------|--------------------|---------------------------|--------------|
| Spamer | ę | ; | (lsd) | 4 22 | 5.54 | 5.12 | 5.27 | 4.43 | 4.43 | 4.32 | 5.17 | 4.79 | 4.59 | 4.87 | 5.04 | 5.18 | 6 6 6 | 5 6 | 5.54 | 5.48 | 5.03 | 5.83 | 5.19 | 5,45 | 4.94 | | 6, 4 6, 4 | 4.4 | 4.82 | 4.59 | 4.72 | 5.18 | 5.07 | 5.4 | - 6 - 6 | 9,03 | 8.87 | 9.57 | 4.84 | 6.12 | 6.28 | 5.63 | , i | 5,0/ 7,33 | 8 89 | 5.31 | 5.17 | 5.18 | 5.12 4.87 | 5.13 | 5.02 |
| > | Overall | | | 25 | <u>8</u> | 155 | 168 | 169 | 181 | 185 | 170 | 166 | 188 | 168 | 185 | 163 | <u> </u> | 2 5 | 172 | 167 | 168 | 163 | 167 | 170 | 155 | 164 184 | 9 9 | <u>8</u> | 151 | 1 54 | 154 | 162 | 128 | ¥ 6 | 147 | 139 | 138 | 135 25 | 159 | 149 | 151 | 147 | 148 077 | 148 | 142 | . £3 | 155 | <u>ቴ</u> የ | 701 8 71 | 5 5 | 148 |
| Reactor | . Vol. Prod. | עם איניים איניים | in popular | 0.118 | 0,119 | 0.119 | 0.107 | 0.105 | 0.091 | 0.088 | 0.087 | 0.090 | 0.093 | 0.093 | 0.092 | 0.094 | 9600 | 0.098 | 0.097 | 0.097 | 0.101 | 0.100 | 0.102 | 0.104 | 0.099 | 0.100 | 0.102 | 0.087 | 0.087 | 0,089 | 0.090 | 0.091 | 0.090 | 0.092 | 0.076 | 0.082 | 0.094 | 0.099 | 0.120 | 0.120 | 0.116 | | 2 5 | 9.10 | 0.102 | 0.10 | 0.102 | 0.105 | 0.09 | 0.089 | 0.084 |
| Catalyst | MeOH Prod. | (omol/hr.ka) | | 32.33 | 35.73 | 35.57 | 31.88 | 30,05 | 30.21 | 30,00 | 30.42 | 29,78 | 29,88 | 30.03 | 30.04 | 30.20 | 2 6 | 29.89 | 29.67 | 29,38 | 29.22 | 29.45 | 29,22 | 29.78 | 29.62 | 30.20 | 23.53 | 23.38 | 22.99 | 23,16 | 23.07 | 23.28 | 23.32 | 22.47 | 21.15 | 20.77 | 20.39 | 20.25 19.08 | 20,80 | 22.15 | 22.5 | 27.28 | 2 F | 20.62 | 20.18 | 21.11 | 20.84 | 20.87 20.7 | 20.85 | 21.03 | 20.85 |
| Raw MeOH | Production | Ē | î | 241.9 | 287.2 | 285.9 | 236.8 | 224.8 | 225.5 | 224.1 | 227.4 | 222.7 | 223.4 | 224.6 | 224.5 | 0227 0230 | 223.1 | 223.6 | 221.9 | 219.7 | 218.5 | 220.3 | 218.6 | 222.8 | 221.9 | 220.0 | 2244 | 221.7 | 218.7 | 220.2 | 219.5 | 221.3 | 8. 2. 2. 2. 3. 2. 3. | 210.9 | 189.7 | 196.0 | 192.4 | 180.8 | 197.6 | 210.6 | 213.6 | 271.8 8.172 | 2225 | 217.1 | 212.2 | 220.0 | 219.3 | 219.7 | 219.4 | 221.3 | 220.8 |
| Syngas | ij | (SCE/Ib) | | 39.9 | 40.7 | 41.4 | 39.1 | 39.3 | 39.1 | 39.2 | 38.4 | 39.2 | 39.5 | 39.3 | 38.8 | 30.7 | 39.4 | 39.0 | 39.5 | 39.8 | 40.0 | 39.7 | 39.8 | 39.1 | 4.66 | 39.0 | 39.3 | 39.4 | 39.9 | 39.9 | 6.1 | 38.2 | 39.00 | 410 | 4.2 | 44.3 | 44.2 | 484 | 44.7 | 41.5 | 40.5 | 39.4 | 39.3 | 39.4 | 40.2 | 39.7 | 39.8 | 39.7 | 40.1 | 39.5 | 39.6 |
| Reactor | O-T-M | Conv. (%) | | 23.2 | 24.2 | 24.3 | 22.9 | 27. | 22.7 | 22.9 | 23.2 | 27 | 22.0 | 27.5 | 22.3 | 214 | 21.2 | 21.4 | 21.1 | 21.0 | 20.6 | 20.8 | 20.8 | 20.B | 0 C | 20.0 | 21.7 | 21.0 | 50.9 | 21.2 | 21.3 | 4.12 | 4.2 | 21.9 | 17.8 | 17.3 | 18.9 | 15.7 | 18.7 | 18.6 | 5.5 | 20.4 | 20.6 | 20.2 | 19.9 | 20.5 | 20.4 | 20.6 | 21.3 | 212 | 21.3 |
| 8 | Conv. | 8 | | 55.4 | 43.2 | 45.9 | 47.4 | 52.5 | 54.0 | 58.4 | 20.8 | 20.8 | 20.9 | 48.4 | 46.9 8.5 | 49.7 | 48.7 | 47.8 | 46.8 | 48.2 | 48.5 | 42.3 | 45.2 | \$. | | . 45. B. 55. | 52.2 | 43.3 | 43.0 | 4.4 | 43.5 | 5.6 2.6 | 40.4 | 47.6 | 12.4 | 12.2 | 15.5 5.5 6.5 7.5 7.5 7.5 7.5 7.5 7.5 7.5 7.5 7.5 7 | 109 | 49.0 | 35.5 | | 43.8 | 412 | 43.1 | 45.3 | 4. | 8.4 | 44.6 6.44.6 | 48.3 | 46.4 | 48.5 |
| Catalyst | Age | (eta) | | 1.28 | - . | 1.15 | 1.12 | 1.18 | 27 | 1.27 | 1.20 | 1. | 1.08 | 8 5 | 5 5 | 10, | 9 | 1.0 | 0.97 | 0.95 | 0.95 | 0.80 | 0.92 | 28.0 | \$ 8 5 6 | 0.95 | 9 | 0.89 | 0.87 | 0.87 | 0.87 | 8.0 | 0.88 | 0.89 | 0.89 | 0.88 | 9. 6 | 0.83 | 0.85 | 0.78 | 2 2 | 9.6 | 0.79 | 0.78 | 0.79 | 0.81 | 8.6 | 0.78 0.80 | 0.84 | 0.82 | 0.82 |
| Catalyst | Inventory | 9 | : | 19,500 | 19,500 | 19,500 | 9,500 | 19,500 | 19,500 | 19,500 | 19,500 | 19,500 | 19,500 | 19,500 | 19,500 | 19 500 | 19,500 | 19,500 | 19,500 | 19,500 | 19,500 | 19,500 | 200,61 | 000 | 20,00 | 19,500 | 24,800 | 24,800 | 24,800 | 24,800 | 24,800 | 24,900 | 24,800 | 24,800 | 24,800 | 24,800 | 24,800 | 24,800 | 24,800 | 24,800 | 200,42 | 27,450 | 27,450 | 27,450 | 27,450 | 27,450 | 27,450 | 27.450 | 27,450 | 27,450 | 27,450 |
| Gassed | Slurry | Hat (m) | | 49.0 | 53.5 | 53.0 | 52.5 | 51.0 | 28.6 | 60.5 | 62.0 | 28.5 | בי מלים | τ. τ. τ | 98.0 | 55.5 | 55.0 | 54.5 | 54.5 | <u>%</u> | 51.5 | 52.5 | 0.0 | 2 2 | 3 E | 51,5 | 61,5 | 60.5 | 0.09 | 28.5 | 20.00 |) u | 57.0 | 55.5 | 62.0 | 57.0 | 49.0 | 40.5 | 39.5 | 42.0 | £ £ | 200 | 20.0 | 48.5 | 49.5 | 50.5 | 51.0 | 49.5 | 57.0 | 59.0 | 62.0 |
| Gas | Holdup | (vol%) | • | 50,6 | 52.5 | 51.0 | 50.4 | 47.7 | 50.6 | 47.7 | 49.7 | 20.0 | 5. C | 200 | 49.0 | 48.7 | 49.5 | 49.2 | 20.0 | 49.6 | 48.5 | 200 | 5 6 5 7 | 40.7 | 49.4 | 48.6 | 48.2 | 47.2 | 48.2 | 47.8 | | 7 7 | 49.3 | 47.8 | 54.2 | 53.0 | 49.4 | 46.9 | 40.6 | 0.4 | 45.5 | 45.2 | 46.3 | 44.2 | 44.9 | 47.8 | 47.0 | 43.4 | 47.8 | 48.5 | 48.8 |
| Slumy | Conc | (wt% ox) | | 32.1 | 31.0 | 30.5 | 30.5 | 28.8 | 28.1 | 4 6 | 5.6.6 | 27.9 | 4,0 | 4.00 | 28.5 | 28.5 | 29.0 | 29.1 | 29.5 | 29.5 | 8 5 7 | 4. 6 | - e | 20.00 | 29.5 | 30.1 | 31.1 | 31.0 | 31.7 | 32.0 | 34.6 | 9.00 | 33.3 | 33,3 | 33.7 | 35.1 | ر ا ا | 40.7 | 38.5 | 37.8 27.0 | 37.0 | 37.1 | 37.6 | 37.4 | 37.2 | 38.0 | 4.75 | 38.5 | 34.9 | 8. 5. 5. 15. | 33.5 |
| Space | Velocity | (Vhr-kg) | | 690'6 | 9,60 | 9,434 | 8,222 | 858'S | 5,843 | 5,748 | 525 | 6,00 | 9 9 | 0 0 | 9.071 | 9,174 | 9,388 | 9,320 | 9,345 | 9,278 | 9,254 | 9,422 | 0,100 | 9270 | 9.391 | 9,450 | 7,030 | 7,255 | 7,17 | 7,112 | 273 | 7 203 | 7,148 | 6,532 | 7,218 | 7,288 | 7,283 | 7,314 | 7,020 | 7,503 | 7.450 | 6,616 | 6,613 | 6,528 | 6,441 | 6,524 | 0,427 | 6,387 | 6,275 | 6,372 | 6,333 |
| Inlet Sup. | Velocity | (fl/sec) | | 0,73 | 0.77 | 0.78 | 9 6 | 7.7 | | 5 5 | 7 5 | 7 2 | 3 6 | 7 2 | 5.73 | 0.73 | 0.73 | 0.73 | 0.73 | 0.72 | 2,72 | 2 5 | 2 2 | 077 | 0.72 | 0.72 | 0.68 | 0.70 | 0.70 | 69.0 | 5 5 | 2.0 | 0.69 | 0.63 | 0.69 | 0.79 | 2,0 | 0.70 | 0.67 | 2 C | 2.5 | 0.70 | 0.70 | 0.69 | 99 | 0.69 | 9 6 | 0.68 | 0.67 | 0.68 | 0.0 |
| Purge | Sas | (KSCFH) | | 29.5 | 92.0 | 119.3 | | 200 | 2 2 | 2 6 | 2,0 | 6. c | 70.0 | 7 4 | 43.7 | 503 | 43.7 | 45,3 | 51.9 | 4.6 | 6.79 0.00 | 60.0 | 3 6 | 200 | 50. | 54.3 | 53.7 | 20.7 | 55.4 | 5.0 | 5.5 | 58. | 58.5 | 65.3 | 133.6 | 128.4 | 131.1 | 152.5 | 133.6 | 78.3 | 83.4 | 54.7 | 53.4 | 54.9 | 88.5 | 62.0 | - 6 | 65.2 | 69.1 | 61.5 | 0%0 |
| Reactor | Feed | (H2:CO) | | 5.34 | 3,70 | 3,99 | 4. r | 07.0 | 5.3 | 3 6 | ÷ 0 | 9,0 | 7. F | 7. Y | 4.4 | 5.07 | 90.9 | 4,88 | 4.87 | 4. r | 5.24 | 47.5 | 5 4 | 483 | 18 | 4.99 | 5.31 | 4.34 | 4.35 | ٠. د د | 4 0 4 | 389 | 4.18 | 4.77 | 0.74 | 0.78 | 8 6 | 0.74 | 5.86 | 349 | 3.83 | 4.48 | 4.1 | 4.43 | 8 | 4.46 6.46 | 4.52 | 4.49 | 83 | 4.59 | 4.00 0.04 |
| Recycle | Gas | (KSCFH) | | 2,211 | 977 | באר"א | 207'7 | 2 40 4 | 2,18 | 2,100 | 2,433 | 202,0 | 2,44 | 2,233 | 2,273 | 2,289 | 2,375 | 2,380 | 2,360 | 7,342 | 2,530 | 2342 | 2.397 | 2 382 | 2,387 | 2,385 | 2,217 | 2,338 | 2,315 | 2.55 | 2,337 | 2,323 | 2,300 | 2,037 | 2,295 | 2,320 | 2,343 | 2,348 | 2,218 | 2,437 | 2,413 | 2,349 | 2,344 | 2,328 | 2,292 | 2,304 | 2.258 | 2,249 | 2,184 | 2,234 | 37, |
| Fresh | Feed | (KSCFH) | | <u>8</u> | 3 3 | 2 2 | 7 2 | 3 5 | ŧ ; | 7 5 | 7 2 | 73.5 | 3 5 | 2 2 2 | 28 | 728 | 732 | 127 | 3 | 9 9 | 2 2 | 725 | 728 | 729 | ¥ | 727 | 735 | 728 | 8 8 | 2 25 | 23 | 732 | 727 | 721 | 735 | \$ £ | 8 8 | 700 | 736 | 2 22 | 128 | 728 | 728 | 712 | 2 8 | 728 827 | 228 | 724 | 73 | 727 | ij |
| | Pres. | (Deg C) (psig) | | 880 | 200 | 2 6 | 9 8 | 9 6 | 9 8 | 9 8 | 9 4 | 9 8 | 8 8 | 8 8 | 680 | 980 | 969 | 8 | 5 5 | 3 8 | 3 5 | 8 2 | 710 | 2 | 202 | 711 | 20 | 5 | 9 9 | 8 8 | 200 | 8 | 200 | 702 | 23 | 5 5 | 2 2 | 710 | 2 2 | 7.0 | 710 | 710 | 11 | 25 | 2 5 | 2 5 | 2.2 | 710 | 219 | 13 | 2 |
| | Төтр | O 60Q) | | 88 | 3 5 | 2 2 | 3 6 | 3 5 | 3 5 | 3 6 | 3 6 | 3 6 | 3 5 | 8 8 | 235 | 235 | 235 | 232 | 235 | 8 8 | 23.5 | 235 | 33 | 235 | 234 | 235 | ន | 525 | 2 2 | 22. | 225 | 522 | 225 | 225 | 52 5 | 8 6 | 2 2 | 224 | 223 | 24 | 225 | 225 | 225 | 82 | 5 5 | 225 | 225 | 225 | 225 | 22 z | 3 |
| | | Gas Type | | Balanced | Dalaricad | Dalanced | Balanced | Balancad | Ralanced | Rainmond | Balancad | Ralanced | Balancad | Balanced | Balanced | Balanced | Balanced | Batanced | Balanced | Dalanced | Balanced | Balanced | Balanced | Balanced | Balanced | Balanced | Balanced | Balanced | Balanced | Balanced | Balanced | Balanced | Balanced | Balanced | Texaco | Texago | Texaco | Техасо | Balanced | Balanced | Balanced | Balanced | Balanced | Balanced | Balanced | Balanced | Balanced | Balanced | Balanced | Balanced | |
| | Days | Onstream | : | 2 9 | 2 ; | ī ţ | 3 & | 2 5 | = == | 2 φ | 2 5 | 3 2 | 3 : | ខេ | 54 | 52 | 8 | 7.7 | 8 8 | 8 8 | 8 2 | 32 | 8 | 88 | 37 | 38 | 2 | Q : | 5 4 | ŧ 4 | . 6 | 47 | | | 8 2 | 3 5 | 8 8 | 25 | 57 | 8 8 | 8 | 2 | 85 | 8 7 | \$ 8 | 3 8 | 8 8 | 89 | | 22 | |
| | | Date | ; | 1-Jan-98 | 2 Inn 00 | A lan-98 | 5-Jan-98 | G-lan-98 | 7-Jan-98 | 8-lan-98 | 9-1an-98 | 10-Jan-98 | 11-Jan-98 | 12-Jan-98 | 13-Jan-98 | 14-Jan-98 | 15-Jan-98 | 16-Jan-98 | 1/-Jan-98 | 10-Jan-98 | 20-Jan-98 | 21-Jan-98 | 22-Jan-98 | 25-Jan-98 | 26-Jan-98 | 27-Jan-98 | 30-Jan-98 | 31-Jan-98 | 1-rep-96 | 3-Feb-98 | 4-Feb-98 | 5-Feb-98 | 6-Feb-98 | 7-Feb-98 | 8-Feb-98 | 9-reb-90 | 11-Feb-98 | 12-Feb-98 | 15-Feb-98 | 17-Feb-98 | 18-Feb-98 | 19-Feb-98 | 20-Feb-98 | 21-Feb-98 | 22-reb-38 | 23-Feb-98 | 25-Feb-98 | 26-Feb-98 | 27-Feb-98 | 28-Feb-98 1-Mar-98 | 20-184 |
| | | Case | , | D 0 | 9 | o e |) e |) C | 9 60 | ω α |) (C | 0 00 | | 0 | 9 | 9 | φ. | D (| 0 4 | · | | | | | | ω | 60 | . | ο« | , w | 0 | 8 | 9 | | | | , w | | ω « | | | | 9 | æ 0 | | . C | 9 | 9 | 90 | 9 6 | , |

TABLE D.4-1

DATA SUMMARY FOR LPMEOHTM DEMONSTRATION UNIT

| Sparger Resistance ("K") | 5.38 5.53 5.53 5.53 5.53 5.53 5.53 5.53 |
|--|---|
| Sparger dP (psl) | 5.39 5.28 5.28 5.09 5.09 5.09 5.09 5.00 5.00 5.00 5.00 |
| U Overall (BTU/hr ft2 F) | 4 5 6 6 7 8 8 8 8 8 8 8 9 9 9 9 9 10 |
| Reactor Vol. Prod. (TPD/Cuft) | 0.088 0.083 0.083 0.083 0.093 0.093 0.093 0.093 0.093 0.093 0.093 0.093 0.094 0.094 0.105 0.105 0.105 0.105 0.105 0.106 |
| Catalyst MeOH Prod. (gmol/hr-kg) | 21.22 21.03 21.03 21.02 20.80 20.80 20.80 20.80 20.80 20.81 |
| Raw MeOH Production (TPD) | 223.4 221.4 221.3 221.3 221.3 221.9 221.4 221.1 21.1 21.1 21.3 21.3 21.3 21.3 21. |
| Syngas Util. (SCF/lb) | 38.8 39.1 39.7 39.7 39.9 39.9 39.9 39.9 39.9 40.0 40.0 40.0 40.0 40.0 40.0 40.0 4 |
| Reactor O-T-M Conv. (%) | 21.2 21.2 21.2 21.4 21.4 21.6 20.7 20.7 20.7 20.7 20.7 20.7 20.7 20.7 |
| % & & | 43.7 42.8 43.2 44.6 44.6 44.6 44.6 44.6 44.6 44.6 44 |
| Catalyst Age (eta) | 0.81 0.78 0.79 0.79 0.70 0.70 0.74 0.74 0.74 0.70 0.69 0.69 0.69 0.69 0.69 0.69 0.69 0.6 |
| Catalyst Inventory (b) | 27.458 27.458 27.458 27.458 27.458 27.458 27.458 27.458 27.458 27.458 27.458 27.458 27.458 27.458 |
| Gassed Slumy Hgt (ft) | 60.5 62.0 62.0 62.0 62.0 63.0 63.0 63.5 63.5 63.5 63.5 63.5 63.5 63.5 63.5 |
| Gas Holdup (vol%) | 51.0 48.10 47.12 47.12 47.13 47.13 47.13 47.13 47.14 4 |
| Slumy Conc. (wf% ox) | 35.1 34.6 32.8 32.8 32.8 33.8 33.8 35.8 35.8 35.8 35.8 35.8 35 |
| Space Velocity (Mr-kg) | 6,421 6,324 6,334 6,232 6,292 6,292 6,411 6,441 6,443 6,443 6,443 6,443 6,443 6,443 6,443 6,443 6,443 6,243 |
| Inlet Sup. Velocity (fVsec) | 0.68 0.69 0.69 0.69 0.69 0.68 0.68 0.68 0.68 0.68 0.68 0.68 0.68 |
| Purge Gas (KSCFH) | 53.0.7 53.0.0 64.1.0 64.1.7 64.1.7 64.7.5 63.3.2 63.3.2 63.3.3 64.7.5 62.3 63.5 63.5 63.5 63.5 63.5 63.5 63.5 63 |
| Reactor Feed (H2:CO) | 4.22 4.25 4.44 4.45 4.33 4.33 4.13 4.13 4.13 4.13 4.13 4.13 |
| Recycle Gas (KSCFH) | 2,284 2,284 2,234 2,237 2,230 2,230 2,236 2,237 2,247 |
| Fresh Feed (KSCFH) | 721 722 728 728 728 731 731 741 733 745 733 733 733 733 733 733 734 735 736 737 738 739 739 739 739 739 739 739 739 739 739 |
| Pres.) (psig) | 710 710 710 710 710 710 710 710 710 710 |
| Temp (Deg C) | 225 22 22 22 22 22 22 22 22 22 22 22 22 |
| Gas Type | Balanced |
| Days Onstream | 2 2 2 4 5 5 5 7 5 6 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 |
| Date | 2-Mar-98 3-Mar-98 5-Mar-98 5-Mar-98 6-Mar-98 7-Mar-98 11-Mar-98 11-Mar-98 11-Mar-98 11-Mar-98 11-Mar-98 12-Mar-98 12-Mar-98 13-Mar-98 13-Mar-98 13-Mar-98 13-Mar-98 23-Mar-98 33-Mar-98 33-Mar-98 |
| Case | |

Appendix F, Table 1 contains the summary of outages for the LPMEOHTM Demonstration Unit during this quarter. Availability exceeded 99%, as the plant continued to operate through the longest continuous campaign to date (45 days) as of 31 March 1998.

During the reporting period, a total of 5,762,047 gallons of methanol was produced at the LPMEOHTM Demonstration Unit. Apart from 12,000 gallons shipped off-site for productuse testing, Eastman accepted all of this methanol for use in the production of methyl acetate, and ultimately cellulose acetate and acetic acid. No safety or environmental incidents were reported during this quarter.

Operations focused on resolution of key issues identified during prior operating periods.

Catalyst Life (eta) - December 1997 - March 1998

The "age" of the methanol synthesis catalyst can be expressed in terms of a dimensionless variable eta (η) , which is defined as the ratio of the rate constant at any time to the rate constant for freshly reduced catalyst (as determined in the laboratory autoclave). Appendix F, Figure 1 plots $\log \eta$ versus days onstream from the restart in December of 1997 through the end of the reporting period. Since catalyst activity typically follows a pattern of exponential decay, the plot of $\log \eta$ is fit to a series of straight lines, with step-changes whenever fresh catalyst was added to the reactor.

As reported in Technical Progress Report No. 14, the operating temperature of the LPMEOHTM Reactor was set at 235°C in December of 1997. At this temperature the nameplate capacity of 80,000 gallons-per-day (260 TPD) of methanol could be achieved at a low syngas utilization (i.e. high overall conversion of syngas to methanol). This result demonstrated the excellent initial activity of the catalyst, in that the design production capacity of methanol could be achieved at a lower reactor temperature and pressure than during the April 1997 operating period (refer to Technical Progress Report No. 12 for these results). In fact, at 235°C the unit initially produced 280 TPD of methanol.

The Balanced Gas flowrate was reduced to a nominal 700 KSCFH on 04 January 1998 to maintain a low syngas utilization for the remainder of the initial material balance period. As shown in Appendix F, Figure 1, the decrease in η with time from the period 20 December 1997 through 27 January 1998 occurred at a rate of 1.0% per day, which represented a significant improvement over the 3.4% per day decline measured during the initial six weeks of operation in April and May of 1997. The deactivation rate also improved from the longer-term rate of 1.6% per day seen throughout the summer and autumn of 1997.

Based on this improvement, DOE accepted a recommendation by Air Products and Eastman to further reduce the reactor temperature to 225°C. The subsequent change in conditions began on 28 January 1998, when two consecutive batches of fresh catalyst were activated and transferred to the LPMEOHTM Reactor, bringing the total inventory to 24,800 pounds, or about 60% of design. Reductant gas uptake for both batches approached the theoretical value to within 1%. Following addition of the second catalyst batch on 30 January, the reactor temperature was reduced to 225°C. Subsequent performance results, as regressed

with the reactor kinetic model, showed a slight increase in η on the temperature transition day, followed by a significant decrease in η at 225°C. No operating transients occurred during this time which could have resulted in such a drastic performance decline. It appears, therefore, that the lower calculated catalyst age is a temperature-related artifact of the reactor kinetic model induced by further departure from the autoclave baseline temperature of 250°C.

On 08 February 1998, a planned five-day outage in Eastman's shift reactor provided an opportunity to continue operations with a Texaco-type (CO-rich) reactor feed, while Eastman's gas-phase methanol plant was forced to shut down. The results from this test are included in Table D.4-1 and Appendix F, Figure 1. Furthermore, Eastman took the opportunity to shut down their methanol distillation equipment for maintenance, leaving no flow path for the crude methanol underflow from the second, rectifier column in the LPMEOH™ Demonstration Unit. However, because of the CO-rich feed, the rectifier column could be shut down for the production of stabilized, "fuel-grade" methanol (98+ wt% methanol, <1 wt% water). Approximately 12,000 gallons of "fuel-grade" methanol was loaded into trailers and shipped off-site for future product-use testing; Appendix G contains a series of analytical reports on the purity of this product. During the remainder of this operating period, approximately 181,800 gallons (600 tons) of stabilized methanol (99.3 wt% methanol, 0.3 wt% water) was pumped directly from the LPMEOH™ Demonstration Unit to Eastman's methyl acetate plant, bypassing the normal route through the distillation equipment. This methanol was considered acceptable by Eastman because of the low levels of all impurities. In particular, the water concentration of the stabilized methanol was significantly lower than what is produced during operation on the normal Balanced Gas supply (typically 3 - 4 wt% water). This is a result of operation on a CO-rich syngas with a relatively low CO₂ concentration. This test was the first attempt to feed a stabilized methanol stream with low water content directly into one of Eastman's downstream chemical processes, providing another indication of the flexibility of the LPMEOH $^{\text{TM}}$ Process. Eastman's only alternative was to flare the syngas stream, which was undesirable both environmentally and economically.

On 19 February 1998, a third batch of catalyst was activated and transferred to the LPMEOHTM Reactor, bringing the total catalyst inventory to 27,450 pounds, or about 67% of design. Prior to the addition of fresh catalyst, the average deactivation rate at 225°C was 0.7% per day, which represented a modest improvement over the 1% per day rate calculated at 235°C. However, most of the activity decline occurred during the period on CO-rich feed gas and immediately after an interruption in the Balanced Gas supply at the end of that test case. This observation more likely indicates a real change in catalyst activity, as opposed to an anomaly of the kinetic model, because deviations from steady-state operation in the syngas generation area could also cause upsets in the level of poisons carried by the gas. This type of behavior seems to have occurred before, and the more frequent catalyst sampling protocol in effect since the December restart may provide clues about the types of poisons that become prevalent during such upsets. So far, samples from mid-February and mid-March of 1998 have shown an increase in arsenic loading, although not nearly to the levels measured in the summer of 1997. Copper crystallite size measurements are still pending, as are analyses from more recent samples which will help complete the picture.

Through the remainder of the reporting period, the Balanced Gas flow rate was maintained at approximately 700 KSCFH, with reactor temperature fixed at 225°C. As shown in Appendix F, Figure 1, two periods of very stable operation ensued, with average activity declines of 0.36% and 0.27% per day. A discontinuity occurred in the data on 15 March 1998, again coincidental with an excursion in the Balanced Gas feed supply. Regressing the entire data set from the catalyst addition on 19 February through 31 March 1998 yields a deactivation rate of 0.60% per day. However, the data were plotted in two separate sets to show the possibility of an improved steady-state baseline deactivation rate, exclusive of any additive effects related to excursions in the Balanced Gas supply. If this conclusion is viable, the current baseline activity decline of about 0.4% per day is a measurable improvement over the 1% per day rate calculated at 235°C in January of 1998 and matches the original target from the 4-month proof-of concept run on a natural-gas derived syngas at the LaPorte AFDU. Additional operating time is necessary to further quantify the catalyst deactivation rate and the effects of operating conditions and syngas supply excursions.

Sparger Resistance

As reported in Technical Progress Report No. 14, flow resistance through the gas sparger of the LPMEOHTM Reactor had been stabilized using a continuous flush of condensed oil and entrained slurry from the 29C-05 secondary oil knock-out drum and 29C-06 cyclone. These streams were gravity-drained back to the reactor through a flush connection at the gas inlet line to the reactor, thus eliminating a batch-transfer operation which had been used during prior operation. The flow rate of the flush was equivalent to the average rate of liquid traffic in the reactor loop (1 to 2 gallons per minute).

This technique was first applied to a clean sparger at the restart of operations on 19 December 1997. Appendix F, Figure 2 plots the average daily sparger resistance coefficient since then, and provides an initial confirmation of the encouraging results reported for the first two weeks of operation at the end of the prior reporting period. As with the original gas sparger design, the return of the internal oil and slurry streams via the flush connection was required to stabilize the pressure drop after extended interruptions of the flush fluid. When compared to the original gas sparger, the alternative gas sparger may have greater flexibility in maintaining stable pressure drop after interruptions of the syngas supply; this may also be a result of greater attention to achieving a proper standby condition during shutdowns, which has inhibited any plugging caused by slurry backflow and stagnation. The data for this plot, along with the corresponding average pressure drop, are included in Table D.4-1. Appendix F, Figure 3 shows the progressive improvement in sparger operation seen since the original startup in April of 1997. This parameter will continue to be closely monitored for any change in flow resistance.

Alternative Fuels Field Trailer Unit (AFFTU) Results - December 1997 - January 1998

The Alternative Fuels Field Test Unit (AFFTU), a transportable laboratory equipped with an autoclave and analytical equipment, was shipped from the Air Products' Iron Run laboratory in Allentown, PA to Kingsport to perform additional testing on the reactor feed gas at the

site. From the restart on 19 December 1998, the autoclave operated in parallel with the Demonstration Unit on the same reactor feed gas, although at 250°C, the typical laboratory baseline condition. Analytical results from the AFFTU showed less than 10 ppbv concentrations of metal carbonyls and hydrogen sulfide within the reactor loop. Carbonyl sulfide was typically less than 10 ppbv in the loop, but occasionally drifted higher; these excursions could not be correlated with any changes in the feed gas cleanup operations upstream of the LPMEOHTM facility. Performance results from the 31-day campaign on coal-derived syngas at Kingsport were generally consistent with other laboratory experiments on poison-free syngas. A post-mortem analysis on the catalyst revealed no unusual levels of catalyst poisons or significant changes in catalyst physical properties. The AFFTU test concluded on 20 January 1998, and the equipment was returned to the Air Products' Iron Run laboratory.

D.5 Planning and Administration

Work has continued on the Final Report - Volume 1 - Public Design. Air Products received the latest comments from DOE (letter dated 12 October 1997). In response to these comments, Air Products has submitted a cost breakdown for both capital and operating costs within the LPMEOH™ Demonstration Unit. These will ultimately be incorporated into an updated version of this report which will be sent to DOE for comment.

The Milestone Schedule Status Report and the Cost Management Report, through the period ending 31 March 1998, are included in Appendix H. These two reports show the current schedule, the percentage completion and the latest cost forecast for each of the Work Breakdown Structure (WBS) tasks. Ninety-nine percent (99%) of the \$38 million of funds forecast for the Kingsport portion of the LPMEOHTM Process Demonstration Project for the Phase 1 and Phase 2 tasks have been expended (as invoiced), as of 31 March 1998. Nineteen percent (19%) of the \$158 million of funds for the Phase 3 tasks have been expended (as invoiced), as of 31 March 1998.

The monthly reports for January, February, and March were submitted. These reports include the Milestone Schedule Status Report, the Project Summary Report, and the Cost Management Report.

A paper entitled "Commercial-Scale Demonstration of the Liquid Phase Methanol (LPMEOHTM) Process: Initial Operating Experience" was submitted for presentation at the Clean Coal Technology Conference in Reno, Nevada on April 29, 1998.

A draft topical report entitled "Design and Fabrication of the First Commercial-Scale LPMEOH™ Reactor" was circulated for internal Air Products review prior to formal submission.

E. Planned Activities for the Next Quarter

- Write and submit the Demonstration Technology Start-up Report to DOE.
- Continue to analyze catalyst slurry samples and gas samples to determine causes for deactivation of methanol synthesis catalyst.
- Continue executing Phase 3, Task 2.1 Methanol Operation per the Demonstration
 Test Plan. Focus activities on increasing catalyst concentration in the LPMEOH™
 Reactor to determine the maximum slurry concentration (Test 9 of Test Plan).
- Reissue the DVT Recommendation for a DME proof-of-concept test run at the LaPorte AFDU to reflect the final delivery date for the dehydration catalyst and the actual schedule for the test run.
- Continue execution of the Off-Site, Product-Use Test Program (Phase 1, Task 1.4).
- Continue to incorporate DOE comments into the Topical Report on Process Economic Studies.
- Reach agreement with DOE on the equipment breakdown and operating cost summary for use in the Final Technical Report, Volume 1, Public Design Report.
- Issue the Topical Report on Liquid Phase Reactor Design to DOE for review and comment.
- Present the paper "Commercial-Scale Demonstration of the Liquid Phase Methanol (LPMEOH™) Process: Initial Operating Experience" at the Clean Coal Technology Conference in Reno, Nevada on April 29, 1998.

F. Conclusion

During this quarter, initial planning and procurement work continued on the seven project sites which have been accepted for participation in the off-site, product-use test program. Approximately 12,000 gallons of fuel-grade methanol (98+ wt% methanol, <1 wt% water) produced during operation on carbon monoxide (CO)-rich syngas at the LPMEOHTM Demonstration Unit was loaded into trailers and shipped off-site for future product-use testing. At one of the projects, three buses have been tested on chemical-grade methanol and on fuel-grade methanol from the LPMEOHTM Demonstration Project. At two other project sites (a flexible fuel vehicle and a fuel cell application), testing on fuel-grade methanol from the LPMEOHTM Demonstration Project is scheduled for the second quarter of calendar year 1998.

During the reporting period, planning for a proof-of-concept test run of the Liquid Phase Dimethyl Ether (LPDMETM) Process at the Alternative Fuels Development Unit (AFDU) in LaPorte, TX continued. The commercial catalyst manufacturer (Calsicat) has prepared the first batch of dehydration catalyst in large-scale equipment. Air Products will test a sample of this material in the laboratory autoclave.

Catalyst activity, as defined by the ratio of the rate constant at any point in time to the rate constant for freshly reduced catalyst (as determined in the laboratory autoclave), was monitored for the initial extended operation at the lower initial reactor operating temperature of 235°C. At this condition, the decrease in catalyst activity with time from the period 20 December 1997 through 27 January 1998 occurred at a rate of 1.0% per day, which represented a significant improvement over the 3.4% per day decline measured during the initial six weeks of operation in April and May of 1997. The deactivation rate also improved from the longer-term rate of 1.6% per day calculated throughout the summer and autumn of 1997.

Based on this improvement, DOE accepted a recommendation by Air Products and Eastman to further reduce the reactor temperature to 225°C. The initial operation at this temperature (from 31 January through 18 February 1998) showed a modest improvement in the deactivation rate to 0.7% per day. However, most of the activity decline occurred during a test period on CO-rich feed gas and immediately after an interruption in the Balanced Gas supply at the end of that test case. This observation more likely indicated a real change in catalyst activity, and this type of behavior seems to have occurred after other excursions in the Balanced Gas supply. During two additional stable operating periods between 19 February and 31 March 1998, deactivation rates of 0.27% and 0.36% per day were measured. A discontinuity occurred in the data on 15 March 1998, again coincidental with an excursion in the Balanced Gas supply. If the current results prove to be correct, the current baseline activity decline of about 0.4% per day is a measurable improvement over the 1% per day rate seen at 235°C in January of 1998 and matches the original target from the 4-month proof-of concept run on a natural-gas derived syngas at the LaPorte AFDU. Additional operating time is necessary to further quantify the catalyst deactivation rate and the effects of operating conditions and syngas supply excursions.

The weight of catalyst in the LPMEOHTM Reactor has reached 67% of the design value, and the slurry concentration approached 40 wt%. Catalyst slurry samples from the LPMEOHTM Reactor have been taken on a regular basis to correlate any change in performance with changes in the physical properties of the catalyst. So far, samples from mid-February and mid-March of 1998 have shown an increase in arsenic loading, although not nearly to the levels measured in the summer of 1997. Copper crystallite size measurements are still pending, as are analyses from more recent samples which will help complete the picture.

The performance of the alternative gas sparger, which was designed by Air Products and installed into the LPMEOHTM Reactor prior to the restart of the LPMEOHTM Demonstration Unit in December of 1997, was monitored throughout the reporting period. Pressure drop through the gas sparger of the LPMEOHTM Reactor was stabilized using a continuous flush of condensed oil and entrained slurry which were gravity-drained from the 29C-05 secondary oil knock-out drum and 29C-06 cyclone. As with the original gas sparger design, the return of the internal oil and slurry streams via the flush connection was required to stabilize the pressure drop after extended interruptions of the flush fluid. When compared to the original gas sparger, the alternative gas sparger may have greater flexibility in maintaining stable pressure drop after interruptions of the syngas supply; this may also be a result of greater attention to achieving a proper standby condition during shutdowns. The most recent results provide an initial confirmation of the encouraging data reported for the

first two weeks of operation at the end of the prior reporting period. This parameter will continue to be closely monitored for any change in flow resistance.

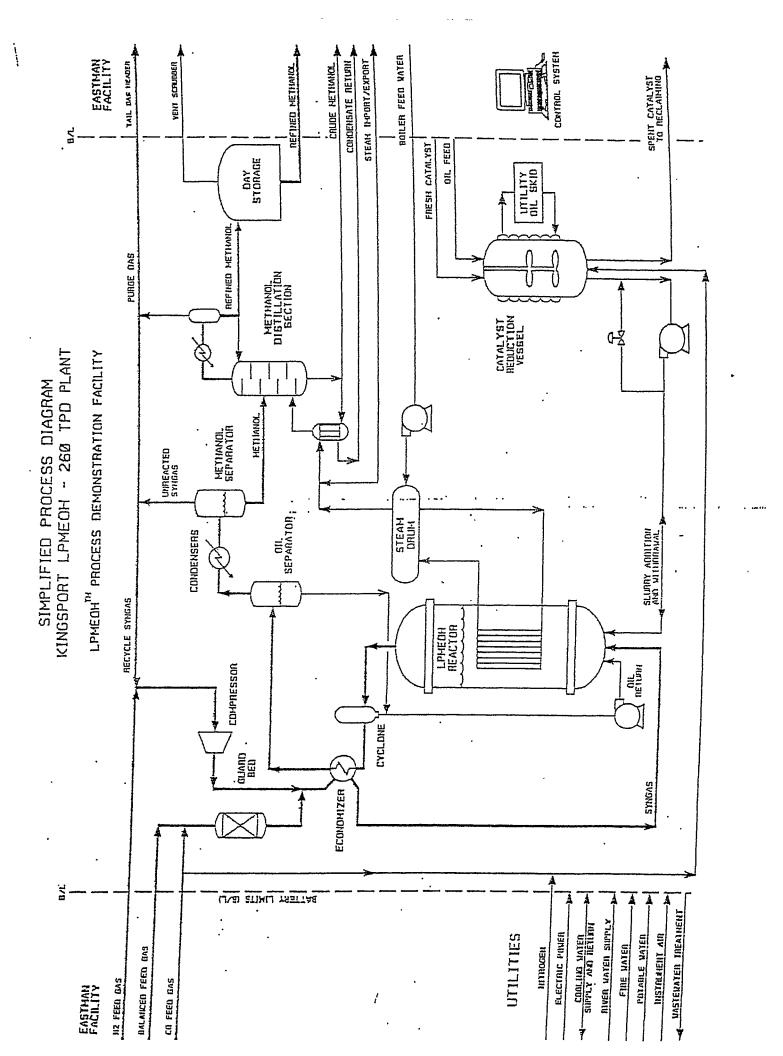
The Alternative Fuels Field Test Unit (AFFTU), a transportable laboratory equipped with an autoclave and analytical equipment, was shipped from the Air Products' Iron Run laboratory in Allentown, PA to Kingsport to perform additional testing on the reactor feed gas at the site. Analytical results from the AFFTU showed less than 10 ppbv concentrations of metal carbonyls and hydrogen sulfide within the reactor loop. Carbonyl sulfide was typically less than 10 ppbv in the loop, but occasionally drifted higher; these excursions could not be correlated with any changes in the feed gas cleanup operations upstream of the LPMEOHTM facility. Performance results from the 31-day campaign on coal-derived syngas at Kingsport were generally consistent with other laboratory experiments on poison-free syngas. A postmortem analysis on the catalyst revealed no unusual levels of catalyst poisons or significant changes in catalyst physical properties. The AFFTU test concluded on 20 January 1998, and the equipment was returned to the Air Products' Iron Run laboratory.

During the reporting period, a total of 5,762,047 gallons of methanol was produced at the LPMEOHTM Demonstration Unit. Apart from 12,000 gallons shipped off-site for productuse testing, Eastman accepted all of this methanol for use in the production of methyl acetate, and ultimately cellulose acetate and acetic acid. During a portion of the operating period on CO-rich syngas, approximately 181,800 gallons (600 tons) of stabilized methanol (99.3 wt% methanol, 0.3 wt% water) was pumped directly from the LPMEOHTM Demonstration Unit to Eastman's methyl acetate plant, bypassing the normal route through the distillation equipment designed to remove water, higher alcohols, and process oil. This test was the first attempt to feed a stabilized methanol stream with low water content directly into one of Eastman's downstream chemical processes, providing another indication of the flexibility of the LPMEOHTM Process. No safety or environmental incidents were reported during this quarter. Availability exceeded 99%, as the demonstration unit continued to operate through the longest continuous campaign to date (45 days) as of 31 March 1998.

Ninety-nine percent (99%) of the \$38 million of funds forecast for the Kingsport portion of the LPMEOH™ Process Demonstration Project for the Phase 1 and Phase 2 tasks have been expended (as invoiced), as of 31 March 1998. Nineteen percent (19%) of the \$158 million of funds for the Phase 3 tasks have been expended (as invoiced), as of 31 March 1998.

APPENDICES

APPENDIX A - SIMPLIFIED PROCESS FLOW DIAGRAM



APPENDIX B - OFF-SITE TESTING (DEFINITION AND DESIGN)

Appendix B-1 - Summary Table of Eight Candidates (one page)

Quarterly Reports:

Appendix B-2 - Acurex FFV (one page)

Appendix B-3 - Stationary Turbine for VOC Control (one page)

Appendix B-4 - West Virginia University Stationary Gas Turbine (two pages)

Appendix B-5 - Aircraft Ground Equipment Emulsion (one page)

Appendix B-6 - University of Florida Fuel Cell (one page)

Appendix B-7 - West Virginia University Tri-Boro Bus (three pages)

Appendix B-8 - Florida Institute of Technology Bus & Light Vehicle (twenty-two pages)

ARCADIS GERAGHTY&MILLER

MEMO

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To:

Coples:

Larry Waterland

TRANSPORATION TECHNOLOGY

From

Doug Coleman

Date:

29 April 1998

Subject:

LPMEOH™ FFV Demonstration Status Report

Progress on the FFV demonstration continues to be hampered in part by problems with the California Energy Commission (CEC) methanol fuel dispensers. The Taurus has often been unable to refuel at sites which were supposedly operational. And in many instances it has not been possible to obtain a readout on the amount of fuel dispensed. Both of these factors have affected the ability to develop as much fuel economy data as desired. Thus, since the inception of this program, while the FFV has traveled roughly 8,000 miles, only 1,300 of these miles have yielded acceptable fuel economy data. The FFV has been achieving a 16.3 mpg fuel economy on regular M85 during this time period.

With the CEC's recent announcement to phase out all of the methanol stations by the end of the year, it appears that the stations will continue to be in a state of disrepair and are no longer usable. Thus, operation on LPMEOHTM will be initiated before data for the originally planned 3,200 miles on regular M85 have been acquired. The first drum of LPMEOHTM -based M85 has been prepared and this phase of the project will now begin. Before doing so, however, the FFV will undergo emissions testing on regular M85 during the week of April 27

During the LPMEOHTM phase, ARCADIS Geraghty & Miller will mix 8.25 gallons of RUL with 46.75 gallons of LPMEOHTM to obtain a LPMEOHTM -based M85 mixture. The fuel will be measured during dispensing with the use of a scale. When the LPMEOHTM phase is completed and the FFV has undergone emissions testing on that fuel, the 1,900 miles remaining on regular M85 will be completed using fuel purchased in drums and stored at ARCADIS Geraghty & Miller in the same manner that was used to fuel with LPMEOHTM -based M85.

ARCADIS GERAGHTY&MILLER

MEMO

ARCADIS Geraghty & Miller, Inc. 555 Clyde Avenue Mountain View California 94043 Tel 650 961 5700 Fax 650 254 2497

Coples:

Larry Waterland

ENGINEERING SYSTEMS

Carlo Castaldini

Date: 29 April 1998

Subject:

Project update report: LPMEOHTM Testing in a GasTurbine for Control

The objective of this project is to demonstrate the use of a mini gas turbine for the destruction of VOC from an emission source while burning LPMEOHTM. Mini gas turbines, with a gross generating capacity of 75 kW or less, promise to be one of the most successful technologies for distributed power generation in the new deregulated power industry. There are two main considerations in the use of these mini turbines. The first is the cost of their operation and the second is their emissions. When the mini turbine is also used to destroy VOC from vented process air, the economics improve. The use of methanol for remote applications or for emission control may alleviate other key obstacles to commercial development.

Efforts since the previous progress report have focused on selecting a host site for the demonstration. Of the four candidate sites identified in the previous report, the one most interested in supporting the project was the Allied Signal facility in Phoenix, Arizona. Allied Signal has agreed to be the host site for the LPMEOHTM tests using their 525 kW ASE8-1000 gas turbine engine in a laboratory set up. On March 5, Carlo Castaldini, the ARCADIS Geraghty & Miller Project Manager for this project, mct at the Allied Signal Phoenix plant with Paul Dodge, Program Manager of Industrial Engines, and Jeff Zimmerman, Project Engineer, Industrial/Marine applications, to discuss the scope and the time frame for the demonstration tests. Allied Signal agreed to the overall objective and confirmed their plans to support the project. Several discussions were held after the meeting to further clarify the proposed approach and logistics for methanol storage, test duration, and measurements. Their laboratory facility can be readily modified to store and handle methanol

Allied Signal is currently reviewing the project scope in greater detail and will provide suggestions regarding the specific testing they would recommend. A followup meeting at Allied Signal is scheduled for May 14 to discuss testing and other project-specific details.

WVU Progress Report

Dated May 1st, 1998

For

Air Products and Chemical Inc.

Methanol Utilization Demonstration Project

WVU Emission Studies on a Dual-Fuel, Methanol/Jet Fuel Stationary Gas Turbine.
350 HP Type GTC-85
Manufactured by Allied Signals Inc.

Report Prepared for

Robert J. Senn Air Products and Chemical Inc 7201 Hamilton Blvd Allentown PA 18195-1501

> Tel: (610) 481-7042 Fax: (610) 706-7299

> > by

John L. Loth and Nigel N. Clark

Department of Mechanical and Aerospace Engineering West Virginia University

P. O. Box 6106, Morgantown WV 26505-6106

Status Summary

The GTC gas turbine has been fully instrumented and the fuel system has been converted to allow convenient fuel type change over between Jet fuel and Methanol. Our operating procedure is geared to prevent methanol cold starting problems. Therefore we always ignite on jet fuel and only after an adequate warm up period (5 minutes), is the fuel change over implemented. Five minutes before shut down, the fuel type is changed back to jet fuel. The turbine has been run successfully on jet fuel and all the instrumentation checked out to be working as planned. Three attempts were made to change over to methanol fuel at idle speed. All three attempts resulted in a flame-out. In view of this problem the gas-turbine combustor and the fuel controller were taken to Pratt and Whitney aircraft for refurbishing. A standard Pratt and Whitney PT6 dual glow plug ignition system was welded into the combustor can. This will be used in addition to the existing spark ignition. Another measure to prevent gas turbine flame-out in the future, is to limit fuel type change to operations at high exhaust gas temperature (EGT at least 1000°F). We have been having some difficulty in procuring a new fuel shutoff solenoid, as the old one leaks. However we are confident to be back on line by June 1 1998. We may have to request a no-cost extension for contract completion till September 15, 1998. Note this seems not unreasonable as WVU did not receive official contract authorization till September 22, 1997.

ARCADIS GERAGHTY&MILLER

MEMO

Copies:

To: Larry Waterland Copies

ENGINEERING SYSTEMS

ARCADIS Geraghty & Miller, Inc.

555 Clyde Avenue Mountain View

California 94043 Tel 650 961 5700 Fax 650 254 2497

From:

Shyam Venkatesh

Date:

May 1, 1998

Subject

Project update report: LPMEOH™ testing with -86 generators at Tyndall AFB

In January 1998, A-55 LP withdrew their participation from the program. The reasons given by A-55 for their withdrawal were specified in the previous progress report. Applied Research Associates (ARA), the operating contractor at Tyndall AFB coordinating the LPMEOHTM program, requested that they be allowed to test their proprietary water-based emulsion fuel. The ARA emulsion fuel is IP-3 based. IP-8 was selected instead of diesel because of the Air Force's desire to universalize its fuels in the future.

ARA began experimentation with preliminary formulations of their fuel in March and April. ARCADIS Geraghty & Miller consulted with ARA in the development of an emulsion mixing system. ARCADIS Geraghty & Miller suggested that a high shear-rate centrifugal pump system be used instead of a more conventional mixer. ARCADIS Geraghty & Miller also procured for ARA the emulsifying agents and other proprietary chemical additives. Due to scheduling conflicts, and prior commitments, ARA was not able to conduct preliminary testing with the emulsion in April. ARA expects to perform scoping tests in May, based on which they will determine the best emulsion composition. Currently the emulsion fuel is designed to use up to 10 percent methanol. The best percentage of methanol to actually use will be determined after the scoping tests. Barring any further schedule conflicts, scoping tests are expected to be completed in May. Following these, the actual testing phase of the project will begin immediately.

K 984 846 1630

To

; Dr. V.P. Roan

From

: Jim Fletcher

Concerning

: Air Products "Coal-based Methanol" Contract Progress Report

Date

: May 10, 1998

This memo details the progress accomplished towards the completion of the Air Products "Coal-based Methanol as a Fuel for PAFC Systems" contract for the February through April time period.

Two 55 gallon barrels of Air Products methanol were delivered at the end of April. The barrels were received, clearly marked, and moved into the fuel storage area.

A second testing laboratory, Intertek Testing Services, has been identified. It is envisioned that both labs will perform a comprehensive analysis of the Air Products methanol. In addition, Intertek will also perform analysis to identify any sulfur or chlorides within the methanol. These two elements have been identified as problems for the fuel cell system. Intertek has performed similar tests for Georgetown University on the methanol to be used in the 40 ft. bus program. The required paperwork is underway and testing should begin within the next week or so. Work is also continuing to further identify any problem constituents.

It was determined that the fuel cell data acquisition system had been damaged during a recent power outage. The system was sent to the manufacturer for repair, and has been returned in working order. Various thermocouples, an air flow meter, and a fuel flow meter have been added to the system. The labview data acquisition software has been upgraded to incorporate the new hardware. Preliminary baseline testing of the fuel cell system has begun using fuel grade methanol.

The gas chromatograph has been ordered and received. Preliminary testing and debugging of the system has begun using known gases (air, etc.). The design of the gas collection system is complete and will be ordered in the near future. The remaining concern is the exact nature of the interface between the gas chromatograph and the collection bottles. The interface will be completed within the next week.

The fuel cell system is operational with the upgrading of various components within the system. The upgrades include the installation of a pressure relief valve on the CO_2 line. The method of in-lab storage and fuel delivery for the Air Products methanol is complete and purchase orders for the necessary equipment have been written.

It is expected that testing of the Air Products methanol within the fuel cell system will commence in June pending successful results of the chemical analysis.

FUEL GRADE METHANOL IN TRANSIT BUS APPLICATIONS

PROGRESS REPORT, APRIL 1998

Submitted by: Nigel N. Clark, Principal Investigator

Department of Mechanical & Aerospace Engineering

West Virginia University Morgantown, WV 26506-6106

The objectives of this program are to quantify the emissions and evaluate the performance of full size transit buses with compression ignition engines using Air Products fuel grade methanol. A comparison will be made from the results of the two fuels, current in use methanol and Air Products fuel grade methanol. This project centers around an intensive experimental effort presently taking place in New York City.

Prior to departing to perform the emissions research in New York City, the test equipment was subjected to a quality audit by performing, propane, alcohol and aldehyde injections to determine the respective recovery percentages from the dilution tunnel. Appropriate sampling flow-rates were established to perform the testing.

A research team transported one of the two West Virginia University's Heavy Duty Vehicle Emissions Transportable Laboratories to the test site at Command Bus Corporation Depot, in New York City. Three methanol powered buses were tested: details are given in Table 1. The buses were subjected to testing using both in-use methanol and the Air Products' fuel grade methanol. The fuel change was accomplished by connecting into the bus's current fuel system. Two fuel lines were routed from the Air Products' fuel container to the bus's fuel pump and fuel return. At least three gallons of the Air Products' fuel grade methanol was pumped through the fuel system before for the return line was placed into the fuel grade container. The test weight (tw) for the vehicles was calculated to be 34,500 lbs. using the following equation;

tw = (curbweight +150+ (seating + standing)/2 * 150)

All three buses were tested using the Central Business District cycle (CBD) and one was also tested using the WVU 5 Mile Route. Figure 1 shows the CBD cycle while figure 2 shows the continuous oxides of nitrogen (NO_x). emissions from bus # 2145 fueled with the Air Products methanol. At this time the laboratory has not yet left New York City and the data processing is not complete. A full report on data is expected within six weeks. Future plans will therefore be centered around data processing and report writing.

Bus Details

Table 1

| Bus Number | Engine Type | Test Weight | Cycle |
|------------|-------------|-------------|--------------|
| 2145 | 6V92 DDC II | 34,408 | CBD |
| 2139 | 6V92 DDC II | 34,408 | CBD |
| 2143 | 6V92 DDC II | 34,408 | CBD |
| | | | 5 Mile Route |

Central Business District Cycle, Bus 2145

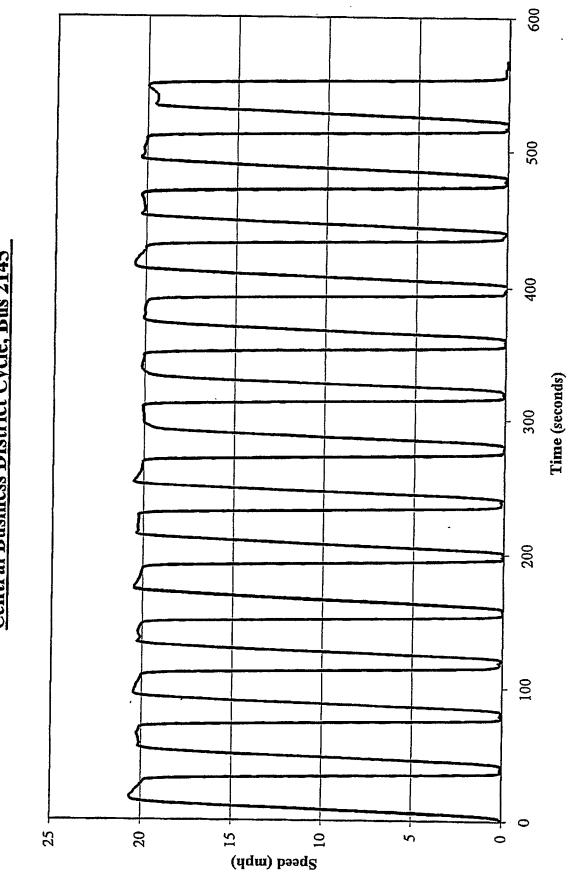


Figure 1:

704 107 45.40

Continuous Oxides of Nitrogen CBD Bus 2145

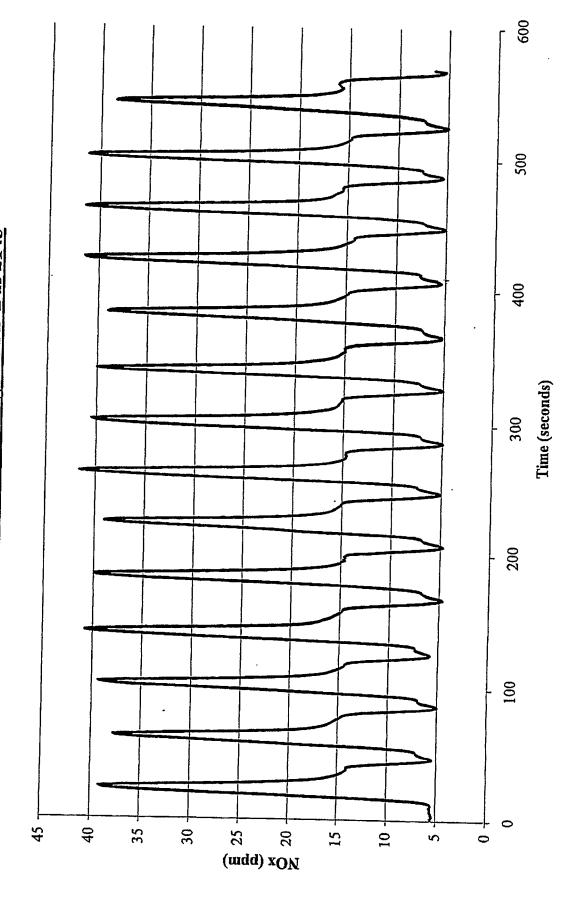


Figure 2:

Quarterly Report (Nov. 25, 1997 – Mar. 11, 1998)

to

Mr. Robert Senn consultant to

Air Products and Chemicals, Inc.

from

Dr. John J. Thomas
Florida Tech
150 W. University Blvd.
Melbourne, Florida 32901
Ph 407-674-7252
Fax 407-984-8461

Fleet Trails for Fuel Grade Methanol

under

USDOE Cooperative Agreement No. DE-FC22-92PC90543 Performance Period 8/11/97 - 10/10/98

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| 5. | Appendix Road Data for the Methanol Car | 6 |

1. Introduction

During this period the methanol car was re-commissioned and the operator, Dr. John Thomas, drove the car on a routine basis between 3325 W. New Haven Ave. and the Florida Tech main campus at 150 W. University Blvd.(please see Appendix). He also drove the car between his house and the above addresses. Before and after these trips he recorded all the gauge readings, the date, the time, and comments. This allowed several MPG calculations. The gear shift did not work properly from the beginning and eventually stopped functioning at all. The problem turned out to be caused by some student modification of a key bearing made some nine years ago. The problem was easily repaired. When the gear shift was operating at its poorest, the mileage dropped dramatically. The electronic temperature gauge was replaced with a mechanical one which now allows us to record the exact temperature in degrees F. The car is now operating ideally. In the meantime we intend to proceed with collection of emission data.

The bus required more extensive work but it too is now operational. Apparently the old Avocet we obtained as ignition enhancer decomposed over the years since the mechanics could not determine any performance difference between methanol containing Avocet and methanol without Avocet. As of now we are relying on glow plug warming to produce ignition. Up to now the system appears to work well. It is now operating on methanol that was put in its tanks five years ago. The vehicle is running as well as can be expected according to our consultants. In the meantime, we intend to proceed with collection of emission data and miscellaneous upgrades

90 46 400 45:47 407 984 8461 PAGE 1

2. Activities (As Recorded by the Staff)

- 1. To use cold start:
 - 1st Try to start car, if car does not start then -
 - 2nd Stop cranking engine but leave the key on, and press injector switch in until it clicks. The switch is located on the underside of the dash board near the radio.
 - 3rd Try to start engine by normal starting procedures
 - 4th If the engine does not start, repeat steps 2 and 3
- 2. Replaced the shift cable on the car because of very hard shifting after warming up. However, shifting was still unacceptable.
- 3. The clutch pedal only disengages in the last inch or so of travel resulting in hard shifting.
- 4. The car was taken to Jim Rathmann's for repair.
- 5. The bus was started with the help of starting fluid. It idled all right but did not rev up.
- 6. The bus is missing very badly when running or idling. Dirt in the gas is suspected or the fuel is too old. Injectors that were just put in might be already clogged due to sediments in the lines. Further testing was needed.
- 7. The bus started again on starting fluid after the governor and other controls were readjusted and freed up. The oil was also changed. Controls worked erratically at first; after familiarization they worked well.
- 8. The bus eventually ran smoothly. It was necessary to replace two elogged injectors. It takes about 20 25 minutes to warm up and run smoothly. It will not let you rev the engine until a certain temperature is reached. It blows white smoke until warmed up and all condensation from system has been burnt off.
- The bus was driven on I-95 to test. It can well but is not really designed for highway due to low gear ratio. Max speed was about 55 mph.
- 10. The car transmission was inspected due to suspicion of bad clutch. Clutch was fine, however the clutch engaging arm and bearings were bad resulting in the clutch not fully engaging. Problem was fixed and the car is now running and working well as a result. More details below.
- 11. An air leak in bus was fixed, all panels were put back on and tightened down. Bus graffiti was removed.

407 984 8461

- 12. Several cleaning materials were tried on the seats, however most either had no result or began eating or rubbing off covers.
- 13. Throwout bearings in the car were replaced in transmission along with clutch fork arm and the bushings. The play that resulted from worn bearings caused the clutch not to fully disengage and resulted in hard shifting. Alternative Automotive in West Melbourne did the work on the transmission.
- 14. Modification to both vehicles for on-board emission samplings were discussed and designed.
- 15. Car air-conditioner was inspected for leaks.
- 16. The other start system was installed in the bus. It is identical to the one in the car and was detailed in the last quarterly report. After installation, the time for the bus to properly warm up only took a few minutes.

3. Results and Discussion

The methanol powered car was operated routinely and the total miles traveled after re-commissioning is 1176 over approximately 3 months. The mileage varied from a high of 12.8 mpg to a low of 5.5 mpg. The low mileage data was obtained when the shifting problem was at its worse. A mechanical temperature gauge was installed which now allows us to determine if any overheating takes place. The old electronic temp gauge never did work well. All the gauges (oil, fuel, and battery) now work well and show nothing except normal readings. The cold-starting system continues to work very well. At this time the car is undergoing repairs because of a defect in the air conditioning system. The operational log is shown in the Appendix.

We are currently installing systems to allow us to determine on-board emissions.

The bus is now operating satisfactorily but we can not operate it routinely because the fuel shipment has not arrived. It did, however, make a 50 mile trip on I-95. An ethyl ether starting system was installed on the bus and it works very well. This system allows operation after less than five minutes of warm-up. This is comparable to the performance of a regular diesel engine. The ether starting system is exactly the same as on the car.

As it turned out, only lack of familiarization caused any problems putting the bus into operation. The only real problem was two clogged injections which were replaced.

4. Work Schedule for Third Quarter

- Complete installation of on-board sampling and emissions data collecting systems.
- Complete air-conditioning repair of car and return it to routine operation.
- Complete installation of on-hoard sampling and emission data collecting systems for the bus.
- 4. Compile the emissions data at 0, 10, 20, 30, 40, and 50 miles/hour for the bus.
- 5. Compile the emissions data at 0,10, 20, 30, 40, 50, and 60 miles/hour for the car.

4.

APR 16 '98 15:18

- 6. Return the car to routine operation and collect operating data.
- 7. Re-commission the bus and use it for biology field trips as other university activities while collecting operating data.

The work scheduled for the second quarter was completed on schedule. The only variance was caused by a decision to determine emissions using on-board systems instead of installing a chassis dynamometer.

Listing of Project Personnel

- 1. Dr. John Thomas, Principal Investigator
- 2. Frank Aransky, Research Assistant
- 3. Greg Palubin, Research Assistant
- 4. Richard MacKenzie, Director, Florida Tech Vehicle Maintenance
- 5. Bert Austin
- 6. David Cash
- 7. JeffReilly

5. Appendix

Road Data for the Methanol Car

6.

407 994 8461 POSE 0

000 46 100 45

| Comments | Service Engine Soon Light On | Started Right Up, Oil Gauge Jumps Around | Service Engine Soon Light On | | Service Engine Soon Light On | Service Engine Spon Light On | | Service Engine Soon Light Not On | Service Engine Spon Light On | | Service Engine Soon Light On | Soon Light | | Service Engine Soon Light On | | | Added 6 Gal of Melhanol Prior to Travel | Service Engine Soon Light Not On | Add 2 Gal of Methanol | Service Engine Soon Light Not On | Service Engine Soon Light Not On | | Service Engine Soon Light Not On | Service Engine Soon Light Not On | | Service Engine Soon Light Not On | Used Starter Button | Service Engine Soon Light Not On | | HOT Gauge | Temperature Gauge Out | | Temperature Gauge Out |
|------------------------|------------------------------|--|------------------------------|------|------------------------------|------------------------------|-------|----------------------------------|------------------------------|-------|------------------------------|------------|-------|------------------------------|--------|-------|---|----------------------------------|-----------------------|----------------------------------|----------------------------------|-------|----------------------------------|----------------------------------|-------|----------------------------------|---------------------|----------------------------------|-------|-----------|-----------------------|-------|-----------------------|
| Place | Biowest | SE | Rooney's | | Rooney's | Biowest | | Biowest | | | FIT | Biowest | | Biowest | FIT | | FIT A | Biowest | | Biowest | Rooney's | | Rooney's . | FIT | | LH | | Biowest | | Biowest | Rooney's | • | Rooney's |
| Start (S) Finish(F) | S | | ட | | S | ഥ | | S | Ŀ | | S | L | | S | L | | S | L | | S | ய | | S | ъ. | | S | * | ட | | S | u. | | S |
| Battery (V) | 1 | | 12 | | 14 | 13 | | 13 | 13 | | 13 | . 13 | | 13 | 14 | | 15 | 14 | | 14 | 13 | | 14 | 13 | | 15 | | 15 | | 16 | 13 | | 14 |
| Fuel | 1/2+ | | 1/2+ | | 1/2+ | 1/2- | , | 112- | 1/2- | | 1/2- | 3/8 | | 1/4 | 1/4 | | 3/8 | 5/8 | | 718 | 3/4+ | | 3/4+ | 3/4+ | | 5/8 | | 2/8 | | 2/8 | 5/8 | | 5/8 |
| Oil (psi) | 40 | | 20 | | 20 | 32 | | 39 | 30 | | 45 | 30 | | 39 | 30 | | 90 | 30 | | 50 | 30 | | 42 | 30 | | 65 | | 39 | | 55 | 32 | | 50 |
| Temp (°F) | 1/4 | | 1/4 | | 1/8 | 3/8 | | 1/4 | 3/8 | | 1/8 | 3/8 | | 1/4 | 3/8 | | 0 | 3/8 | | 1,8 | 1/4 | | 1/8 | 1/4 | | 1/16 | | 1/16 | | 3/4 | Out | | Out |
| Mileage 1 | | 89.5 | 6954.3 | 97.4 | = | 6964.2 | 107.3 | : | 6969.1 | 112.3 | £ | 6974.0 | 117.1 | le . | 6978.6 | 121.7 | ۵ | 6983.3 | 126.4 | <i>=</i> | 6991.3 | 134.4 | = | 6995.3 | 138.4 | 6995.6 | 138.7 | 7000.2 | 143.3 | ב | 7008.3 | 151.4 | 2 |
| Time | 11:30AM | | 11:49 | | 12:40PM | 1:00 | | 1:30 | 1:39 | • | 2:40 | 2:56 | | 3:12 | 3:32 | | 11:16AM | 11:35 | | 1:03PM | 1:20 | | 1:58 | 2:10 | | 9:55AM | | 10:10 | | 11:28 | 11:47 | | 12:40PM |
| Date | 1/6/98 | | 1/6/98 | | 1/6/98 | 1/6/98 | | 1/6/98 | 1/6/98 | | 1/6/98 | 1/6/98 | | 1/6/98 | 1/6/98 | | 1/7/98 | 17/98 | | 17798 | 1/7/98 | | 177/98 | 1/7/98 | | 1/9/98 | | 1/9/98 | | 1/9/98 | 1/9/98 | | 1/9/98 |
| Operator | TC | ļ | 5 | 1 | ן ה | ±ς | | Τſ | JŢ | | ٦٢ | ٦ | | ٦٢ | ٦٢ | | 5 | LS | - | | 10 | 1 | 2 | 2 | 1 | ار | 1 | | | To | 16 | | 15 |

Dane 1

| 1/8/98 1/12/94 1/12/94 1/12/94 F Blowest Temperature Gauge Out 1/8/98 1/47 7018.2 Out 45 1/2+ 1/4 S Blowest Temperature Gauge Out 1/8/98 2.48 702.8 Out 45 1/2+ 1/4 S FIT Temperature Gauge Out 1/8/98 2.48 702.8 Out 45 1/2+ 1/3 F FIT Temperature Gauge Out 1/8/98 3.05 702.5 Out 60 1/2+ 1/3 F FIT Temperature Gauge Out 1/8/98 5.50 702.4 Out 60 1/2+ 1/3 F FIT Temperature Gauge Out 1/10/98 5.50 702.4 Out 60 1/2+ 1/3 S Blowest Temperature Gauge Out 1/10/98 6.50 704.4 1/2- 1/3 7/2- 1/3 1/2- 1/3 F F F F 1/4 B A 1/8 <th>Operator</th> <th>Date</th> <th>Time</th> <th>Mileage 1</th> <th>Temp (°F)</th> <th>Oil (psi)</th> <th>Fuel</th> <th>Battery (V)</th> <th>Start (S) Finish(F)</th> <th>Place</th> <th>Comments</th> | Operator | Date | Time | Mileage 1 | Temp (°F) | Oil (psi) | Fuel | Battery (V) | Start (S) Finish(F) | Place | Comments |
|--|----------|---------|---------|-----------|-----------|-----------|------|-------------|------------------------|---------|---|
| 147 7018.2 Out 45 1/2+ 14 S Blowest 2:48 7027.5 Out 45 1/2+ 14 S FIT 165.9 Out 45 1/2+ 13 F Blowest 170.6 Out 60 1/2+ 13 F Blowest 4:37 7027.5 Out 60 1/2+ 15 S Blowest 4:37 7027.1 Out 60 1/2+ 15 S Blowest 4:37 7024.9 Out 60 1/2+ 15 F FIT 8:50 7044.9 Out 60 1/2- 15 F H19B 1:46PM " 0ut 60 1/2- 15 F A19B 1:46PM " 0ut 60 1/2- 15 F A19B 1:2:13PM 7082.0 Out 60 1/2- 15 S A19B | | 1/9/98 | 1:03AM | 7018.1 | Out | 30 | 5/8 | 14 | ı. | Biowest | Temperature Gauge Out |
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| 5.53 · 7032.1 Out 30 1/2+ 13 F IT 8.22 " Out 60 1/2+ 15 5 FIT 8.50 7044.9 Out 60 1/2- 15 F 419B 1:44PM " Out 60 1/2- 15 F 419B 1:44PM " Out 60 1/2- 15 F 419B 1:44PM " Out 60 1/2- 15 F 419B 1:56 7050.1 Out 60 1/2- 15 S Walmart 2:42 " Out 60 1/2- 15 S Walmart 4:00 205.1 30 1/2- 15 S Walmart 4:00 205.1 30 1/2- 15 S 419B 4:00 12:13PM 7052.0 Out 65 1/2- 15 S 419B 8:3BAM " Out 65 1/2- 15 S 419B | 1 | 1/9/98 | 4:37 | | Out | 69 | 1/2+ | 15 | S | Biowest | Temperature Gauge Out |
| 8:22 " Out 60 1/2+ 15 S FIT 8:50 7044.9 Out 60 1/2- 15 F 419B 1:44PM " Out 60 1/2- 15 S 419B 1:56 7050.1 Out 60 1/2- 15 S 419B 1:56 7050.1 Out 60 1/2- 15 S 419B 1:56 7050.1 Out 60 1/2- 15 S Walmart 2:42 " Out 60 1/2- 15 S Walmart 3:08 7062.0 Out 60 1/2- 15 S Walmart 4:00 205.1 1/2- 15 S Walmart 4:00 205.1 1/2- 15 S 419B 8:38AM " Out 65 1/2- 15 S 419B 9:08 7095.2 Out 60 1/2- 15 S 810Best 10:00 | 1 | 1,9/98 | 5:53 | 7032.1 | Out | 30 | 1/2+ | 13 | L | FIT | Temperature Gauge Out |
| 8:22 " Out 60 1/2+ 15 S FIT 8:50 7044.9 Out 38 1/2- 15 F 419B 1:44PM " Out 60 1/2- 15 S 419B 1:56 7050.1 Out 40 1/2- 13 F Walmart 2:42 " Out 60 1/2- 15 S 419B 2:42 " Out 60 1/2- 15 S Walmart 3:08 7062.0 Out 60 1/2- 15 S Walmart 4:00 2:05.1 1 14 F 419B 4:00 2:05.1 1 419B 419B 12:53 7082.8 Out 65 1/2- 15 S 419B 9:08 7085.2 Out 60 1/2- 15 S 419B 9:08 7085.2 Out | | | | 175.2 | | | | | | | |
| 8:50 7044:9 Oul 38 1/2- 15 F 419B 1:44PM " 0ut 60 1/2- 15 S 419B 1:56 7959.1 Out 60 1/2- 13 F Walmart 2:42 " Out 60 1/2- 15 S Walmart 2:42 " Out 60 1/2- 15 S Walmart 2:42 " Out 60 1/2- 15 S Walmart 2:42 " Out 60 1/4 14 F 419B 2:42 " Out 63 5/8 14 F 419B 4:00 205.1 3 1/2- 15 S 419B 4:05 Out 65 1/2- 15 S 419B 8:38AM " Out 65 1/2- 15 S 419B 9:08 | | 1/9/98 | 8:22 | 3 | Out | 99 | 1/2+ | .15 | S | FIT | Temperature Gauge Out |
| 118B 1:44PM " Out 60 1/2- 15 S 419B 1:56 7050.1 Out 40 1/2- 13 F Walmart 2:42 " Out 60 1/2- 15 S Walmart 3:08 7062.0 Out 60 1/2- 15 S Walmart 4:00 205.1 30 1/4 14 F 419B 12:13PM 7062.0 Out 63 5/8 14 S 419B 12:13PM 7082.8 Out 63 5/8 14 S 419B 12:13PM 7082.8 Out 63 1/2- 15 S 419B 12:13PM 7082.8 Out 65 1/2- 15 S 419B 8:38AM " Out 65 1/2- 15 S 419B 9:08 7095.2 Out 60 1/2+ 14 F FIT 10:10-0 " Out 60 <t< td=""><td></td><td>1:9/98</td><td>8:50</td><td>7044.9</td><td>Ont</td><td>38</td><td>1/2-</td><td>15</td><td>ц</td><td>419B</td><td>Temperalure Gauge Out</td></t<> | | 1:9/98 | 8:50 | 7044.9 | Ont | 38 | 1/2- | 15 | ц | 419B | Temperalure Gauge Out |
| 1:4PM " Out 60 1/2- 15 S 419B 1:56 7050.1 Out 40 1/2- 13 F Walmart 2:42 " Out 60 1/2- 15 S Walmart 2:42 " Out 60 1/2- 15 S Walmart 2:42 " Out 60 1/2- 15 S Walmart 4:00 205.1 419B 12:13PM 7062.0 Out 63 5/8 14 S 419B 12:13PM 7062.0 Out 63 5/8 14 S 419B 12:13PM 7082.8 Out 65 1/2- 15 S 419B 12:53 7095.2 Out 65 1/2- 15 S 419B 9:08 7095.2 Out 60 1/2- 15 F FIT 10:10 " Out 36 1/2- | | | | 188 | | | | | | | |
| 1:56 7950.1 Out 40 1/2- 13 F Walmart 2:42 " Out 60 1/2- 15 S Walmart 3:08 7062.0 Out 60 1/2- 15 S Walmart 4:00 205.1 7062.0 Out 63 5/8 14 F 419B 12:13PM 7062.0 Out 63 5/8 14 S 419B 12:13PM 7062.8 Out 63 1/2- 15 S 419B 8:38AM " Out 65 1/2- 15 S 419B 9:08 7095.2 Out 65 1/2- 15 S 419B 10:00 " Out 60 1/2+ 14 F Biowest 10:10 " Out 60 1/2+ 14 F FIT 10:25 7100.0 Out 36 1/2+ 14 F FIT 10:25 7100.0 1/2+ 1/2+ 14 | | 1/10/98 | 1:44PM | : | Out | 09 | 112- | 15 | S | 419B | Temperature Gauge Out |
| 2:42 " Out 60 1/2- 15 S Walmart 3:08 7062.0 Out 30 1/4 14 F 419B 4:00 205.1 419B 4:00 205.1 419B 12:13PM 7062.0 Out 63 5/8 14 S 419B 12:53 7082.8 Out 30 1/2 13 F 419B 8:38AM " Out 65 1/2- 15 S 419B 9:08 7095.2 Out 65 1/2- 15 S 419B 10:00 " Out 60 1/2+ 14 F Biowest 1 10:10 " Out 60 1/2+ 14 F Biowest 2 10:25 7100.0 Out 60 1/2+ 14 F FIT 10:25 7100.0 Out 36 1/2+ 14 F FIT | | 1/10/98 | 1:56 | 7050.1 | Ort | 40 | 1/2- | 13 | ட | Walmart | Temperature Gauge Out |
| 2:42 " Out 60 1/2- 15 S Walmart 3:08 7062.0 Out 30 1/4 F 419B 419B 4:00 205.1 419B 419B 419B 12:13PM 7062.0 Out 63 5/8 1/4 S 419B 12:13PM 7062.0 Out 30 1/2 13 F 419B 12:53 7082.8 Out 65 1/2- 15 S 419B 8:38AM " Out 65 1/2- 15 S 419B 9:08 7095.2 Out 65 1/2- 14 F Biowest 10:00 " Out 60 1/2+ 14 S Biowest 10:10 " Out 60 1/2+ 14 F FIT 10:25 7100.0 Out 60 1/2+ 14 F FIT | : | | N | 193.2 | | | | | | | |
| 3:08 7062.0 Out 30 1/4 14 F 419B 4:00 205.1 419B 419B 12:13PM 7062.0 Out 63 5/8 14 S 419B 12:13PM 7062.0 Out 30 1/2 13 F 419B 12:53 7082.8 Out 65 1/2- 15 S 419B 8:38AM " Out 65 1/2- 15 S 419B 9:08 7095.2 Out 3/8 14 F Biowest 10:10 " Out 60 1/2+ 14 S Biowest 10:10 " Out 60 1/2+ 14 F FIT 10:25 7100.0 Out 35 1/2+ 14 F FIT 243.1 F FIT | | 1/10/58 | 2:42 | 2 | Ont | 09 | 1/2- | 15 | S | Walmart | Temperature Gauge Out |
| 4:00 4:205.1 419B 42:13PM 7062.0 Out 63 5/8 14 S 419B 12:13PM 7062.0 Out 63 5/8 14 S 419B 12:53 7082.8 Out 30 1/2- 15 S 419B 8:38AM " Out 65 1/2+ 14 S Biowest 10:10 " Out 60 1/2+ 14 F FIT 10:25 7100.0 Out 60 1/2+ 14 F FIT 243.1 | | 1/10/98 | 3:08 | 7062.0 | Out | 30 | 1/4 | 14 | 1 | 419B | Temperature Gauge Out |
| 4:00 419B 12:13PM 7062.0 Out 63 5/8 14 S 419B 12:53 7082.8 Out 30 1/2 13 F 419B 8:38AM " Out 65 1/2- 15 S 419B 9:08 7095.2 Out 30 3/8 14 F Biowest 10:00 " Out 60 1/2+ 14 S Biowest 10:25 7100.0 Out 35 1/2+ 14 F FIT 243.1 * Out 35 1/2+ 14 F FIT | | | | 205.1 | | - | | | | | |
| 12:13PM 7062.0 Out 63 5/8 14 S 419B 205.1 205.1 102.6 1/2 13 F 419B 12:53 7082.8 Out 30 1/2- 15 S 419B 8:38AM " Out 65 1/2- 15 S 419B 9:08 7095.2 Out 3/8 14 F Biowest 10:10 " Out 60 1/2+ 14 S Biowest 10:25 7100.0 Out 35 1/2+ 14 F FIT 243.1 243.1 F F F F F | | 1/17/98 | 4:00 | | | | | | | 419B | Added 3.5 Gal of Methanol |
| 205.1 12:53 7082.8 Out 30 1/2 13 F 419B 8:38AM " Out 65 1/2- 15 S 419B 9:08 7095.2 Out 30 3/B 14 F Biowest 10:00 " Out 60 1/2+ 14 S Biowest 10:10 " Out 60 1/2+ 14 F FIT 243.1 243.1 | | 1/18/98 | 12:13PM | 7062.0 | Ood | 63 | 5/8 | 14 | S | 419B | Very Difficult Starting, Pressed Starter 4x |
| 12:53 7082.8 Out 30 1/2 13 F 419B 225.9 8:38AM " Out 65 1/2- 15 S 419B 9:08 7095.2 Out 30 3/8 14 F Biowest 10:00 " Out 60 1/2+ 14 S Biowest 10:25 7100.0 Out 35 1/2+ 14 F FIT 243.1 | | | | 205.1 | | | | | | | Service Engine Soon Light On |
| 225.9 B:3BAM " Out 65 1/2- 15 S 419B 9:08 7095.2 Out 30 3/8 14 F Biowest 10:00 " Out 60 1/2+ 14 S Biowest 10:10 " Out 60 1/2+ 14 F FIT 243.1 243.1 | | 1/18/98 | 12:53 | 7082.8 | Out | 30 | 1/2 | 13 | 14. | 419B | Service Engine Soon Light On |
| 8:38AM " Out 65 1/2- 15 S 419B 9:08 7095.2 Out 30 3/8 14 F Biowest 10:00 " Out 60 1/2+ 14 S Biowest 10:10 " Out 35 1/2+ 14 F FIT 243.1 243.1 | | | | 225.9 | | | | | | | |
| 9:08 7095.2 Out 30 3/8 14 F Biowest 10:00 " Out 60 1/2+ 14 S Biowest 10:25 7100.0 Out 35 1/2+ 14 F FIT 243.1 243.1 | | 1/19/98 | 8:38AM | 18 | Out | 65 | 1/2- | 15 | S | 419B | Very Difficult Starting, Presses Starter 6x |
| 9:08 7095.2 Out 30 3/8 14 F Biowest 233.3 233.3 201 80 1/2+ 14 80 80 10:10 " Out 60 1/2+ 14 8 80 10:25 7100.0 Out 35 1/2+ 14 F FIT 243.1 | | | | | | | | | | | Service Engine Soon Light On |
| 233.3 10:00 " Out 60 1/2+ 14 S Biowest 10:25 7100.0 Out 35 1/2+ 14 F FIT 243.1 | | 1/19/98 | 9:08 | 7095.2 | Out | 30 | 3/8 | 14 | ш. | Biowest | Service Engine Soon Light On |
| 10:00 " Out 60 1/2+ 14 S Biowest 10:10 " Out 80 1/2+ 14 S Biowest 10:25 7100.0 Out 35 1/2+ 14 F FIT 243.1 | | | | 233.3 | | | | | | | |
| 10:10 " Out 60 1/2+ 14 S Biowest 10:25 7100.0 Out 35 1/2+ 14 F FIT 243.1 | | 1/19/98 | 10:00 | | Out | | | | | | Added 3.0 Gal of Methanol |
| 10:25 7100.0 Out 35 1/2+ 14 F FIT 243.1 | | 1/19/98 | 10:10 | .1 | Out | 09 | 1/2+ | 14 | S | Biowest | Easy Start, Service Eng. Soon Light Not On |
| | ì | 1/19/98 | 10:25 | 7100.0 | Out | 35 | 112+ | 14 | <u> </u> | FIT | Service Engine Soon Light Not On |
| | | | | 243.1 | | | | | | | |

| Comments | Service Engine Soon Light Nol On | Service Engine Soon Light Not On | | Service Engine Soon Light Not On | Instant Start | Service Engine Soon Light Not On | | Starter Fixed at 3:00PM | Service Engine Soon Light Not On | | Service Engine Soon Light Not On | Service Engine Soon Light Not On | | Very Difficult Starting, Presses Starter 2x | Added 5.25 Gal Methanol | | | | | | | Not Bad Starting | | | Filled Fuel Tank ~8.2 Gal | Service Engine Soon Light Not On | | | | | | | |
|------------------------|----------------------------------|----------------------------------|-------|----------------------------------|---------------|----------------------------------|-------|-------------------------|----------------------------------|-------|----------------------------------|----------------------------------|-------|---|-------------------------|-----------|----------|-------|----------|------------|-------|------------------|---------|-------|---------------------------|----------------------------------|---------|-------|---------|---------|-------|---------|---|
| Place | FIT | Rooney's | | Rooney's | | 'IT Via Biowe | | FIT | Biowest | | Biowest | 419B | | 419B | | 1082B/STT | Rooney's | | Rooney's | 419B | | 419B | Biowest | | | Biowest | FIT | | FIT | Biowest | | Biowest | |
| Slart (S) Finish(F) | S | L | | S | | Ŀ | | S | 11. | | S | L | | S | | FIS | F/S | | S | <u>u</u> . | | S | ഥ | | | S | 12 | | S | Ŀ | | S | |
| Battery (V) | 14 | 14 | | 15 | | 14 | | 15 | 14 | | 14 | 14 | | 15 | | 14 | 14 | | 14 | 13 | | 15 | 14 | | | 14 | 14 | | 14 | 14 | - | 14 | |
| Fuel | 1/2+ | 1/2+ | | 1/2+ | | 1/2+ | | 1/2+ | 1/2- | | 172- | 1/4 | | 3/4 | | 2/8 | 5/8 | | 5/8 | 1/2+ | | 1/2+ | 1/2+ | | | 土 | ÷ | | 1. | i | | 古 | |
| (isd) liO | 90 | 38 | | 55 | | 30 | | Ω ₉ | 30 | | 55 | 35 | | 9 | | 45 | 40 | | 9 | 35 | | 70 | 35 | | | 09 | 40 | | 55 | 35 | | 40 | |
| Temp (² F) | Out | Out | | Out | | 0प | | Out | Out | | Out | Out | | Out | | Out | Out | | Ont | Out | | Out | Out | | | Out | Out | | Out | Out | | Out | |
| Mileage 1 Mileage 2 | = | 7103.8 | 245.9 | 7103.8 | 240.9 | 7118.2 | 261.5 | | 7123.1 | 266.2 | £ | 7136.7 | 279.8 | : | | 7143.1 | 7154.6 | 297.9 | 5 | 7172.7 | 315.8 | | 7188.4 | 331.5 | | - | 7192.7 | 335.8 | ٠ | 7197.5 | 340.6 | = | |
| | 11:38 | 11:50 | | 12:35PM | | 1:12 | | 4:00 | 4:15 | | 4:55 | 5:24 | | 11:23AM | | 11:38 | 12:05PM | | 1.20 | 2:05 | | 2:44PM | 2:44 | | 3:00 | 3:32 | 3:47 | | 4:29 | 4:47 | | 5:03 | |
| Dafe | 1/19/98 | 1/19/98 | | 1/19/98 | | 1/19/98 | | 1/19/98 | 1/19/98 | | 1/19/98 | 1/19/98 | | 1/20/98 | | 1/20/98 | 1/20/98 | | 1/20/98 | 1/20/98 | | 1/21/98 | 1/21/98 | | 1/21/98 | 1/21/98 | 1/21/98 | | 1/21/98 | 1/21/98 | | 1/21/98 | • |
| Operator | TC. | J. | | 15 | | -F | | 10 | J. | | 75 | 5 | | F | | 10 | 5 | | 15 | JT | | ٦٢ | JT | | ĴŢ | لخ | 5 | | ۲, | JŢ | | T | |

| Commonto | COMMISSION | | Started Fairly Facy No Buffer | Control and Easy, to Cutton | | | | | Easy Start | | | | | | | | | | | | Difficult Start - Rain | | | | | | | 1.95 ln the rain (192) | | | I - 95 to Wickham | | Very Difficult |
|------------------------|------------|-------|-------------------------------|-----------------------------|-------|---------|------------|-------|------------|---------|-------|---------|---------|-------|---------|---------|-------|---------|---------|-------|------------------------|---------|-------|---------|---------|-------|---------|------------------------|-------|-----------|-------------------|-------|----------------|
| Diace | 419B | | 419B | 114 | | FIT | Rooney's | | Rooney's | Biowest | | Biowest | FIT | | FIT | Biowest | | Biowest | 419B | | 419B | Biowest | | Biowest | FIT | | FIT | Rockledge | | Rockledge | 419B | | 419B |
| Start (S) Finish(F) | L | | S | L | | S | ш | | S | ш. | | S | L | | S | u_ | | S | ш | | S | Ŀ | | S | ш | | S | Ľ | | S | ı | | S |
| Battery | 13 | | 15 | 13 | | 14 | 14 | | 14 | 74 | | 13 | 13 | | 14 | 13 | | 14 | 13 | | 15 | 13 | | 14 | 13 | | 14 | 13 | | 13 | 13 | | 15 |
| Fuel | i | | ı, | i. | | 뇨 | ı <u>.</u> | | ഥ | ᅶ | | 3/4+ | 3/4+ | | 3/4+ | 3/4 | | 3/4 | 3/4- | | 3/4- | 1/2+ | | 1/2+ | 1/2+ | | 1/2+ | 1/2- | | 1/2- | 1/4 | | 1/4 |
| Oil (psi) | 30 | | 70 | 35 | | 99 | 40 | | 90 | 35 | | 45 | 38 | | 60 | 38 | | 90 | 35 | | 90 | 35 | | 42 | 32 | | 50 | 35 | | 45 | 35 | | 70 |
| Temp (°F) | ont | | Out | Ont | | ont | Out | | Out | Out | | Out | Out | | Out | Out | | Out | Out | | Out | Ont | | Out | Out | | Out | Out | | Out | Out | | Out |
| Mileage 1 | 7210 | 353.1 | = | 7222 | 365.1 | z | 7225.8 | 368.9 | 1 | 7235.7 | 378.8 | = | 7240 | 383.1 | E | 7244.8 | 387.9 | z | 7258.4 | 401.5 | Ξ | 7270.8 | 413.9 | 2 | 7275.1 | 418.2 | = | 7299 | 442.1 | 11 | 7315.6 | 458.7 | = |
| Time | 5:37 | | 8:20AM | 8:50 | | 11:25 | 11:38 | | 12:33PM | 12:53 | | 1:17 | 1:32 | | 2.49 | 3:05 | | 4:43 | 5:13 | | 8:52AM | 9:20 | | 9:33 | 9:45 | | 10:18 | 10:54 | | 11.18 | 11:49 | | 8:37AM |
| Date | 1/21/98 | | 1/22/98 | 172298 | | 1/22/98 | 1/22/98 | | 1/22/98 | 1/22/98 | | 1/22/98 | 1/22/98 | | 1/22/98 | 1/22,98 | | 1/22/98 | 1/22/98 | | 1/23/98 | 1/23/98 | | 1/23/98 | 1/23/98 | | 1/23/98 | 1/23/98 | | 1/23/98 | 1/23/98 | | 1/26/98 |
| Operator | TC | | ۲, | 5 | | 5 | TC | | ٦٢ | J. | | 5 | בן | | JT | 片 | | | 7. | | | Ľ, | | | Τſ | | | ΤC | | | 75 | | T.C |

| Comments | Made it! Total miles since 1/16/98 - 382 8 miles | 1 | Filled with 11.0 Gal MeOH => 12.8 mm | Rdi I | | | | Pressed starter hitton 4x | VI 101100 101100 101000 1 | | Started immediately | | | | | | | Had to return to Biowest to Steno nad | | | | | Started immediately | | | | | | | | | | |
|------------------------|--|-------|--------------------------------------|---------|-------|---------|-------|---------------------------|---------------------------|-------|---------------------|----------|-------|----------|---------|-------|---------|---------------------------------------|-------|---------|---------|-------|---------------------|----------|-------|---------|---------|-------|------------|----------|-------|---------|--|
| Place | Biowest | | | Biowest | | 419B | | | H | | FIT | Roonev's | | Raoney's | Biowest | | Biowest | Biowest | | Biowest | 늗 | | FIT | Biowest | | Biowest | ARI | | ARL | Biowest | | Biowest | |
| Start (S) Finish(F) | 1 | | | S | | L | | တ | ш | | S | ഥ | | S | u. | | S | IL. | | S | 14. | | တ | ш | | S | 1_ | | S | <u> </u> | | S | |
| Battery (V) | 14 | | | 15 | | 14 | | 15 | 14 | | 14 | 4 | | 14 | 4 | | 14 | 13 | | 13 | 13 | | 14 | 13 | | 14 | 7 | | 15 | 14 | | 14 | |
| Fuel | ш | | | 土 | | ÷ | | 土 | 止 | | Ľ | 止 | | 止 | ᇿ | | ı | ıŁ | | 3/4+ | 3/4 | | 3/4+ | 3/4 | | 3/4- | 3/4 | | 3,4 | 3/4- | | 3/4 | |
| Oil (psi) | 35 | | | 99 | | 35 | | . 70 | 35 | | 99 | 40 | | 9 | 35 | | 49 | 35 | | 38 | 30 | | 90 | 35 | | 45 | 35 | | 60 | 40 | | 45 | |
| Тетр (°F) | Ont | | | Oot | | Out | | Oat | Out | | Out | Ont | | Out | Out | | Out | Ont | | ont | mo | | ō | Out | | Out | Out | | on | Onl | | Out . | |
| Mileage 1 | 7329.2 | 472.3 | | 7329.8 | 472.3 | 7342.8 | 483.9 | = | 7354.6 | 497.7 | = | 7358.6 | 501.7 | = | 7368.4 | 511.5 | | 7377.4 | 520.5 | £ | 7381.7 | 524.8 | 9 | 7386.5 | 529.6 | ε | 7390 | 533.1 | . 1 | 7393.5 | 536.6 | ÷ | |
| Тіте | 9:05AM | | 1:00PM | 7:25 | | 7:52 | | 8:47AM | 9:13 | | 11:28 | 11:42 | | 12:40PM | 12:58 | | 1:10 | 1:37 | | 1:43 | 1:55 | | 2:53 | 3:10 | 38 | 3:28 | 3:39 | | 4:26 | 4:37 | ٠ | 4:50 | |
| Date | 1/26/98 | | 1/26/98 | 1/26/98 | | 1/26/98 | | 1/27/98 | 1/27/98 | | 1/27/98 | 1/27/98 | | 1/27/98 | 1/27/98 | | 1/27/98 | 1/27/98 | | 1727/98 | 1/27/98 | | 1/27/98 | 1/27/98 | | 1/27/98 | 1/27/98 | | 1/27/98 | 1/27/98 | | 1/27/98 | |
| Operator | J.C | | Τſ | JL | | ۲, | • | 5 | Τſ | | ۲5 | ۲ | | 5 | 16 | | T. | JL | | T. | JŢ | | Τſ | 5 | | JT | JŢ | | JT | 片 | | ٦٢ | |

| Comments | | | | | | | Overhead light out | | Presses starter button 6x, Cold (55°F) | | | | | | | | | | | | | | | | | | Filled with 11 Gal Methanol => 11.64 mpg | | | | | | |
|------------------------|----------|-------|----------|---------|-------|----------|--------------------|-------|--|---------|-------|-----------|-----|---------|-------|---------|-------|---------|---------|-------|---------|----------|-------|----------|----------|-------|--|---------|---------|-------|---------|----------|-------|
| Place | Rooney's | | Rooney's | FIT | | . EIT | 419B | | 419B | Biowest | • | Biowest · | FIT | FIT | | ARL | | ARL | Biowest | | Biowest | Rooney's | | Rooney's | Biowest | | | Biowest | FIT | | FIT | Biowest | |
| Start (S) Finish(F) | ᄔ | | , S | ட | | S | ц. | | လ | ட | | တ | ᄔ | S | | 1 | | တ | 4 | | S | LL. | | S | ட | | | S | ப | | တ | တ | |
| Battery (V) | 13 | | 14 | 13 | | 14 | 14 | | 15 | 14 | | 14 | | 15 | | 14 | | 14 | 14 | | 14 | 14 | | 14 | 14 | | | 14 | 13 | | 14 | 14 | |
| Fuel | 5/8 | | 5/8 | 5/8 | | 3/8 | 1/2+ | | 1/2+ | -2/1 | | -712- | | 112- | | 112- | | 112- | 112- | | -21 | 1/4 | | 1/4 | Red Mark | | | 土 | i. | | ±. | <u>‡</u> | |
| Oil (psi) | 30 | | 09 | 35 | | 09 | 35 | | 70 | 38 | | 42 | | 9 | | 40 | | 45 | 38 | | 90 | 30 | | 09 | 38 | | | 09 | 35 | | 90 | 38 | |
| Temp (°F) | ΙΛΟ | | Out | Ont | | Out | Out | | Out | Out | | Out | | Ont | | Out | | Out | Out | | Out | Out | | Out | Out | | | Ont | Onl | | Out | Out | |
| Mileage 1 Mileage 2 | 7401.5 | 544.6 | = | 7405.5 | 548.6 | = | 7417.2 | 560.4 | = | 7429.6 | 572.7 | | | 7434 | 577.1 | 7435.7 | 578.8 | ı | 7439.3 | 582.4 | ī, | 7447.3 | 590.4 | = | 7457.2 | 600.3 | | = | 7461.6 | 604.7 | = | 7466.6 | 609.7 |
| Time | 5:12PM | | 5:50 | 9:00 | | 8:03 | 8:28 | | 8:18AM | 8:48. | | 9:03 | | 9:55 | | 10:03 | | 10:08 | 10:18 | | 11:38 | 11:56 | | 12:42PM | 1:03 | | 1:40 | 2:00 | 2.15 | | 3:20 | 3:40 | |
| Date | 1/27/98 | | 1/27/98 | 1/27/98 | | 1,27,198 | 1/27/98 | | 1/28/98 | 1,28/98 | | 1/28/98 | | 1/28/98 | | 1/28!98 | | 1/28/98 | 1/28/98 | | 1/28/98 | 1/28/98 | | 1/28/98 | 1/28/98 | | 1/28/98 | 1/28/98 | 1/26/98 | • | 1/28/98 | 1/28/98 | |
| Operator | JT | | JT | JŢ | | Ţ | JŢ | | JL | ٦ | | TC | | JL | | 15 | | 5 | Tr | | TC | JĽ | | ΤL | JŢ | | JT | 15 | JT | | JL | JŢ | |

| Commonle | | | | | Very difficult start (46°F). More than 10 attempt | | | | | | | Very difficult shifting in tow gears | | | Vew difficult shifting in low gears | | | | | | | | Terrath Ohibina | giiniilg | | Facy efad | וופור לכמם | | Smeli of humino | | - | Easy start, Clutch no problem | |
|------------------------|---------|-------|---------|-------|---|---------|-------|---------|---------|-------|---------|--------------------------------------|-------|----------|-------------------------------------|-------|----------|---------|-------|---------|----------|---------------|-----------------|--------------|-------|-----------|------------|-------|-----------------|---------|-------|-------------------------------|--|
| Place | Biowest | | 419B | | 4198 | | | Biowest | FIT | | FIT | Biowest | | Biowest | Roonev's | | Roonev's | Biowest | | E | 1 | = | a | Biowest | Conce | = | FIT | | FIT | 419B | | 419B | |
| Start (S) Finish(F) | S | | u_ | | S | <u></u> | | S | L | | S | L | | S | 11 | | S | 11- | | U | ١١٥ | ۱ | U |) - | • - | C. | , | | S | ш | | S | |
| Battery | 4 | | 14 | | 15 | | | 14 | 13 | | 14 | 14 | | 14 | 13 | | 14 | 13 | | 7. | <u> </u> | 2 | 13 | 2 5 | | 14 | 13 | | 14 | 14 | | 15 | |
| Fuel | 走 | | 吐 | | 止 | | | ıŁ | 3/4+ | | 3/4+ | 3/4+ | | 3/4+ | 3/4+ | | 3,4+ | 3/4 | | 3/4- | 776 | - | 5/R | 5/8 | | 5/8 | 1/2+ | | 112+ | 1/2+ | | 1/2+ | |
| Oil (pst) | 99 | | 35 | | 22 | | | 69 | 40 | | 09 | 35 | | 90 | 35 | | 50 | 35 | | 45 | 2 2 | 3 | 50 | 35 | | 09 | 45 | | 09 | 35 | | 90 | |
| Temp (³F) | Out | | Out | | Out | | | Out | Out | | Out | Out | | Out | Out | | Out | Out | | į | į | | Out | Ont | | Out | Out | | oni | Ont | | Out | |
| Mileage 1 Mileage 2 | 7466.6 | 609.7 | 7480.2 | 623.3 | 1 | 7492.6 | 635.7 | = | 7496.8 | 639.9 | = | 7502 | 645.1 | <u>-</u> | 7510 | 653.1 | = | 7519.8 | 662.9 | = | 75258 | 668.9 | - | 7530.3 | 673.4 | Ξ | 7534.4 | 677.5 | Ŀ | 7546.3 | 689.4 | 13 | |
| Time | 5:08PM | | 5:45 | | 8:09AM | | | 9:08 | 9:20 | | 10:02 | 10:20 | | 11:55 | 12:15PM | | 1:03 | 1:22 | | 1:53 | 2.12 | | 2:50 | 3:08 | | 5:26 | 5:42 | | 8:00 | 8:25 | | 10:35AM | |
| Date | 1/28/98 | | 1/28/98 | | 1/29/98 | | | 1/29/98 | 1/29/98 | | 1/29/98 | 1/29/98 | | 1/29/98 | 1/29/98 | | 1/29/98 | 1/29/98 | | 1/29/98 | 1/29/98 | | 1/29/98 | 1/29/98 | | 1/29/98 | 1/25/98 | | 1/29/98 | 1/29/98 | | 2/2/98 | |
| Operator | 15 | | ٦٦ | | 5 | | | Τſ | ŢĹ | | Τζ | Τζ | | 5 | JT. | | ᅡ | 5 | | 片 | F5 | | 7. | Ţ | | JT | Τſ | | Τſ | Τſ | | TC | |

| Comments | | | Easy start, Clutch no problem | Easy start, Clutch no problem | | Easy start, Clutch no problem | | | Filled with 10.2 Gal Methanol => 11.27 mpg | | | | Very fough shifting | Shifting not too bad | | | Car shipped out for repairs | | Starting a little difficult, Clock not right | | | | Instant start | | | | | Filled with 7.0 Gal Methanol | | | | | |
|------------------------|---------|-------|-------------------------------|-------------------------------|-------|-------------------------------|---------|-------|--|---------|----------|-------|---------------------|----------------------|-------|---------|-----------------------------|-------|--|-------|---------|-------|---------------|----------|------------|--------|-------|------------------------------|-----|---------|--------|-------|--------|
| Place | FIT | | FIT | Rooney's | | н | Biowest | | III EII | Biowest | ᄪ | | FIT | Biowest | | Biowest | FIT | | FIT | | Biowest | | Biowest | FIT | | FIT | | Biowest | | Biowest | FIT | | FIT |
| Start (S) Finish(F) | Ŀ | | S | ı. | | S | 11 | | | S | ш | | S | ш. | | S | ıι | | S | | ட | | S | ıL | | S | | u. | | S | IL. | | သ |
| Battery (V) | 14 | | 14 | 13 | | 14 | 13 | | | 14 | 13 | | 14 | 13 | | 14 | 14 | | 15 | | 13 | | 13 | 13 | | 14 | | 13 | | 13 | 13 | | 14 |
| Fuel | 1/2- | | 1/2- | 1/2- | | 1/2- | 3/8 | | | F+ | <u>규</u> | | ±. | ‡ | | ‡± | 土 | | 3/4 | | 3/4- | | 3/4- | 1/2+ | | 1/2+ | | 1/2+ | | ц. | F+ | | # |
| Oil (psi) | 35 | | 20 | 35 | | 55 | 35 | | | 60 | 35 | | 99 | 35 | | 90 | 40 | | 20 | | 40 | | 09 | 38 | | 9 | | 42 | | 55 | 55 | | 90 |
| Temp (PF) | Out | | Out | ١. | | Out | Ont | | | Ont | Out | | oni | Out | | Out | Out | | Ont | | Out | | Ont | Out | | Out | | Out | | Ont | Out | | Out |
| Mileage 1 | 7558.5 | 701.6 | = | 7562.4 | 705.3 | | 7572.3 | 715.4 | | = | 7576.5 | 719.6 | - | 7581.4 | 724.5 | 11 | 7586.1 | 729.2 | 7602.2 | 745.3 | 7606.8 | 749.9 | = | 7611.1 | Can'l Read | 7611.1 | 754.2 | 7615.9 | 759 | = | 7620.2 | 763.3 | = |
| Time | 11:00AM | | 11:32 | 11:42 | | 12:28PM · | 12:47PM | | 1:00 | 2:00 | 2:17 | | 3:29 | 3:50 | | 2:28PM | 2:48 | | 10:25AM | | 10:42 | | 11:35 | 11:49 | | 1:05PM | | 1:23 | | 2:28 | 2:44 | | 4:13 |
| Date | 2/2/98 | | 2/2/98 | 2/2/98 | | 2/2/98 | 2/2/98 | | 2/2/98 | 2,2,98 | 2/2/98 | | 2/2/98 | 2/2/98 | | 2/3/98 | 2/3/98 | | 3/2/98 | | 3/2/98 | | 3/2/98 | 3,72,198 | | 3/2/98 | | 3,2/98 | | 3/2/98 | 3/2/98 | | 3/2/98 |
| Operator | JT | | JL | Τſ | | TU | Тſ | | 5 | 5 | Τζ | | T.C | با | | ٦٢ | 片 | | JT | | Tſ | | JT | JT | | Τſ | | JĽ | | ٦٢ | JL | | Τſ |

| Comments | | | Filled with 7 Gal of Methanol => 5.54 mpg | | | | Very hard starting, too much Ether | | | Instant start | By Wickham Road | | Instant start | Via Riverside and FIT | | | | | | | | | | | | | | Instant slart | | | Tough starting, Pressed starter 3x | | |
|------------------------|---------|-------|---|---------|---------|-------|------------------------------------|---------|-------|---------------|-----------------|-------|---------------|-----------------------|-------|---------|--------|-------|--------|---------|-------|---------|--------|-------|--------|--------|-------|---------------|--------|-------|------------------------------------|---------|-------|
| Place | Biowest | | | Biowest | FIT | | FIT | Biowest | | Biowest | 419B | | 419B | Biowest | | Biowest | FIT | | FIT | Biowest | | Biowest | 4198 | | 419B | FIT | | FIT | 419B | | 419B | Biowest | |
| Start (S) Finish(F) | L | | | တ | 止 | | တ | u. | | တ | ı. | | တ | ш | | S | Ħ | | တ | ıι | | S | ഥ | | S | u | | ಽ | L | | S | ᄔ | |
| Battery (V) | 13 | | | 14 | 13 | | | 13 | | 14 | 13 | | 14 | 13 | | 13 | | | 13 | 13 | | 13 | 13 | | 15 | 14 | | 14 | 14 | | 16 | 14 | |
| Fuel | ti | |] | Ī | 4 | | ц. | 芷 | | uL. | ı <u>.</u> | | L | 3/4 | | 3/4 | 3/4+ | | 3/4+ | 3/4- | | 3/4- | 1/2+ | | 1/2+ | 1/2 | | 1/2+ | 1/2 | | 1/2- | 1/4 | |
| Oil (psi) | 35 | | | 09 | 35 | | | 40 | | 90 | 32 | | 90 | 35 | | 45 | | | ಜ | 49 | | 9 | 35 | | 90 | 39 | | 9 | 35 | | 70 | 35 | |
| Temp (³F) | Ont | | | Out |) MO | | OM | Out | | Ont | Out | | Out | Out | Out | Out | Ont | | Out | Out | | Out | Out | | Out | Out | | Ont | Ont | | Out | Out | |
| Mileage 1 | 7625 | 768.1 | | 7625 | 7529.5 | 772.6 | = | 7634.2 | 777.3 | = | 7647.8 | 790.9 | - | 7664.4 | 807.5 | | 7668.7 | 811.8 | = | 7673.6 | 816.7 | = | 7687.2 | 830,3 | | 7699.3 | 842.4 | = | 7711.3 | 854.4 | = | 7723.7 | 866.8 |
| Time | 4:31 | | | 5:13 | 5:30 | | | 10:28AM | | 11:18 | 11:43 | | 12:50PM | 1:33 | | 1:55 | | | 3:10 | 3:25 | | 3:33 | 4:08 | | 6:05 | 6:29 | | 8:14 | 8:40 | | 8:19AM | 8:53 | |
| Date | 3/2/98 | | | 3/2/98 | 372/98 | | 3/3/98 | 3/3/98 | | 3/3/98 | 3/3/98 | | 3/3/98 | 3,3/98 | | 3/3/98 | 3/3/98 | | 3/3/98 | 3/3/98 | | 3/3/98 | 3/3/98 | | 3/3/98 | 3/3/98 | | 3/3/98 | 3/3/98 | | 3/4/98 | 3/4/98 | |
| Operator | ΤĽ | | | JŢ | JT | | Τſ | F, | | Τſ | JL | | F, | ۲, | | JL | JL | | ΤĽ | J.C | | ŗ | Τſ | | ΤC | ΤĊ | | JT | ΤĹ | | JT | Τſ | |

| Comments | | | | | | Performed well at low fuel | Filled with 11.6 Gal of Methanol => 9.28 mpg | | | | | | | | | | | | | | | | | | | Fairly easy starting | Via FIT and South Patrick | | | | | | |
|------------------------|---------|-------|--------|-------|--------|----------------------------|--|---------|--------|-------|--------------|---------|-------|----------|--------|-------|----------|---------|-------|---------|----------|-------|----------|--------|-------|----------------------|---------------------------|-------|---------|--------|-------|--------|--|
| Place | Biowest | | FIT | | = | Biowest | | Biowest | FIT | | FIT | Biowest | | Biowest | FIT | | FIT | Biowest | | Biowest | Rooney's | | Rooney's | 419B | | 419B | Biowest | | Browest | FIT | | FIT | |
| Start (S) Finish(F) | S | | ъ. | | S | II. | | S | LL. | | S | L. | | တ | F | | တ | ഥ | | S | ഥ | | S | ш | | S · | ц. | | S | பட | | S | |
| Battery (V) | 14 | | 14 | | 15 | 13 | | 14 | 13 | | 14 | .13 | | 14 | 13 | | 13 | 13 | | 14 | 13 | | 13 | 13 | | 15 | 13 | | 13 | 13 | | 14 | |
| Fuel | 1/4 | | 1/4 | | 114 | Red Mark | | 土 | Ŧ. | | 1 | ‡ L | | <u>†</u> | 亡 | | <u>†</u> | ш | | ıi. | ᅹ | | <u>.</u> | Ľ. | | 14. | 3/4 | | 3,4 | 3/4- | | 3/4- | |
| Oit (psi) | 40 | | 40 | | 90 | 35 | | 09 | 40 | | 09 | 40 | | 9 | 35 | | 45 | 35 | | 40 | 35 | | 42 | 35 | | 20 | 30 | | 40 | 40 | | 65 | |
| Temp (PF) | Out | | Out | | Out | Out | | Ont | Out | | Out | Out | | Out | Out | | ino | Out | | Out | Out | | Out | Out | | Out | Out | | Out | · | | . Out | |
| Mileage 1 Mileage 2 | 7723.7 | 866.8 | 7728 | 871.1 | = | 7732.6 | 873.9 | = | 7737.3 | 880.4 | " | 7742.1 | 885.2 | : | 7746,4 | 889.5 | , | 7751.2 | 894.4 | | 7759.3 | 902.4 | : | 7773.7 | 916.8 | = | 7790.2 | 933.3 | 2 | 7794.7 | 937.8 | H | |
| Time | 9:00AM | | 9:12 | | 10:15 | 10:30 | | 1:23PM | 1:37 | - | 2:43 | 2:58 | | 3:53 | 4:08 | | 4:20 | 4:38 | | 4:51 | 5:13 | | 5:48 | 6:16 | | 12:33PM | 1:13 | | 1:25 | 1:40 | | 3:43 | |
| Date | 3/4/98 | | 3/4/98 | | 3/4/98 | 3/4/98 | | 3/4/98 | 3/4/98 | | 3/4/98 | 3/4/98 | | 3/4/98 | 3,4198 | | 3/4/98 | 3/4/98 | | 3/4/98 | 3/4/98 | | 3/4/98 | 3/4/98 | | 3/5/98 | 3/5/98 | | 3,5798 | 3/5/98 | | 3/5/98 | |
| Operator | 15 | | ŢĹ | | JT | JL | | الم | FC | | רט | TC | | 75 | JL | | ار ا | TC | | 15 | J. | | 5 | JT | | Tr | JT | | JŢ | TC | | Tſ | |

| Oil (psi) Fuel (V) Finish(F) Place Comments | 3/4- 13 | | 45 3/4- 13 S Biowest | 40 1/2+ 13 F Rooney's | | 60 1/2+ 14 S Rooney's | 40 1/2+ 13 F FIT | | 60 1/2+ 14 S FIT | 45 1/2+ 13 F Rooney's | | 60 1/2+ 1/4 S Rooney's | 35 1/2 13 F 419B | 60 F+ 14 S Biowest New temperature gauge installed | Filled with 11.05 Gal Methanol | 40 F+ 13 F FIT | | 55 F+ 13 S FIT | 40 F+ 13 F Biowest | | 60 F+ 13 S Biowest | 35 F- 12 F 419B Via Wickham Rd. | | F- 15 | 35 F- 13 F Biowest Via South Patrick | | 45 3/4+ 13 S Biowest | 35 3/4 13 F FIT | | |
|---|---------|-------|----------------------|-----------------------|-------|-----------------------|------------------|-------|------------------|-----------------------|-------|------------------------|------------------|--|--------------------------------|----------------|------|----------------|--------------------|------|--------------------|---------------------------------|---------|---------|--------------------------------------|-------|----------------------|-----------------|-----|------------------|
| | | | | | | Ont 60 | Out 40 | | Out 60 | Out 45 | | Out 60 | Out 35 | 165 60 | | 190 40 | | 120 55 | 198 40 | | 100 60 | 190 35 | | | 195 35 | | 190 45 | 190 35 | | 125 GO |
| | 7799.4 | 942.3 | | | 920.6 | s. | 7811.5 | 954.6 | | 7815.4 | 958.5 | E | 7829.1 | | | 7944.7 | 84.8 | | 7946.3 1 | 89.4 | = | 7959.8 | 102.9 | | 7972.2 1 | 115.3 | | 7976.9 | 120 | * |
| Time | 4:03AM | | 4:20 | 4:40 | | 5:17 | 5:28 | | 8:05 | 8:16 | | 8:52 | 9:20 | 3:33PM | | 3:51 | | 4:18 | 4:33 | | 9:05 | 9:29 | | 7:34AM | 8:09 | | 8:21 | 8:35 | | 40.40 |
| Date | 3/5/98 | | 3/5/98 | 3/5/98 | | 3/5/38 | 3/5/98 | | 3/5/98 | 3/5/98 | | 3/5/98 | 3/5/98 | 3/18/98 | | 3,18,98 | | 3/18/98 | 3/18/98 | | 3/18/98 | 3/18/98 | 3/18/98 | 3/19/98 | 3/19/98 | | 3/19/98 | 3,19,98 | | 2/20/2 2/20/2 |
| Operator | ΤC | | 드 | 片 | | <u>ا</u> | ٦٢ | | L | JT | | 5 | JT | 5 | | 片 | | JT | 占 | | Τſ | JT | ٦٢ | 片 | JT | | JT | Τſ | | <u>L</u> |

| Comments | | | | | | | | | | | | | | | | | | | | | | | Turned key, hit button, instant start | | | | | | | Filled with 11.6 Gal Methanol => 11.48 mpg | | |
|------------------------|---------|-------|----------|-------|----------|---------|-------|---------|---------|-------|---------|---------|-------|---------|------------|-------|------------|---------|-------|---------|---------|-------|---------------------------------------|---------|-------|---------|---------|-------|---------|--|-------|---------|
| Place | FIT | | Rooney's | | Rooney's | Biowest | | Biowest | FIT | | FIT | Biowest | | Biowest | Rom Bakery | | Rom Bakery | FIT | | FIT | 419B | | 4198 | Biowest | | Biowest | FIT | | FIT | Biowest | | Biowest |
| Start (S) Finish(F) | S | | ı. | | S | ĽL. | | S | u. | | S | Li. | | S | ட | | S | Œ | | S | L | | S | L | | S | Ľ. | | S | ഥ | | S |
| Battery (V) | 14 | | 13 | | 14 | 13 | | 14 | 13 | | 13 | 13 | | 14 | 13 | | 13 | 13 | | 14 | 13 | | 15 | 13 | | 14 | 13 | | 14 | 13 | | 15 |
| Fue | 3/4 | | 3/4- | | 3/4 | 3/4- | | 3/4- | 1/2+ | | 1/2+ | 1/2+ | | 1/2+ | 1,2+ | | 1/2+ | 1/2 | | 1/2+ | 1/2 | | 1/2- | 1/4 | | 1/4+ | 1/4 | | 1/4 | Red Mark | | π † |
| Oil (psi) | 90 | | 35 | | 90 | 35 | | 90 | 35 | | 90 | 35 | | 60 | 20 | | 09 | 40 | | 90 | 35 | | 70 | 30 | | 40 | 38 | | 90 | 40 | | 09 |
| Temp (°F) | 160 | | 203 | | 150 | 195 | | 172 | 200 | : | 165 | 200 | | 160 | 185 | | 160 | 190 | | 110 | 195 | | 100 | 193 | | 193 | 198 | | 160 | 190 | | 100 |
| Mileage 1 | 7981,6 | 124.7 | 9.6867 | 132.7 | = | 7999.5 | 142.6 | I | 8003.8 | 146.9 | = | 8008.8 | 151.9 | 2 | 8009.2 | 152.3 | 5 | 8013.1 | 156.2 | | 8025.7 | 168.8 | | 8032.2 | 181.3 | | 8042.1 | 185.9 | a | 8047.5 | 190.6 | z |
| Time | 11:35AM | | 11-54 | | 1:15PM | 1:35 | | 2:03 | 2:17 | • | 3:13 | 3:33 | | 4:24 | 4:28 | | 4:58 | 5:10 | | 7:42 | 8:07 | | 8:18AM | 8:47 | | 8:53 | 9:08 | | 10:03 | 10:16 | • | 3:08PM |
| Date | 3/19/98 | | 3/19/98 | | 3/19/98 | 3/19/98 | | 3/19/98 | 3/19/98 | | 3/19/98 | 3/19/98 | | 3/19/98 | 3/19/98 | | 3/19/98 | 3/19/98 | | 3/19/98 | 3/19/98 | | 3/23/98 | 3/23/98 | | 3/23/98 | 3/23/98 | | 3/23/98 | 3/23/98 | | 3/23/98 |
| Operator | JT | | JŢ | | Τſ | TC | | Τſ | 5 | | TC | TC | | JJ | JT | | JT | T, | | F | TC . | | ا ا | Τſ | | T.C | TC | | | JT | | Τſ |

| Comments | | | | | | | | | | Instant Start | | | | | | | | | | | | | | | | | | | | | | | |
|------------------------|---------|-------|---------|---------|-------|---------|-------|---------|-------|---------------|---------|-------|---------|---------|-------|----------|-------|---------|-------|---------|---------|-------|---------|---------|-------|---------|----------|----------|-------|---------|-------|---------|--|
| Place | FIT | | FIT | Biowest | | Biowest | | 419B | | 419B | Biowest | | Biowest | FIT | | Rooney's | | Biowest | | Biowest | FIT | | FIT | Biowest | | Biowest | Raoney's | Rooney's | | FIT | | FIT | |
| Start (S) Finish(F) | L. | | တ | Œ | | S | | L | | S | L. | | S | щ | | S | | Ŀ | | S | u_ | | တ | Щ | | S | L. | S | | ഥ | | S | |
| Battery (V) | 14 | | 14 | 13 | | 13 | | . 13 | | 14 | 13 | | 4 | 13 | | 13 | 13 | 13 | | 13 | 13 | | 14 | 13 | | 14 | 13 | 13 | | 13 | | 14 | |
| Fuel | ţ. | | F÷ | Ε÷ | | Ę. | | Ľ | | ď. | Ľ | | 3/4+ | 3/4+ | | 3/4+ | 3/4+ | 3/4 | | 3/4 | 3/4- | | 3/4- | 1/2+ | | 1/2+ | 1/2+ | 1/2+ | | 1/2+ | | 1/2+ | |
| Oil (psi) | 45 | | 09 | 35 | | 90 | | 35 | | 90 | 35 | | 09 | 40 | | 99 | | 35 | | 20 | 35 | | 60 | 35 | | 90 | 35 | 50 | | 35 | | 60 | |
| Temp (°F) | 190 | | 150 | 195 | | 175 | | 198 | | 100 | 203 | | 150 | 203 | | 170 | | 195 | | 170 | 203 | | 165 | 203 | | 150 | 203 | 180 | | 195 | | 150 | |
| Mileage 1 Mileage 2 | 8051.3 | 194.8 | п | 8056.6 | 199.7 | 8056.7 | 199.7 | 8070.2 | 213.3 | : | 8082.6 | 225.7 | s | 8087 | 230.1 | 8091.5 | 234.6 | 8101.5 | 244.6 | = | 8105.7 | 248.8 | = | 8110.4 | 256.7 | • | 8118.7 | = | 261.7 | 8122.7 | 265.7 | = | |
| Time | 3:20PM | | 4:28 | 4:45 | | 5:08 | | 5:40 | | 7:29AM | 8:25 | | 9:38 | 9:55 | | 12:33PM | | 12:49 | | 1:30 | 1:44 | | 2:40 | 2:56 | | 4:35 | 4:58 | 5:27 | | 5:40 | | 7:57 | |
| Date | 3/23/98 | | 3/23/98 | 3/23/98 | | 3/23/98 | | 3/23/98 | | 3/24/98 | 3/24/98 | | 3/24/98 | 3/24/98 | | 3/24/98 | | 3/24/98 | | 3/24/98 | 3/24/98 | | 3/24/98 | 3/24/98 | | 3/24/98 | 3/24/98 | 3/24/98 | | 3/24/98 | | 3/24/98 | |
| Operator | JŢ | | JT | JŢ | | 나 | | ΤĽ | | F, | 5 | | ΤC | ΤC | | TC | | ΤL | | Ţ | TC | | JT | JT | | Τſ | ΤĽ | 5 | JT. | ТС | ٦. | TC . | |

Page 1:

| Comments | | | | Instant start, key, button, ignition (order) | | | | | | | Filled with 11.0 Gal Methanol => 9.85 mpg | | | | | | | | | Via Wickham Rd. | | Instant start with Ether | | | | | | | | | | | |
|------------------------|----------|-------|---------|--|-------|---------|-------|---------|-------|----------|---|-------|---------|---------|-------|---------|---------|-------|---------|-----------------|-------|--------------------------|---------|-------|---------|---------|-------|---------|----------|-------|----------|---------|---------|
| Place | 419B | | | Biowest | | Biowest | | FIT | | FIT | Biowest | | Biowest | FIT | | FIT | Biowest | | Biowest | 4198 | | 419B | Biowest | | Biowest | FIT | | FIT | Rooney's | | Rooney's | Biowest | |
| Start (S) Finish(F) | <u>ь</u> | | | L. | | S | | ıL | | တ | ᄔ | | S | L | | S | ш | | တ | Ŀ | | S | ı. | | S | L. | | S | ഥ | | တ | ᄣ | • |
| Battery (V) | 13 | | | 13 | | 14 | | 13 | | 13 | 13 | - | 14 | 13 | | 14 | 13 | | 14 | 13 | | 15 | 13 | | 13 | 13 | | 13 | 13 | | 13 | 13 | |
| Fuel | 1/2 | | | 1/2- | | 112- | ٠ | 1/4 | | 1/4 | Red Mark. | | ţ. | ‡ | | 走 | ‡ | | ţ. | ΐ | | Ľ | ك | | Ľ | 3/4 | | 3/4+ | 3/4+ | | ., | 3/4 | |
| Oil (psi) | 40 | | | 35 | | 50 | | 40 | | 55 | 35 | | 9 | 55 | | 90 | 35 | | 90 | 35 | | 20 | 35 | | 45 | 40 | | 09 | 35 | • | : 09 | 35 | |
| Temp (⁹ F) | 192 | | | 205 | | 170 | • | 200 | | 170 | 199 | | 110 | 192 | | 150 | 200 | | 160 | 195 | - | 100 | 193 | • | 190 | 193 | | 120 | 195 | | 160 | 195 | |
| Mileage 1 Mileage 2 | 8134.3 | 277.4 | - | 8146.7 | 289.8 | 8146.7 | 289.8 | 8151 | 294.1 | <u>.</u> | 8155.8 | 298.9 | = | 8160.7 | 306.7 | 2 | 8165.1 | 308.2 | = | 8178.7 | 321.8 | = | 8191.2 | 334.3 | a | 8195.5 | 338.6 | = | 8199.4 | 342.3 | u | 8209.3 | 362.4 |
| Time | 8:21PM | | 8:04AM | 8:40 | | 9:15 | | 9:29 | | 10:10 | 10:23 | | 2:07PM | 2:20 | | 3:25 | 3:39 | | 4:50 | 5:20 | | 8:21AM | 8:51 | | 9:00 | 9:11 | | 11:31 | 11:43 | | 12:45PM | 1:06 | |
| Date | 3/24/98 | | 3/25/98 | 3/25/98 | | 3/25/98 | | 3/25/98 | | 3/25/98 | 3/25/98 | | 3/25/98 | 3/25/98 | | 3/25/98 | 3/25/98 | | 3/25/98 | 3/25/98 | | 3/27/98 | 3/27/98 | | 3/27/98 | 3/27/98 | | 3/27/98 | 3/27/98 | | 3127/98 | 3/27/98 | 3127/98 |
| Operator | Τſ | | Τŗ | JT | | Η | | Ţſ | | Τζ | Tť | | ŢĻ | 15 | | TC | F7 | | ŢĻ | JŢ | | ŢĻ | Tſ | | Τſ | TC. | | ŢĻ | ЭŢ | | TC | JŢ | Τſ |

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