

APPENDIX I-A  
PROGRAM LISTINGS

I-A-1

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SIMULATOR SOURCE CODE (SIM.FOR)

C -----  
C SIMULATOR FOR PREHEATER AND REACTOR/REACTORS  
C FOR A COAL LIQUEFACTION PLANT  
C -----

C List of variables defined in program:  
C -----

C AG - Concentration of hydrogen in gas phase [-]  
C AGPI - Inlet concentration of hydrogen in the gas [-]  
C AL - Concentration of hydrogen in liquid phase [-]  
C ALPI - Inlet concentration of hydrogen in the liquid [-]  
C BO - Bond number  
C CGI - Inlet hydrogen concentration in the gas phase [gmole/cc]  
C CPG - Specific heat of gas [cal/gm.deg C]  
C CPBAR - Weighted average specific heat of liquid [cal/gm.deg C]  
C CPI - Initial concentration of each species [gm/gm]  
C D - Diameter of preheater/reactors [cm]  
C DHR - Heat of Reaction [cal/gm]  
C DHS - Heat of Dissolution [cal/gm]  
C DHSTAR - Dimensionless Heat of Dissolution [-]  
C DI - Diffusivity of gas [sq.cm/sec]  
C E - Activation energy for Hydrogen consumption kinetics [cal/gmole]  
C ECP - Activation energy for reactions in preheater [cal/gmole]  
C ECR - Activation energy for reactions in reactor [cal/gmole]  
C ESTAR - Dimensionless activation energy [-]  
C FR - Froude number  
C FRAC - Mole fraction of Hydrogen in inlet gas to preheater [-]  
C FGAS - Mass flow rate of gas [kg/hr]  
C FSLUR - Mass flow rate of slurry [kg/hr]  
C G - Acceleration due to gravity [cm/sec/sec]  
C H - Henry's law constant [gm/cc(liq)/gm/cc(gas)]  
C HBAR - Preexponential factor  
C HIL - Solubility of hydrogen at inlet conditions  
C KBARP - Arrhenius factor for rate constant in preheater [1/sec]  
C KBARR - Arrhenius factor for rate constant in reactor [1/sec]  
C L - Length of preheater/reactors [cm]  
C NAME - Name of Species  
C NKP - Number of non-zero rate constants for preheater  
C NKR - Number of non-zero rate constants for reactor  
C NSPH - Number of species for preheater  
C NSPR - Number of species for reactor  
C P - Operating pressure [atm]

C PEH - Peclet number for heat  
 C PEL - Peclet number for mass  
 C R - Gas constant, cal/gmole.deg K  
 C RR - Gas constant, cc.atm/gmole.deg K  
 C SC - Schimdt number  
 C RL - Dimensionless parameter  
 C RP - Dimensionless parameter  
 C TIL - Temperature at inlet to preheater [deg C]  
 C TEMP - Dimensionless temperature [-]  
 C TEMPI - Inlet temperature [deg C]  
 C TEMW - Dimensionless furnace temperature [-]  
 C TH - Temperature of furnace [deg C]  
 C TIME - Residence time of slurry in preheater/reactors [sec]  
 C VG - Superficial Gas Velocity in preheater/reactors [cm/sec]  
 C VL - Superficial Liquid Velocity in preheater/reactors [cm/sec]  
 C VOLG - Volumetric flow rate of gas to preheater [cc/sec]  
 C VOLL - Volumetric flow rate of slurry to preheater [cc/sec]  
 C X - Dimensionless axial distance [-]  
 C Z - Axial distance [cm]  
 C ZKLA - Mass transfer coefficient [1/sec]  
 C ZKBAR - Preexponential factor [1/sec]  
 C ZNO - Galileo Number

Greek Symbols:

-----

C EG - Gas holdup in preheater/reactors [-]  
 C ALFA - Dimensionless parameter  
 C BETA - Dimensionless parameter  
 C GAMR - Dimensionless parameter for preheater/reactors  
 C GAMS - Dimensionless parameter for preheater/reactors  
 C ZMEW - Viscosity [poise]  
 C RHOG - Density of gas [gm/cc]  
 C RHOA - Weighted average density of slurry [gm/cc]  
 C SIG - Surface Tension of slurry [dyne/cm]

IMPLICIT REAL \*8(A-H,O-Z)  
 COMMON /B/ TIL,HIL,CGI,AGPI,ALPI,TEMPI,TEMW  
 COMMON /AN/N

OPEN (UNIT=1,FILE='SIM1.DAT')  
 OPEN (UNIT=11,FILE='SIM2.DAT')  
 OPEN (UNIT=3,FILE='SUMRY.DAT')  
 OPEN (UNIT=21,FILE='RHYGAS.DAT')  
 OPEN (UNIT=31,FILE='RHYLIQ.DAT')

```

OPEN (UNIT=41,FILE='RTEMP.DAT')
OPEN (UNIT=23,FILE='RCONC.DAT')

CALL INPUT
CALL INPUT1(TIL)

IDUM=1

CALL PHEATR
CALL CHEM1
CALL OUTPUT(IDUM,1)

IDUM=2

DO 10 I=2,N
NR=I
CALL REATEM(NR)
CALL CHEM2(NR)
CALL OUTPUT(IDUM,NR)
10  CONTINUE

IDUM=3

DO 20 I=1,N
NR=I
CALL COST(NR)
CALL OUTPUT(IDUM,NR)
20  CONTINUE

CLOSE (UNIT=23)
CLOSE (UNIT=41)
CLOSE (UNIT=31)
CLOSE (UNIT=21)
CLOSE (UNIT=3)
CLOSE (UNIT=11)
CLOSE (UNIT=1)

WRITE(6,100)
100  FORMAT(70('-'),/,
* 25X,'SIMULATION COMPLETE',/,
* 70('-'),/,
* 10X,'OUTPUT IS CONTAINED IN THE FOLLOWING FILES',/,
* 10X,'Output Summary',T50,'SUMRY.DAT',/,
* 10X,'Hydrodynamic Parameters',T50,'HYDRO.DAT',/,
* 10X,'Preheater:',/,
* 15X,'Temperature Profile',T50,'PTEMP.DAT',/,
* 15X,'Hydrogen Profile (Gas Phase)',T50,'PHYGAS.DAT',/,
* 15X,'Hydrogen Profile (Liquid Phase)',T50,'PHYLIQ.DAT',/,

```

```

* 15X,'Viscosity Profile',T50,'PVISCO.DAT',/,
* 15X,'Species Concentration Profile',T50,'PCONC.DAT',/,
* 10X,'Reactor/Reactors :',/,
* 15X,'Temperature Profile',T50,'RTEMP.DAT',/,
* 15X,'Hydrogen Profile (Gas Phase)',T50,'RHYGAS.DAT',/,
* 15X,'Hydrogen Profile (Liquid Phase)',T50,'RHYLIQ.DAT',/,
* 15X,'Species Concentration Profile',T50,'RCONC.DAT',/,
* 70(' -'))
STOP
END

```

# SUBROUTINE PHEATR

```

C      THIS SUBROUTINE CALCULATES THE HYDROGEN CONCENTRATION IN THE
C      GAS AND LIQUID PHASES AND TEMPERATURE DISTRIBUTION WITHIN THE
C      PREHEATER. THIS IS DONE BY SOLVING THE FIRST ORDER DIFFERENTIAL
C      EQUATIONS WHICH DESCRIBE THE HEAT AND MASS BALANCES FOR THE
C      PREHEATER.

```

```

IMPLICIT REAL *8(A-H,O-Z)
INTEGER RUNGE
DOUBLE PRECISION L

```

```

DIMENSION VG(5),VL(5),L(5),D(5)
DIMENSION GAMMA(5),GAMS(5),GAMR(5),
* FLUX(5),HT(5),ALFA(5)
DIMENSION RL(5),RP(5),PEL(5),PEH(5)
DIMENSION AG(5),AL(5),TEMP(5)
DIMENSION Y(3),F(3)
DIMENSION PAG(101),PAL(101),PTEMP(101)

COMMON /A/ VG,VL,L,D
COMMON /B/ TIL,HIL,CGI,AGPI,ALPI,TEMPI,TEMW
COMMON/DD/ HBAR
COMMON /DDD/ DHSTAR,ESTAR,GAMMA,GAMS,GAMR,RL,RP
* ,FLUX,HT,ALFA
COMMON /FF/ AG,AL,TEMP
COMMON/Z9/ PEL,PEH
COMMON/Z15/ TEMPA,AGPA,ALPA,TEMPO,AGPO,ALPO
COMMON/QT/ QT

```

```

OPEN (UNIT=10,FILE='PVISCO.DAT')
OPEN (UNIT=20,FILE='PHYGAS.DAT')

```

```

OPEN (UNIT=30,FILE='PHYLIQ.DAT')
OPEN (UNIT=40,FILE='PTMP.DAT')

WRITE(6,300)
300  FORMAT(10X,'SIMULATING PREHEATER',/)
WRITE(10,496)
496  FORMAT(T21,'VISCOSITY PROFILE IN PREHEATER',/,
* 70('-'),/,
* T7,'DISTANCE ALONG PREHEATER',18X,'VISCOSITY',/,
* T5,'DIMENSIONLESS',4X,'CENTIMETERS',18X,'POISE',/,
* 70('-'),/)
WRITE(20,497)
497  FORMAT(T21,'HYDROGEN PROFILE IN PREHEATER',/,
* T30,'(GAS PHASE)',/,
* 70('-'),/,
* T7,'DISTANCE ALONG PREHEATER',12X,'HYDROGEN CONCENTRATION',/,
* T5,'DIMENSIONLESS',4X,'CENTIMETERS',8X,'DIMENSIONLESS',
* 4X,'GM/CM**3',/,
* 70('-'),/)

WRITE(30,498)
498  FORMAT(T21,'HYDROGEN PROFILE IN PREHEATER',/,
* T28,'(LIQUID PHASE)',/,
* 70('-'),/,
* T7,'DISTANCE ALONG PREHEATER',12X,'HYDROGEN CONCENTRATION',/,
* T5,'DIMENSIONLESS',4X,'CENTIMETERS',8X,'DIMENSIONLESS',
* 4X,'GM/CM**3',/,
* 70('-'),/)

WRITE(40,499)
499  FORMAT(T20,'TEMPERATURE PROFILE IN PREHEATER',/,/,
* 70('-'),/,
* T7,'DISTANCE ALONG PREHEATER',18X,'TEMPERATURE',/,
* T5,'DIMENSIONLESS',4X,'CENTIMETERS',8X,'DIMENSIONLESS',
* 4X,'DEGREES C',/,
* 70('-'),/)

X=0.0
QT=0.0
Y(1)=AGPI
Y(2)=ALPI
Y(3)=TEMPI

TEMPA=TIL*(1.0+TEMPI)
AGPA=CGI*AGPI
ALPA=CGI*HIL*ALPI
ICOUNT=1
PAG(ICOUNT)=Y(1)

```



```

PAL(ICOUNT)=Y(2)
PTMP(ICOUNT)=Y(3)
ZMEW=VISCOS(TEMP)
ZX=X*L(1)
ZPAG=PAG(ICOUNT)*CGI
ZPAL=PAL(ICOUNT)*CGI*HIL
ZPTMP=PTMP(ICOUNT)*TIL+TIL-273.0
WRITE(10,502) X,ZX,ZMEW
WRITE(20,500) X,ZX,PAG(ICOUNT),ZPAG
WRITE(30,500) X,ZX,PAL(ICOUNT),ZPAL
WRITE(40,500) X,ZX,PTMP(ICOUNT),ZPTMP
500  FORMAT(8X,F5.2,8X,F8.1,12X,F8.4,6X,E11.4)
502  FORMAT(8X,F5.2,8X,F8.1,18X,E11.4)
HH=0.01

10  K=RUNGE(3,Y,F,X,HH)
    IF(K.NE.1) GO TO 15
    H=HBAR*EXP(-DHSTAR/(1+Y(3)))
    TEMPP=Y(3)
    ZMEW=VISCOS(TEMPP)
    F(1)=-RL(1)*(H*Y(1)/HIL-Y(2))
    F(2)=-F(1)/(GAMMA(1)*HIL)-RP(1)*(EXP(-ESTAR/(1.0+Y(3))))*Y(2)
    * /GAMMA(1)
    F(3)=ALFA(1)*ZMEW**(-0.47)*
    * (TEMW-Y(3))+HIL*RP(1)*GAMR(1)*EXP(-ESTAR/(1+Y(3)))*Y(2)
    * +RL(1)*GAMS(1)*(H*Y(1)/HIL-Y(2))
    Q=ALFA(1)*ZMEW**(-0.47)*(TEMW-Y(3))*HH
    QT=QT+Q
    GO TO 10
15  CONTINUE
    ICOUNT=ICOUNT+1
    PAG(ICOUNT)=Y(1)
    PAL(ICOUNT)=Y(2)
    PTMP(ICOUNT)=Y(3)
    ZX=X*L(1)
    ZPAG=PAG(ICOUNT)*CGI
    ZPAL=PAL(ICOUNT)*CGI*HIL
    ZPTMP=PTMP(ICOUNT)*TIL+TIL-273.0
    WRITE(10,502) X,ZX,ZMEW
    WRITE(20,500) X,ZX,PAG(ICOUNT),ZPAG
    WRITE(30,500) X,ZX,PAL(ICOUNT),ZPAL
    WRITE(40,500) X,ZX,PTMP(ICOUNT),ZPTMP
    IF(X.GE.1.0) GO TO 16
    GO TO 10
16  CONTINUE
    AG(1)=Y(1)
    AL(1)=Y(2)
    TEMP(1)=Y(3)

```

```

WRITE(10,501)
WRITE(20,501)
WRITE(30,501)
WRITE(40,501)
501  FORMAT(/,70('-'))
TEMPO=TIL*(1.0+Y(3))
AGPO=CGI*Y(1)
ALPO=CGI*HIL*Y(2)
CLOSE (UNIT=10)
CLOSE (UNIT=20)
CLOSE (UNIT=30)
CLOSE (UNIT=40)
RETURN
END

```

#### FUNCTION REACTR(ALR)

```

C      THIS FUNCTION SUBPROGRAM CALCULATES THE HYDROGEN CONCENTRATION
C      IN THE GAS AND LIQUID PHASES AND THE TEMPERATURE DISTRIBUTION WITHIN
C      THE REACTOR. THIS IS DONE BY SOLVING A SERIES OF COUPLED FIRST ORDER
C      DIFFERENTIAL EQUATIONS WHICH DESCRIBE THE HEAT AND MASS BALANCES FOR
C      THE REACTOR.

```

```

IMPLICIT REAL *8(A-H,O-Z)
INTEGER RUNGE

```

```

DIMENSION Y(5),F(5)
DIMENSION XX(101),RAG(101),RAL(101),RTEMP(101)
DIMENSION GAMMA(5),GAMS(5),GAMR(5),
* FLUX(5),HT(5),ALFA(5)
DIMENSION RL(5),RP(5),PEL(5),PEH(5)
DIMENSION AG(5),AL(5),TEMP(5)

COMMON /B/ TIL,HIL,CGI,AGPI,ALPI,TEMPI,TEMW
COMMON /DUM/ XX,RAG,RAL,RTEMP
COMMON /NUM/ ICOUNT
COMMON/DD/ HBAR
COMMON /DDD/ DHSTAR,ESTAR,GAMMA,GAMS,GAMR,RL,RP
* ,FLUX,HT,ALFA
COMMON /FF/ AG,AL,TEMP
COMMON /REACT/ AGRI,ALRI,DALRI,TEMPRI,DTEMPI
COMMON /REACT1/ DTEMP,DALR
COMMON /REACT2/ MM,J
COMMON/Z9/PEL,PEH

```

```

ICOUNT=1
X=0.0
ALRI=ALR
DALRI=(ALR-AL(J))*PEL(MM)
Y(1)=AGRI
Y(2)=ALR
Y(3)=DALRI
Y(4)=TEMPRI
Y(5)=DTEMPI
XX(ICOUNT)=X
RAG(ICOUNT)=Y(1)
RAL(ICOUNT)=Y(2)
RTEMP(ICOUNT)=Y(4)
HH=0.01
10  K=RUNGE(5,Y,F,X,HH)
    IF(K.NE.1) GO TO 15
    H=HBAR*EXP(-DHSTAR/(1+Y(4)))
    F(1)=-RL(MM)*(H*Y(1)/HIL-Y(2))
    F(2)=Y(3)
    F(3)=(Y(3)+F(1)/(GAMMA(MM)*HIL)+RP(MM)/GAMMA(MM))*(EXP(-ESTAR/
* (1.0+Y(4))))*Y(2))*PEL(MM)
    F(4)=Y(5)
    F(5)=(Y(5)-(RL(MM)*GAMS(MM)*(H/HIL*Y(1)-Y(2)))
* -HIL*RP(MM)*GAMR(MM)*EXP(-ESTAR/(1.0+Y(4)))*Y(2))*PEH(MM)
    GO TO 10
15  CONTINUE
    ICOUNT=ICOUNT+1
    XX(ICOUNT)=X
    RAG(ICOUNT)=Y(1)
    RAL(ICOUNT)=Y(2)
    RTEMP(ICOUNT)=Y(4)
    IF(X.GE.1.0) GO TO 16
    GO TO 10
16  CONTINUE
    AG(MM)=Y(1)
    AL(MM)=Y(2)
    DALR=Y(3)
    TEMP(MM)=Y(4)
    DTEMP=Y(5)
    REACTR=DALR
    RETURN
    END

```

```

FUNCTION RUNGE(N,Y,F,X,H)

```

C        THE FUNCTION RUNGE EMPLOYS THE FOURTH ORDER RUNGE-KUTTA METHOD  
 C        WITH GILL'S COEFFICIENTS TO INTEGRATE A SYSTEM OF N SIMULTANEOUS  
 C        FIRST ORDER DIFFERENTIAL EQUATIONS ACROSS ONE STEP OF LENGTH H IN  
 C        THE INDEPENDENT VARIABLE X, SUBJECT TO THE INITIAL CONDITIONS.

IMPLICIT REAL \*8(A-H,O-Z)  
 INTEGER RUNGE

DIMENSION PHI(50),SAVEY(50),Y(20),F(20)

DATA M /0/

M=M+1  
 GO TO (1,2,3,4,5),M  
 1    RUNGE=1  
     RETURN  
 2    DO 22 J=1,N  
     SAVEY(J)=Y(J)  
     PHI(J)=F(J)  
 22   Y(J)=SAVEY(J)+0.5\*H\*F(J)  
     X=X+0.5\*H  
     RUNGE=1  
     RETURN  
 3    DO 33 J=1,N  
     PHI(J)=PHI(J)+2.0\*F(J)  
 33   Y(J)=SAVEY(J)+0.5\*H\*F(J)  
     RUNGE=1  
     RETURN  
 4    DO 44 J=1,N  
     PHI(J)=PHI(J)+2.0\*F(J)  
 44   Y(J)=SAVEY(J)+H\*F(J)  
     X=X+0.5\*H  
     RUNGE=1  
     RETURN  
 5    DO 55 J=1,N  
 55   Y(J)=SAVEY(J)+(PHI(J)+F(J))\*H/6.0  
     M=0  
     RUNGE=0  
     RETURN  
 END

SUBROUTINE HYDRO(N)

C        THIS SUBROUTINE EVALUATES THE HYDRODYNAMIC PARAMETERS FOR THE  
 C        PREHEATER AND REACTORS. CORRELATIONS FOR PECLET NUMBER, MASS  
 C        TRANSFER COEFFICIENT, AND GAS HOLDUP ARE CALCULATED ACCORDING TO THE  
 C        CORRELATIONS PRESENTED IN THE REPORT. THESE PARAMETERS CAN BE  
 C        MODIFIED ACCORDINGLY. NOTE THAT SINCE THE CORRELATION FOR THE GAS  
 C        HOLDUP IS AN IMPLICIT EQUATION IN EG, AN INTERVAL HALVING TECHNIQUE  
 C        IS USED TO CALCULATE EG. IF EXPLICIT CORRELATIONS FOR EG ARE  
 C        AVAILABLE , THEN IT IS NOT NECESSARY TO CALL INTHAL.

IMPLICIT REAL\*8(A-H,O-Z)  
 DOUBLE PRECISION L

EXTERNAL FEG

DIMENSION VG(5),VL(5),L(5),D(5)  
 DIMENSION ZKLA(5),EG(5),PL(5),PH(5)

COMMON /A/ VG,VL,L,D  
 COMMON /B/ TIL,HIL,CGI,AGPI,ALPI,TEMPI,TEMW  
 COMMON /C/ RHOA,RHOG,DI,SIG,R,G  
 COMMON /D/ CPG,CPBAR,E,DHR,DHS,ZKBAR  
 COMMON /E/ ZKLA,EG  
 COMMON /INT/ EEG,DEG  
 COMMON /INT1/ ERR  
 COMMON /HYD/BO,ZNO,FR  
 COMMON /Z9/ PL,PH

OPEN (UNIT=29,FILE='HYDRO.DAT')

DO 10 I=1,N  
 V=VG(I)  
 DC=D(I)  
 ZMEW=VISCOS(TEMPI)  
 BO=((DC\*\*2.0)\*G\*RHOA)/SIG  
 FR=V/(G\*DC)\*\*0.5  
 SC=ZMEW/RHOA/DI  
 ZNO=(G\*DC\*\*3.0)\*((RHOA/ZMEW)\*\*2.0)  
 EEG=0.2  
 DEG=0.025  
 ERR=1.0E-04  
 CALL INTHAL(FEG)  
 EG(I)=EEG  
 ZKLA(I)=(0.6\*DI/DC\*\*2.0)\*(SC\*\*0.5)\*(BO\*\*0.62)\*  
 \* (ZNO\*\*0.31)\*(EG(I)\*\*1.1)  
 PL(I)=(13.0\*FR\*(L(I)/D(I))\*(VL(I)/VG(I)))  
 \* /(1.0+8.0\*FR\*\*0.85)  
 PH(I)=(RHOG\*VG(I)\*CPG+RHOA\*CPBAR\*VL(I))

```

* /(RHOA*CPBAR*VL(I)/PL(I))

IF(I.NE.1) GO TO 21
WRITE(29,100)
GO TO 31
21  K=I-1
    WRITE(29,101) K
31  WRITE(29,102) EG(I),ZKLA(I),PL(I),PH(I)
10  CONTINUE

100  FORMAT(/////5X,'HYDRODYNAMIC PARAMETERS FOR PREHEATER',///)
101  FORMAT(/5X,'HYDRODYNAMIC PARAMETERS FOR REACTOR # ',I3,///)
102  FORMAT(5X,'Gas Holdup ',T50,E12.5,/,
* 5X,'Volumetric mass transfer coefficient ',T50,E12.5,/,
* 5X,'Peclet Number for mass dispersion ',T50,E12.5,/,
* 5X,'Peclet Number for heat dispersion ',T50,E12.5,/)

CLOSE (UNIT=29)
RETURN
END

```

#### FUNCTION VISCOS(TEMP)

```

C      THIS FUNCTION EVALUATES THE VISCOSITY OF THE COAL SLURRY IN THE
C      PREHEATER AS A FUNCTION OF TEMPERATURE. THE VISCOSITY IS CALCULATED
C      FROM AN EQUATION FITTED TO DATA FOR 35 WT % KENTUCKY NO. 9 COAL
C      WITH WILSONVILLE RECYCLE SOLVENT. THE USER HAS TO CHANGE THE
C      FUNCTION STATEMENTS TO OBTAIN VISCOSITY-TEMPERATURE RELATION FOR
C      THE COAL-SOLVENT SYSTEM USED.

```

```

IMPLICIT REAL *8(A-H,O-Z)
DOUBLE PRECISION M

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COMMON/B/ TIL

```

```

A=-1.608
B=9.8578E+11
M=4.773
ATEMP=TEMP*TIL+TIL
IF(ATEMP.GE.550.0.AND.ATEMP.LE.675.0) GO TO 2
ZMU=10.0**((A+B/ATEMP**M))
GO TO 3
2  ZMU=0.14
3  CONTINUE
VISCOS=ZMU

```

RETURN  
END

SUBROUTINE INTHAL(FUNC)

C        THIS SUBROUTINE IS USED TO SOLVE IMPLICIT ALGEBRAIC EQUATIONS.

IMPLICIT REAL\*8(A-H,O-Z)

EXTERNAL FEG,REACTR

COMMON /INT/ X,DX  
COMMON /INT1/ ERR

U=-1.0

V=-1.0

1        F=FUNC(X)

IF(ABS(F).LE.ERR) GO TO 2

IF(F.GE.0.0) GO TO 3

IF(V.LE.0.0) GO TO 4

DX=DX/2.0

4        X=X+DX

U=1.0

GO TO 1

3        IF(U.LE.0.0) GO TO 5

DX=DX/2.0

5        CONTINUE

X=X-DX

GO TO 1

2        CONTINUE

RETURN

END

SUBROUTINE INPUT

C        THIS SUBROUTINE READS THE INPUT DATA ON THE PHYSICAL DIMENSIONS  
C        OF THE UNITS, PHYSICAL AND THERMAL PROPERTIES AND HYDROGEN  
C        CONSUMPTION KINETICS.

IMPLICIT REAL \*8(A-H,O-Z)  
DOUBLE PRECISION L

DIMENSION VG(5),VL(5),L(5),D(5)  
DIMENSION GAMMA(5),GAMS(5),GAMR(5),  
\* FLUX(5),HT(5),ALFA(5),TIME(5)  
DIMENSION RL(5),RP(5)  
DIMENSION ZKLA(5),EG(5),PL(5),PH(5)

COMMON/Z9/ PL,PH  
COMMON /A/ VG,VL,L,D  
COMMON /B/ TIL,HIL,CGI,AGPI,ALPI,TEMPI,TEMW  
COMMON /C/ RHOA,RHOG,DI,SIG,R,G  
COMMON /D/ CPG,CPBAR,E,DHR,DHS,ZKBAR  
COMMON/DD/ HBAR  
COMMON /DDD/ DHSTAR,ESTAR,GAMMA,GAMS,GAMR,RL,RP  
\* ,FLUX,HT,ALFA  
COMMON /E/ ZKLA,EG  
COMMON/Z5/ TIME  
COMMON/Z20/ FSLUR,FGAS  
COMMON /AN/ N

READ(01,\*) N  
READ(01,\*) VOLG,VOLL,(L(I),I=1,N),(D(I),I=1,N),TIL,P,FRAC,TH  
TIL=TIL+273.0  
TH=TH+273.0

READ(01,\*) CPG,CPBAR,ZKBAR,E,DHR,DHS,HBAR,DI,SIG,RHOA  
RR=82.057  
R=1.98  
G=981.0  
DO 10 I=1,N  
VG(I)=VOLG/(D(I)\*\*2.0\*0.786)  
VL(I)=VOLL/(D(I)\*\*2.0\*0.786)

10 CONTINUE

CGI=P/(RR\*TIL)\*FRAC\*2.0  
RHOG=CGI  
AGPI=1.0  
ALPI=0.0  
TEMPI=0.0  
TEMW=(TH-TIL)/TIL  
DHSTAR=DHS/(R\*TIL)  
ESTAR=E/(R\*TIL)  
HIL=HBAR\*(EXP(-DHSTAR))  
CALL HYDRO(N)



```

FSLUR=VOLL*RHOA*3600.0/1000.0
FGAS=VOLG*RHOG*3600.0/1000.0
DO 11 I=1,N
RL(I)=ZKLA(I)*L(I)*HIL/VG(I)
GAMMA(I)=VL(I)/VG(I)
RP(I)=ZKBAR*(1-EG(I))*L(I)/VG(I)
TIME(I)=L(I)*(1-EG(I))/VL(I)
FLUX(I)=VG(I)*RHOG*CPG+VL(I)*RHOA*CPBAR
GAMS(I)=(CGI*VG(I)*DHS)/TIL/FLUX(I)
GAMR(I)=(CGI*VG(I)*DHR)/TIL/FLUX(I)
BETA=0.0045
HT(I)=BETA*VL(I)**0.8/D(I)**0.2
ALFA(I)=HT(I)/D(I)*L(I)/FLUX(I)
11  CONTINUE
RETURN
END

```

FUNCTION FEG(X)

C THIS FUNCTION CALCULATES THE GAS HOLDUP ACCORDING TO THE  
C CORRELATION OF AKITA AND YOSHIDA.

IMPLICIT REAL \*8(A-H,O-Z)

COMMON /HYD/ BO,ZNO,FR

F1=X/((1.0-X)\*\*4.0)

F2=0.2\*(BO\*\*0.125)\*(ZNO\*\*0.083)\*FR

FEG=F1-F2

RETURN

END

SUBROUTINE REATEM(NR)

C THIS SUBROUTINE SIMULATES THE THERMAL BEHAVIOR OF THE REACTOR.

IMPLICIT REAL \*8(A-H,O-Z)  
DOUBLE PRECISION L

EXTERNAL REACTR

DIMENSION AG(5),AL(5),TEMP(5),L(5),D(5),VG(5),VL(5)  
DIMENSION XX(101),RAG(101),RAL(101),RTEMP(101)  
DIMENSION ZKLA(5),EG(5),PL(5),PH(5),RRTEMP(101)

COMMON /A/ VG,VL,L,D  
COMMON /B/ TIL,HIL,CGI,AGPI,ALPI,TEMPI,TEMW  
COMMON /REACT/AGRI,ALRI,DALRI,TEMPRI,DTEMPRI  
COMMON /DUM/ XX,RAG,RAL,RTEMP  
COMMON /NUM/ ICOUNT  
COMMON /REACT1/ DTEMP,DALR  
COMMON /REACT2/ M,J  
COMMON /INT/ ALR,DAL  
COMMON /INT1/ ERR  
COMMON /FF/ AG,AL,TEMP  
COMMON /E/ ZKLA,EG  
COMMON/Z8/ RRTEMP  
COMMON/Z9/ PL,PH  
COMMON/Z16/ ZRTEMP,ZRAG,ZRAL

J=NR-1

WRITE(6,300) J

300 FORMAT(10X,'SIMULATING REACTOR # ',I3,/,

WRITE(21,497) J

497 FORMAT('1',T22,'HYDROGEN PROFILE IN REACTOR # ',I3,/,

\* T30,'(GAS PHASE)',/,

\* 70(' '),/,

\* T8,'DISTANCE ALONG REACTOR',13X,'HYDROGEN CONCENTRATION',/,

\* T5,'DIMENSIONLESS',4X,'CENTIMETERS',8X,'DIMENSIONLESS',

\* 4X,'GM/CM\*\*3',/,

\* 70(' '),/)

WRITE(31,498) J

498 FORMAT('1',T22,'HYDROGEN PROFILE IN REACTOR # ',I3,/,

\* T28,'(LIQUID PHASE)',/,

\* 70(' '),/,

\* T8,'DISTANCE ALONG REACTOR',13X,'HYDROGEN CONCENTRATION',/,

\* T5,'DIMENSIONLESS',4X,'CENTIMETERS',8X,'DIMENSIONLESS',

\* 4X,'GM/CM\*\*3',/,

\* 70(' '),/)

WRITE(41,499) J

499 FORMAT('1',T21,'TEMPERATURE PROFILE IN REACTOR # ',I3,/,

\* 70(' '),/,

\* T8,'DISTANCE ALONG REACTOR',19X,'TEMPERATURE',/,

\* T5,'DIMENSIONLESS',4X,'CENTIMETERS',8X,'DIMENSIONLESS',

\* 4X,'DEGREES C',/)

\* 70('-.)/)

ERR= 0.001

M=NR

U=-1.0

V=-1.0

TEMPRI=TEMP(J)\*1.5

DTEMP=(TEMPRI-TEMP(J))\*PH(NR)

DTMPI=0.1

AGRI=AG(J)

ALRI=AL(J)\*0.9

ALR=ALRI

DAL=0.2

1 CONTINUE

CALL INTHAL(REACTR)

DAL=0.01

IF(ABS(DTEMP).LE.0.001) GO TO 2

IF(DTEMP.GE.0.0)GO TO 3

IF(V.LE.0.0)GO TO 4

ERR=0.001

DTMPI=DTMPI/2.0

4 TEMPRI=TEMPRI+DTMPI

DTEMP=(TEMPRI-TEMP(J))\*PH(NR)

U=1.0

GO TO 1

3 IF(U.LE.0.0)GO TO 5

ERR=0.001

DTMPI=DTMPI/2.0

5 TEMPRI=TEMPRI-DTMPI

DTEMP=(TEMPRI-TEMP(J))\*PH(NR)

GO TO 1

2 CONTINUE

DO 23 II=1,ICOUNT

RRTEMP(II)=RTEMP(NR)

ZX=XX(II)\*L(NR)

ZRAG=RAG(II)\*CGI

ZRAL=RAL(II)\*CGI\*HIL

ZRTEMP=RTEMP(II)\*TIL+TIL-273.0

WRITE(21,500) XX(II),ZX,RAG(II),ZRAG

WRITE(31,500) XX(II),ZX,RAL(II),ZRAL

WRITE(41,500) XX(II),ZX,RTEMP(II),ZRTEMP

500 FORMAT(8X,F5.2,8X,F8.1,12X,F8.4,6X,E11.4)

23 CONTINUE

10 CONTINUE

WRITE(21,501)

WRITE(31,501)

WRITE(41,501)

501   FORMAT(/,70('-'))

      RETURN  
      END

      SUBROUTINE INPUT1(TIL)

C       THIS SUBROUTINE READS THE INPUT DATA ON COAL CONVERSION KINETICS.

      IMPLICIT REAL \*8(A-H,O-Z)  
      DOUBLE PRECISION KBARP,KBARR  
      CHARACTER\*20 NAME(10,2)

      DIMENSION KBARP(20,20),KBARR(20,20),COEFFP(20,20)  
      DIMENSION COEFFR(20,20),ECP(20,20),ECR(20,20),CPI(10)

      COMMON/Z1/ KBARP,ECP,COEFFP  
      COMMON/Z11/ KBARR,ECR,COEFFR  
      COMMON/Z2/ CPI  
      COMMON/Z6/ NSPH,NSPR

      DATA R/1.98/

      DO 1 I=1,20  
      DO 1 J=1,20  
      KBARP(I,J)=0.0  
      KBARR(I,J)=0.0  
      ECP(I,J)=0.0  
      ECR(I,J)=0.0  
      COEFFP(I,J)=0.0  
      COEFFR(I,J)=0.0

1       CONTINUE

      READ(11,\*) NSPH  
      DO 2 I=1,NSPH  
      READ(11,102) NAME(I,1)

102    FORMAT(A20)

2       CONTINUE

      READ(11,\*) NKP  
      DO 4 I=1,NKP  
      READ(11,\*) II  
      READ(11,\*) JJ  
      READ(11,\*) KBARP(II,JJ)  
      READ(11,\*) ECP(II,JJ)

```

      ECP(IJ,JJ)=ECP(IJ,JJ)/(R*TIL)
      COEFFP(IJ,JJ)=1.0
4     CONTINUE

```

```

      READ(11,*) NSPR
      DO 6 I=1,NSPR
      READ(11,102) NAME(I,2)
6     CONTINUE
      READ(11,*) NKR
      DO 7 I=1,NKR
      READ(11,*) II
      READ(11,*) JJ
      READ(11,*) KBARR(IJ,JJ)
      READ(11,*) ECR(IJ,JJ)
      ECR(IJ,JJ)=ECR(IJ,JJ)/(R*TIL)
      COEFFR(IJ,JJ)=1.0
7     CONTINUE

```

```

      DO 5 I=1,NSPR
      READ(11,*) CPI(I)
5     CONTINUE
      RETURN
      END

```

SUBROUTINE EQTNS(TEMP,ECSTAR,KBAR,COEFF,NSP)

C      THIS SUBROUTINE CALCULATES THE RATES OF CHEMICAL SPECIES REACTION.

```

      IMPLICIT REAL *8(A-H,O-Z)
      DOUBLE PRECISION KBAR,K

```

```

      DIMENSION KBAR(20,20),ECSTAR(20,20),RATE(10)
      DIMENSION COEFF(20,20),TEMP(101),K(20,20)
      DIMENSION C(10,101)

```

```

      COMMON/Z3/ C,RATE,ICOUNT

```

```

      DO 1 IJ=1,NSP
      RATE(IJ)=0.0
      DO 1 I=1,NSP
      DO 1 J=1,NSP
      IF(COEFF(I,J).EQ.0.0) GO TO 1

```

```

      IF((IJ.NE.I).AND.(IJ.NE.J)) GO TO 1
      K(I,J)=KBARP(I,J)*EXP(-ECSTAR(I,J)/(1.0+TEMP(ICOUNT)))
      IF(IJ.EQ.I) RATE(IJ)=RATE(IJ)-COEFF(I,J)*K(I,J)*C(I,ICOUNT)
      IF(IJ.EQ.J) RATE(IJ)=RATE(IJ)+COEFF(I,J)*K(I,J)*C(I,ICOUNT)
1      CONTINUE
      RETURN
      END

```

#### SUBROUTINE PHEATC

```

C      THIS SUBROUTINE SIMULATES THE CONVERSION OF THE CHEMICAL SPECIES
C      IN THE PREHEATER.

```

```

      IMPLICIT REAL *8(A-H,O-Z)
      DOUBLE PRECISION KBARP
      INTEGER RUNGE

```

```

      DIMENSION CPI(10),CPO(10),RATE(10),PTEMP(101),C(10,101),TIME(5)
      DIMENSION Y(20),F(20),XX(101)
      DIMENSION KBARP(20,20),ECP(20,20),COEFFP(20,20)

```

```

      COMMON/Z1/ KBARP,ECP,COEFFP
      COMMON/Z2/ CPI
      COMMON/Z3/ C,RATE,ICOUNT
      COMMON/Z4/ PTEMP
      COMMON/Z5/ TIME
      COMMON/Z6/ NSPH,NSPR
      COMMON/Z7/ CPO
      COMMON/Z13/ XX

```

```

      X=0.0
      ICOUNT=1
      NSP=NSPH
      XX(ICOUNT)=X
      DO 25 I=1,NSP
      Y(I)=CPI(I)
      C(I,ICOUNT)=Y(I)
25      CONTINUE
      HH=0.01

```

```

10      K=RUNGE(NSP,Y,F,X,HH)
      IF(K.NE.1) GO TO 15
      CALL EQTNS(PTEMP,ECP,KBARP,COEFFP,NSPH)
      DO 26 I=1,NSP
      F(I)=RATE(I)*TIME(1)

```

```

      C(I,ICOUNT)=Y(I)
26    CONTINUE
      GO TO 10
15    CONTINUE
      ICOUNT=ICOUNT+1
      XX(ICOUNT)=X
      DO 27 I=1,NSP
      C(I,ICOUNT)=Y(I)
27    CONTINUE
      IF(X.GE.1.0) GO TO 16
      GO TO 10
16    CONTINUE
      DO 28 I=1,NSP
      CPO(I)=Y(I)
28    CONTINUE
      IF(NSPH.EQ.NSPR) RETURN
      DO 29 I=NSPH,NSPR
      CPO(I)=CPI(I)
29    CONTINUE

      RETURN
      END

```

# SUBROUTINE CHEM1

```

C      THIS SUBROUTINE INITIALIZES SIMULATION OF CHEMICAL SPECIES
C      CONVERSION IN THE PREHEATER.

```

```

      IMPLICIT REAL *8(A-H,O-Z)
      DOUBLE PRECISION L

```

```

      DIMENSION C(10,101),RATE(10),XX(101),VG(5),VL(5),L(5),D(5)

```

```

      COMMON /A/ VG,VL,L,D
      COMMON/Z3/ C,RATE,ICOUNT
      COMMON/Z6/ NSPH,NSPR
      COMMON/Z13/ XX

```

```

      CALL PHEATC
      OPEN (UNIT=22,FILE='PCONC.DAT')
      NSP=NSPH
      WRITE(22,499)

```

```

499  FORMAT(T30,'CONCENTRATION PROFILE IN PREHEATER',/)
      IF(NSP.EQ.2) WRITE(22,502)
      IF(NSP.EQ.3) WRITE(22,503)

```

```

IF(NSP.EQ.4) WRITE(22,504)
IF(NSP.EQ.5) WRITE(22,505)
IF(NSP.EQ.6) WRITE(22,506)
IF(NSP.EQ.7) WRITE(22,507)
IF(NSP.EQ.8) WRITE(22,508)
IF(NSP.EQ.9) WRITE(22,509)
IF(NSP.EQ.10) WRITE(22,510)
502  FORMAT(T30,70('-'),/,
*   T37,'DISTANCE ALONG PREHEATER',12X,'CHEMICAL SPECIES',/,
*   T35,'DIMENSIONLESS',4X,'CENTIMETERS',12X,'1',10X,'2',/,
*   T30,70('-'))
503  FORMAT(T5,80('-'),/,
*   T12,'DISTANCE ALONG PREHEATER',19X,'CHEMICAL SPECIES',/,
*   T10,'DIMENSIONLESS',4X,'CENTIMETERS',12X,'1',11X,'2',11X,'3',/,
*   T5,80('-'))
504  FORMAT(T20,90('-'),/,
*   T27,'DISTANCE ALONG PREHEATER',24X,'CHEMICAL SPECIES',/,
*   24X,'DIMENSIONLESS',4X,'CENTIMETERS',12X,'1',11X,'2',11X,'3',
*   11X,'4',/,
*   T20,90('-'))
505  FORMAT(T15,100('-'),/,
*   T22,'DISTANCE ALONG PREHEATER',29X,'CHEMICAL SPECIES',/,
*   19X,'DIMENSIONLESS',4X,'CENTIMETERS',12X,'1',11X,'2',11X,'3',
*   11X,'4',11X,'5',/,
*   T15,100('-'))
506  FORMAT(T10,110('-'),/,
*   T17,'DISTANCE ALONG PREHEATER',34X,'CHEMICAL SPECIES',/,
*   14X,'DIMENSIONLESS',4X,'CENTIMETERS',12X,'1',11X,'2',11X,'3',
*   11X,'4',11X,'5',11X,'6',/,
*   T10,110('-'))
507  FORMAT(T5,125('-'),/,
*   T12,'DISTANCE ALONG PREHEATER',39X,'CHEMICAL SPECIES',/,
*   9X,'DIMENSIONLESS',4X,'CENTIMETERS',12X,'1',11X,'2',11X,'3',
*   11X,'4',11X,'5',11X,'6',11X,'7',/,
*   T5,125('-'))
508  FORMAT(132('-'),/,
*   T7,'DISTANCE ALONG PREHEATER',44X,'CHEMICAL SPECIES',/,
*   4X,'DIMENSIONLESS',4X,'CENTIMETERS',12X,'1',11X,'2',11X,'3',
*   11X,'4',11X,'5',11X,'6',11X,'7',11X,'8',/,
*   132('-'))
509  FORMAT(132('-'),/,
*   T4,'DISTANCE ALONG PREHEATER',47X,'CHEMICAL SPECIES',/,
*   1X,'DIMENSIONLESS',3X,'CENTIMETERS',11X,'1',10X,'2',10X,'3',
*   10X,'4',10X,'5',10X,'6',10X,'7',10X,'8',10X,'9',/,
*   132('-'))
510  FORMAT(132('-'),/,
*   T3,'DISTANCE ALONG PREHEATER',49X,'CHEMICAL SPECIES',/,
*   1X,'DIMENSIONLESS',2X,'CENTIMETERS',10X,'1',9X,'2',9X,'3',

```



```

* 9X,'4',9X,'5',9X,'6',9X,'7',9X,'8',9X,'9',9X,'10',/,
* 132('-'))
DO 1 J=1,ICOUNT
ZX=XX(J)*L(1)
IF(NSP.EQ.2) WRITE(22,602) XX(J),ZX,(C(I,J),I=1,NSP)
IF(NSP.EQ.3) WRITE(22,603) XX(J),ZX,(C(I,J),I=1,NSP)
IF(NSP.EQ.4) WRITE(22,604) XX(J),ZX,(C(I,J),I=1,NSP)
IF(NSP.EQ.5) WRITE(22,605) XX(J),ZX,(C(I,J),I=1,NSP)
IF(NSP.EQ.6) WRITE(22,606) XX(J),ZX,(C(I,J),I=1,NSP)
IF(NSP.EQ.7) WRITE(22,607) XX(J),ZX,(C(I,J),I=1,NSP)
IF(NSP.EQ.8) WRITE(22,608) XX(J),ZX,(C(I,J),I=1,NSP)
IF(NSP.EQ.9) WRITE(22,609) XX(J),ZX,(C(I,J),I=1,NSP)
IF(NSP.EQ.10) WRITE(22,610) XX(J),ZX,(C(I,J),I=1,NSP)
1 CONTINUE
IF(NSP.EQ.2) WRITE(22,702)
IF(NSP.EQ.3) WRITE(22,703)
IF(NSP.EQ.4) WRITE(22,704)
IF(NSP.EQ.5) WRITE(22,705)
IF(NSP.EQ.6) WRITE(22,706)
IF(NSP.EQ.7) WRITE(22,707)
IF(NSP.EQ.8) WRITE(22,708)
IF(NSP.EQ.9) WRITE(22,708)
IF(NSP.EQ.10) WRITE(22,708)
602 FORMAT(38X,F5.2,8X,F8.1,10X,E9.3,2X,E9.3)
603 FORMAT(13X,F5.2,8X,F8.1,10X,E9.3,2(3X,E9.3))
604 FORMAT(28X,F5.2,8X,F8.1,10X,E9.3,3(3X,E9.3))
605 FORMAT(23X,F5.2,8X,F8.1,10X,E9.3,4(3X,E9.3))
606 FORMAT(18X,F5.2,8X,F8.1,10X,E9.3,5(3X,E9.3))
607 FORMAT(13X,F5.2,8X,F8.1,10X,E9.3,6(3X,E9.3))
608 FORMAT(8X,F5.2,8X,F8.1,10X,E9.3,7(3X,E9.3))
609 FORMAT(5X,F5.2,7X,F8.1,9X,E9.3,8(2X,E9.3))
610 FORMAT(5X,F5.2,6X,F8.1,9X,E9.3,9(1X,E9.3))
702 FORMAT(T30,70('-'))
703 FORMAT(T5,80('-'))
704 FORMAT(T20,90('-'))
705 FORMAT(T15,100('-'))
706 FORMAT(T10,110('-'))
707 FORMAT(T5,125('-'))
708 FORMAT(132('-'))
CLOSE (UNIT=22)
RETURN
END

```

SUBROUTINE REACTC(NR)

C        THIS SUBROUTINE SIMULATES THE CHEMICAL SPECIES CONVERSION IN  
C        THE PREHEATER.

IMPLICIT REAL \*8(A-H,O-Z)  
DOUBLE PRECISION KBARR  
INTEGER RUNGE,ORDER

DIMENSION CPO(10),RATE(10),RTEMP(101),C(10,101),TIME(5)  
DIMENSION Y(20),F(20),A(20,20),PEL(5),B(20),ZETA(20),PEH(5)  
DIMENSION ORDER(20),GUESS(20,20),FACTOR(50),RRATE(10)  
DIMENSION AA(20,20),XX(101)  
DIMENSION KBARR(20,20),ECR(20,20),COEFFR(20,20)

COMMON/Z11/ KBARR,ECR,COEFFR  
COMMON/Z7/ CPO  
COMMON/Z13/ XX  
COMMON/Z9/ PEL,PEH  
COMMON/Z3/ C,RATE,ICOUNT  
COMMON/Z8/ RTEMP  
COMMON/Z5/ TIME  
COMMON/Z6/ NSPH,NSPR

ITEST=0

ICOUNT=1

NSP=NSPR

DO 8 I=1,NSP

B(I)=CPO(I)

C(I,ICOUNT)=CPO(I)

B(I+NSP)=0.0

8        CONTINUE

CALL EQTNS(RTEMP,ECR,KBARR,COEFFR,NSPR)

DO 90 J=1,NSP

RRATE(J)=RATE(J)

90        CONTINUE

HH=0.01

NNSP=2\*NSP

SEED=1

DO 1 I=1,NNSP

ICOUNT=1

X=0.0

XX(ICOUNT)=X

DO 20 J=1,NNSP

FACTOR(J)=RAN(SEED)

20        CONTINUE

DO 2 N=1,NSP

Y(N)=CPO(N)\*(1+(-1)\*\*I\*FACTOR(N)\*0.2)

Y(N+NSP)=RRATE(N)/ABS(RRATE(N))\*(0.5\*FACTOR(N+NSP))

2        CONTINUE

```

DO 43 N=1,NSP
A(N,I)=Y(N)-Y(N+NSP)/PEL(NR)
C(N,ICOUNT)=Y(N)
43  CONTINUE
DO 6 J=1,NNSP
GUESS(J,I)=Y(J)
6  CONTINUE

10  CONTINUE
K=RUNGE(NNSP,Y,F,X,HH)
IF(K.NE.1) GO TO 15
CALL EQTNS(RTEMP,ECR,KBARR,COEFFR,NSPR)
DO 26 J=1,NSP
F(J)=Y(J+NSP)
F(J+NSP)=PEL(NR)*(Y(J+NSP)-RATE(J)*TIME(NR))
C(J,ICOUNT)=Y(J)
26  CONTINUE
GO TO 10
15  CONTINUE
ICOUNT=ICOUNT+1
XX(ICOUNT)=X
DO 17 J=1,NSP
C(J,ICOUNT)=Y(J)
17  CONTINUE
IF(X.GE.1.0) GO TO 16
GO TO 10
16  CONTINUE
IF(ITEST.NE.0) GO TO 12
DO 55 J=1,NSP
A(NSP+J,I)=Y(NSP+J)
55  CONTINUE
1  CONTINUE
DO 45 I1=1,NNSP
45  CONTINUE
C  DO 68 I1=NSP+1,NNSP
C  DO 68 I2=1,NNSP
C  A(I1,I2)=A(I1,I2)/A(I1,1)
68  CONTINUE
DO 69 I1=1,NNSP
DO 69 I2=1,NNSP
AA(I1,I2)=A(I1,I2)
69  CONTINUE
CALL LUDCMP(A,NNSP,NNSP,ORDER)
CALL SOLVLU(A,B,ZETA,NNSP,NNSP,ORDER)
C
C
DO 70 I1=1,NNSP
BTOT=0.0

```

```

DO 71 I2=1,NNSP
BTOT=BTOT+AA(I1,I2)*ZETA(I2)
71  CONTINUE
70  CONTINUE
ITEST=1
ICOUNT=1
X=0.0
DO 7 J=1,NNSP
Y(J)=0.0
DO 7 I=1,NNSP
Y(J)=Y(J)+ZETA(I)*GUESS(J,I)
7  CONTINUE
DO 18 I=1,NSP
C(I,ICOUNT)=Y(I)
18  CONTINUE
GO TO 10
12  CONTINUE
DO 28 I=1,NSP
28  CPO(I)=Y(I)

RETURN
END

```

#### SUBROUTINE CHEM2(NR)

C        THIS SUBROUTINE INITIALIZES THE SIMULATION OF THE CHEMICAL SPECIES  
C        CONVERSION IN THE REACTOR.

```

IMPLICIT REAL *8(A-H,O-Z)
DOUBLE PRECISION L

```

```

DIMENSION C(10,101),RATE(10),XX(101),VG(5),VL(5),L(5),D(5)

```

```

COMMON/A/ VG,VL,L,D
COMMON/Z3/ C,RATE,ICOUNT
COMMON/Z6/ NSPH,NSPR
COMMON/Z13/ XX

```

```

CALL REACTC(NR)
K=NR-1
NSP=NSPR
WRITE(23,499) K

```

```

499  FORMAT('1',T31,'CONCENTRATION PROFILE IN REACTOR # ',I3,/)
IF(NSP.EQ.2) WRITE(23,502)
IF(NSP.EQ.3) WRITE(23,503)

```

```

IF(NSP.EQ.4) WRITE(23,504)
IF(NSP.EQ.5) WRITE(23,505)
IF(NSP.EQ.6) WRITE(23,506)
IF(NSP.EQ.7) WRITE(23,507)
IF(NSP.EQ.8) WRITE(23,508)
IF(NSP.EQ.9) WRITE(23,509)
IF(NSP.EQ.10) WRITE(23,510)
502  FORMAT(T30,70('-'),/,
*   T38,'DISTANCE ALONG REACTOR',13X,'CHEMICAL SPECIES',/,
*   T35,'DIMENSIONLESS',4X,'CENTIMETERS',12X,'1',10X,'2',/,
*   T30,70('-'))
503  FORMAT(T5,80('-'),/,
*   T13,'DISTANCE ALONG REACTOR',20X,'CHEMICAL SPECIES',/,
*   T10,'DIMENSIONLESS',4X,'CENTIMETERS',12X,'1',11X,'2',11X,'3',/,
*   T5,80('-'))
504  FORMAT(T20,90('-'),/,
*   T28,'DISTANCE ALONG REACTOR',25X,'CHEMICAL SPECIES',/,
*   24X,'DIMENSIONLESS',4X,'CENTIMETERS',12X,'1',11X,'2',11X,'3',
*   11X,'4',/,
*   T20,90('-'))
505  FORMAT(T15,100('-'),/,
*   T23,'DISTANCE ALONG REACTOR',30X,'CHEMICAL SPECIES',/,
*   19X,'DIMENSIONLESS',4X,'CENTIMETERS',12X,'1',11X,'2',11X,'3',
*   11X,'4',11X,'5',/,
*   T15,100('-'))
506  FORMAT(T10,110('-'),/,
*   T18,'DISTANCE ALONG REACTOR',35X,'CHEMICAL SPECIES',/,
*   14X,'DIMENSIONLESS',4X,'CENTIMETERS',12X,'1',11X,'2',11X,'3',
*   11X,'4',11X,'5',11X,'6',/,
*   T10,110('-'))
507  FORMAT(T5,125('-'),/,
*   T13,'DISTANCE ALONG REACTOR',40X,'CHEMICAL SPECIES',/,
*   9X,'DIMENSIONLESS',4X,'CENTIMETERS',12X,'1',11X,'2',11X,'3',
*   11X,'4',11X,'5',11X,'6',11X,'7',/,
*   T5,125('-'))
508  FORMAT(132('-'),/,
*   T8,'DISTANCE ALONG REACTOR',45X,'CHEMICAL SPECIES',/,
*   4X,'DIMENSIONLESS',4X,'CENTIMETERS',12X,'1',11X,'2',11X,'3',
*   11X,'4',11X,'5',11X,'6',11X,'7',11X,'8',/,
*   132('-'))
509  FORMAT(132('-'),/,
*   T5,'DISTANCE ALONG REACTOR',48X,'CHEMICAL SPECIES',/,
*   1X,'DIMENSIONLESS',3X,'CENTIMETERS',11X,'1',10X,'2',10X,'3',
*   10X,'4',10X,'5',10X,'6',10X,'7',10X,'8',10X,'9',/,
*   132('-'))
510  FORMAT(132('-'),/,
*   T4,'DISTANCE ALONG REACTOR',50X,'CHEMICAL SPECIES',/,
*   1X,'DIMENSIONLESS',2X,'CENTIMETERS',10X,'1',9X,'2',9X,'3',

```

```

* 9X,'4',9X,'5',9X,'6',9X,'7',9X,'8',9X,'9',9X,'10',/,
* 132('-'))
DO 1 J=1,ICOUNT
ZX=XX(J)*L(NR)
IF(NSP.EQ.2) WRITE(23,602) XX(J),ZX,(C(I,J),I=1,NSP)
IF(NSP.EQ.3) WRITE(23,603) XX(J),ZX,(C(I,J),I=1,NSP)
IF(NSP.EQ.4) WRITE(23,604) XX(J),ZX,(C(I,J),I=1,NSP)
IF(NSP.EQ.5) WRITE(23,605) XX(J),ZX,(C(I,J),I=1,NSP)
IF(NSP.EQ.6) WRITE(23,606) XX(J),ZX,(C(I,J),I=1,NSP)
IF(NSP.EQ.7) WRITE(23,607) XX(J),ZX,(C(I,J),I=1,NSP)
IF(NSP.EQ.8) WRITE(23,608) XX(J),ZX,(C(I,J),I=1,NSP)
IF(NSP.EQ.9) WRITE(23,609) XX(J),ZX,(C(I,J),I=1,NSP)
IF(NSP.EQ.10) WRITE(23,610) XX(J),ZX,(C(I,J),I=1,NSP)
1 CONTINUE
IF(NSP.EQ.2) WRITE(23,702)
IF(NSP.EQ.3) WRITE(23,703)
IF(NSP.EQ.4) WRITE(23,704)
IF(NSP.EQ.5) WRITE(23,705)
IF(NSP.EQ.6) WRITE(23,706)
IF(NSP.EQ.7) WRITE(23,707)
IF(NSP.EQ.8) WRITE(23,708)
IF(NSP.EQ.9) WRITE(23,708)
IF(NSP.EQ.10) WRITE(23,708)
602 FORMAT(38X,F5.2,8X,F8.1,10X,E9.3,2X,E9.3)
603 FORMAT(13X,F5.2,8X,F8.1,10X,E9.3,2(3X,E9.3))
604 FORMAT(28X,F5.2,8X,F8.1,10X,E9.3,3(3X,E9.3))
605 FORMAT(23X,F5.2,8X,F8.1,10X,E9.3,4(3X,E9.3))
606 FORMAT(18X,F5.2,8X,F8.1,10X,E9.3,5(3X,E9.3))
607 FORMAT(13X,F5.2,8X,F8.1,10X,E9.3,6(3X,E9.3))
608 FORMAT(8X,F5.2,8X,F8.1,10X,E9.3,7(3X,E9.3))
609 FORMAT(5X,F5.2,7X,F8.1,9X,E9.3,8(2X,E9.3))
610 FORMAT(5X,F5.2,6X,F8.1,9X,E9.3,9(1X,E9.3))
702 FORMAT(T30,70('-'))
703 FORMAT(T5,80('-'))
704 FORMAT(T20,90('-'))
705 FORMAT(T15,100('-'))
706 FORMAT(T10,110('-'))
707 FORMAT(T5,125('-'))
708 FORMAT(132('-'))
CLOSE (UNIT=22)
RETURN
END

```

SUBROUTINE SOLVLU(LU,B,X,N,NDIM,ORDER)

C THIS SUBROUTINE IS USED TO FIND THE SOLUTION TO A SYSTEM  
 C OF EQUATIONS,  $AX = B$ , AFTER THE LU EQUIVALENT OF A HAS BEEN FOUND.  
 C BEFORE USING THIS ROUTINE, THE VECTOR B SHOULD BE SCALED IF MATRIX A WAS  
 C SCALED, USING THE SAME SCALE FACTORS. WITHIN THIS ROUTINE, THE ELEMENTS  
 C OF B ARE REARRANGED IN THE SAME WAY THAT THE ROWS OF A WERE  
 C INTERCHANGED, USING THE ORDER VECTOR WHICH HOLDS THE ROW ORDERINGS.  
 C THE SOLUTION IS RETURNED IN X.

C PARAMETERS ARE -  
 C LU THE LU EQUIVALENT OF THE COEFFICIENT MATRIX  
 C B THE VECTOR OF RIGHT HAND SIDES  
 C X SOLUTION VECTOR  
 C N NUMBER OF EQUATIONS  
 C NDIM FIRST DIMENSION OF A IN THE MAIN PROGRAM  
 C ORDER INTEGER ARRAY OF ROW ORDER AS REARRANGED DURING PIVOTING

IMPLICIT REAL\*8(A-H,O-Z)  
 DOUBLE PRECISION LU(20,20)  
 INTEGER ORDER(20)

DIMENSION B(20),X(20)

DO 10 I=1,N  
 J=ORDER(I)  
 X(I)=B(J)  
 10 CONTINUE

X(1)=X(1)/LU(1,1)  
 DO 50 IROW=2,N  
 IM1=IROW-1  
 SUM=0.  
 DO 40 JCOL=1,IM1  
 SUM=SUM+LU(IROW,JCOL)\*X(JCOL)  
 40 CONTINUE  
 X(IROW)=(X(IROW)-SUM)/LU(IROW,IROW)  
 50 CONTINUE

DO 70 IROW=2,N  
 NVBL=N-IROW+1  
 SUM=0.  
 NP1=NVBL+1  
 DO 60 JCOL=NP1,N  
 SUM=SUM+LU(NVBL,JCOL)\*X(JCOL)  
 60 CONTINUE  
 X(NVBL)=X(NVBL)-SUM  
 70 CONTINUE  
 RETURN  
 END

SUBROUTINE LUDCMP(A,N,NDIM,ORDER)

C THIS SUBROUTINE COMPUTES THE L AND U TRIANGULAR MATRICES  
C EQUIVALENT TO THE A MATRIX, SUCH THAT  $LU=A$ . THESE MATRICES  
C ARE RETURNED IN THE SPACE OF A, IN COMPACT FORM. THE U MATRIX  
C HAS ONES ON ITS DIAGONAL.  
C PARTIAL PIVOTING IS USED TO GIVE MAXIMUM VALUED ELEMENTS ON THE  
C DIAGONAL OF L. THE ORDER OF THE ROWS AFTER PIVOTING IS RETURNED IN  
C THE INTEGER VECTOR ORDER.  
C VECTORS BEFORE SOLVING THE SYSTEM  $AX=B$

C PARAMETERS ARE-  
C A THE N X N MATRIX OF COEFFICIENTS  
C A THE NUMBER OF EQUATIONS  
C NDIM THE FIRST DIMENSION OF A IN THE CALLING PROGRAM  
C ORDER INTEGER VECTOR ROW ORDER AFTER PIVOTING

C THIS ROUTINE CALLS A SUBROUTINE APVT TO LOCATE THE PIVOT ROW AND  
C MAKE INTERCHANGES

IMPLICIT REAL\*8(A-H,O-Z)  
DIMENSION A(20,20)  
INTEGER ORDER(20)

DO 10 I=1,N  
ORDER (I)=I  
10 CONTINUE

CALL APVT(A, N, NDIM, ORDER,1)

IF (ABS(A(1,1)) .LT. 1.E-20) GO TO 99  
DO 20 KCOL=2,N  
A(1,KCOL)=A(1,KCOL)/A(1,1)  
20 CONTINUE

NM1=N-1  
DO 80 JCOL=2,NM1  
JCOL1=JCOL

JM1=JCOL-1  
DO 50 IROW=JCOL,N  
SUM=0.  
DO 40 KCOL=1,JM1  
SUM=SUM+A(IROW,KCOL)\*A(KCOL,JCOL)



```

40  CONTINUE
   A(IROW,JCOL)= A(IROW,JCOL)-SUM
50  CONTINUE

   CALL APVT (A,N, NDIM,ORDER, JCOL1)
   IF (ABS(A(JCOL,JCOL)).LT. 1.E-20) GO TO 99

   JP1=JCOL+1
   DO 70 KCOL=JP1,N
   SUM=0.
   DO 60 IROW=1,JM1
   SUM=SUM+A(JCOL,IROW)*A(IROW,KCOL)
60  CONTINUE
   A(JCOL,KCOL) =(A(JCOL,KCOL)-SUM)/A(JCOL,JCOL)
70  CONTINUE
80  CONTINUE

   SUM=0
   DO 90 KCOL=1,NM1
   SUM=SUM+A(N,KCOL)*A(KCOL,N)
90  CONTINUE
   A(N,N)=A(N,N)-SUM
   RETURN

99  WRITE (6,100)
100 FORMAT (1H0,60H VERY SMALL PIVOT ELEMENT INDICATES A NEARLY SINGU
+LAR MATRIX)
   RETURN
   END

```

SUBROUTINE APVT (A,N,NDIM,ORDER,JCOL)

C THIS SUBROUTINE FINDS THE LARGEST ELEMENT FOR PIVOT IN JCOL OF  
C MATRIX A, PERFORMS INTERCHANGES THE ELEMENTS IN A AND ALSO  
C INTERCHANGES THE ELEMENTS IN THE ORDER VECTOR.

C PARAMETERS ARE-

C A MATRIX OF COEFFICIENTS WHOSE ROWS ARE TO BE INTERCHANGED  
C N NUMBER OF EQUATIONS  
C NDIM FIRST DIMENSION OF A IN THE MAIN PROGRAM  
C ORDER INTEGER VECTOR TO HOLD ROW ORDERING  
C JCOL COLUMN OF A BEING SEARCHED FOR PIVOT ELEMENT

IMPLICIT REAL\*8(A-H,O-Z)

```

DIMENSION A(20,20)
      INTEGER ORDER(20)

      IPVT=JCOL
      BIG=ABS(A(JCOL,JCOL))
      JP1=JCOL+1
      DO 10 IROW=JP1,N
      ANEXT=ABS(A(IROW,JCOL))
      IF (ANEXT .LE. BIG) GO TO 10
      BIG=ANEXT
      IPVT=IROW
10  CONTINUE

      IF (IPVT .EQ. JCOL) GO TO 25
      DO 20 KCOL=1,N
      SAVE =A(JCOL,KCOL)
      A(JCOL,KCOL)=A(IPVT,KCOL)
      A(IPVT,KCOL)=SAVE
20  CONTINUE

      ISAVE=ORDER(JCOL)
      ORDER(JCOL)=ORDER(IPVT)
      ORDER(IPVT)=ISAVE
25  RETURN
      END

```

SUBROUTINE OUTPUT(IDUM,NR)

C .....PRINTS OUTPUT.

IMPLICIT REAL\*8(A-H,O-Z)

DIMENSION CPI(10),CPO(10),C(10,101),RATE(10)

COMMON/Z15/ TEMPA,AGPA,ALPA,TEMPO,AGPO,ALPO

COMMON/Z16/ ZRTEMP,ZRAG,ZRAL

COMMON/Z2/ CPI

COMMON/Z3/C,RATE,ICOUNT

COMMON/Z6/ NSPH,NSPR

COMMON/Z7/ CPO

COMMON/COST1/ PCCOST,POCOST,PMCOST,PFCOST,PVCOST,RCCOST,ROCOST

\* ,RMCOST,RFCOST,RVCOST

COMMON/Z20/ FSLUR,FGAS

COMMON/AN/ N

C

IF(IDUM-2) 32,33,34

```

32  WRITE(3,200)
200  FORMAT(80('-'))
    WRITE(3,300)
300  FORMAT(T33'OUTPUT SUMMARY',/,80('-'),/)
    WRITE(3,99) NSPH,NSPR,FSLUR,FGAS
99   FORMAT(5X,'Number of Species in Preheater ',T60,I3,/,
*    5X,'Number of Species in Reactor ',T60,I3,/,
1    5X,'Flow Rate of Slurry <kg/hr>',T60,E12.4,/,
2    5X,'Flow Rate of Gas <kg/hr>',T60,E12.4,/)
    TEMPA=TEMPO-273.0
    WRITE(3,100) TEMPA,AGPA,ALPA
100  FORMAT(/,15X,'Conditions at Preheater Inlet',/,
*    5X,'Temperature <Degrees C>',T60,E12.4,/,
*    5X,'Hydrogen Concentration (Gas Phase) <gm/cm**3>',T60,E12.4,/,
*    5X,'Hydrogen Concentration (Liquid Phase) <gm/cm**3>',T60,E12.4
*    ,/)
    DO 1 I=1,NSPH
    WRITE(3,102) I,CPI(I)
102  FORMAT(5X,'Concentration of Species',I3,' <gm/gm>',T60,E12.4)
1    CONTINUE
    TEMPO=TEMPO-273.0
    WRITE(3,101) TEMPO,AGPO,ALPO
101  FORMAT(/,15X,'Conditions at Preheater Outlet (Reactor Inlet)',/,
*    5X,'Temperature <Degrees C>',T60,E12.4,/,
*    5X,'Hydrogen Concentration (Gas Phase) <gm/cm**3>',T60,E12.4,/,
*    5X,'Hydrogen Concentration (Liquid Phase) <gm/cm**3>',T60,E12.4
*    ,/)

    DO 2 I=1,NSPH
    WRITE(3,103) I,CPO(I)
103  FORMAT(5X,'Concentration of Species',I3,' <gm/gm>',T60,E12.4)
2    CONTINUE
    RETURN

33   CONTINUE

    K=NR-1
    WRITE(3,104) K,ZRTEMP,ZRAG,ZRAL
104  FORMAT(/,15X,'Conditions at Outlet of Reactor # ',I3,/,
*    5X,'Temperature <Degrees C>',T60,E12.4,/,
*    5X,'Hydrogen Concentration (Gas Phase) <gm/cm**3>',T60,E12.4,/,
*    5X,'Hydrogen Concentration (Liquid Phase) <gm/cm**3>',T60,E12.4
*    ,/)
    DO 3 I=1,NSPR
    WRITE(3,105) I,CPO(I)
105  FORMAT(5X,'Concentration of Species',I3,' <gm/gm>',T60,E12.4)
3    CONTINUE

```

RETURN

```
34  CONTINUE
    IF(NR.NE.1) GO TO 35
    WRITE(3,106)
106  FORMAT('1',25X,'COST ESTIMATES',/)
    WRITE(3,107) PCCOST,POCOST,PM COST,PFCOST,PVCOST
107  FORMAT(15X,'PREHEATER',/,
    * 5X,'Capital Cost <$>',T60,E12.4,/,
    * 5X,'Operating Cost <$ /YR>',T60,E12.4,/,
    * 5X,'Maintenance Cost <$ /YR>',T60,E12.4,/,
    * 5X,'Fixed Cost <$ /YR>',T60,E12.4,/,
    * 5X,'Variable Cost <$ /YR>',T60,E12.4,/)
    RETURN

35  K=NR-1
    WRITE(3,108) K,RCCOST,RO COST,RM COST,RFCOST,RVCOST
108  FORMAT(15X,'REACTOR # ',I3,/,
    * 5X,'Capital Cost <$>',T60,E12.4,/,
    * 5X,'Operating Cost <$ /YR>',T60,E12.4,/,
    * 5X,'Maintenance Cost <$ /YR>',T60,E12.4,/,
    * 5X,'Fixed Cost <$ /YR>',T60,E12.4,/,
    * 5X,'Variable Cost <$ /YR>',T60,E12.4,/)
    IF(NR.EQ.N) WRITE(3,200)
    CALL STEADY
    RETURN
    END
```

SUBROUTINE COST(NR)

C ....CALCULATE COSTS OF PREHEATER/REACTORS

IMPLICIT REAL\*8(A-H,O-Z)  
DOUBLE PRECISION L

DIMENSION VG(5),VL(5),L(5),D(5)  
DIMENSION GAMMA(5),GAMS(5),GAMR(5),RL(5),RP(5)  
DIMENSION FLUX(5),HT(5),ALFA(5)

COMMON/A/ VG,VL,L,D  
COMMON/B/ TIL,HIL,CGI,AGPI,ALPI,TEMPI,TEMW  
COMMON/DDD/ DHSTAR,ESTAR,GAMMA,GAMS,GAMR,RL,RP,  
\* FLUX,HT,ALFA  
COMMON/QT/ QT  
COMMON/COST1/ PCCOST,POCOST,PM COST,PFCOST,PVCOST,RCCOST,RO COST  
\* ,RM COST,RFCOST,RVCOST

```

IF(NR.NE.1) GO TO 33
PCCOST=5.0E+05*(3.142/4.0*D(1)**2*L(1)/13.0)**0.6
PMCCOST=0.03*PCCOST*(0.5+0.5*(300.0/365.0))
PFCOST=0.03*PCCOST*0.5
PVCOST=(QT*FLUX(1)*TIL*3.142*D(1)*L(1))/0.8*3600.0*24.0*300.0
* /(252.0*1.0E+06)*5.0+0.03*PCCOST*0.5*(300.0/365.0)
POCOST=PFCOST+PVCOST
RETURN
33  CONTINUE

```

```

RCCOST=2.0E+06*(3.142*D(NR)**2*L(NR)/6400.0)**0.6
RMCOST=0.03*RCCOST*(0.5+0.5*(300.0/365.0))
RFCOST=0.03*RCCOST*0.5
RVCOST=0.03*RCCOST*0.5*(300.0/365.0)
ROCOST=RFCOST+RVCOST
RETURN
END

```

#### SUBROUTINE STEADY

```

C ... This subroutine determines whether the steady state in the
C reactor is stable or not. The analysis assumes the liquid phase
C in the reactor to be completely mixed.

```

```

IMPLICIT REAL*8(A-H,O-Z)

```

```

DIMENSION GAMMA(5),GAMS(5),GAMR(5),RL(5),RP(5)
DIMENSION AG(5),AL(5),TEMP(5),FLUX(5),HT(5),ALFA(5)

```

```

COMMON/B/ TIL,HIL,CGI,AGPI,ALPI,TEMPI,TEMW
COMMON/DD/ HBAR
COMMON/DDD/ DHSTAR,ESTAR,GAMMA,GAMS,GAMR,RL,RP,
* FLUX,HT,ALFA
COMMON/FF/ AG,AL,TEMP

```

```

H=HBAR*EXP(-DHSTAR/(1.0+TEMP(2)))
HPM=H*DHSTAR/(1.0+TEMP(2))**2.
TER=1.-EXP(-H*RL(2)/HIL)

```

```

Y1=ESTAR*EXP(-ESTAR/(1.+TEMP(2)))/(1.+TEMP(2))**2
Y2=H*RL(2)*EXP(-H*RL(2)/HIL)*HPM/HIL

```

T1=1.0+RP(2)\*EXP(-ESTAR/(1.0+TEMP(2)))/GAMMA(2)

T2=TER/(H\*GAMMA(2))

T3=(T1+T2)\*AG(1)\*Y2/(GAMMA(2)\*HIL)

T4=AL(1)+AG(1)\*TER/(GAMMA(2)\*HIL)

T5=Y1\*RP(2)/GAMMA(2)+Y2/(H\*GAMMA(2))-TER/(GAMMA(2)\*H\*\*2.)

Y4=HBAR\*DHSTAR\*EXP(-DHSTAR/(1.0+TEMP(2)))/(1.0+TEMP(2))\*\*3

T6=T4\*T5\*Y4

T7=T3-T6

T8=1.0+RP(2)\*EXP(-ESTAR/(1.0+TEMP(2)))/GAMMA(2)+TER/(H\*GAMMA(2))

T8=T8\*(-2.)

Y3=T7\*T8

T9=RP(2)\*GAMR(2)\*AL(2)\*Y1+GAMS(2)\*Y2\*(H\*AG(1)/HIL-AL(2))/H+

\* (RP(2)\*GAMR(2)\*EXP(-ESTAR/(1.0+TEMP(2)))+GAMS(2)\*TER/H)\*Y3-

\* Y4\*GAMS(2)\*AL(2)/H\*\*2.

IF(T9.LT.1.0) RETURN

WRITE(6,100)

100 FORMAT(//,5X,'WARNING!! OPERATING CONDITIONS ARE SUCH THAT IF'

\* ,/5X,'LIQUID PHASE IN THE REACTOR WAS COMPLETELY MIXED

\* ,/5X,'THEN THE STEADY STATE LIES IN A REGION OF MULTIPLE

\* ,/5X,'STEADY STATES AND IS AN UNSTABLE STEADY STATE'//)

RETURN

END

PROGRAM FOR ESTIMATION OF KINETIC  
PARAMETERS (FIT.FOR)

```

C -----
C      PROGRAM TO OPTIMIZE KINETIC CONSTANTS FROM
C      EXISTING DATA
C -----

```

```

IMPLICIT REAL*8(A-H,O-Z)
REAL*4 ZXMN(20),ZMX(20),XCALC(20)
REAL*4 WORK,FMIN,H,G,W
EXTERNAL SIMUL
EXTERNAL SIMUL1
DIMENSION CPOUT(10),XCALC(20),XMIN(20),XMAX(20)
DIMENSION WORK(430),IW(20),H(210),G(20),W(60)
COMMON/FIT/XCALC,XMIN,XMAX,NTRIAL,NDATA,NVAR,CPOUT
COMMON/B/TIL,HIL,CGI,AGPI,ALPI,TEMPI,TEMW
COMMON/IND/IND
CALL INPUT(2,1)
CALL INPUT1(TIL,1)
DO 2 I=1,NVAR
  ZXMN(I)=XMIN(I)
  ZMX(I)=XMAX(I)
2  XCALC(I)=XCALC(I)
  IF(IND.EQ.1) GO TO 20
  GO TO 30
20  CALL ZXMIN(SIMUL,NVAR,6,100,0,ZXCALC,H,G,FMIN,W,IER)

  GO TO 40
30  CALL ZXMIN(SIMUL1,NVAR,6,100,0,ZXCALC,H,G,FMIN,W,IER)

40  CONTINUE
  WRITE(6,200)
200  FORMAT(' JOB DONE')
  CALL EXIT
  END

```

```

SUBROUTINE SIMUL1(N,X,FMIN)
IMPLICIT REAL*8(A-H,O-Z)
REAL*4 X,FMIN
DIMENSION C(10,101),RATE(10),CPOUT(10)
DIMENSION XCALC(20),XMIN(20),XMAX(20)
DIMENSION X(20)

```



```

COMMON/B/TIL,HIL,CGI,AGPI,ALPI,TEMPI,TEMW
COMMON/Z6/NSP
COMMON/FIT/XCALC,XMIN,XMAX,NTRIAL,NDATA,NVAR,CPOUT
COMMON/Z3/C,RATE,ICOUNT
DO 3 I=1,N
3   XCALC(I)=X(I)
   NVAR=N
   WRITE(6,50)
50  FORMAT(//,5X,'PARAMETER VALUES',/)
   WRITE(6,51)(X(I),I=1,N)
51  FORMAT(5X,E12.5)

FMIN=0.
OPEN(UNIT=2,FILE='FIT02.DAT')
DO 1 I=1,NDATA
CALL INPUT(2,2)
CALL INPUT1(TIL,2)
CALL PHEATR
CALL PHEATC
CALL REACTC
DO 2 J=1,NSP
WRITE(6,*) C(J,ICOUNT)
2   FMIN=FMIN+(C(J,ICOUNT)-CPOUT(J))**2
1   CONTINUE
CLOSE(UNIT=2)
WRITE(6,52)FMIN
52  FORMAT(' FMIN=', E12.5)
RETURN
END

```

```

SUBROUTINE SIMUL(N,X,FMIN)
IMPLICIT REAL*8(A-H,O-Z)
REAL*4 X,FMIN
EXTERNAL FCN
DIMENSION C(10,101),RATE(10),CPOUT(10),CTEMP(1)
DIMENSION XCALC(20),XMIN(20),XMAX(20)
DIMENSION X(20),Y(3),F(3),AG(2),AL(2),TEMP(2)
COMMON/B/TIL,HIL,CGI,AGPI,ALPI,TEMPI,TEMW
COMMON/Z6/NSP
COMMON/FIT/XCALC,XMIN,XMAX,NTRIAL,NDATA,NVAR,CPOUT
COMMON/Z3/C,RATE,ICOUNT
COMMON/TEMP/CTEMP
COMMON/FF/AG,AL,TEMP

```

```

DO 31 I=1,N
31  XCALC(I)=X(I)

```

```

NVAR=N
WRITE(6,50)
50  FORMAT(//,5X,'PARAMETER VALUES',/)
WRITE(6,51)(X(I),I=1,N)
51  FORMAT(5X,E12.5)

FMIN=0.
OPEN(UNIT=2,FILE='FIT02.DAT')
DO 1 K=1,NDATA
CALL INPUT(2,2)
CALL INPUT1(TIL,2)
CALL PHEATR
CALL PHEATC
Y(1)=AL(1)*.6
Y(2)=TEMP(1)*2.
CALL NLSYST(FCN,2,100,Y,F,.01,1.0E-4,1.0E-4,I)
CTEMP(1)=Y(2)
CALL CSTR
DO 2 J=1,NSP
WRITE(6,*) C(J,1)
2  FMIN=FMIN+(C(J,1)-CPOUT(J))**2
WRITE(6,52) FMIN
1  CONTINUE
CLOSE(UNIT=2)
52  FORMAT(' FMIN=', E12.5)
RETURN
END

```

#### SUBROUTINE PHEATR

```

IMPLICIT REAL *8(A-H,O-Z)
INTEGER RUNGE
DOUBLE PRECISION L
DIMENSION VG(2),VL(2),L(2),D(2)
DIMENSION GAMMA(2),GAMS(2),GAMR(2),
* FLUX(2),HT(2),ALFA(2)
DIMENSION RL(2),RP(2),PEL(2),PEH(2)
DIMENSION AG(2),AL(2),TEMP(2)
DIMENSION Y(3),F(3)
DIMENSION PAG(101),PAL(101),PTEMP(101)

COMMON /A/ VG,VL,L,D
COMMON /B/ TIL,HIL,CGI,AGPI,ALPI,TEMPI,TEMW
COMMON/DD/ HBAR
COMMON /DDD/ DHSTAR,ESTAR, GAMMA,GAMS,GAMR,RL,RP
* ,FLUX,HT,ALFA
COMMON /FF/ AG,AL,TEMP

```

COMMON/Z15/ TEMPA,AGPA,ALPA,TEMPO,AGPO,ALPO

X=0.0  
Y(1)=AGPI  
Y(2)=ALPI  
Y(3)=TEMPI

C

TEMPA=TIL\*(1.0+TEMPI)  
AGPA=CGI\*AGPI  
ALPA=CGI\*HIL\*ALPI  
ICOUNT=1  
PAG(ICOUNT)=Y(1)  
PAL(ICOUNT)=Y(2)  
PTEMP(ICOUNT)=Y(3)  
ZX=X\*L(1)  
ZPAG=PAG(ICOUNT)\*CGI  
ZPAL=PAL(ICOUNT)\*CGI\*HIL  
ZPTEMP=PTEMP(ICOUNT)\*TIL+TIL-273.0  
HH=0.01.

10 K=RUNGE(3,Y,F,X,HH)  
IF(K.NE.1) GO TO 15  
H=HBAR\*EXP(-DHSTAR/(1+Y(3)))  
TEMPP=Y(3)  
ZMEW=VISCOS(TEMPP)  
F(1)=-RL(1)\*(H\*Y(1)/HIL-Y(2))  
F(2)=-F(1)/(GAMMA(1)\*HIL-RP(1)\*(EXP(-ESTAR/(1.0+Y(3))))\*Y(2)  
\* /GAMMA(1)  
F(3)=ALFA(1)\*ZMEW\*\*(-0.47)\*  
\* (TEMW-Y(3))+HIL\*RP(1)\*GAMR(1)\*EXP(-ESTAR/(1+Y(3)))\*Y(2)  
\* +RL(1)\*GAMS(1)\*(H\*Y(1)/HIL-Y(2))  
GO TO 10  
15 CONTINUE  
ICOUNT=ICOUNT+1  
PAG(ICOUNT)=Y(1)  
PAL(ICOUNT)=Y(2)  
PTEMP(ICOUNT)=Y(3)  
ZX=X\*L(1)  
ZPAG=PAG(ICOUNT)\*CGI  
ZPAL=PAL(ICOUNT)\*CGI\*HIL  
ZPTEMP=PTEMP(ICOUNT)\*TIL+TIL-273.0  
IF(X.GE.1.0) GO TO 16  
GO TO 10  
16 CONTINUE  
AG(1)=Y(1)  
AL(1)=Y(2)

```

TEMP(1)=Y(3)
TEMPO=TIL*(1.0+Y(3))
AGPO=CGI*Y(1)
ALPO=CGI*HIL*Y(2)
RETURN
END

```

FUNCTION REACTR(ALR)

```

IMPLICIT REAL *8(A-H,O-Z)
INTEGER RUNGE
DIMENSION Y(5),F(5)
DIMENSION XX(101),RAG(101),RAL(101),RTEMP(101)
DIMENSION GAMMA(2),GAMS(2),GAMR(2),
* FLUX(2),HT(2),ALFA(2)
DIMENSION RL(2),RP(2),PEL(2),PEH(2)
DIMENSION AG(2),AL(2),TEMP(2)

COMMON /B/ TIL,HIL,CGI,AGPI,ALPI,TEMPI,TEMW
COMMON /DUM/ XX,RAG,RAL,RTEMP
COMMON /NUM/ ICOUNT
COMMON/DD/ HBAR
COMMON /DDD/ DHSTAR,ESTAR, GAMMA,GAMS,GAMR,RL,RP
* ,FLUX,HT,ALFA
COMMON /FF/ AG,AL,TEMP
COMMON /REACT/ AGRI,ALRI,DALRI,TEMPRI,DTEMPI
COMMON /REACT1/ DTEMP,DALR
COMMON /REACT2/ MM,J
COMMON/Z9/PEL,PEH

ICOUNT=1
X=0.0
ALRI=ALR
DALRI=(ALR-AL(J))*PEL(MM)
Y(1)=AGRI
Y(2)=ALR
Y(3)=DALRI
Y(4)=TEMPRI
Y(5)=DTEMPI
XX(ICOUNT)=X
RAG(ICOUNT)=Y(1)
RAL(ICOUNT)=Y(2)

```

```

      RTEMP(ICOUNT)=Y(4)
      HH=0.01
10    K=RUNGE(5,Y,F,X,HH)
      IF(K.NE.1) GO TO 15
      H=HBAR*EXP(-DHSTAR/(1+Y(4)))
      F(1)=-RL(MM)*(H*Y(1)/HIL-Y(2))
      F(2)=Y(3)
      F(3)=(Y(3)+F(1)/(GAMMA(MM)*HIL)+RP(MM)/GAMMA(MM)*(EXP(-ESTAR/
* (1.0+Y(4))))*Y(2))*PEL(MM)
      F(4)=Y(5)
      F(5)=(Y(5)-(RL(MM)*GAMS(MM)*(H/HIL*Y(1)-Y(2)))
* -HIL*RP(MM)*GAMR(MM)*EXP(-ESTAR/(1.0+Y(4)))*Y(2))*PEH(MM)
      GO TO 10
15    CONTINUE
      ICOUNT=ICOUNT+1
      XX(ICOUNT)=X
      RAG(ICOUNT)=Y(1)
      RAL(ICOUNT)=Y(2)
      RTEMP(ICOUNT)=Y(4)
      IF(X.GE.1.0) GO TO 16
      GO TO 10
16    CONTINUE
      AG(MM)=Y(1)
      AL(MM)=Y(2)
      DALR=Y(3)
      TEMP(MM)=Y(4)
      DTEMP=Y(5)
      REACTR=DALR
      RETURN
      END

```

FUNCTION RUNGE(N,Y,F,X,H)

```

      IMPLICIT REAL *8(A-H,O-Z)
      INTEGER RUNGE
      DIMENSION PHI(50),SAVEY(50),Y(20),F(20)
      DATA M /0/
      M=M+1
      GO TO (1,2,3,4,5),M
1    RUNGE=1
      RETURN
2    DO 22 J=1,N
      SAVEY(J)=Y(J)
      PHI(J)=F(J)

```

```

22  Y(J)=SAVEY(J)+0.5*H*F(J)
    X=X+0.5*H
    RUNGE=1
    RETURN
3   DO 33 J=1,N
    PHI(J)=PHI(J)+2.0*F(J)
33  Y(J)=SAVEY(J)+0.5*H*F(J)
    RUNGE=1
    RETURN
4   DO 44 J=1,N
    PHI(J)=PHI(J)+2.0*F(J)
44  Y(J)=SAVEY(J)+H*F(J)
    X=X+0.5*H
    RUNGE=1
    RETURN
5   DO 55 J=1,N
55  Y(J)=SAVEY(J)+(PHI(J)+F(J))*H/6.0
    M=0
    RUNGE=0
    RETURN
    END

```

```

SUBROUTINE HYDRO(N)
IMPLICIT REAL *8(A-H,O-Z)
EXTERNAL FEG
DOUBLE PRECISION L
DIMENSION VG(2),VL(2),L(2),D(2)
DIMENSION ZKLA(2),EG(2),PL(2),PH(2)
COMMON /A/ VG,VL,L,D
COMMON /B/ TIL,HIL,CGI,AGPI,ALPI,TEMPI,TEMW
COMMON /C/ RHO,RHOA,RHOG,DI,SIG,R,G
COMMON /D/ CPG,CPBAR,E,DHR,DHS,ZKBAR
COMMON /E/ ZKLA,EG
COMMON /INT/ EEG,DEG
COMMON /INT1/ ERR
COMMON /HYD/BO,ZNO,FR
COMMON/Z9/PL,PH

```

```

DO 10 I=1,N
V=VG(I)
DC=D(I)
ZMEW=VISCOS(TEMPI)
BO=((DC**2.0)*G*RHOA)/SIG
FR=V/(G*DC)**0.5

```

```

SC=ZMEW/RHOA/DI
ZNO=(G*DC**3.0)*((RHOA/ZMEW)**2.0)
EEG=0.2
DEG=0.025
ERR=1.0E-04
CALL INTAL(FEG)
EG(I)=EEG
ZKLA(I)=(0.6*DI/DC**2.0)*(SC**0.5)*(BO**0.62)*
* (ZNO**0.31)*(EG(I)**1.1)
PL(I)=(13.0*FR*(L(I)/D(I))*(VL(I)/VG(I)))
* /(1.0+8.0*FR**0.85)
PH(I)=(RHO*VG(I)*CPG+RHOA*CPBAR*VL(I))
* /(RHOA*CPBAR*VL(I)/PL(I))
10  CONTINUE
RETURN
END

```

FUNCTION VISCOS(TEMP)

```

IMPLICIT REAL *8(A-H,O-Z)
DOUBLE PRECISION M
COMMON/B/ TIL

```

```

A=-1.608
B=9.8578E+11
M=4.773
ATEMP=TEMP*TIL+TIL
IF(ATEMP.GE.550.0.AND.ATEMP.LE.675.0) GO TO 2
ZMU=10.0**((A+B/ATEMP**M))
GO TO 3
2  ZMU=0.14
3  CONTINUE
VISCOS=ZMU
RETURN
END

```

```

SUBROUTINE INTAL(FUNC)
IMPLICIT REAL *8(A-H,O-Z)
EXTERNAL FEG,REACTR
COMMON /INT/ X,DX
COMMON /INT1/ ERR

```

```

      U=-1.0
      V=-1.0
1     F=FUNC(X)
      IF(ABS(F).LE.ERR) GO TO 2
      IF(F.GE.0.0) GO TO 3
      IF(V.LE.0.0) GO TO 4
      DX=DX/2.0
4     X=X+DX
      U=1.0
      GO TO 1
3     IF(U.LE.0.0) GO TO 5
      DX=DX/2.0
5     CONTINUE
      X=X-DX
      GO TO 1
2     CONTINUE
      RETURN
      END

```

```

SUBROUTINE INPUT(N,NTIME)
IMPLICIT REAL *8(A-H,O-Z)
DOUBLE PRECISION L
DIMENSION VG(2),VL(2),L(2),D(2)
DIMENSION GAMMA(2),GAMS(2),GAMR(2),
* FLUX(2),HT(2),ALFA(2),TIME(2)
DIMENSION RL(2),RP(2)
DIMENSION ZKLA(2),EG(2),PL(2),PH(2)

COMMON/Z9/ PL,PH
COMMON /A/ VG,VL,L,D
COMMON /B/ TIL,HIL,CGI,AGPI,ALPI,TEMPI,TEMW
COMMON /C/ RHO,RHOA,RHOG,DI,SIG,R,G
COMMON /D/ CPG,CPBAR,E,DHR,DHS,ZKBAR
COMMON/DD/ HBAR
COMMON /DDD/ DHSTAR,ESTAR, GAMMA,GAMS,GAMR,RL,RP
* ,FLUX,HT,ALFA
COMMON /E/ ZKLA,EG
COMMON/Z5/ TIME
COMMON/IND/IND

IF(NTIME.EQ.2)GO TO '100
OPEN(UNIT=1,FILE='FIT01.DAT')

```



```

READ(1,*) IND
READ(01,*) (L(I),I=1,N),(D(I),I=1,N)
READ(01,*) CPG,CPBAR,ZKBAR,E,DHR,DHS,HBAR,DI,SIG,RHOA
RETURN
100  CONTINUE
READ(2,*) VOLG,VOLL,TIL,P,FRAC,TH
TIL=TIL+273.0
TH=TH+273.0
RR=82.057
R=1.98
G=981.0
DO 10 I=1,N
VG(I)=VOLG/(D(I)**2.0*0.786)
VL(I)=VOLL/(D(I)**2.0*0.786)
10  CONTINUE

CGI=P/(RR*TIL)*FRAC*2.0
RHOG=CGI
AGPI=1.0
ALPI=0.0
TEMPI=0.0
TEMW=(TH-TIL)/TIL
DHSTAR=DHS/(R*TIL)
ESTAR=E/(R*TIL)
HIL=HBAR*(EXP(-DHSTAR))
CALL HYDRO(N)

DO 11 I=1,N
TIME(I)=L(I)*(1.-EG(I))/VL(I)
RL(I)=ZKLA(I)*L(I)*HIL/VG(I)
GAMMA(I)=VL(I)/VG(I)
RP(I)=ZKBAR*(1.-EG(I))*L(I)/VG(I)
FLUX(I)=VG(I)*RHOG*CPG+VL(I)*RHOA*CPBAR
GAMS(I)=(CGI*VG(I)*DHS)/TIL/FLUX(I)
GAMR(I)=(CGI*VG(I)*DHR)/TIL/FLUX(I)
BETA=0.0045
HT(I)=BETA*VL(I)**0.8/D(I)**0.2
ALFA(I)=HT(I)/D(I)*L(I)/FLUX(I)
11  CONTINUE
RETURN
END

```

```

FUNCTION FEG(X)
IMPLICIT REAL *8(A-H,O-Z)

```

```

COMMON /HYD/ BO,ZNO,FR
F1=X/((1.0-X)**4.0)
F2=0.2*(BO**0.125)*(ZNO**0.083)*FR
FEG=F1-F2
RETURN
END

```

C

```

SUBROUTINE REATEM(N)

IMPLICIT REAL *8(A-H,O-Z)
DOUBLE PRECISION L
EXTERNAL REACTR
DIMENSION AG(2),AL(2),TEMP(2),L(2),D(2),VG(2),VL(2)
DIMENSION XX(101),RAG(101),RAL(101),RTEMP(101)
DIMENSION ZKLA(2),EG(2),PL(2),PH(2),RRTEMP(101)
COMMON /A/ VG,VL,L,D
COMMON /B/ TIL,HIL,CGI,AGPI,ALPI,TEMPI,TEMW
COMMON /REACT/AGRI,ALRI,DALRI,TEMPRI,DTEMPRI
COMMON /DUM/ XX,RAG,RAL,RTEMP
COMMON /NUM/ ICOUNT
COMMON /REACT1/ DTEMP,DALR
COMMON /REACT2/ M,J
COMMON /INT/ ALR,DAL
COMMON /INT1/ ERR
COMMON /FF/ AG,AL,TEMP
COMMON /E/ ZKLA,EG
COMMON/Z8/ RRTEMP
COMMON/Z16/ ZRTEMP,ZRAG,ZRAL
COMMON/Z9/PL,PH
ERR= 0.01
DO 10 I=2,N
M=I
U=-1.0
V=-1.0
J=I-1
TEMPRI=TEMP(J)*1.5
DTEMPRI=(TEMPRI-TEMP(J))*PH(I)
DTMPI=0.1
AGRI=AG(J)
ALRI=AL(J)*0.9
ALR=ALRI
DAL=0.2
1 CONTINUE
CALL INTHAL(REACTR)

```

```

DAL=0.01
IF(ABS(DTEMP).LE.0.001) GO TO 2
IF(DTEMP.GE.0.0)GO TO 3
IF(V.LE.0.0)GO TO 4
ERR=0.0001
DTMPI=DTMPI/2.0
4  TEMPRI=TEMPRI+DTMPI
   DTEMPI=(TEMPRI-TEMP(J))*PH(I)
   U=1.0
   GO TO 1
3  IF(U.LE.0.0)GO TO 5
   ERR=0.0001
   DTMPI=DTMPI/2.0
5  TEMPRI=TEMPRI-DTMP
   DTEMPI=(TEMPRI-TEMP(J))*PH(I)
   GO TO 1
2  CONTINUE
   DO 23 II=1,ICOUNT
   RRTEMP(II)=RTEMP(I)
   ZX=XX(II)*L(2)
   ZRAG=RAG(II)*CGI
   ZRAL=RAL(II)*CGI*HIL
   ZRTEMP=RTEMP(II)*TIL+TIL-273.0
23 CONTINUE
10 CONTINUE
RETURN
END

```

```

SUBROUTINE INPUT1(TIL,NTIME)
IMPLICIT REAL *8(A-H,O-Z)
DOUBLE PRECISION K,KBAR,L,KBAR1,KBAR2
DIMENSION K(20,20),KBAR(20,20),EC(20,20),COEFF(20,20),CPI(10)
DIMENSION KBAR1(20,20),KBAR2(20,20),EC1(20,20),EC2(20,20)
DIMENSION CPOUT(10)
DIMENSION II(20),JJ(20),XCALC(20),XMIN(20),XMAX(20)
DIMENSION ECSTAR(20,20),PL(2),PH(2),VL(2),VG(2)
DIMENSION D(2),L(2),X(20),Y(20),TABLE(20,20)
CHARACTER*20 NAME(10)
COMMON/Z1/ KBAR,ECSTAR,COEFF
COMMON/Z2/ CPI
COMMON/Z6/ NSP
COMMON/FIT/XCALC,XMIN,XMAX,NTRIAL,NDATA,NVAR,CPOUT
COMMON/Z9/PL,PH
COMMON/A/VG,VL,L,D
COMMON/C/ RHO,RHOA,RHOG,DI,SIG,R,G
COMMON/D/CPG,CPBAR,E,DHR,DHS,ZKBAR

```

```
COMMON/PINT/ X,Y,TABLE,NDT,MNDT
COMMON/IND/IND
DATA R/1.98/
```

C  
C

```
IF(NTIME.EQ.2)GO TO 100
DO 1 I=1,20
DO 1 J=1,20
K(I,J)=0.0
KBAR(I,J)=0.0
EC(I,J)=0.0
COEFF(I,J)=0.0
CONTINUE
```

1  
C  
C

```
READ(01,*) NSP
DO 2 I=1,NSP
READ(01,102) NAME(I)
102  FORMAT(A20)
2    CONTINUE
READ(01,*) NK
DO 4 I=1,NK
READ(01,*) II(I)
READ(01,*) JJ(I)
READ(1,*)KBAR1(II(I),JJ(I)),KBAR2(II(I),JJ(I))
XMIN(2*I-1)=KBAR1(II(I),JJ(I))
XMAX(2*I-1)=KBAR2(II(I),JJ(I))
READ(1,*)EC1(II(I),JJ(I)),EC2(II(I),JJ(I))
XMIN(2*I)=EC1(II(I),JJ(I))
XMAX(2*I)=EC2(II(I),JJ(I))
XCALC(2*I-1)=(XMIN(2*I-1)+XMAX(2*I-1))/2.
XCALC(2*I)=(XMIN(2*I)+XMAX(2*I))/2.
COEFF(II(I),JJ(I))=1.0
4    CONTINUE
NVAR=2*NK
```

```
READ(1,*)NDATA
CLOSE(UNIT=1)
RETURN
```

100 CONTINUE

```
DO 250 I=1,NK
EC(II(I),JJ(I))=XCALC(2*I)
KBAR(II(I),JJ(I))=XCALC(2*I-1)
ECSTAR(II(I),JJ(I))=EC(II(I),JJ(I))/(R*TIL)
250 CONTINUE
DO 5 I=1,NSP
```

```

5  READ(02,*) CPI(I)
   CONTINUE
   DO 6 I=1,NSP
   READ(02,*) CPOUT(I)
6  CONTINUE
   IF(IND.EQ.1) RETURN
   READ(02,*) NDT
   DO 10 I=1,NDT
   READ(02,*) X(I),Y(I)
   X(I)=X(I)/L(2)
   Y(I)=Y(I)+273.
   Y(I)=(Y(I)-TIL)/TIL
10  CONTINUE
   MNDT=NDT-1
   CALL DTABLE(X,Y,TABLE,NDT,MNDT,TRUBL,20)
   IF(TRUBL.NE.0.0) CALL EXIT

   RETURN
   END

```

```

SUBROUTINE EQTNS(TEMP)
IMPLICIT REAL *8(A-H,O-Z)
DOUBLE PRECISION K,KBAR
DIMENSION K(20,20),KBAR(20,20),ECSTAR(20,20),RATE(10)
DIMENSION COEFF(20,20),TEMP(101)
DIMENSION C(10,101)
COMMON/Z1/ KBAR,ECSTAR,COEFF
COMMON/Z3/ C,RATE,ICOUNT
COMMON/Z6/ NSP

```

C  
C

```

DO 1 IJ=1,NSP
RATE(IJ)=0.0
DO 1 I=1,NSP
DO 1 J=1,NSP
IF(COEFF(I,J).EQ.0.0) GO TO 1
IF((IJ.NE.I).AND.(IJ.NE.J)) GO TO 1
K(I,J)=KBAR(I,J)*EXP(-ECSTAR(I,J)/(1.0+TEMP(ICOUNT)))
IF(IJ.EQ.I) RATE(IJ)=RATE(IJ)-COEFF(I,J)*K(I,J)*C(I,ICOUNT)
IF(IJ.EQ.J) RATE(IJ)=RATE(IJ)+COEFF(I,J)*K(I,J)*C(I,ICOUNT)
1  CONTINUE
   RETURN
   END

```

SUBROUTINE PHEATC

```

IMPLICIT REAL *8(A-H,O-Z)
INTEGER RUNGE
DIMENSION CPI(10),CPO(20),RATE(10),PTEMP(101),C(10,101),TIME(2)
DIMENSION Y(20),F(20),XX(101)
COMMON/Z2/ CPI
COMMON/Z3/ C,RATE,ICOUNT
COMMON/Z4/ PTEMP
COMMON/Z5/ TIME
COMMON/Z6/ NSP
COMMON/Z7/ CPO
COMMON/Z13/ XX

X=0.0
ICOUNT=1
XX(ICOUNT)=X
DO 25 I=1,NSP
Y(I)=CPI(I)
C(I,ICOUNT)=Y(I)
25  CONTINUE
HH=0.01
•
10  K=RUNGE(NSP,Y,F,X,HH)
IF(K.NE.1) GO TO 15
CALL EQTNS(PTEMP)
DO 26 I=1,NSP
F(I)=RATE(I)*TIME(1)
C(I,ICOUNT)=Y(I)
26  CONTINUE
GO TO 10
15  CONTINUE
ICOUNT=ICOUNT+1
XX(ICOUNT)=X
DO 27 I=1,NSP
C(I,ICOUNT)=Y(I)
27  CONTINUE
IF(X.GE.1.0) GO TO 16
GO TO 10
16  CONTINUE
DO 28 I=1,NSP
CPO(I)=Y(I)
CPO(I+NSP)=F(I)
28  CONTINUE
RETURN
END

SUBROUTINE REACTC

```

```

IMPLICIT REAL *8(A-H,O-Z)
INTEGER RUNGE
INTEGER ORDER
DIMENSION CPO(20),RATE(10),RTEMP(101),C(10,101),TIME(2)
DIMENSION Y(20),F(20),A(20,20),PEL(2),B(20),ZETA(20)
DIMENSION ORDER(20),GUESS(20,20),FACTOR(50),RRATE(10)
DIMENSION AA(20,20),XX(101),XD(20),YD(20),TABLE(20,20)
COMMON/Z7/ CPO
COMMON/Z13/ XX
COMMON/Z9/ PEL,PEH
COMMON/Z3/ C,RATE,ICOUNT
COMMON/Z8/ RTEMP
COMMON/Z5/ TIME
COMMON/Z6/ NSP
COMMON/PINT/XD,YD,TABLE,NDT,MNDT

```

```

ITEST=0
ICOUNT=1
X=0.0
XX(ICOUNT)=X
XARG=X
RTEMP(ICOUNT)=FNEWT(XD,YD,TABLE,NDT,MNDT,7,XARG,TRUBL,20)

```

```

DO 8 I=1,NSP
  B(I)=CPO(I)
  C(I,ICOUNT)=CPO(I)
  B(I+NSP)=0.0
8  CONTINUE
  CALL EQTNS(RTEMP)
  DO 90 J=1,NSP
    RRATE(J)=RATE(J)
90  CONTINUE
  HH=0.1
  NNSP=2*NSP
  SEED=1
  DO 1 I=1,NNSP
    ICOUNT=1
    X=0.0
    XX(ICOUNT)=X
    DO 20 J=1,NNSP
      FACTOR(J)=RAN(SEED)
20  CONTINUE
    DO 2 N=1,NSP
      Y(N)=CPO(N)*(1+(-1)**I*FACTOR(N)*0.2)
      Y(N+NSP)=RRATE(N)/ABS(RRATE(N))*(0.5*FACTOR(N+NSP))
2  CONTINUE
    DO 43 N=1,NSP

```

```

      A(N,I)=Y(N)-Y(N+NSP)/PEL(2)
      C(N,ICOUNT)=Y(N)
43    CONTINUE
      DO 6 J=1,NNSP
      GUESS(J,I)=Y(J)
6     CONTINUE

10    CONTINUE
      K=RUNGE(NNSP,Y,F,X,HH)
      IF(K.NE.1) GO TO 15
      XARG=X
      RTEMP(ICOUNT)=FNEWT(XD,YD,TABLE,NDT,MNDT,7,XARG,TRUBL,20)
      CALL EQTNS(RTEMP)
      DO 26 J=1,NSP
      F(J)=Y(J+NSP)
      F(J+NSP)=PEL(2)*(Y(J+NSP)-RATE(J)*TIME(2))
      C(J,ICOUNT)=Y(J)
26    CONTINUE
      GO TO 10
15    CONTINUE
      ICOUNT=ICOUNT+1
      XX(ICOUNT)=X
      DO 17 J=1,NSP
      C(J,ICOUNT)=Y(J)
17    CONTINUE
      IF(X.GE.1.0) GO TO 16
      GO TO 10
16    CONTINUE
      IF(ITEST.NE.0) GO TO 12
      DO 55 J=1,NSP
      A(NSP+J,I)=Y(NSP+J)
55    CONTINUE
1     CONTINUE
      DO 69 I1=1,NNSP
      DO 69 I2=1,NNSP
      AA(I1,I2)=A(I1,I2)
69    CONTINUE
      CALL LUDCMP(A,NNSP,NNSP,ORDER)
      CALL SOLVLU(A,B,ZETA,NNSP,NNSP,ORDER)
C
C
      DO 70 I1=1,NNSP
      BTOT=0.0
      DO 71 I2=1,NNSP
      BTOT=BTOT+AA(I1,I2)*ZETA(I2)
71    CONTINUE
70    CONTINUE
      ITEST=1

```



```

        ICOUNT=1
        X=0.0
        DO 7 J=1,NNSP
        Y(J)=0.0
        DO 7 I=1,NNSP
        Y(J)=Y(J)+ZETA(I)*GUESS(J,I)
7      CONTINUE
        DO 18 I=1,NSP
        C(I,ICOUNT)=Y(I)
18     CONTINUE
        GO TO 10
12     CONTINUE
        RETURN
        END

```

```

SUBROUTINE SOLVLU(LU,B,X,N,NDIM,ORDER)
  IMPLICIT REAL*8(A-H,O-Z)
  DOUBLE PRECISION LU(20,20)
  DIMENSION B(20),X(20)
  INTEGER ORDER(20)
  DO 10 I=1,N
  J=ORDER(I)
  X(I)=B(J)
10  CONTINUE
  X(1)=X(1)/LU(1,1)
  DO 50 IROW=2,N
  IM1=IROW-1
  SUM=0.
  DO 40 JCOL=1,IM1
  SUM=SUM+LU(IROW,JCOL)*X(JCOL)
40  CONTINUE
  X(IROW)=(X(IROW)-SUM)/LU(IROW,IROW)
50  CONTINUE
  DO 70 IROW=2,N
  NVBL=N-IROW+1
  SUM=0.
  NP1=NVBL+1
  DO 60 JCOL=NP1,N
  SUM=SUM+LU(NVBL,JCOL)*X(JCOL)
60  CONTINUE
  X(NVBL)=X(NVBL)-SUM
70  CONTINUE
  RETURN
  END

```

```

SUBROUTINE LUDCMP(A,N,NDIM,ORDER)

```

```

    IMPLICIT REAL*8(A-H,O-Z)
    DIMENSION A(20,20)
    INTEGER ORDER(20)
    DO 10 I=1,N
    ORDER (I)=I
10  CONTINUE
    CALL APVT(A, N, NDIM, ORDER,1)
    IF (ABS(A(1,1)) .LT. 1.E-20) GO TO 99
    DO 20 KCOL=2,N
    A(1,KCOL)=A(1,KCOL)/A(1,1)
20  CONTINUE
    NM1=N-1
    DO 80 JCOL=2,NM1
    JCOL1=JCOL
    JM1=JCOL-1
    DO 50 IROW=JCOL,N
    SUM=0.
    DO 40 KCOL=1,JM1
    SUM=SUM+A(IROW,KCOL)*A(KCOL,JCOL)
40  CONTINUE
    A(IROW,JCOL)= A(IROW,JCOL)-SUM
50  CONTINUE
    CALL APVT (A,N, NDIM,ORDER, JCOL1)
    IF (ABS(A(JCOL,JCOL)).LT. 1.E-20) GO TO 99
    JP1=JCOL+1
    DO 70 KCOL=JP1,N
    SUM=0.
    DO 60 IROW=1,JM1
    SUM=SUM+A(JCOL,IROW)*A(IROW,KCOL)
60  CONTINUE
    A(JCOL,KCOL) =(A(JCOL,KCOL)-SUM)/A(JCOL,JCOL)
70  CONTINUE
80  CONTINUE
    SUM=0
    DO 90 KCOL=1,NM1
    SUM=SUM+A(N,KCOL)*A(KCOL,N)
90  CONTINUE
    A(N,N)=A(N,N)-SUM
    RETURN
99  write (6,100)
100 FORMAT (1H0,60H VERY SMALL PIVOT ELEMENT INDICATES A NEARLY SINGU
+LAR MATRIX)
    RETURN
    END

```

```

SUBROUTINE APVT (A,N,NDIM,ORDER,JCOL)

```

```

    IMPLICIT REAL*8(A-H,O-Z)

```

```

    DIMENSION A(20,20)
    INTEGER ORDER(20)
    IPVT=JCOL
    BIG=ABS(A(JCOL,JCOL))
    JP1=JCOL+1
    DO 10 IROW=JP1,N
    ANEXT=ABS(A(IROW,JCOL))
    IF (ANEXT .LE. BIG) GO TO 10
    BIG=ANEXT
    IPVT=IROW
10  CONTINUE
    IF (IPVT .EQ. JCOL) GO TO 25
    DO 20 KCOL=1,N
    SAVE =A(JCOL,KCOL)
    A(JCOL,KCOL)=A(IPVT,KCOL)
    A(IPVT,KCOL)=SAVE
20  CONTINUE
    ISAVE=ORDER(JCOL)
    ORDER(JCOL)=ORDER(IPVT)
    ORDER(IPVT)=ISAVE
25  RETURN
    END

```

SUBROUTINE NLSYST (FCN, N, MAXIT, X, F, DELTA, XTOL, FTOL, I)

IMPLICIT REAL\*8(A-H,O-Z)

C THIS SUBROUTINE SOLVES A SYSTEM OF N NON-LINEAR EQUATIONS BY  
C NEWTON'S METHOD. THE PARTIAL DERIVATIVES OF THE FUNCTIONS  
C ARE ESTIMATED BY DIFFERENCE QUOTIENTS WHEN A VARIABLE IS PERTURBED  
C BY AN AMOUNT EQUAL TO DELTA (DELTA IS ADDED.) THIS IS DONE FOR EACH  
C VARIABLE IN EACH FUNCTION. INCREMENTS TO IMPROVE THE ESTIMATES  
C FOR THE X-VALUES ARE COMPUTED FROM A SYSTEM OF EQUATIONS USING  
C SUBROUTINE ELIM.

C PARAMETERS ARE

C FCN SUBROUTINE THAT COMPUTES VALUES OF THE FUNCTIONS. MUST  
C BE DECLARED EXTERNAL IN THE CALLING PROGRAM  
C N THE NUMBER OF EQUATIONS  
C MAXIT LIMIT TO THE NUMBER OF ITERATIONS THAT WILL BE USED  
C X ARRAY TO HOLD X VALUES. INITIALLY THIS ARRAY HOLDS THE  
C INITIAL GUESSES. IT RETURNS THE FINAL VALUES.  
C F AN ARRAY THAT HOLDS VALUES OF THE FUNCTIONS  
C DELTA A SMALL VALUE USED TO PERTURB THE X VALUES SO PARTIAL  
C DERIVATIVES CAN BE COMPUTED BY DIFFERENCE QUOTIENT  
C XTOL TOLERANCE VALUE FOR CHANGE IN X VALUES TO STOP  
C ITERATIONS. WHEN THE LARGEST CHANGE IN ANY X MEETS  
C XTOL, THE SUBROUTINE TERMINATES.  
C FTOL TOLERANCE VALUE ON F TO TERMINATE. WHEN THE LARGEST F

```

C          VALUE IS LESS THAN FTOL, SUBROUTINE TERMINATES.
C      I    RETURNS VALUES TO INDICATE HOW THE ROUTINE TERMINATED.
C          I = 1    XTOL WAS MET
C          I = 2    FTOL WAS MET
C          I = -1    MAXIT EXCEEDED BUT TOLERANCES NOT MET
C          I = -2    VERY SMALL PIVOT ENCOUNTERED IN GAUSSIAN
C                  ELIMINATION STEP. NO RESULTS OBTAINED
C          I = -3    INCORRECT VALUE OF N WAS SUPPLIED. N MUST BE
C                  BETWEEN 2 AND 10

          DIMENSION X(N), F(N), A(10,11), XSAVE(10), FSAVE(10)
          LOGICAL PRINT
C CHECK VALIDITY OF VALUE OF N
          IF (N .LT. 2 .OR. N .GT. 10) GO TO 999
          PRINT = .TRUE.
          IF (I.NE. 0) PRINT = .FALSE.
C BEGIN ITERATIONS
C SAVE X VALUES, THEN GET F VALUES
          NP = N + 1
          IDT=0
          DO 100 IT = 1,MAXIT
              DO 10 IVBL = 1, N
                  XSAVE(IVBL) = X(IVBL)
10          CONTINUE
              CALL FCN (X, F)
C TEST F VALUES AND SAVE THEM
              ITEST = 0
              DO 20 IFCN = 1,N
                  IF (ABS(F(IFCN)) .GT. FTOL) ITEST = ITEST + 1
                  FSAVE(IFCN) = F(IFCN)
20          CONTINUE
C PRINT CURRENT VALUES IF PRINT IS .TRUE.
              IF (.NOT. PRINT) GO TO 30
                  WRITE(6,1000) IT, X
1000          FORMAT (1H0, 23HAFTER ITERATION NUMBER , I3,
+                  19H X AND F VALUES ARE / 1H0, 10F13.5)
                  WRITE (6,1001) F
1001          FORMAT (1H0, 10F13.5)
C SEE IF FTOL IS MET. IF NOT, CONTINUE. IF SO, SET I = 2 AND RETURN.
30          IF (ITEST .NE. 0) GO TO 35
              I = 2
              RETURN
C THIS DOUBLE LOOP COMPUTES THE PARTIAL DERIVATIVES OF EACH FUNCTION
C FOR EACH VARIABLE AND STORES THEM IN A COEFFICIENT ARRAY
35          DO 50 JCOL = 1,N
              X(JCOL) = XSAVE(JCOL) + DELTA
              CALL FCN (X, F)
              DO 40 IROW = 1,N

```

```

      A(IROW,JCOL) = (F(IROW) - FSAVE(IROW))/DELTA
40      CONTINUE
C  RESET X VALUES FOR NEXT COLUMN OF PARTIALS
      X(JCOL) = XSAVE(JCOL)
50      CONTINUE
C  NOW WE PUT NEGATIVE OF F VALUES AS RIGHT HAND SIDES AND CALL ELIM
      DO 60 IROW = 1,N
        A(IROW,NP) = -FSAVE(IROW)
60      CONTINUE
      CALL ELIM ( A,N,NP,10 )
C  BE SURE THAT COEFFICIENT MATRIX NOT TOO ILL-CONDITIONED
      DO 70 IROW = 1,N
        IF (ABS(A(IROW,IROW)) .LE. 1.E-5) GO TO 998
70      CONTINUE
C  APPLY THE CORRECTIONS TO THE X VALUES, ALSO SEE IF XTOL IS MET.
      ITEST = 0
      DO 80 IVBL = 1,N
        X(IVBL) = XSAVE(IVBL) + A(IVBL,NP)
        IF (ABS(A(IVBL,NP)) .GT. XTOL) ITEST = ITEST + 1
80      CONTINUE
C  IF XTOL IS MET, PRINT LAST VALUES AND RETURN, ELSE DO
C  ANOTHER ITERATION
      IF (ITEST .EQ. 0) GO TO 997
100     CONTINUE
C  WHEN WE HAVE DONE MAXIT ITERATIONS, SET I = -1 AND RETURN
      I = -1
      RETURN
C  WE COME HERE WHEN XTOL IS MET. PRINT LAST VALUES, SET I = 1, RETURN
997     I = 1
      IF (.NOT. PRINT) GO TO 110
110     RETURN
C  WE COME HERE WHEN PARTIALS FORM A NEARLY SINGULAR MATRIX. SET I = -2
C  PRINT MESSAGE, RETURN
998     I = -2
      WRITE (6,1003)
1003    FORMAT (1H0, 44HCANNOT SOLVE SYSTEM. MATRIX NEARLY SINGULAR )
      RETURN
C  WE COME HERE WHEN NUMBER OF EQUATIONS PASSED TO NLSYST IS INVALID.
C  PRINT MESSAGE, RETURN
999     I = -3
      WRITE (6,1004) N
1004    FORMAT (1H0, 81HNUMBER OF EQUATIONS PASSED TO NLSYST IS INVALID.
      + MUST BE 1 < N < 11. VALUE WAS , I3)
      RETURN
      END

```

SUBROUTINE ELIM (AB,N,NP,NDIM)

IMPLICIT REAL\*8(A-H,O-Z)

DIMENSION AB(NDIM,NP)

C THIS SUBROUTINE SOLVES A SET OF LINEAR EQUATIONS  
C THE GUASS ELIMINATION METHOD IS USED  
C MULTIPLE RIGHT HAND SIDES ARE PERMITTED, THEY SHOULD BE SUPPLIED  
C AS COLUMNS THAT AUGMENT THE COEFFICIENT MATRIX.  
C PARAMETERS ARE -

C AB COEFFICIENT MATRIX AUGMENTED WITH R.H.S. VECTORS  
C N NUMBER OF EQUATIONS  
C NP TOTAL NUMBER OF COLUMNS IN THE AUGMENTED MATRIX  
C NDIM FIRST DIMENSION OF MATRIX AB IN THE CALLING PROGRAM.  
C THE SOLUTION VECTOR(S) ARE RETURNED IN THE AUGMENTATION  
C COLUMNS OF AB.  
C BEGIN THE REDUCTION

NM1=N-1

DO 35 I=1,NM1

C FIND THE ROW NUMBER OF THE PIVOT ROW, WE WILL THEN  
C INTERCHANGE ROWS TO PUT THE PIVOT ELEMENT ON THE DIAGONAL.

IPVT=I

IP1=I+1

DO 10 J=IP1,N

IF(ABS(AB(IPVT,I)) .LT. ABS(AB(J,I))) IPVT=J

10 CONTINUE

C CHECK THE PIVOT ELEMENT TO BE SURE THAT IT IS NOT TOO SMALL, IF SO  
C PRINT A MESSAGE AND RETURN

IF ((ABS(AB(IPVT,I)) .LT. 1.E-5)) GO TO 99

C NOW INTERCHANGE, EXCEPT IF THE PIVOT ELEMENT IS ALREADY ON  
C THE DIAGONAL, DON'T NEED TO.

IF (IPVT.EQ.I) GO TO 25

DO 20 JCOL=I,NP

SAVE=AB(I,JCOL)

AB(I,JCOL)=AB(IPVT,JCOL)

AB(IPVT,JCOL)=SAVE

20 CONTINUE

C NOW REDUCE ALL ELEMENTS BELOW THE DIAGONAL IN THE I-TH ROW.  
C CHECK FIRST TO SEE IF A ZERO IS ALREADY PRESENT. IF SO  
C CAN SKIP REDUCTION FOR THAT ROW

25 DO 32 JROW=IP1,N

IF (AB(JROW,I) .EQ. 0) GO TO 32

RATIO=AB(JROW,I)/AB(I,I)

DO 30 KCOL=IP1,NP

AB(JROW,KCOL)=AB(JROW,KCOL) - RATIO\*AB(I,KCOL)

30 CONTINUE

32 CONTINUE

35 CONTINUE

C WE STILL NEED TO CHECK A(N,N) FOR SIZE.

IF (ABS(AB(N,N)) .LT. 1.E-5) GO TO 99

C NOW WE BACK SUBSTITUTE.

```
NP1=N+1
DO 50 KCOL=NP1,NP
  AB(N,KCOL)=AB(N,KCOL)/AB(N,N)
  DO 45 J=2,N
    NVBL=NP1-J
    L=NVBL+1
    VALUE=AB(NVBL,KCOL)
    DO 40 K=L,N
      VALUE=VALUE-AB(NVBL,K)*AB(K,KCOL)
40    CONTINUE
    AB(NVBL,KCOL)=VALUE/AB(NVBL,NVBL)
45    CONTINUE
50    CONTINUE
  RETURN
C MESSAGE FOR A SINGULAR MATRIX
99  WRITE (6,100)
100 FORMAT(1H0, 57HSOLUTION NOT FEASIBLE. A NEAR ZERO PIVOT WAS ENCOUN
+TRED. )
  RETURN
END
```

SUBROUTINE FCN(X,F)

```
IMPLICIT REAL*8(A-H,O-Z)
DIMENSION X(10),F(10),GAMMA(2),GAMS(2),GAMR(2),FLUX(2),HT(2),
*   ALFA(2),RL(2),RP(2)
DIMENSION AG(2),AL(2),TEMP(2)

COMMON/DD/HBAR
COMMON/FF/AG,AL,TEMP
COMMON/DDD/ DHSTAR,ESTAR,GAMMA,GAMS,GAMR,RL,RP,
*   FLUX,HT,ALFA
COMMON/B/TIL,HIL,CGI,AGPI,ALPI,TEMPI,TEMW
COMMON/IDT/IDT

H=HBAR*EXP(-DHSTAR/(1.+X(2)))
T1=(H*AG(1)/HIL-X(1))*(1.0-EXP(-RL(2)*H/HIL))
T2=EXP(-ESTAR/(1.+X(2)))

F(1)=AL(1)-X(1)-RP(2)*T2*X(1)/GAMMA(2)
* +T1/(H*GAMMA(2))
F(2)=X(2)-TEMP(1)-GAMR(2)*RP(2)*T2*X(1)*HIL-
* GAMS(2)*T1*HIL/H
```

```
C10  H=HBAR*EXP(-DHSTAR/(1.+X(3)))
C    F(1)=X(1)-AG(1)+RL(2)*(H*X(1)/HIL-X(2))
```

```

C      F(2)=AL(1)-X(2)+RL(2)*(H*X(1)/HIL-X(2))/(GAMMA(2)*HIL)
C      *      -RP(2)*EXP(-ESTAR/(1.+X(3)))*X(2)/GAMMA(2)
C      F(3)=TEMP(1)-X(3)+RL(2)*GAMS(2)*(H*X(1)/HIL-X(2))
C      *      +RP(2)*GAMR(2)*HIL*EXP(-ESTAR/(1.+X(3)))*X(2)

```

```

      RETURN
      END

```

```

      SUBROUTINE CSTR

```

```

      IMPLICIT REAL*8(A-H,O-Z)
      DIMENSION CPO(20),RATE(10),C(10,101),TIME(2),TEMP(1)
      DIMENSION XOLD(10),FOLD(10)
      COMMON/Z3/ C,RATE,ICOUNT
      COMMON/Z5/TIME
      COMMON/Z6/NSP
      COMMON/Z7/CPO
      COMMON/TEMP/TEMP

```

```

      ICOUNT=1
C      DELC=.0001
      SEED=1.
      DO 10 I=1,NSP
10      C(I,ICOUNT)=CPO(I)*RAN(SEED)

```

```

      DO 11 I=1,NSP
      XL=1.0E-6
      XR=1.0
      C(I,ICOUNT)=XL
      CALL EQTNS(TEMP)
      FXL=CPO(I)-XL+RATE(I)*TIME(2)
      C(I,ICOUNT)=XR
      CALL EQTNS(TEMP)
      FXR=CPO(I)-XR+RATE(I)*TIME(2)

```

```

      IF (FXL*FXR) 5,3,2
2      WRITE(6,201)
      RETURN

```

```

3      ITER=1
      IF(FXL.NE.0.) GO TO 4
      C(I,ICOUNT)=XL
      FX2=0.0
      GO TO 11
4      C(I,ICOUNT)=XR
      FX2=0.0
      GO TO 11

```



```

5   DO 7 ITER=1,100
    C(I,ICOUNT)=(XL*FXR-XR*FXL)/(FXR-FXL)
    CALL EQTNS(TEMP)
    FX2=CPO(I)-C(I,ICOUNT)+RATE(I)*TIME(2)

    IF(ABS(FX2).LE.1.0E-4) GO TO 11

    IF(FX2*FXL.LT.0.) GO TO 6
    XL=X2
    FXL=FX2

    GO TO 7
6   XR=X2
    FXR=FX2
7   CONTINUE
    WRITE(6,202)

11  CONTINUE

201  FORMAT(5X,'NO POSSIBLE ROOT ON STARTING INTERVAL')
202  FORMAT(5X,'NO CONVERGENCE OBTAINED IN CSTR')

```

```

RETURN
END

```

```

SUBROUTINE DTABLE (X,Y,TABLE,N,M,TRUBL,K)
IMPLICIT REAL*8(A-H,O-Z)
DIMENSION X(N),Y(N),TABLE(K,K)
IF(M.LT.N) GO TO 2
TRUBL=1.0
RETURN

```

```

2   NM1=N-1
    DO 3 I=1,NM1
3   TABLE(I,1)=(Y(I+1)-Y(I))/(X(I+1)-X(I))
    IF(M.LE.1) GO TO 6

    DO 5 J=2,M
    DO 5 I=J,NM1
    ISUB=I+1-J
5   TABLE(I,J)=(TABLE(I,J-1)-TABLE(I-1,J-1))/(X(I+1)-X(ISUB))

6   TRUBL=0.0
    RETURN
END

```

```

FUNCTION FNEWT(X,Y,TABLE,N,M,IDEG,XARG,TRUBL,K)

```

```

      IMPLICIT REAL*8(A-H,O-Z)
      DIMENSION X(N),Y(N),TABLE(K,K)
      IF(IDEG.LE.M) GO TO 2
      TRUBL=1.0
      FNEWT=0.0
      RETURN

2     DO 4 I=1,N
      IF(I.EQ.N.OR.XARG.LE.X(I)) GO TO 5
4     CONTINUE
5     MAX=I+IDEG/2

      IF(MAX.LE.IDEG) MAX=IDEG+1
      IF(MAX.GT.N) MAX=N

      YEST=TABLE(MAX-1,IDEG)
      IF(IDEG.LE.1) GO TO 13
      IDEGM1=IDEG-1
      DO 12 I=1,IDEGM1
      ISUB1=MAX-I
      ISUB2=IDEG-I
12     YEST=YEST*(XARG-X(ISUB1))+TABLE(ISUB1-1,ISUB2)
13     ISUB1=MAX-IDEG
      TRUBL=0.0
      FNEWT=YEST*(XARG-X(ISUB1))+Y(ISUB1)

      RETURN
      END

```

PROGRAM TO INPUT DATA TO  
SIMULATOR (SIMDAT.FOR)

```

C -----
C      PROGRAM FOR CREATING INPUT DATA FILE FOR SIMULATOR
C -----
C      This is an interactive program by which the user can supply
C      the necessary data to run the simulator.
C -----

```

```

IMPLICIT REAL*8(A-H,O-Z)
DOUBLE PRECISION L,KBARP,KBARR
DIMENSION L(5),D(5),CPI(10),KBARP(20,20),KBARR(20,20)
DIMENSION ECP(20,20),ECR(20,20)
DIMENSION II(10,2),JJ(10,2)
CHARACTER*20 NAME(10,2)

```

```

OPEN (UNIT=11,FILE='SIM2.DAT')

```

```

WRITE(6,899)
899  FORMAT(5X,'IF THE USER WISHES TO TEST DIFFERENT REACTION ',/,
* 5X,'NETWORKS FOR THE SAME SET OF INPUT CONDITIONS ,THEN',/,
* 5X,'AFTER "SIM1.DAT" HAS BEEN CREATED , THE USER SHOULD',/,
* 5X,'SPECIFY "IDUM = 1" IN SUBSEQUENT RUNS TO SKIP READING',/,
* 5X,'THE SAME INPUT CONDITIONS. OTHERWISE SET IDUM = 2',/,
* 5X,'WHAT IS THE VALUE OF IDUM ? '$)
READ(6,*) IDUM

```

```

IF(IDUM.EQ.1) GO TO 33

```

```

OPEN (UNIT=1,FILE='SIM1.DAT')
WRITE(06,100)
100  FORMAT(////20X,'SIMULATION OF DIRECT COAL LIQUEFACTION',///,
* 2X,'IF ONE REACTOR : ENTER 1',/,
* 2X,'IF TWO REACTORS IN SERIES : ENTER 2, AND SO ON',
* '(MAXIMUM OF 4) '$)
READ(5,101) NN
101  FORMAT(I)
N=NN+1
WRITE(01,*) N

```

```

WRITE(06,200)
200  FORMAT(//20X,'ENTER INLET CONDITIONS:',/,

```

```

* 2X,'Flowrate of gas to preheater (cm**3/sec)'/,
* 2X,'Flowrate of slurry to preheater (cm**3/sec)'/,
* 2X,'Length of preheater coil (cm)'/,
* 2X,'Length of reactor/reactors (cm)'/,
* 2X,'Diameter of preheater coil (cm)'/,
* 2X,'Diameter of reactor/reactors (cm)'/,
* 2X,'Inlet temperature of the slurry to preheater (degrees C)'/,
* 2X,'Operating pressure (atm)'/,
* 2X,'Mole fraction of hydrogen in inlet gas to preheater'/',
* 2X,'Temperature of furnace (degrees C)'/,
* 2X,'ALL ENTRIES TO BE MADE IN FREE FORMAT'//)
READ(06,*) VOLG,VOLL,(L(I),I=1,N),(D(I),I=1,N),TIL,P,FRAC,TH
WRITE(01,*) VOLG,VOLL,(L(I),I=1,N),(D(I),I=1,N),TIL,P,FRAC,TH

WRITE(06,201)
201  FORMAT(/,20X,'ENTER VALUES OF VARIABLES LISTED BELOW:'/,
* 2X,'Heat capacity of gas (cal/gm C)'/,
* 2X,'Heat capacity of slurry (cal/gm C)'/,
* 2X,'Arrhenius frequency factor for hydrogen consumption ',
* 'kinetics (1/sec)'/,
* 2X,'Activation energy for hydrogen consumption kinetics ',
* '(cal/gmole)'/,
* 2X,'Heat of reaction (cal/gm)'/,
* 2X,'Heat of dissolution (cal/gm)'/,
* 2X,'Solubility constant (<gm/cm**3>liq/<gm/cm**3>gas)'/,
* 2X,'Diffusivity of the gas (cm**2/sec)'/,
* 2X,'Surface tension of the slurry (dynes/cm)'/,
* 2X,'Density of the slurry (gm/cm**3)'/,
* 2X,'ALL ENTRIES TO BE MADE IN FREE FORMAT'//)
READ(06,*) CPG,CPBAR,ZKBAR,E,DHR,DHS,HBAR,DI,SIG,RHOA
WRITE(01,*) CPG,CPBAR,ZKBAR,E,DHR,DHS,HBAR,DI,SIG,RHOA

CLOSE(UNIT=1)

33  WRITE(6,990)
990  FORMAT(/,5X,'Enter total number of species present in',
* 'preheater '$)
READ(6,*) NSP
WRITE(11,*) NSP
DO 2 I=1,NSP
WRITE(6,991) I
991  FORMAT(/,5X,'Enter Name of Species Number',I2,3X,$)
READ(6,102) NAME(I,1)
WRITE(11,102) NAME(I,1)
102  FORMAT(A20)
2    CONTINUE
WRITE(6,203)
203  FORMAT(/,5X,'The Species have been Coded as:'/)

```

```

DO 3 I=1,NSP
WRITE(6,103) I,NAME(I,1)
103  FORMAT(10X,I2,2X,'=',2X,A20)
3    CONTINUE
WRITE(6,105)
105  FORMAT(///,5X,'Enter Total Number of Non-Zero Rate Constants',/,
* 5X,' for reaction network in preheater '$)
READ(6,*) NKP
WRITE(11,*) NKP
WRITE(6,106)
106  FORMAT(5X,/,5X,'Enter the Following Data for Each Rate Constant')
DO 4 I=1,NKP
WRITE(6,107) I
107  FORMAT(///,5X,'For Rate Constant Number',I2,' Enter')
WRITE(6,108)
108  FORMAT(5X,'Code of Reacting Species '$)
READ(6,*) II(I,1)
WRITE(11,*) II(I,1)
WRITE(6,109)
109  FORMAT(5X,'Code of Product Species '$)
READ(6,*) JJ(I,1)
WRITE(11,*) JJ(I,1)
WRITE(6,110)
110  FORMAT(5X,'Arrhenius Factor for Rate Constant (1/sec) '$)
READ(6,*) KBARP(II(I,1),JJ(I,1))
WRITE(11,*) KBARP(II(I,1),JJ(I,1))
WRITE(6,111)
111  FORMAT(5X,'Activation Energy (cal/gmol) '$)
READ(6,*) ECP(II(I,1),JJ(I,1))
WRITE(11,*) ECP(II(I,1),JJ(I,1))
4    CONTINUE

WRITE(6,400)
400  FORMAT(///,5X,'Enter total number of species present in',
* ' reactor '$)
READ(6,*) NSPR
WRITE(11,*) NSPR
DO 6 I=1,NSPR
WRITE(6,991) I
READ(6,102) NAME(I,2)
WRITE(11,102) NAME(I,2)
6    CONTINUE
WRITE(6,203)
DO 7 I=1,NSPR
WRITE(6,103) I,NAME(I,2)
7    CONTINUE
WRITE(6,115)
115  FORMAT(///,5X,'Enter total number of non-zero rate constants',/,

```

```

* 5X,' for reaction network in reactor '$)
  READ(6,*) NKR
  WRITE(11,*) NKR
  WRITE(6,106)
  DO 8 I=1,NKR
    WRITE(6,107) I
    WRITE(6,108)
    READ(6,*) II(I,2)
    WRITE(11,*) II(I,2)
    WRITE(6,109)
    READ(6,*) JJ(I,2)
    WRITE(11,*) JJ(I,2)
    WRITE(6,110)
    READ(6,*) KBARR(II(I,2),JJ(I,2))
    WRITE(11,*) KBARR(II(I,2),JJ(I,2))
    WRITE(6,111)
    READ(6,*) ECR(II(I,2),JJ(I,2))
    WRITE(11,*) ECR(II(I,2),JJ(I,2))
8    CONTINUE

  WRITE(6,112)
112  FORMAT(///5X,'Enter Initial Concentration of Each Species',
*      '(gm/gm)')
      DO 5 I=1,NSPR
        WRITE(6,113) I
113  FORMAT(5X,'Species Number ',I2,2X,$)
      READ(6,*) CPI(I)
      WRITE(11,*) CPI(I)
5    CONTINUE

  OPEN(UNIT=2,NAME='INPUT.DAT')

  IF(IDUM.EQ.1) GO TO 34
  WRITE(2,222) VOLG,VOLL,L(1),(L(I),I=2,N),D(1),(D(I),I=2,N),TIL,
*      P,FRAC,TH
222  FORMAT(/////20X,'LIST OF INPUT DATA :',/////////,
*      2X,'Flowrate of gas to preheater (cm**3/sec)',T70,E12.4,/,
*      2X,'Flowrate of slurry to preheater (cm**3/sec)',T70,E12.4,/,
*      2X,'Length of preheater coil (cm)',T70,E12.4,/,
*      2X,'Length of reactor/reactors (cm)',T70,E12.4,/,
*      2X,'Diameter of preheater coil (cm)',T70,E12.4,/,
*      2X,'Diameter of reactor/reactors (cm)',T70,E12.4,/,
*      2X,'Inlet temperature of slurry to preheater (deg. C)',T70,E12.4
*      ,/,2X,'Operating pressure (atm)',T70,E12.4,/,
*      2X,'Mole fraction of hydrogen in inlet gas to preheater',T70,
*      E12.4,/,2X,'Temperature of furnace (deg. C)',T70,E12.4,/)

  WRITE(2,223) CPG,CPBAR,ZKBAR,E,DHR,DHS,HBAR,DI,SIG,RHOA

```

```

223  FORMAT(2X,'Heat capacity of gas (cal/gm C)',T70,E12.4,/,
* 2X,'Heat capacity of slurry (cal/gm C)',T70,E12.4,/,
* 2X,'Arrhenius frequency factor for hydrogen consumption ',
* 'kinetics (1/sec)',T70,E12.4,/,
* 2X,'Activation energy for hydrogen consumption kinetics ',
* '(cal/gmole)',T70,E12.4,/,
* 2X,'Heat of reaction (cal/gm)',T70,E12.4,/,
* 2X,'Heat of dissolution (cal/gm)',T70,E12.4,/,
* 2X,'Solubility constant (<gm/cm**3>)liq/<gm/cm**3>gas',T70,
* E12.4,/,2X,'Diffusivity of the gas (cm**2/sec)',T70,E12.4,/,
* 2X,'Surface tension of the slurry (dynes/cm)',T70,E12.4,/,
* 2X,'Density of the slurry (gm/cm**3)',T70,E12.4,/

34  WRITE(2,224) NSP
224  FORMAT('1',5X,'Total number of species present in',
* 'preheater =' ,I3,/)
      WRITE(2,225) NKP
225  FORMAT(5X,'Total Number of Non-Zero Rate Constants',
* ' for reaction network in preheater =' ,I3,/)

      WRITE(2,230)
230  FORMAT(5X,'The Reaction Pathways for preheater are: '//)

      DO 10 I=1,NKP
      WRITE(2,231) II(I,1),JJ(I,1),KBARP(II(I,1),JJ(I,1)),
*          ECP(II(I,1),JJ(I,1))
231  FORMAT(5X,'For the reaction path ',I3,' to ',I3,/,
* 5X, 'k0 = ',E12.4,2X, ' E = ',E12.4,/)
10  CONTINUE

      WRITE(2,226) NSPR
226  FORMAT('1',5X,'Total number of species present in reactor =' ,I3,/)
      WRITE(2,227) NKR
227  FORMAT(5X,'Total number of non-zero rate constants for reaction',
* ' network in reactor =' ,I3,/)

      WRITE(2,232)
232  FORMAT(5X,'The Reaction pathways for reactor are: '//)

      DO 11 I=1,NKR
      WRITE(2,231) II(I,2),JJ(I,2),KBARR(II(I,2),JJ(I,2)),
*          ECR(II(I,2),JJ(I,2))
11  CONTINUE
      WRITE(2,228)
228  FORMAT('1',5X,'Initial Concentration of Each Species (gm/gm)',///)
      DO 47 I=1,NSPR

```



```

WRITE(2,229) I,CPI(I)
229  FORMAT(5X,'Concentration of species # ',I2,' = ',E12.4,/)
47   CONTINUE
      CLOSE (UNIT=2)
      WRITE(6,300)
300  FORMAT(/////70('*'),/,10X,'DATA FILES HAVE BEEN CREATED'//,
* 10X,'THE INPUT DATA ARE LISTED IN THE FILE "INPUT.DAT"',/,
* 5X,'THE SIMULATOR CAN NOW BE RUN IN BATCH OR TIME SHARING MODE',
* /,70('*'))
      STOP
      END

```

PROGRAM TO INPUT DATA TO  
FIT.FOR (FITDAT.FOR)

```

C -----
C PROGRAM FOR CREATING INPUT DATA FOR PARAMETER ESTIMATION
C -----

```

```

C This is an interactive program by which the user can
C input data required for parameter estimation.

```

```

IMPLICIT REAL*8(A-H,O-Z)
DOUBLE PRECISION L
DOUBLE PRECISION K,KBAR1,KBAR2
DIMENSION K(20,20),KBAR1(20,20),EC1(20,20),COEFF(20,20),CPI(10)
DIMENSION KBAR2(20,20),EC2(20,20)
DIMENSION ECSTAR(20,20)
DIMENSION L(2),D(2),X(20),T(20)
CHARACTER*20 NAME(10)
OPEN (UNIT=1,FILE='FIT01.DAT')
OPEN (UNIT=2,FILE='FIT02.DAT')

```

```

WRITE(6,99)
99  FORMAT(///,5X,'IF ISOTHERMAL REACTOR SPECIFY IND=1',/,
* 5X,'FOR NON-ISOTHERMAL REACTOR SPECIFY IND=2',/,
* 5X,'WHAT IS THE VALUE OF IND ? ', $)
READ(6,*) IND
WRITE(01,*) IND
WRITE(06,200)
200  FORMAT(//20X,'ENTER EQUIPMENT SIZES',/,
* 2X,'Length of preheater (cm)',/,
* 2X,'Length of reactor (cm)',/,
* 2X,'Diameter of preheater (cm)',/,
* 2X,'Diameter of reactor (cm)',/,
* 2X,'ALL ENTRIES TO BE MADE IN FREE FORMAT',//)
READ(06,*) (L(I),I=1,2),(D(I),I=1,2)
WRITE(01,*) (L(I),I=1,2),(D(I),I=1,2)
WRITE(06,201)
201  FORMAT(//20X,'ENTER PHYSICO-CHEMICAL PARAMETERS',/,
* 2X,'Heat capacity of gas (cal/gm C)',/,
* 2X,'Heat capacity of slurry (cal/gm C)',/,
* 2X,'Arrhenius frequency factor for hydrogen consumption '
* 'kinetics (1/sec)',/,
* 2X,'Activation energy for hydrogen consumption kinetics ',
* '(cal/gmole)',/,
* 2X,'Heat of reaction (cal/gm)',/,
* 2X,'Heat of dissolution (cal/gm)',/,
* 2X,'Solubility constant (<gm/cm**3>|liq/<gm/cm**3>gas)',/,

```

```

* 2X,'Diffusivity of the gas (cm**2/sec)',/,
* 2X,'Surface tension of the slurry (dynes/cm)',/,
* 2X,'Density of the slurry (gm/cm**3)',/,
* 2X,'ALL ENTRIES TO BE MADE IN FREE FORMAT',//)

```

```

      READ(06,*) CPG,CPBAR,ZKBAR,E,DHR,DHS,HBAR,DI,SIG,RHOA
      WRITE(01,*) CPG,CPBAR,ZKBAR,E,DHR,DHS,HBAR,DI,SIG,RHOA
      WRITE(6,100)
100   FORMAT(/,5X,'Enter Total Number of Species' $)
      READ(6,*) NSP
      WRITE(1,*) NSP
      DO 2 I=1,NSP
      WRITE(6,101) I
101   FORMAT(/,5X,'Enter Name of Species Number',I2, $)
      READ(6,102) NAME(I)
      WRITE(1,102) NAME(I)
102   FORMAT(A20)
2     CONTINUE
      DO 3 I=1,NSP
      WRITE(6,103) I,NAME(I)
103   FORMAT(10X,I2,2X,'=',2X,A20)
3     CONTINUE
      WRITE(6,105)
105   FORMAT(/,5X,'Enter Total Number of Non-Zero Rate Constants' $)
      READ(6,*) NK
      WRITE(1,*) NK
      WRITE(6,106)
106   FORMAT(/,5X,'Enter the Following Data for Each Rate Constant' $)
      DO 4 I=1,NK
      WRITE(6,107) I
107   FORMAT(/,5X,'For Rate Constant Number',I2,' Enter')
      WRITE(6,108)
108   FORMAT(5X,'Code of Reacting Species' $)
      READ(6,*) II
      WRITE(1,*) II
      WRITE(6,109)
109   FORMAT(5X,'Code of Product Species' $)
      READ(6,*) JJ
      WRITE(1,*) JJ
      WRITE(6,110)
110   FORMAT(5X,'Lower',
*      ' & Upper bounds on Arrhenius Factor for Rate Constant (1/sec)')
      READ(6,*) KBAR1(II,JJ),KBAR2(II,JJ)
      WRITE(1,*) KBAR1(II,JJ),KBAR2(II,JJ)
      WRITE(6,111)
111   FORMAT(5X,'Lower',
*      ' & Upper Bounds on Activation Energy (cal/gmol)')

```

```

      READ(6,*) EC1(II,JJ),EC2(II,JJ)
      WRITE(1,*) EC1(II,JJ),EC2(II,JJ)
4      CONTINUE
      WRITE(6,500)
500    FORMAT(//,5X,'Enter no. of data points' $)
      READ(6,*)NDATA
      WRITE(1,*)NDATA
      CLOSE(UNIT=1)
      WRITE(6,502)
502    FORMAT(/,5X,' FOR EACH DATA POINT, ENTER THE FOLLOWING')
      DO 501 IQ=1,NDATA
      WRITE(6,503)IQ
503    FORMAT('          FOR DATA PT NO', I3)
      WRITE(6,504)
504    FORMAT('          Gas flowrate (cm**3/sec)',/,
      * 2x,'Slurry flowrate (cm**3/sec)',/,
      * 2x,'Inlet temp of slurry to preheater (deg C)',/,
      * 2x,'Operating pressure (atm)',/,
      * 2x,'Mole frac of hydrogen in inlet to preheater',/,
      * 2X,'Temp of heating medium',/,
      * 2x,'ENTER IN FREE FORMAT',/)
      READ(6,*)VOLG,VOLL,TIL,P,FRAC,TH
      WRITE(2,*)VOLG,VOLL,TIL,P,FRAC,TH
      WRITE(6,507)
507    FORMAT(//,5X,' ENTER INLET CONC OF EACH SPECIES, GM/GM')
      DO 508 IIQ=1,NSP
      WRITE(6,113)IIQ
      READ(6,*)CPI(IIQ)
      WRITE(2,*)CPI(IIQ)
508    CONTINUE
      WRITE(6,505)
505    FORMAT(//,5X,' ENTER OUTLET CONC OF EACH SPECIES, GM/GM')
      DO 506 IIQ=1,NSP
      WRITE(6,113)IIQ
113    FORMAT(5X,'Species Number ',I2, $)
      READ(6,*) CPI(IIQ)
      WRITE(2,*) CPI(IIQ)
506    CONTINUE
501    CONTINUE

      IF(IND.EQ.1) GO TO 31
      WRITE(6,204)
204    FORMAT(5X,'ENTER DATA FOR TEMPERATURE PROFILE IN REACTOR',/)
      WRITE(6,202)
202    FORMAT(5X,'ENTER NUMBER OF POSITIONS AT WHICH TEMPERATURE WAS '
      * 'MEASURED ', $)
      READ(6,*) NDT

```

```

        WRITE(2,*) NDT
        WRITE(6,203)
203    FORMAT(5X,'ENTER PAIRS OF POSITION-TEMPERATURE DATA',/,
        * 5X,'POSITION IN CM, TEMPERATURE IN DEG. C',/)
        DO 11 I=1,NDT
        READ(6,*) X(I),T(I)
        WRITE(2,*) X(I),T(I)
11    CONTINUE
31    CLOSE(UNIT=2)
        WRITE(6,300)
300    FORMAT(16X,'DATA FILES "FIT01.DAT" & "FIT02.DAT" HAVE' ,/,
        * 'BEEN CREATED. THE SIMULATOR MAY NOW BE RUN IN BATCH MODE',
        * /,70('*'))
        STOP
        END

```