

**APPENDIX C - Publications, Conference Papers, and Presentations  
based on this work**

## *Publications*

### *Refereed*

- Postula, W.S., Z. Feng, C.V. Philip, A. Akgerman, and R.G. Anthony, "Conversion of Synthesis Gas to Isobutylene over Zirconium Dioxide Based Catalysts," *J. Catal.* **145**, 126 (1994).
- Postula, W.S., A. Akgerman, and R.G. Anthony, "The Effect of Hydrogen Sulfide on Isosynthesis over 7% (wt) Cerium Zirconia Catalyst," *Applied Catalysis A:General* **112**, 175-185 (1994).
- Feng, Z., W.S. Postula, C. Erkey, C.V. Philip, A. Akgerman, and R.G. Anthony, "Selective Formation of Isobutane and Isobutene from Synthesis Gas over Zirconia Catalysts Prepared by a Modified Sol Gel Method," *J. Catal.* **148**, 84-90 (1994).
- Feng, Z., W.S. Postula, A. Akgerman, and R.G. Anthony, "Synthesis and Characterization of Zirconia Based Catalysts Prepared by Precipitation, Calcination, and Modified Sol-Gel Methods," to be submitted to *I&EC Research (Kinetics and Catalysis)*.
- Feng, Z., A. Akgerman, and R.G. Anthony, "Selective Formation of Isobutane and Isobutene from Synthesis over Calcium Promoted Zirconias," to be submitted to *Appl. Catal. A*.
- Erkey, C., J. Wang, W.S. Postula, Z. Feng, C.V. Philip, A. Akgerman, and R.G. Anthony, "Isobutylene Production from Synthesis Gas over Zirconia in a Slurry Reactor," to be submitted to *I&EC Research (Kinetics and Catalysis)*.

### *Papers for Technical Conferences*

- Anthony, R.G., A. Akgerman, C. Erkey, Z. Feng, W. Postula, and C.V. Philip, "Catalyst and Process Development for Synthesis Gas Conversion to Isobutylene," *Proceedings of DOE Liquefaction Contractors' Review Meeting*, Pittsburgh, PA, September 3-5, 1991.
- Anthony, R.G., W. Postula, Z. Feng, and A. Akgerman, "Use of Zirconia in the Conversion of Hydrogen Lean Synthesis Gas to Isobutylene," Preprint Paper-*Am. Chem. Soc., Div. Fuel Chem.*, **37**, 247-53 (1992). Preprints of Symposium on Coal Liquefaction at the Spring ACS National Meeting in San Francisco, CA, April 1992.
- Anthony, R.G., A. Akgerman, W.S. Postula, Z. Feng, C.V. Philip, and C. Erkey, "Catalyst and Process Development for Synthesis Gas Conversion to Isobutylene," *Proceedings of DOE Liquefaction Contractors' Review Meeting*, Pittsburgh, PA, September 22-24, 1992.

Anthony, R.G., W.S. Postula, Z. Feng, C.V. Philip, and A. Akgerman, "Isobutylene Synthesis Using Zirconia and Modified Zirconia," *Proceedings of the Ninth Annual International Pittsburgh Coal Conference*, Pittsburgh, PA, October 12-16, 1992.

Anthony, R.G., A. Akgerman, W.S. Postula, Z. Feng, C.V. Philip, and C. Erkey, "Catalyst and Process Development for Synthesis Gas Conversion to Isobutylene," *Proceedings of DOE Liquefaction Contractors' Review Meeting*, Pittsburgh, PA, September 27-29, 1993.

Also, monthly and quarterly reports were filed at the appropriate times with DOE.

### *Presentations*

Anthony, R.G., "Catalyst and Process Development for Synthesis Gas Conversion to Isobutylene," DOE Liquefaction Contractors' Review Meeting, Pittsburgh, PA, September 3-5, 1991.

Postula, W.S., "Conversion of SynGas to Isobutylene over Zirconium Dioxide Catalyst," Second Annual Chemical Engineering Graduate Research Symposium, Texas A&M University, College Station, Texas, January 9, 1992.

Anthony, R.G., "Use of Zirconia in the Conversion of Hydrogen Lean Synthesis Gas to Isobutylene," Symposium on Coal Liquefaction at the Spring ACS National Meeting in San Francisco, CA, April 1992.

Anthony, R.G., "Catalyst and Process Development for Synthesis Gas Conversion to Isobutylene," DOE Liquefaction Contractors' Review Meeting, Pittsburgh, PA, September 22-24, 1992.

Anthony, R.G., "Isobutylene Synthesis Using Zirconia and Modified Zirconia," Ninth Annual International Pittsburgh Coal Conference, Pittsburgh, PA, October 12-16, 1992.

Anthony, R.G., "Catalyst and Process Development for Synthesis Gas Conversion to Isobutylene," DOE Liquefaction Contractors' Review Meeting, Pittsburgh, PA, September 27-29, 1993.

Postula, W.S., "Isobutylene Synthesis Over Zirconia-Based Catalysts," 49<sup>th</sup> American Chemical Society Southwest Regional Meeting, Hyatt Regency Hotel, Austin, Texas, October 27, 1993.

**APPENDIX D - TABLES**

**List of Tables 1.1 - 3.35 on pages viii-x**

TABLE 1.1. Conversions and product distributions<sup>a</sup> of CO/H<sub>2</sub> reactions at equilibrium

Pressure (atm)	50		70	
	653	723	653	723
CO	0.000339	0.001660	0.000295	0.001401
H <sub>2</sub>	0.000886	0.001936	0.000750	0.001639
CO <sub>2</sub>	0.338798	0.360891	0.338427	0.360205
H <sub>2</sub> O	0.331568	0.312950	0.331927	0.313742
C	0.223619	0.214070	0.223464	0.213770
CH <sub>4</sub>	0.104789	0.108471	0.105138	0.109227
C <sub>2</sub> H <sub>6</sub>	0	0.000016	0.000016	0.000016
CO conversion	0.999636	0.998214	0.999732	0.998675
H <sub>2</sub> conversion	0.986799	0.97117	0.990141	0.97848

<sup>a</sup> Distributions are on a weight basis, 1/1 CO/H<sub>2</sub> in the feed.

TABLE 2.1. Chemicals utilized in precipitated, hydrothermal, and calcination catalyst preparation

Compound	Purity	Main impurities (ppm)
$\text{ZrO}(\text{NO}_3)_2 \cdot 5\text{H}_2\text{O}$	tech	Hf-3700, Fe-400, Si-250
NaOH	97%	$\text{Na}_2\text{CO}_3$ -10000, K-2000
$\text{LiNO}_3$	99.99%	Cs-16, Ca-7, K-1, Na-0.8
$\text{Ba}(\text{NO}_3)_2$	99.98%	Sr-100, Si-25, Ni-10
$\text{Cu}(\text{NO}_3)_2 \cdot 3\text{H}_2\text{O}$	99.999%	None detected
$\text{Mg}(\text{NO}_3)_2 \cdot 6\text{H}_2\text{O}$	99.995+%	Na-9, Mn-1, Zn-1
$\text{Mn}(\text{NO}_3)_2 \cdot 6\text{H}_2\text{O}$	98%	No analysis
$\text{Al}(\text{NO}_3)_3 \cdot 9\text{H}_2\text{O}$	99.997%	Si-2, Na-1
$\text{Ce}(\text{NO}_3)_3 \cdot 6\text{H}_2\text{O}$	99%	La-2000, Ca-65, Si-25
$\text{Dy}(\text{NO}_3)_3 \cdot 5\text{H}_2\text{O}$	99.9%	Si-100, Er-35, Ca-4
$\text{TiCl}_3$	99%	No analysis
$\text{Y}(\text{NO}_3)_3 \cdot 5\text{H}_2\text{O}$	99.9%	Si-25, La-10, Ca, Mg < 0.2
$\text{Th}(\text{NO}_3)_4 \cdot 4\text{H}_2\text{O}$	98%	La < 2000, Ti-100, Fe-20
$\text{TaF}_5$	98%	No analysis
$(\text{CH}_3)_4\text{NOH}$ (25 wt% in MeOH)		No analysis
$(\text{C}_4\text{H}_9)_4\text{NBr}$	99%	No analysis
$\text{Ti}(\text{i-OC}_3\text{H}_7)_4$	97%	No analysis
$\text{Zr}(\text{OC}_3\text{H}_7)_4$ (70 wt% in 1- $\text{C}_3\text{H}_7\text{OH}$ )		No analysis

TABLE 2.2. Chemicals used in modified sol gel catalyst preparation

Chemical	Formula	Manufacturer	Purity and State
Tetraisopropyl titanate	$\text{Ti}(\text{OC}_3\text{H}_7)_4$	Aldrich	97%, liquid
Tetraorthoethyl silicate	$\text{Si}(\text{OC}_2\text{H}_5)_4$	Aldrich	97%, liquid
Zirconium isopropoxide	$\text{Zr}(\text{OC}_3\text{H}_7)_4$	Aldrich	70% in $\text{C}_3\text{H}_7\text{OH}$
Aluminum <i>tri sec</i> butoxide	$\text{Al}(\text{C}_4\text{H}_9\text{O})_3$	Aldrich	97%, liquid
Zirconyl chloride	$\text{ZrOCl}_2 \cdot 8\text{H}_2\text{O}$	Aldrich	98%, solid
Sodium hydroxide	$\text{NaOH}$	Aldrich	97%, solid
Potassium hydroxide	$\text{KOH}$	Aldrich	87.1%, solid
Methanol	$\text{CH}_3\text{OH}$	Mallinckrodt	99.9%, liquid
Acetone	$\text{CH}_3\text{COCH}_3$	Mallinckrodt	99.8%, liquid
Hydrochloric acid	$\text{HCl}$	Baker	37.3%, liquid
Sulfuric acid	$\text{H}_2\text{SO}_4$	Baker	95.9%, liquid
Nitric acid	$\text{HNO}_3$	Mallinckrodt	70.3%, liquid
Ammonium hydroxide	$\text{NH}_4\text{OH}$	Baker	30%, liquid
Tetramethylammonium hydroxide	$(\text{CH}_3)_4\text{NOH}$	Aldrich	25% in $\text{MeOH}$
Rubidium hydroxide	$\text{RbOH}$	Aldrich	50% in $\text{H}_2\text{O}$
Lithium hydroxide	$\text{LiOH}$	Aldrich	98%, solid
Cesium hydroxide	$\text{CsOH}$	Aldrich	50% in $\text{H}_2\text{O}$
Barium hydroxide	$\text{Ba}(\text{OH})_2$	Aldrich	98%, solid
Calcium nitrate	$\text{Ca}(\text{NO}_3)_2 \cdot x\text{H}_2\text{O}$	Aldrich	83.5%, solid
Magnesium nitrate	$\text{Mg}(\text{NO}_3)_2 \cdot 6\text{H}_2\text{O}$	Aldrich	99%, solid

TABLE 3.1. Effect of calcination time on properties of zirconia

Calcination time (min)	N <sub>2</sub> BET surface area (m <sup>2</sup> /g)	Crystal phase <sup>a</sup>
5	87	C
30	80	C/M
180	61	M/C

<sup>a</sup> C: cubic, M: monoclinic, predominant phase listed first

TABLE 3.2. d spacings and relative intensities of peaks in zirconia XRD patterns

Monoclinic (#36-420) <sup>a</sup>		Tetragonal (#24-1164)		Cubic (#27-997)	
d (Å)	Intensity	d (Å)	Intensity	d (Å)	Intensity
3.694	18	2.995	100	2.93	100
3.636	12	2.635	10	2.55	25
3.163	100	2.574	13	1.801	50
2.839	64	1.8412	23	1.534	20
2.620	22	1.820	13		
2.605	12	1.5821	8		
2.540	14	1.5553	15		
2.2131	12				
1.8480	16				
1.8186	18				
1.8032	12				
1.6567	12				

<sup>a</sup> The number given is the catalog number in the Powder Diffraction File (37).



TABLE 3.3. Effect of calcination temperature on properties of zirconia

Calcination conditions		N <sub>2</sub> BET surface area (m <sup>2</sup> /g)	Crystal phase <sup>a</sup>	Bulk density (g/cm <sup>3</sup> )
T (K)	Time (hr)			
383	24	270	A	1.64
723	2½	89	C/M	2.14
1273	2½ <sup>b</sup>	0.36	M	3.57

<sup>a</sup> A: amorphous, C: cubic, M: monoclinic, predominant phase listed first

<sup>b</sup> 5 K/min heat-up from 348 K and 5 K/min cool-down to 348 K

TABLE 3.4. Changes in catalyst properties with preparation method

Method	Pore volume (cm <sup>3</sup> /g)	Pore diameter (Å)	Bulk density (g/cm <sup>3</sup> )
Precipitation	0.10	30-40	2.2
Hydrothermal	0.28	150-200	1.0
Calcining	0.20	30-40, 150-200	1.7

TABLE 3.5. Properties of isobutylene synthesis catalysts

Batch #	Precipitated catalysts <sup>a</sup>	N <sub>2</sub> BET Surface area <sup>b</sup> (m <sup>2</sup> /g)			Crystal phase <sup>c</sup>	Bulk density (g/cm <sup>3</sup> )
		B.R.	A.R.	R.C.		
1	ZrO <sub>2</sub>	55	42		M	1.65
2	ZrO <sub>2</sub>	52	35	40	M	1.88
3	1.6% Na, ZrO <sub>2</sub>	58	45	49	M/C	2.11
4	3.2% Ti, 2% Th, ZrO <sub>2</sub>	49	14	46	C/M	2.62
5	2% Mn, ZrO <sub>2</sub>	35	0.4		C	2.82
6	7% Ce, ZrO <sub>2</sub>	103	49		C	2.28
7	7% Ce, ZrO <sub>2</sub>	93	55		C	2.39
8	7% Ce, ZrO <sub>2</sub>	98	42	79	C	2.32
9	ZrO <sub>2</sub>	89	35	84	C/M	2.14
10	0.22% Li, ZrO <sub>2</sub>	98	41	87	C/M	2.18
11	0.34% Li, ZrO <sub>2</sub>	99	40	85	C/M	2.10
12	0.67% Li, ZrO <sub>2</sub>	101	36	83	C/M	2.13
13	0.79% Mg, ZrO <sub>2</sub>	86	29	79	C/M	2.18
14	1.16% Mg, ZrO <sub>2</sub>	98	45	86	C/M	2.18
15	1.72% Mg, ZrO <sub>2</sub>	85	46	79	C/M	2.19

<sup>a</sup> Catalyst composition is wt%

<sup>b</sup> B.R.-after calcination but before reaction, A.R.-after reaction, R.C.-recalcined

<sup>c</sup> C-cubic, T-tetragonal, M-monoclinic, A-amorphous, predominant phase listed first

TABLE 3.5. Continued

Batch #	Precipitated catalysts <sup>a</sup>	N <sub>2</sub> BET Surface area <sup>b</sup> (m <sup>2</sup> /g)			Crystal phase <sup>c</sup>	Bulk density (g/cm <sup>3</sup> )
		B.R.	A.R.	R.C.		
16	2.28% Mg, ZrO <sub>2</sub>	99	36	84	C/M	2.20
17	0.86% Al, ZrO <sub>2</sub>	115	38	100	C	2.00
18	2.50% Al, ZrO <sub>2</sub>	133	51	109	C	1.93
19	4.97% Dy, ZrO <sub>2</sub>	96	46	80	C	2.32
20	13.39% Dy, ZrO <sub>2</sub>	92	33	86	C	2.55
21	5.48% Ta, ZrO <sub>2</sub>	35	34		C/M	1.93
22	24.64% Ta, ZrO <sub>2</sub>	38	36		M/C	1.60
23	1.30% Y, 4.03% Ba, 2.80% Cu, ZrO <sub>2</sub>	85	79	84	C	2.32
24	1.30% Y, 4.03% Ba, 2.80% Cu, ZrO <sub>2</sub>	92	70	81	C	2.29
25	ZrO <sub>2</sub>	82	55	79	C/M	2.05
26	ZrO <sub>2</sub>	93	57	82	C/M	2.14
27	ZrO <sub>2</sub>	99	18	83	C/M	2.32
28	7% Ce, ZrO <sub>2</sub>	88	71	84	C	2.18
Hydrothermal catalysts <sup>a</sup>						
29	1.6% Na, 10.3% Ti, ZrO <sub>2</sub>	70	68	70	C	0.94

<sup>a</sup> Catalyst composition is wt%<sup>b</sup> B.R.-after calcination but before reaction, A.R.-after reaction, R.C.-recalcined<sup>c</sup> C-cubic, T-tetragonal, M-monoclinic, A-amorphous, predominant phase listed first

TABLE 3.5. Continued

Batch #	Hydrothermal catalysts <sup>a</sup>	N <sub>2</sub> BET Surface area <sup>b</sup> (m <sup>2</sup> /g)		Crystal phase <sup>c</sup>	Bulk density (g/cm <sup>3</sup> )
		B.R.	A.R.		
30	0.6% Na, 2% Ti, 2% Th, ZrO <sub>2</sub>	53	50	53	1.08
	Calcination of zirconyl nitrate				
31	ZrO <sub>2</sub>	39	36	39	1.71
	Commercial zirconia				
32	ZrO <sub>2</sub> (H-0304)	35			2.4
	Sol gel catalysts <sup>a</sup>				
33	2.2% Al, ZrO <sub>2</sub> (CSG)	13			0.71
34	ZrO <sub>2</sub> (MSG)	24			2.2
35	5.8% Si, ZrO <sub>2</sub> (MSG)	24			2.3
36	4.0% Al, ZrO <sub>2</sub> (MSG)	51			2.0
37	0.41% Li, ZrO <sub>2</sub> (MSG)	10			2.0
38	0.48% Na, ZrO <sub>2</sub> (MSG)	18			2.3
39	0.52% K, ZrO <sub>2</sub> (MSG)	32			2.3
40	0.44% Rb, ZrO <sub>2</sub> (MSG)	27			2.0
41	0.93% Cs, ZrO <sub>2</sub> (MSG)	22			2.4

<sup>a</sup> Catalyst composition is wt%

<sup>b</sup> B.R.-after calcination but before reaction, A.R.-after reaction, R.C.-recalcined

<sup>c</sup> C-cubic, T-tetragonal, M-monoclinic, A-amorphous, predominant phase listed first

TABLE 3.5. Continued

Batch #	Sol gel catalysts <sup>a</sup>	N <sub>2</sub> BET Surface area <sup>b</sup> (m <sup>2</sup> /g)		Crystal phase <sup>c</sup>	Bulk density (g/cm <sup>3</sup> )	
		B.R.	A.R.			R.C.
42	0.46% Mg, ZrO <sub>2</sub> (MSG)	25			T	2.4
43	0.53% Ca, ZrO <sub>2</sub> (MSG)	26			T	2.3
44	1.8% Ca, ZrO <sub>2</sub> (MSG)	34			T	2.3
45	0.54% Ba, ZrO <sub>2</sub> (MSG)	22			T	2.3
46	7.0% Si, ZrO <sub>2</sub> (MSG) (using NaOH)	99			T	1.5

<sup>a</sup> Catalyst composition is wt%

<sup>b</sup> B.R.-after calcination but before reaction, A.R.-after reaction, R.C.-recalcined

<sup>c</sup> C-cubic, T- tetragonal, M-monoclinic, A-amorphous, predominant phase listed first

TABLE 3.6. Ionic radii for 8 coordinated cations

Cation <sup>a</sup>	Ionic Radius (Å)	Cation	Ionic Radius (Å)
Li <sup>+</sup>	0.700	Ho <sup>+3</sup>	0.917
Na <sup>+</sup>	0.979	Lu <sup>+3</sup>	0.876
Ba <sup>+2</sup>	1.39	Nd <sup>+3</sup>	1.03
Ca <sup>+2</sup>	1.02	Sc <sup>+3</sup>	0.834
Cu <sup>+2</sup>	0.989	Sm <sup>+3</sup>	0.989
Mg <sup>+2</sup>	0.670	Y <sup>+3</sup>	0.956
Al <sup>+3</sup>	0.515	Yb <sup>+3</sup>	0.886
Dy <sup>+3</sup>	0.937	Zr <sup>+4</sup>	0.814
Gd <sup>+3</sup>	0.968	Ta <sup>+5</sup>	0.721

<sup>a</sup> Cations used in this study are indicated in outline type.

TABLE 3.7. Details of vacancies created by various dopants

Molar Ratio (M/100 Zr)	Vacancies/100 Zr <sup>a</sup>						Zr defects/100 Zr sites					
	Li	Mg	Al	Dy	Ta	YBaCu <sup>b</sup>	Li	Mg	Al	Dy	Ta	YBaCu
4	6	4	2	2	1	-	4	4	4	4	4	-
6	9	6	-	-	-	-	6	6	-	-	-	-
9	-	9	-	-	-	-	-	9	-	-	-	-
12	18	12	6	6	-	11	12	12	12	12	-	12
24	-	-	-	-	6	-	-	-	-	-	24	-

<sup>a</sup> Refers to oxygen vacancies in the cases of lower valence dopants and zirconium vacancies in the case of higher valence dopants.

<sup>b</sup> Molar ratio refers to total (Y+Ba+Cu)/Zr molar ratio.

TABLE 3.8. Typical coke deposition on catalysts under reaction conditions

Batch #	Precipitated catalysts	Time used <sup>a</sup> (hr)	$\frac{g_{\text{coke}}}{g_{\text{cat}}}$
2	ZrO <sub>2</sub>	264	0.0374
3	1.6% Na, ZrO <sub>2</sub>	1848	0.0378
8	7% Ce, ZrO <sub>2</sub>	308	0.0640
11	0.34% Li, ZrO <sub>2</sub>	26	0.0740
20	13.39% Dy, ZrO <sub>2</sub>	26	0.0395
Hydrothermal catalyst			
28	1.6% Na, 10.3% Ti, ZrO <sub>2</sub>	768	0.0415
Calcination catalyst			
31	ZrO <sub>2</sub>	36	0.0060

<sup>a</sup> Refers to time spent at reaction conditions.

TABLE 3.9. Comparison of hydrocarbon distribution for precipitated, calcination, and hydrothermal catalysts at 673 K, 50 atm, and 1/1 CO/H<sub>2</sub> ratio

Precipitated catalysts	Space time <sup>a</sup>		Hydrocarbon distribution (wt%)							
	(sec)	(%)	C <sub>1</sub>	C <sub>2</sub>	C <sub>3</sub>	C <sub>4</sub>	C <sub>5</sub> +	i-C <sub>4</sub> /ΣC <sub>4</sub>		
ZrO <sub>2</sub> <sup>b</sup>	45	12.8	10.2	2.6	2.0	21.2	64.0	70.7		
1.6% Na, ZrO <sub>2</sub>	30	11.6	6.6	3.0	1.5	18.4	70.5	76.7		
3.2% Ti, 2% Th, ZrO <sub>2</sub>	30	12.4	31.1	8.5	5.8	27.3	27.3	74.2		
7% Ce, ZrO <sub>2</sub>	30	13.1	27.8	9.6	8.0	30.7	23.9	63.2		
Calcination catalyst										
ZrO <sub>2</sub>	60	11.6	27.9	7.5	5.1	33.5	26.0	66.5		
Hydrothermal catalysts										
1.6% Na, 10.3% Ti, ZrO <sub>2</sub>	90	11.4	35.6	3.4	6.1	29.6	25.4	99.3		
0.6% Na, 2% Ti, 2% Th, ZrO <sub>2</sub>	90	11.7	27.5	2.8	2.4	14.9	52.4	100		

<sup>a</sup> Space time ( $\tau$ ) is defined as  $V_{bed}/v_0$  ( $v_0$  is inlet volumetric flow rate at reaction P and T).

<sup>b</sup> Reaction pressure is 95 atm in this case.



TABLE 3.10. Comparison of activity and selectivity of commercial, modified sol gel, and precipitated zirconias at 70 atm and 1/1 CO/H<sub>2</sub> ratio

Catalyst	ZrO <sub>2</sub> (H-0304)	ZrO <sub>2</sub> (MSG)	ZrO <sub>2</sub> (ppt.)
Temperature (K)	723	723	673
Space time (sec)	80	80	45
CO conversion (%)	11.8	17.0	13.2
Hydrocarbon distribution (wt%)			
C <sub>1</sub>	11.8	22.5	15.3
C <sub>2</sub>	3.60	3.71	2.9
C <sub>3</sub>	2.91	2.14	2.3
C <sub>4</sub>	9.01	15.63	25.3
C <sub>5</sub> +	72.68	56.02	54.2
C <sub>4</sub> distribution (wt%)			
isobutane	30.10	25.20	9.1
<i>n</i> -butane	6.14	2.48	2.0
1-butene	3.26	2.98	9.1
isobutylene	47.60	63.90	67.6
<i>trans</i> -2-butene	7.23	2.07	5.5
<i>cis</i> -2-butene	5.66	3.36	6.7

TABLE 3.11. A summary of time on stream experiments over Th-ZrO<sub>2</sub> (HT) at 723 K, 50 atm, 1/1 CO/H<sub>2</sub> ratio, and 40 second space time

Experiment	A	B	C	D
Time on stream, hr	4	20	55	88
CO conversion, %	18.1	17.8	18.7	19.5
CH <sub>4</sub> /iso-C <sub>4</sub> 's, wt/wt	0.827	0.804	0.872	1.36

TABLE 3.12. Comparison of activity and selectivity between iron and aluminum CO cylinders at 673 K, 50 atm, and 1/1 CO/H<sub>2</sub> ratio over 7% Ce-ZrO<sub>2</sub>

	Iron cylinder			Aluminum cylinder		
	60	90	120	60	90	120
Space time (sec)						
CO conversion (%)	20.0	26.7	30.6	23.1	29.2	34.0
Hydrocarbon distribution (wt%)						
C <sub>1</sub>	29.5	30.8	32.6	36.1	44.7	47.7
C <sub>2</sub>	8.3	7.5	6.6	9.4	8.8	8.5
C <sub>3</sub>	7.1	5.3	4.6	8.5	5.0	4.4
C <sub>4</sub>	29.0	29.4	28.8	19.8	19.5	20.1
C <sub>5</sub> +	26.2	27.0	27.4	26.4	22.0	19.3

TABLE 3.13. Comparison of activity and selectivity at 673 K, 50 atm, and 1/1 CO/H<sub>2</sub> [or CO/(H<sub>2</sub>+H<sub>2</sub>S)] ratio

	without H <sub>2</sub> S			with H <sub>2</sub> S			
	60 <sup>a</sup>	60	90	120	60	90	120
Space time (sec)							
	23.56	23.12	29.23	33.96	23.55	27.93	33.07
CO conv (%)							
Hydrocarbon distribution (wt%)							
C <sub>1</sub>	29.61	36.05	44.65	47.66	26.46	29.40	32.33
C <sub>2</sub> 's + C <sub>3</sub> 's	20.23	17.83	13.81	12.87	10.75	8.26	8.20
C <sub>4</sub> 's	28.84	19.75	19.54	20.14	22.71	24.51	26.91
C <sub>5</sub> + 's	21.23	26.37	22.00	19.33	39.09	37.83	32.57
Oxy/HC <sup>b</sup>	1.6	0.7	1.1	0.8	2.1	2.3	1.6
C <sub>4</sub> distribution (wt%)							
isobutane	10.12	12.30	21.90	29.00	13.97	22.60	30.98
n-butane	3.13	6.03	5.73	6.55	3.03	3.64	4.53
1-butene	8.36	7.75	6.81	6.45	7.26	6.72	6.23
isobutylene	52.11	49.52	43.55	37.29	53.20	46.10	38.70
trans-2-butene	15.82	14.38	13.00	12.26	13.41	12.41	11.57
cis-2-butene	10.47	10.03	9.01	8.44	9.15	8.54	7.99

<sup>a</sup> Run performed as an activity check on second batch of catalyst before feeding H<sub>2</sub>S.

<sup>b</sup> Oxygenate produced/hydrocarbon produced (g/100 g)

TABLE 3.14. Effect of hydrogen sulfide on C<sub>5</sub> selectivity at 673 K, 50 atm, and 1/1 CO/H<sub>2</sub> [or CO/(H<sub>2</sub>+H<sub>2</sub>S)] ratio

	without H <sub>2</sub> S	with H <sub>2</sub> S
Space time (sec)	60	60
CO conversion (%)	23.6	23.6
C <sub>5</sub> distribution (wt%)		
3-m <sup>a</sup> -1-C <sub>4</sub> <sup>=</sup>	4.0	73.0
2-m C <sub>4</sub> , 1-C <sub>5</sub> <sup>=</sup> , 2-m-1-C <sub>4</sub> <sup>=</sup>	32.5	8.5
<i>n</i> -C <sub>5</sub> , <i>trans</i> -2-C <sub>5</sub> <sup>=</sup> , <i>cis</i> -2-C <sub>5</sub> <sup>=</sup> , 2-m-2-C <sub>4</sub> <sup>=</sup>	63.5	18.5

<sup>a</sup> m=methyl

TABLE 3.15. Gibbs free energy of formation at 700 K for C<sub>5</sub> alkanes and alkenes

C <sub>5</sub> hydrocarbon	$\Delta G_f^\circ$ (kcal/mol)
3-methyl-1-butene	53.96
2-methyl butane	45.18
1-pentene	54.20
2-methyl-1-butene	51.55
<i>n</i> -pentane	46.19
<i>trans</i> -2-pentene	52.60
<i>cis</i> -2-pentene	52.71
2-methyl-2-butene	50.47

TABLE 3.16. Changes in activity and selectivity with temperature at 50 atm, 1/1 CO/(H<sub>2</sub>+H<sub>2</sub>S) ratio, and 90 second space time

T (K)	CO conv. (%)	Hydrocarbon distribution (wt%)					C <sub>4</sub> distribution (wt%)						
		C <sub>1</sub>	C <sub>2+3</sub> <sup>a</sup>	C <sub>4</sub>	C <sub>5</sub>	C <sub>6</sub> + O/HC <sup>b</sup>	i-C <sub>4</sub>	n-C <sub>4</sub>	1-C <sub>4</sub> <sup>c</sup>	i-C <sub>4</sub> <sup>c</sup>	t-2-C <sub>4</sub> <sup>c</sup>	c-2-C <sub>4</sub> <sup>c</sup>	
648	14.42	33.55	3.56	20.64	22.04	20.21	26.1	18.57	1.64	6.36	59.83	6.78	6.83
673	27.93	29.40	8.26	24.51	16.17	21.66	2.3	22.60	3.64	6.72	46.10	12.41	8.54
698	38.96	37.21	8.57	27.14	12.24	14.84	0.2	45.43	7.38	5.14	26.73	9.09	6.22
723	52.08	50.68	8.97	25.70	7.42	7.22	0.0	66.93	12.2	2.82	10.22	4.75	3.12
C <sub>5</sub> distribution (wt%)													
		3-m <sup>c</sup> -1-C <sub>4</sub> <sup>c</sup>	2-m C <sub>4</sub> , 1-C <sub>5</sub> <sup>c</sup> , 2-m-1-C <sub>4</sub> <sup>c</sup>	n-C <sub>5</sub> , t-2-C <sub>5</sub> <sup>c</sup> , c-2-C <sub>5</sub> <sup>c</sup> , 2-m-2-C <sub>4</sub> <sup>c</sup>									
648	14.42	93.95	0.55	5.49									
673	27.93	67.59	12.26	20.15									
698	38.96	50.55	30.30	19.15									
723	52.08	25.17	60.47	14.36									

<sup>a</sup> C<sub>2</sub> plus C<sub>3</sub> hydrocarbons

<sup>b</sup> Oxygenate produced/hydrocarbon produced (g/100 g)

<sup>c</sup> m = methyl

TABLE 3.17. Comparison of activity and selectivity at 673 K, 50 atm, and 1/1 CO/(H<sub>2</sub>+H<sub>2</sub>S) ratio over 7% Ce-ZrO<sub>2</sub> without and with presulfiding

	without presulfiding		with presulfiding
	60	90	90
Space time (sec)			
CO conversion (%)	23.55	27.93	21.22
<hr/>			
Hydrocarbon distribution (wt%)			
C <sub>1</sub>	26.46	29.40	31.52
C <sub>2</sub>	5.93	4.83	5.49
C <sub>3</sub>	5.82	3.43	3.18
C <sub>4</sub>	22.71	24.51	22.51
C <sub>5</sub>	20.46	16.17	23.98
C <sub>6</sub> +	18.63	21.66	13.31
<hr/>			
C <sub>4</sub> distribution (wt%)			
isobutane	13.97	22.60	11.14
<i>n</i> -butane	3.03	3.64	2.77
1-butene	7.26	6.72	5.55
isobutylene	53.20	46.10	65.75
<i>trans</i> -2-butene	13.41	12.41	8.02
<i>cis</i> -2-butene	9.15	8.54	6.77
<hr/>			
C <sub>5</sub> distribution (wt%)			
3-m-1-C <sub>4</sub> =	73.1	67.6	82.6
2-m C <sub>4</sub> , 1-C <sub>5</sub> =, 2-m-1-C <sub>4</sub> =	8.5	12.3	4.8
<i>n</i> -C <sub>5</sub> , <i>trans</i> -2-C <sub>5</sub> =, <i>cis</i> -2-C <sub>5</sub> =, 2-m-2-C <sub>4</sub> =	18.4	20.1	12.6
Oxygenate/HC (g/100 g)	2.1	2.3	1.9

TABLE 3.18. Comparison of activity and selectivity for vacancy theory isosynthesis at 673 K, 50 atm, 1/1 CO/H<sub>2</sub> [for CO/(H<sub>2</sub> + H<sub>2</sub>S)] ratio, and 90 second space time

Run	CO conv. (%)	Hydrocarbon distribution (wt%)						C <sub>4</sub> distribution (wt%)					
		C <sub>1</sub>	C <sub>2</sub>	C <sub>3</sub>	C <sub>4</sub>	C <sub>5</sub> +	O/HC <sup>a</sup>	i-C <sub>4</sub>	n-C <sub>4</sub>	1-C <sub>4</sub> <sup>b</sup>	i-C <sub>4</sub> <sup>c</sup>	t-2-C <sub>4</sub> <sup>d</sup>	c-2-C <sub>4</sub> <sup>e</sup>
PurZ	23.59	32.71	7.65	5.07	23.80	30.77	1.4	19.02	4.08	6.78	49.29	12.31	8.52
LiZ04	25.63	34.09	8.12	5.06	25.36	27.38	1.5	17.99	3.49	6.74	51.63	11.96	8.19
LiZ06	23.47	33.96	8.16	5.09	24.05	28.75	1.5	18.72	3.67	6.30	51.43	11.85	8.03
LiZ12	23.71	33.89	8.23	5.01	24.70	28.17	1.4	17.99	3.84	6.52	51.77	11.75	8.13
MgZ04	22.25	36.13	8.42	5.20	23.64	26.62	1.4	19.96	4.14	6.85	48.37	12.37	8.31
MgZ06	25.55	34.65	8.27	4.99	26.25	25.83	1.4	24.71	2.79	5.97	47.56	11.26	7.71
MgZ09	29.13	31.95	7.95	4.96	29.11	26.02	1.9	18.60	4.52	6.47	51.25	11.33	7.83
MgZ12	25.96	34.21	7.94	5.04	25.49	27.32	1.6	18.05	2.88	6.72	52.82	11.74	7.79
AlZ04	22.89	35.79	8.45	5.50	25.10	25.16	2.2	23.77	3.03	6.52	45.92	12.46	8.31
AlZ12	21.16	38.58	9.17	5.76	24.66	21.84	2.3	17.42	3.73	7.06	49.89	13.15	8.76
DyZ04	24.10	34.50	8.44	6.18	27.53	23.35	2.6	17.52	5.20	7.60	46.77	13.73	9.19
DyZ12	22.44	31.60	8.31	4.99	27.66	27.44	5.5	13.12	5.27	8.01	50.09	13.99	9.50

<sup>a</sup> Oxygenate produced/hydrocarbon produced (g/100 g)

TABLE 3.18. Continued

Run	CO conv. (%)	Hydrocarbon distribution (wt%)					C <sub>4</sub> distribution (wt%)						
		C <sub>1</sub>	C <sub>2</sub>	C <sub>3</sub>	C <sub>4</sub>	C <sub>5</sub> +	O/HC <sup>a</sup>	i-C <sub>4</sub>	n-C <sub>4</sub>	1-C <sub>4</sub> <sup>≡</sup>	i-C <sub>4</sub> <sup>≡</sup>	t-2-C <sub>4</sub> <sup>≡</sup>	c-2-C <sub>4</sub> <sup>≡</sup>
TaZ04	4.55	40.53	16.70	10.89	11.62	20.26	0.0	9.40	0.00	13.78	27.87	29.27	19.68
TaZ24	1.10	46.79	29.37	13.79	3.62	6.43	0.0	24.28	0.00	9.71	18.82	33.52	13.67
YBCZ	33.64	51.77	5.53	3.38	17.78	21.53	0.6	31.52	4.65	6.64	36.04	12.93	8.22
YBCZS	44.85	73.54	3.21	2.36	9.52	11.37	0.0	54.92	4.24	2.55	30.97	4.23	3.09

<sup>a</sup> Oxygenate produced/hydrocarbon produced (g/100 g)



TABLE 3.19. Effect of temperature cycles and H<sub>2</sub>S on activity and selectivity over 7% Ce-ZrO<sub>2</sub> at 673 K, 50 atm, and 1/1 CO/H<sub>2</sub> [or CO/(H<sub>2</sub>+H<sub>2</sub>S)] ratio

	Fresh		Cycled	Reheat	Reheat w/H <sub>2</sub> S
	60	90			
Space time (sec)	60	90	90	60	60
CO conversion (%)	19.98	26.52	24.77	16.24	15.20
Hydrocarbon distribution (wt%)					
C <sub>1</sub>	29.46	30.83	57.96	46.45	24.42
C <sub>2</sub> 's	8.29	7.48	8.04	15.24	6.43
C <sub>3</sub> 's	7.05	5.29	4.09	11.41	6.96
C <sub>4</sub> 's	29.00	29.38	18.40	12.54	17.35
C <sub>5</sub> +s	26.21	27.02	11.51	14.35	44.83
Oxy/HC	1.6	1.6	2.0	0.2	0.5
C <sub>4</sub> distribution (wt%)					
isobutane	13.28	23.35	35.05	11.41	13.24
<i>n</i> -butane	4.66	5.28	7.61	14.94	2.48
1-butene	7.31	6.77	5.33	9.31	8.54
isobutylene	51.66	42.89	35.71	33.24	48.70
<i>trans</i> -2-butene	13.62	12.83	9.40	18.51	16.15
<i>cis</i> -2-butene	9.48	8.88	6.90	12.60	10.90

TABLE 3.20. Variation of CO conversion with time on stream at 673 K, 60 atm, 1050/hr, and 2/1 CO/H<sub>2</sub> over ZrO<sub>2</sub> (ppt.)

Time on stream (hr)	2	11	14	17
CO conversion (%)	12.4	13.2	13.3	13.5

TABLE 3.21. Comparison of fixed bed and slurry reactors at 673 K and 1/1 CO/H<sub>2</sub> over ZrO<sub>2</sub> (ppt.)

	CO conversion (%)	wt% C <sub>1</sub>	wt% C <sub>2</sub>	wt% C <sub>3</sub>	wt% C <sub>4</sub>	wt% C <sub>5+</sub>
Slurry (60 atm, 1050/hr)	13.0	13.6	15.4	16.5	38.8	15.7
Fixed bed (50 atm, 900/hr)	25.0	31.8	7.9	5.4	28.0	26.8

TABLE 3.22. Comparison of C<sub>4</sub> distribution in slurry and fixed bed reactors at 673 K and 1/1 CO/H<sub>2</sub> over ZrO<sub>2</sub> (ppt.)

weight %	isobutane	n-butane	1-butene	isobutylene	trans-2-butene	cis-2-butene
Slurry (60 atm, 1050/hr)	5.3	6.3	10.2	57.1	12.3	8.9
Fixed bed (50 atm, 900/hr)	14.5	3.4	6.1	58.7	10.2	7.1

TABLE 3.23. Comparison of hydrocarbon distribution at different CO/H<sub>2</sub> ratios in the slurry reactor at 679 K, 60 atm, and 400/hr over commercial zirconia

	CO conversion (%)	wt% C <sub>1</sub>	wt% C <sub>2</sub>	wt% C <sub>3</sub>	wt% C <sub>4</sub>	wt% C <sub>5</sub> +
2/1 CO/H <sub>2</sub>	10.0	28.9	11.8	16.3	22.4	20.6
3/2 CO/H <sub>2</sub>	11.0	30.2	12.1	19.1	22.5	16.1
1/1 CO/H <sub>2</sub>	11.0	31.8	11.6	28.5	14.0	14.0

TABLE 3.24. Comparison of C<sub>4</sub> distribution at different CO/H<sub>2</sub> ratios in the slurry reactor at 679 K, 60 atm, and 400/hr over commercial zirconia

weight %	isobutane	n-butane	1-butene	isobutylene	trans-2-butene	cis-2-butene
2/1 CO/H <sub>2</sub>	7.2	5.6	11.4	59.8	9.0	7.1
3/2 CO/H <sub>2</sub>	7.8	4.9	11.0	57.7	10.3	8.9
1/1 CO/H <sub>2</sub>	6.7	5.1	13.6	62.8	11.0	8.0

TABLE 3.25. Product distributions for the slurry reactor at 673 K, 60 atm, and 1050/hr over ZrO<sub>2</sub> (ppt.)

	CO conversion (%)	wt% C <sub>1</sub>	wt% C <sub>2</sub>	wt% C <sub>3</sub>	wt% C <sub>4</sub>	wt% C <sub>5</sub> +
2/1 CO/H <sub>2</sub>	13.3	25.7	19.7	12.0	30.1	12.4
1/1 CO/H <sub>2</sub>	13.0	13.6	15.4	16.5	38.8	15.7

TABLE 3.26. Rate constants and CO<sub>2</sub> adsorption equilibrium constants obtained from SimuSolv<sup>®</sup> at 673 K, 50 atm, and 1/1 CO/H<sub>2</sub> ratio

Catalyst	$k_p \times 10^6$ $\left( \frac{\text{mol}}{\text{kg}_{\text{cat}} \text{ atm}^{1.5} \text{ sec}} \right)$	$K_{\text{CO}_2}$ (atm <sup>-1</sup> )	$\rho_b k_p \times 10^6$ $\left( \frac{\text{mmol}}{\text{cm}^3 \text{ atm}^{1.5} \text{ sec}} \right)$	Rank	
				Model	Exp.
7% Ce-ZrO <sub>2</sub> (ppt., Al CO cyl.)	11.52	0.504	26.23	1	1
7% Ce-ZrO <sub>2</sub> (ppt., H <sub>2</sub> S, Al CO cyl.)	10.97	0.503	25.45	2	2
1.6% Na-ZrO <sub>2</sub> (ppt.)	11.55	1.001	24.37	3	5
7% Ce-ZrO <sub>2</sub> (ppt., Iron CO cyl.) <sup>a</sup>	10.52 ± 0.79	0.596 ± 0.039	23.99	4	3
3.2% Ti, 2% Th -ZrO <sub>2</sub> (ppt.)	8.79	0.641	23.06	5	4
ZrO <sub>2</sub> (ppt.)	6.90	0.330	14.77	6	6
ZrO <sub>2</sub> (CAL.)	5.79	0.643	9.90	7	7
1.6% Na, 10.3% Ti -ZrO <sub>2</sub> (HT)	8.18	0.736	7.65	8	8
0.6% Na, 2% Ti, 2% Th -ZrO <sub>2</sub> (HT)	6.83	0.642	7.36	9	9

<sup>a</sup> Errors given in this case are representative of those obtained for other simulations.

TABLE 3.27. Rate constants and CO<sub>2</sub> adsorption equilibrium constants for other reaction conditions obtained from SimuSolv®

Catalyst	T(K)	P (atm)	CO/H <sub>2</sub> or [CO/(H <sub>2</sub> +H <sub>2</sub> S)]	$k_p \times 10^6$ $\left( \frac{\text{mol}}{\text{kg}_{\text{cat}} \text{ atm}^{1.5} \text{ sec}} \right)$	$K_{\text{CO}_2}$ (atm <sup>-1</sup> )
7% Ce-ZrO <sub>2</sub> (ppt., H <sub>2</sub> S, Al CO cyl.)	648	50	1/1	4.73	0.804
	698	50	1/1	14.85	0.350
	723	50	1/1	20.55	0.255
1.6% Na-ZrO <sub>2</sub> (ppt.)	673	95	2/1	11.55	0.601
	698	50	1/1	14.27	0.430
7% Ce-ZrO <sub>2</sub> (ppt., Iron CO cyl.)	723	50	1/1	15.38	0.235
	673	95	2/1	6.12	0.202
ZrO <sub>2</sub> (ppt.)	673	95	1/1	6.12	0.306
	673	95	1/3	6.12	0.459
	648	50	1/1	4.55	1.001
1.6% Na, 10.3% Ti-ZrO <sub>2</sub> (HT)	698	50	1/1	12.11	0.508
	723	70	1/1	5.88	0.331
ZrO <sub>2</sub> (MSG)					

TABLE 3.28. Activation energies and CO<sub>2</sub> heats of adsorption found using SimuSolv<sup>®</sup> rate parameters

Catalyst	$E_a$ (kcal/mol) <sup>a</sup>	$\Delta H_{ads}$ CO <sub>2</sub> (kcal/mol)
7% Ce-ZrO <sub>2</sub> (ppt.) [H <sub>2</sub> S, Al CO cyl.]	12.14 ± 0.50	14.22 ± 0.58
7% Ce-ZrO <sub>2</sub> (ppt.) [Iron CO cyl.]	7.39 ± 2.42	17.91 ± 3.48
1.6% Na, 10.3% Ti, ZrO <sub>2</sub> (HT)	17.64 ± 1.65	12.15 ± 0.92

<sup>a</sup> To convert to kJ/mol multiply by 4.184

TABLE 3.29. Gamma values at 673 K, 50 atm, and 1/1 CO/H<sub>2</sub> ratio

<i>i</i>	7% Ce, ZrO <sub>2</sub> (ppt.)		1.6% Na, ZrO <sub>2</sub> (ppt.)		3.2% Ti, 2% Th, ZrO <sub>2</sub> (ppt.)	
	$\gamma_i \times 10^3$	$\gamma_d \times 10^3$	$\gamma_i \times 10^3$	$\gamma_d \times 10^3$	$\gamma_i \times 10^3$	$\gamma_d \times 10^3$
1	137.1 ± 1.4	274.2 ± 2.8	38.30 ± 0.87	76.60 ± 1.7	198.3 ± 3.4	396.6 ± 6.8
2	17.86 ± 1.0	71.44 ± 4.0	8.87 ± 0.25	35.48 ± 1.0	17.99 ± 1.0	71.96 ± 4.0
3	9.33 ± 0.72	55.98 ± 4.3	2.96 ± 0.06	17.76 ± 0.36	8.00 ± 0.46	48.00 ± 2.8
4	39.14 ± 0.38	313.1 ± 3.0	31.27 ± 0.59	250.2 ± 4.7	36.98 ± 1.3	296 ± 10
5+	28.54 ± 0.44	285.4 ± 4.4	62.00 ± 0.58	620.0 ± 5.8	18.77 ± 2.9	188 ± 29

TABLE 3.30. Parameters in the semi-empirical kinetic model

Catalyst	$\alpha$	$\kappa$
ZrO <sub>2</sub> (H-0304)	0.333±0.043	3.80±0.08
ZrO <sub>2</sub> (MSG)	0.508±0.060	2.26±0.34
Li-ZrO <sub>2</sub> (MSG)	0.232	1.76
K-ZrO <sub>2</sub> (MSG)	0.464	3.98
Mg-ZrO <sub>2</sub> (MSG)	0.408	4.49
Ca-ZrO <sub>2</sub> (MSG)	0.480	5.17

TABLE 3.31. Kinetic parameters for the two catalysts used in slurry modeling

	Precipitated catalyst	Commercial catalyst
$k_p, \times 10^6$ mol/(kg <sub>cat</sub> atm <sup>1.5</sup> s)	6.12	6.397
$K_{CO_2}, atm^{-1}$	0.306	1.694

TABLE 3.32. Phase equilibrium constants used in the slurry modeling

	CH <sub>4</sub>	C <sub>2</sub> H <sub>4</sub>	C <sub>3</sub> H <sub>6</sub>	C <sub>4</sub> H <sub>8</sub>	C <sub>5</sub> H <sub>10</sub>
$K_i$ values	4.0	3.0	2.2	1.5	1.15

TABLE 3.33. Slurry modeling results for the precipitated catalyst at 673 K, 60 atm, 1/1 CO/H<sub>2</sub> ratio, GHSV 1050 1/hr, liquid mass rate 0.08 g/sec, and  $W_{cat}=20$  g

	CH <sub>4</sub>	C <sub>2</sub> H <sub>4</sub>	C <sub>3</sub> H <sub>6</sub>	C <sub>4</sub> H <sub>8</sub>	C <sub>5</sub> H <sub>10</sub>
$\gamma_i$ used in the modeling	0.06167	0.03828	0.02743	0.05115	0.01497
weight percentage, %	13.86	15.05	16.17	40.20	14.71

TABLE 3.34. Slurry modeling results for the commercial catalyst at 679 K, 60 atm, 1/1 CO/H<sub>2</sub> ratio, GHSV 419 1/hr, liquid mass rate 0.04 g/sec, and W<sub>cat</sub>=15.9 g

	CH <sub>4</sub>	C <sub>2</sub> H <sub>4</sub>	C <sub>3</sub> H <sub>6</sub>	C <sub>4</sub> H <sub>8</sub>	C <sub>5</sub> H <sub>10</sub>
$\gamma_i$ used in the modeling	0.1462	0.03095	0.04838	0.01852	0.01452
weight percentage, %	32.10	11.88	27.86	14.22	13.94

TABLE 3.35. Predicted synthesis conversions for precipitated and commercial catalyst

H <sub>2</sub> /CO	Conversion, %			
	Precipitated catalyst		Commercial catalyst	
	CO	H <sub>2</sub>	CO	H <sub>2</sub>
1.0	12.30	6.91	13.53	8.74
1.5			12.11	11.74
2.0	10.41	11.69	11.16	14.43