



DE82019425

**NTIS**<sup>®</sup>  
Information is our business.

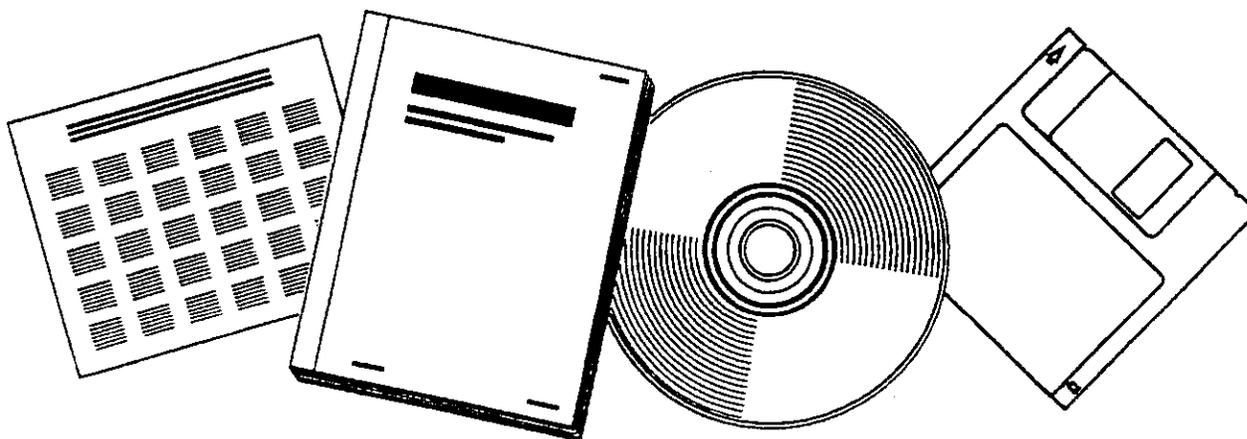
---

---

**FISCHER-TROPSCH SYNTHESIS IN  
SLURRY-REACTOR SYSTEMS. QUARTERLY REPORT,  
MAY 1, 1982-JULY 31, 1982**

MASSACHUSETTS INST. OF TECH., CAMBRIDGE

1982



U.S. DEPARTMENT OF COMMERCE  
National Technical Information Service

---

Fischer-Tropsch Synthesis in Slurry-Reactor Systems

Quarterly Report for Period

May 1, 1982 to July 31, 1982

DOE/PC/40771--5

DE82 019425

**MASTER**

Department of Chemical Engineering

and

Energy Laboratory

Massachusetts Institute of Technology

Cambridge, Massachusetts

Report No.: DCE/PC40771-5

Grant No.: DE-FG22-81PC40771

**DISCLAIMER**

This report was prepared as an account of work sponsored by an agency of the United States Government. Neither the United States Government nor any agency thereof nor any of their employees makes any warranty, express or implied, or assumes any legal liability or responsibility for the accuracy, completeness, or usefulness of any information, apparatus, product, or process disclosed, or represents that its use would not infringe privately owned rights. Reference herein to any specific commercial product, process, or service by trade name, trademark, manufacturer, or otherwise, does not necessarily constitute or imply its endorsement, recommendation, or favoring by the United States Government or any agency thereof. The views and opinions of authors expressed herein do not necessarily state or reflect those of the United States Government or any agency thereof.

Submitted by:

C.N. Satterfield

T. Bartos

G.A. Huff, Jr.

E. Stenger

Robert Summerhayes

## I. SUMMARY

In the quarterly report for the period ending July 31, 1981 we listed four papers that were being submitted for publication. All four have now been published and we list them here for reference:

C.N. Satterfield, G.A. Huff, Jr., and H. Stenger, "Effect of Carbon Formation on Liquid Viscosity and Performance of Fischer-Tropsch Bubble-Column Reactors," Ind. Eng. Chem., Process Des. Develop., 20, 666-670 (1981).

C.N. Satterfield and G.A. Huff, Jr., "Usefulness of a Slurry-Type Fischer-Tropsch Reactor for Processing Synthesis Gas of Low Hydrogen-Carbon Monoxide Ratios," Can. J. Chem. Eng., 60, 159-162 (1982).

C.N. Satterfield and G.A. Huff, Jr., "Carbon Number Distribution of Fischer-Tropsch Products Formed on an Iron Catalyst in a Slurry Reactor," J. Catalysis, 73, 187-197 (1982).

C.N. Satterfield, G.A. Huff, Jr., and J.P. Longwell, "Product Distribution from Iron Catalysts in Fischer-Tropsch Slurry Reactors," Ind. Eng. Chem., Process Design Develop., 21, 465-470, 1982.

Our paper entitled, "A Stirred Autoclave Apparatus for Study of the Fischer-Tropsch Synthesis in a Slurry Bed. I. Reactor and Trapping Procedures," a copy of which was appended to the August-October, 1981 quarterly report, is now in press in Ind. Eng. Chem., Fundamentals.

During June, Professor Satterfield presented invited lectures on recent M.I.T. work on Fischer-Tropsch synthesis, at the British Petroleum laboratories in London and at the Engler-Bunte Institute, West Germany, University of Karlsruhe. He also participated in the Symposium on

"Catalytic Reactions of One Carbon Molecules" held in Bruges, Belgium in June.

We have previously reported that our studies with addition of olefin to synthesis gas on an iron catalyst showed no evidence of incorporation of ethylene into the growing chains, contrary to a report by Dwyer and Somorjai. Some additional runs were made and the whole subject has been reviewed and interpreted. A copy of a manuscript describing this work is attached. It will be submitted shortly to J. Catalysis.

A summary of the doctoral thesis of George A. Huff, Jr., which covers most of our work on reduced fused magnetite to date, was prepared and a copy is attached.

Particularly interesting was the finding that the total product distribution on a carbon number basis clearly followed a double  $\alpha$  value. From  $C_1$  to  $C_{10}$  an  $\alpha$  of about 0.70 was typical, but above  $C_{20}$   $\alpha$  was about 0.93. This means that the % conversion of synthesis gas to liquid fuels would be significantly greater than predicted from the usual single  $\alpha$  plot based on light gas analysis. The results are interpreted in terms of a 2-site mechanism. Similar observations were reported in Germany during World War II, in the Schwarzheide test on iron catalysts, but subsequently there was considerable questioning as to whether the effect was real. The present findings clearly support the German observations.

OLEFIN INCORPORATION IN THE  
FISCHER-TROPSCH SYNTHESIS ON AN IRON CATALYST

Charles N. Satterfield, George A. Huff, Jr., and  
Robert Summerhayes  
Department of Chemical Engineering  
Massachusetts Institute of Technology  
Cambridge, Mass. 02139

ABSTRACT

Addition of ethylene or 1-butene to synthesis gas caused no change in the molecular weight distribution of products,  $\alpha$ . Material balances showed the possibility of a slight degree of incorporation of ethylene into growing chains. Some ethylene was hydrogenated to ethane but no hydrogenation of 1-butene occurred. Studies were with a reduced alkalized fused iron catalyst in a well stirred slurry reactor, at 248°C and 790 or 1480 kPa total pressure.

---

The extent to which olefins may be incorporated into growing chains during Fischer-Tropsch synthesis is of mechanistic significance and also of practical importance since it is a possible means of altering the molecular weight distribution of the products or increasing the formation of higher molecular weight hydrocarbons. At the usual synthesis temperatures the incorporation of, e.g. ethylene or 1-butene into synthesis products is highly favorable thermodynamically although that for 1-butene is somewhat less favorable than for ethylene (1).

Two early studies with C-labelled ethylene or propylene (2,3) indicated that on iron catalysts only a few percent of the added olefins were incorporated into higher hydrocarbons but in a more recent study (4) it was reported that the addition of ethylene or propylene markedly shifted the selectivity to heavier products. The present studies were

designed to help resolve this disagreement.

Hall et al. (2) passed synthesis gas of  $H_2/CO$  ratio equal to 1 and containing 1 to 1.25 mole % radioactive ethylene over either of two reduced fused iron catalysts in a fixed bed reactor at 224°C. With an iron catalyst promoted with 0.6%  $SiO_2$ , 0.6%  $Cr_2O_3$ , 4.6%  $MgO$  and 0.6%  $K_2O$  at 790 kPa, about 6 mole % of the ethylene was incorporated into higher hydrocarbons. With an iron catalyst promoted with 0.64%  $Al_2O_3$  and 2.0%  $ZrO_2$  but containing no potassium at 100 kPa, about 12% of the ethylene was incorporated into higher hydrocarbons. In both experiments most of the labelled ethylene was hydrogenated to ethane.

Schulz et al. (3) investigated the effect of  $^{14}C$ -labelled ethylene or propylene over an alkalized iron catalyst in a fixed-bed reactor at 2.1 MPa and 220°C. They added 0.2 to 0.3 mole% olefin to synthesis gas with a  $H_2/CO$  molar ratio of 2.0. About 9% of the  $^{14}C$ -labelled ethylene but only 1% of the propylene was converted to higher hydrocarbons. In both cases, the major portion of the tagged olefins was hydrogenated to the saturated paraffins.

In a more recent study, Dwyer and Somorjai (4) reported that the addition of 0.04 to 2.7 mole% ethylene or propylene to synthesis gas with a  $H_2/CO$  molar ratio of 3 noticeably shifted the selectivity to heavier products. Experiments were conducted with an initially evacuated, unalkalized iron foil at 610 kPa and 300°C in an isolation cell over a catalyst lifetime of 2 to 3 hr. Loss of Fischer-Tropsch activity was attributed to excessive carbon deposition on the catalytic surface. Total conversion of CO was <1% in their runs. In a representative experiment, after 90 min of reaction most of the ethylene had been converted to ethane but 8 mole % of the original ethylene at 2.7 mole% concentration had been converted to higher

hydrocarbons. A chain growth probability factor  $\alpha$  of 0.56 was calculated, based on a Schulz-Flory distribution for  $C_1$  and  $C_3$  to  $C_5$  hydrocarbons. A much lower value of  $\alpha = 0.30$  was observed when only 0.04 mole% ethylene was added. When propylene was added, a value of  $\alpha = 0.70$  was reported. Dwyer and Somorjai reasoned that the increase in  $\alpha$  with increasing ethylene partial pressure, indicative of a higher average molecular-weight product, indicated that ethylene participated directly in the propagation step. Their results suggested that incorporation of alpha-olefins into growing chains on the catalyst surface was a major reaction pathway for producing higher molecular-weight products.

#### EXPERIMENTAL

The apparatus and analytical procedures used in this study are described in detailed elsewhere (5,6). Synthesis gas either with or without added ethylene or 1-butene was passed continuously into a 1-liter, mechanically-stirred autoclave about half-filled with an essentially nonvolatile and inert liquid, normal-octacosane of > 99% purity, in which the catalyst was suspended. The contents were well mixed so the reactor behaved as a C.S.T.R. Volatile products were removed overhead continuously while the catalyst and inert liquid remained in the reactor for the duration of a run. After an initial period, steady-state operation with regard to catalytic activity and selectivity was obtained over the entire run.

The catalyst (from United Catalysts, Inc., and designated C-73) was a fused iron containing 2.0-3.0%  $Al_2O_3$ , 0.5-0.8%  $K_2O$ , 0.1-1.2%  $CaO$ , and < 0.4%  $SiO_2$ , on an unreduced basis. About 75 g of crushed catalyst was prereduced in a separate vessel with hydrogen at a space velocity of  $10,000 \text{ hr}^{-1}$ ,  $400^\circ\text{C}$ , and atmospheric pressure. It was then slurried

with the octacosane to produce a 15 wt% suspension (unreduced basis).

Premixed gases from cylinders were employed. The synthesis gas composition was about 55 mole% hydrogen and 45 mole% carbon monoxide. To this was added 1.5 mole% ethylene or 0.86 mole% 1-butene. The gas was fed to the reactor at a space velocity of approximately 6.5 L gas (at STP)/min-kg catalyst (unreduced basis). Reactor temperature was 248°C, and total pressure was either 790 or 1480 kPa. At these reaction conditions, carbon monoxide conversions greater than 90% were obtained. These were sought since significant readsorption of olefins would seem to be most likely when competition with carbon monoxide, which is strongly bound onto the catalyst, is minimized.

A run was also conducted in which synthesis gas with added ethylene was fed to the reactor filled with octacosane, but without catalyst. No secondary hydrogenation was observed which established that the stainless-steel reactor walls were effectively inert and that homogeneous reaction was negligible.

The products were analyzed by gas chromatography. They were characterized by carbon number on a total organic basis, which included hydrocarbons plus oxygenates.

#### RESULTS

We will show that our products follow the same Flory distribution in the presence of added ethylene and 1-butene as they do in the absence of added olefin. For this to be true, alpha-olefins must either be incorporated with the same chain propagation rate as for addition of single carbon units or not be significantly incorporated into growing chains. A significant fraction of the ethylene was hydrogenated to ethane but the 1-butene remained unreacted.

The Fischer-Tropsch products over an iron catalyst, including C<sub>1</sub> and C<sub>2</sub> species have been shown to follow closely a Flory distribution (6), which is derived assuming that single carbon units are added one at a time onto the terminus of a growing linear chain. The mole fraction m<sub>n</sub> of molecules in the product mixture of carbon number n is given by:

$$m_n = (1 - \alpha)\alpha^{n-1}, \quad (1)$$

where  $\alpha$  is the probability of chain growth and is taken to be independent of molecular size. The term m<sub>n</sub> in this expression is based on the total moles of organic product synthesized, and here does not include the moles of ethylene or 1-butene added to the feed.

Considering studies with ethylene addition, it is difficult to determine with high accuracy the quantity of C<sub>2</sub> compounds that would be expected to exist in the exit stream in the absence of ethylene incorporation for comparison with experimental results, in part because a considerable part of the C<sub>2</sub> product is ethanol. Therefore we considered only the C<sub>3</sub> to C<sub>8</sub> fraction of the product for analysis of results. Equation (1) then becomes:

$$m'_n = (M_T/M_{3-8})(1 - \alpha)\alpha^{n-1}, \quad (2)$$

where m'<sub>n</sub> is the mole fraction of carbon number n (where 3 ≤ n ≤ 8), within the C<sub>3</sub> to C<sub>8</sub> portion, M<sub>3-8</sub> is the moles of C<sub>3</sub> to C<sub>8</sub> organic, and M<sub>T</sub> is the total moles of organic produced by the synthesis.

Data are more conveniently represented by the logarithmic form of Eq. (2):

$$\ln(m'_n) = \lg\left[\frac{M_T(1 - \alpha)}{M_{3-8} \alpha}\right] + n \ln(\alpha). \quad (3)$$

A plot of ln(m'<sub>n</sub>) as a function of n yields the value of  $\alpha$  from the slope. The value of  $\alpha$  cannot be calculated from the ordinate

intercept as  $M_T$  is not generally known. However, with the value of  $\alpha$  calculated from the slope, the ratio of  $M_{3-8}/M_T$  backcalculated from the intercept must be less than one for internal consistency.

Runs with and without added olefin were conducted at various times-on-stream with each of two batches of catalyst to establish reproducibility and to verify steady-state behavior. Table 1 gives the % conversion of  $H_2$  and of CO (note that some CO disappears and  $H_2$  is formed by the water gas shift reaction) and the ethylene and butylene partial pressures in the exit gas. The  $H_2/CO$  molar feed ratio was 1.27 for Runs 1-1 and 1-2, and was 1.20 for Runs 1-3, 1-4 and 2-1 to 2-4. The product distribution by carbon number for each of the four data sets without added olefin (Runs 1-1, 1-4, 2-1 and 2-2) is plotted in Fig. 1 according to the modified Flory relationship given by Eq. (3). There was no trend with time on stream, catalyst batch, carbon monoxide conversion or partial pressure of ethylene or butene, which in this case were all formed by the synthesis.

From the line in the figure, an  $\alpha$  of 0.59 was calculated from the slope by Eq. (3) [as  $\ln(\alpha)$ ]. The term  $M_{3-8}/M_T$ , estimated from the ordinate intercept [as  $M_T(1 - \alpha)\alpha^2/M_{3-8}$  at  $n = 3$ ], equaled 0.34. As expected, the value was less than one. For these same data, the experimental ratio for the four runs was calculated to be 0.40, which is good agreement.

Figure 2 shows data for Runs 1-3, 2-3 and 2-4 in which 1.5 mole% ethylene was added to the synthesis gas. The chain growth probability was 0.59, the same value as for runs without added ethylene; i.e., adding ethylene did not alter the product distribution.

Table 2 compares matched pairs of runs with and without added ethylene (e.g. 2-2 with 2-4, 1-4 with 1-3 and 2-1 with 2-3). From 18 to 32% of the added ethylene became hydrogenated to ethane, more at the higher pressure. Dry (7) also observed that ethylene appreciably reacted with hydrogen when it was added to the feed gas over an iron catalyst at 335°C. He reported that  $C_{3+}$  olefins were not hydrogenated under similar conditions. Comparison of matched pairs shows no significant effect of ethylene addition on olefin-paraffin ratio of, e.g., the  $C_4$  or  $C_6$  product.

For each run with added ethylene a material balance on the  $C_2$  fraction could be made by comparison with a matched run without added ethylene. In such a comparison adjustment must be made for slightly different flow rates and slightly different catalyst activities between the pair of runs.

The amount of  $C_2$  products expected if no added ethylene were incorporated into growing chains was calculated with adjustment from the base run using the amounts of  $C_3$  products formed in each of the two runs. This adjustment on average was  $\pm 8\%$ . By this procedure it was calculated that a slight amount of ethylene disappeared beyond conversion to ethane. The disappearance averaged about 5% and was the greatest at high % CO conversions.

The  $C_3$  to  $C_8$  carbon number distribution is depicted in Fig. 3 for run 1-3 in which 0.86 mole% 1-butene was added to the feed. Unlike the case with ethylene, less than 0.5% of the 1-butene was hydrogenated to n-butane under the synthesis conditions. Hence, the  $C_4$  produced by synthesis could be readily calculated by subtracting the 1-butene added to the feed from the total  $C_4$  in the exit stream. This permitted Fig. 3 to be constructed on the same

C<sub>3</sub> to C<sub>8</sub> basis as Figures 1 and 2 for simpler comparison of the results. The product distribution was similar to those obtained with pure synthesis gas (Fig. 1) and the same probability of chain growth  $\alpha = 0.59$  was calculated.

#### DISCUSSION

A slight degree of incorporation of an olefin into the product might be difficult to identify as a perturbation from a straight line on a semi-logarithmic plot, but we can find no evidence for this by calculation of  $\alpha$  values. Material balances indicate that it may occur to the extent of 5 to 10%.

This finding agrees with studies conducted at SASOL (7) in which a fluidized-bed reactor was operated at 335°C with an iron catalyst. An olefin-rich oil cut in the gasoline boiling range was extensively recycled to the reactor (2 volumes oil recycled/volume oil produced). There was no indication that the oil had been chemically altered even with 93% synthesis gas conversion; incorporation of the light oil did not occur.

Studies by Feimer et al. (8) also support this conclusion. They studied a precipitated, copper-potassium promoted, iron catalyst operating at steady state in a fixed-bed reactor. The C<sub>1</sub> to C<sub>5</sub> hydrocarbon product distribution, measured at five points along the bed, was independent of reactor length, and hence ethylene partial pressure, at 233°C, 1490 kPa, and H<sub>2</sub>/CO molar feed ratio of 2.3 and CO conversion up to 67%. This observation implies that olefin incorporation was negligible. At very high CO conversions the reactor profile for ethylene and ethane suggested that ethylene hydrogenation and/or incorporation into product might be more important under these conditions.

The different results of Dwyer and Somorjai (4) might be related to the absence of alkali in the catalyst they used. In pulsing type studies with a Ru catalyst Nijs and Jacobs (9) reported that incorporation of alpha-olefins into growing organic chains was significantly higher on an acidic support than on a neutral support, and the results of Hall et al. (2) could be interpreted as primarily an effect of potassium content causing lesser ethylene incorporation into products.

Alternately, and more probably, Dwyer and Somorjai's results can be attributed to the fact that their catalyst had not reached steady-state activity and was probably an incompletely carburized, polycrystalline iron. Krebs et al. (8) showed with a reduced magnetite catalyst that the product distribution and value of  $\alpha$  changed markedly during the first few hours on stream, and Raupp and Delgass (11) and Amelse et al. (12) related major changes in catalyst properties over the first few hours to surface reconstruction and iron carbide formation.

Some have contended that the typically low value for  $C_2$  on a Schulz-Flory plot of hydrocarbon products resulted from significant ethylene incorporation, and hence, loss of ethylene into growing chains on the iron surface. However, Satterfield and Huff (6) demonstrated that a low value at  $C_2$  was caused by neglecting oxygenates. On a total organic basis, a Flory plot of the products from  $C_1$  to about  $C_{20}$  was completely linear for an alkalized iron catalyst at steady state.

#### ACKNOWLEDGMENT

The work was supported by the Department of Energy under Grant No. DE-FG22-81PC40771.

#### REFERENCES

1. Anderson, R.B., in Catalysis, Vol. 4 (P.H. Emmett, ed.), Reinhold, New York, 1956, p. 15.
2. Hall, W.K., Kokes, R.J., and Emmett, P.H., J. Am. Chem. Soc., **82**, 1027 (1960).
3. Schulz, H., Rao, B.R., and Eistner, W., Erdoel Kohle Erdgas Petrochem. Brennst. Chem. **23**, 651 (1970).
4. Dwyer, D.J., and Somorjai, G.A., J. Catal. **56**, 249 (1979).
5. Huff, G.A., Jr., and Satterfield, C.N., Ind. Eng. Chem. Fundam., in press.
6. Satterfield, C.N., and Huff, G.A., Jr., J. Catal. **73**, 187 (1982).
7. Dry, M.E., in Catalysis - Science and Technology, Vol 1 (J.R. Anderson and M. Boudart, eds.), Springer-Verlag, Berlin, 1981. - What pp.?
8. Feimer, J.L., Silveston, P.L., and Hudgins, R.R., I&EC Prod. Res. Dev. **20**, 609 (1981).
9. Nijs, H.H., and Jacobs, P.A., J. Catal. **66**, 401 (1980).
10. Krebs, H.J., Bonzel, H.P., and Schwarting, W., J. Catal. **72**, 199 (1981).
11. Raupp, G.B., and Delgass, W.N., J. Catal. **58**, 361 (1979).
12. Amelse, J.A., Schwartz, L.H., and Butt, J.B., J. Catal. **72**, 95 (1981).

$\frac{H}{D}$

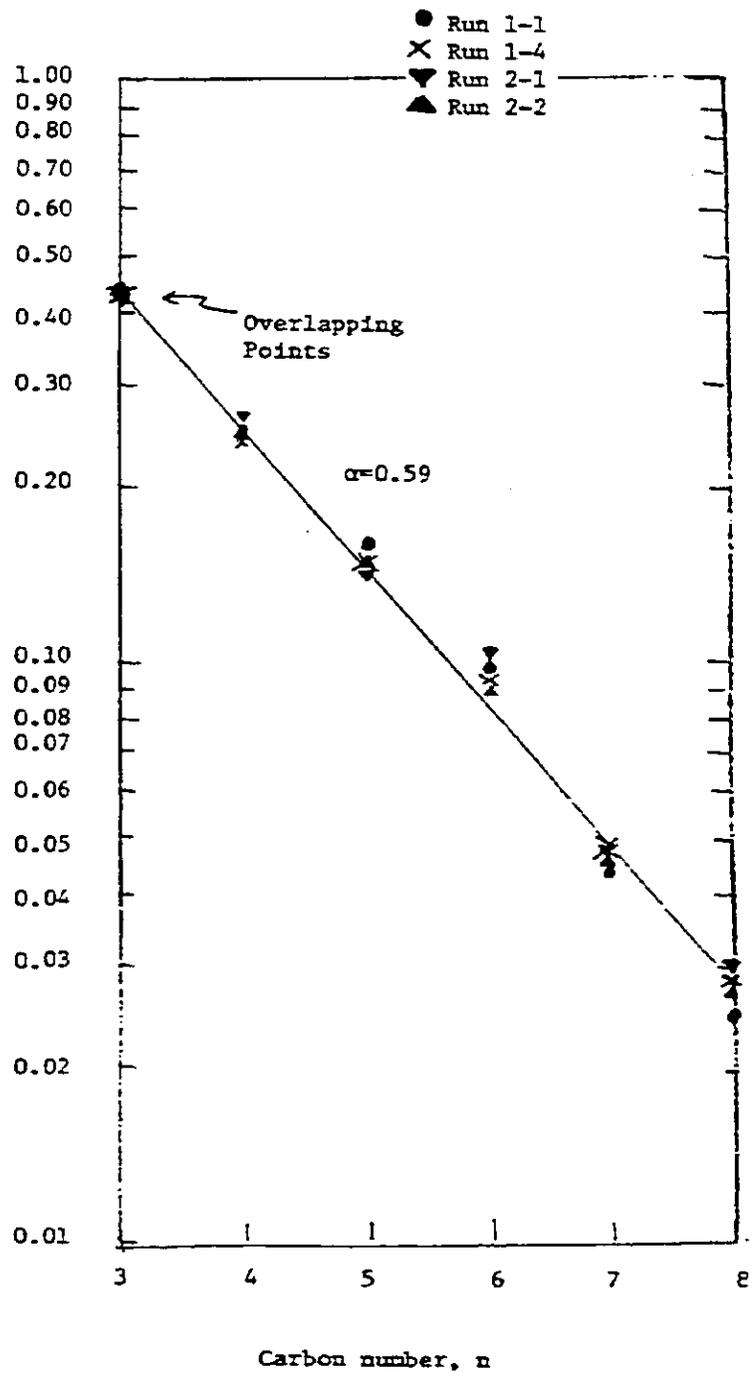


Figure 1. Flory Distribution. Synthesis Gas Alone.

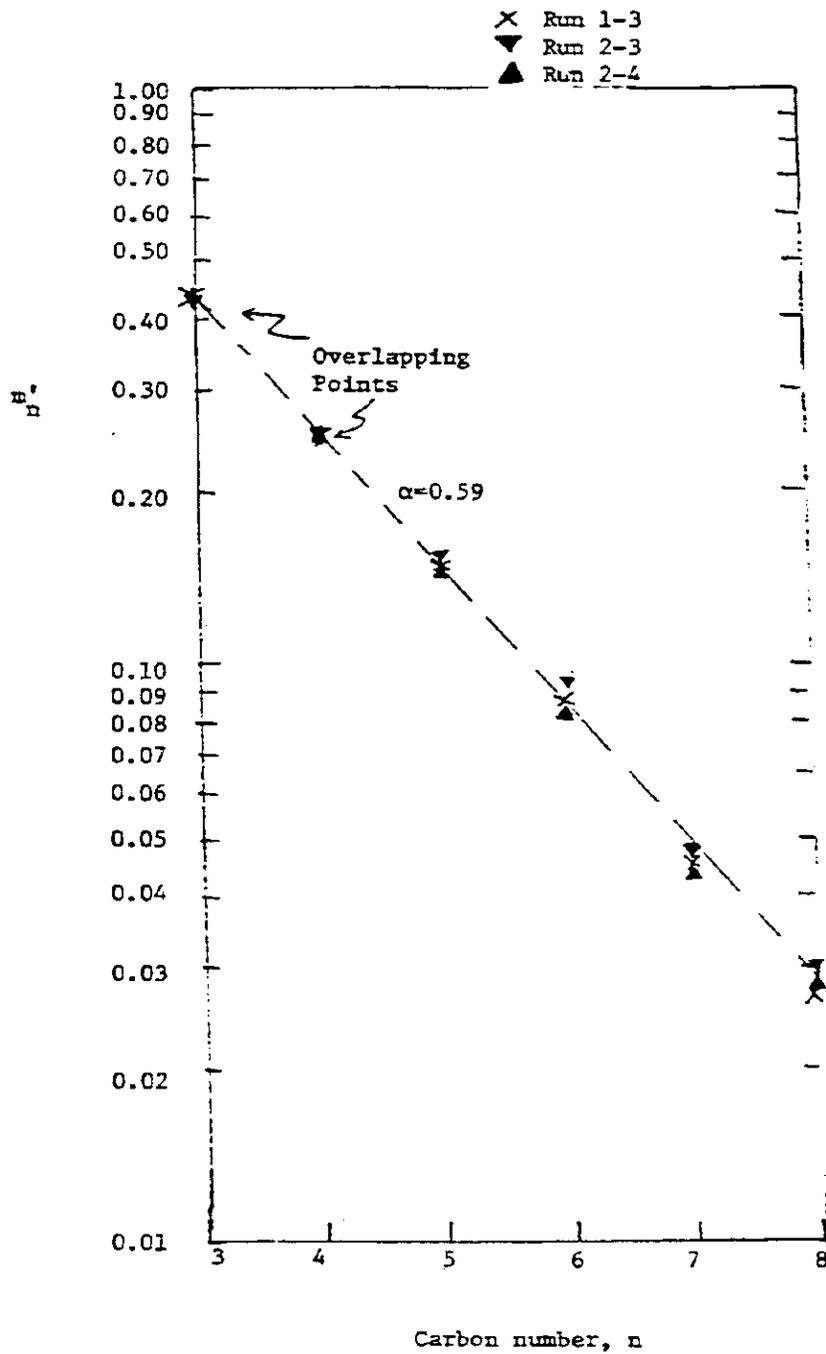


Figure 2. Flory Distribution.  
 1.5 mole% Ethylene Added to the  
 Synthesis Gas

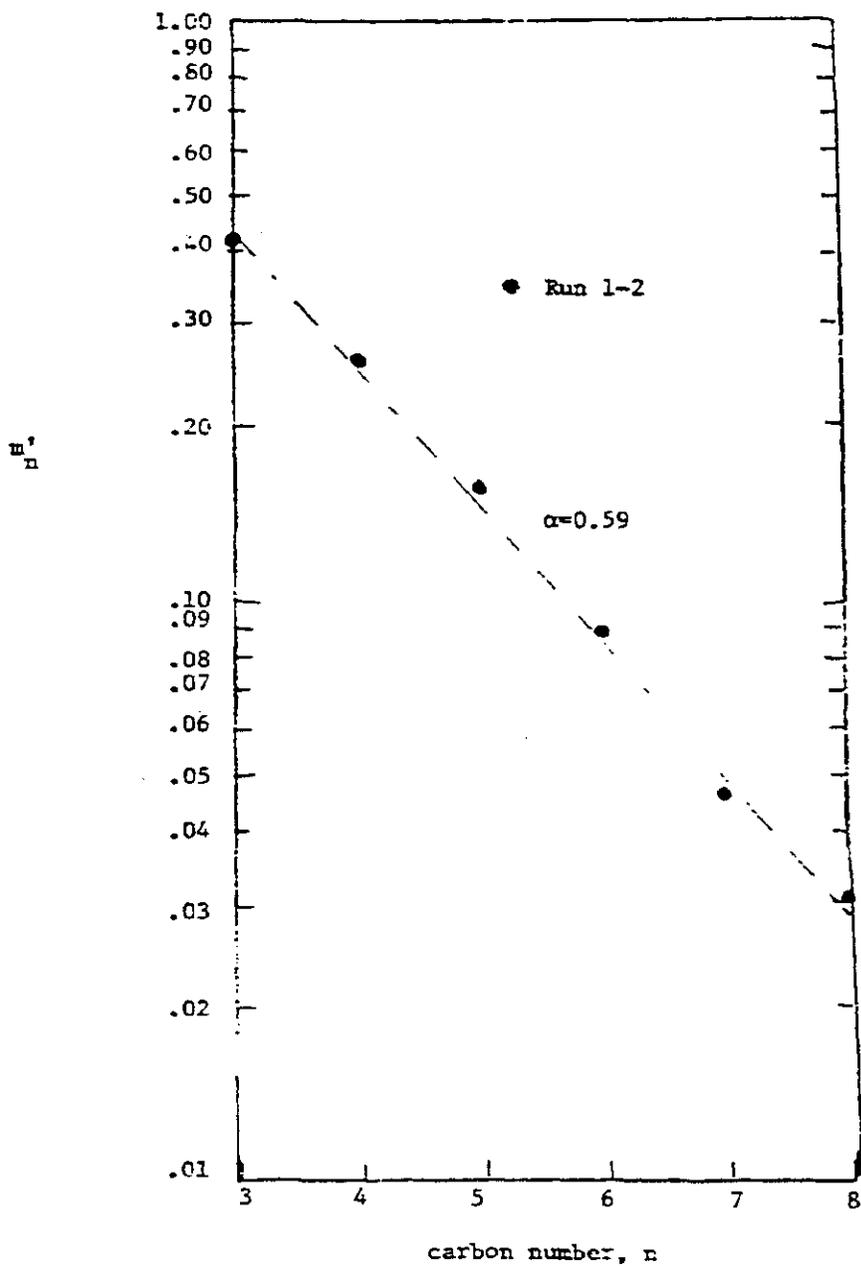


Figure 3. Flory Distribution  
0.86 mole% 1-butene added to  
the synthesis gas.

Table 1. Summary of Experimental Results

Run No.	Time on Stream (hr)	Exit $P_{C_2H_4}$ (kPa)	Exit $P_{C_4H_8}$ (kPa)	$P_{total}$ (kPa)	% Conversion	
					$H_2$	CO
<u>Catalyst Batch 1</u>						
1-1	220	21.8	15.2	1480	57	97
1-2 <sup>a</sup>	290	21.6	41.2	1480	60	97
1-3 <sup>b</sup>	625	25.1	6.4	790	49	93
1-4	675	9.9	6.1	790	51	93
<u>Catalyst Batch 2</u>						
2-1	120	10.0	6.1	790	48	90
2-2	150	19.9	14.7	1480	57	96
2-3 <sup>b</sup>	170	24.2	5.6	790	48	89
2-4 <sup>b</sup>	210	43.9	13.5	1480	56	95

<sup>a</sup>0.86 mole % 1-butene added to feed.

<sup>b</sup>1.5 mole % ethylene added to feed.

Table 2. Effect of Added Ethylene on  
Molar Ratio of Alpha-Olefin/Normal Paraffin

Run No.	$C_2^a$	$C_4$	$C_6$	Mole % of Added $C_2H_4$ Hydrogenated	$P_{total}$ (kPa)
<u>Pure Synthesis Gas</u>					
2-2	1.4	4.7	3.9	-	1480
1-4	1.9	4.9	3.9	-	790
2-1	1.8	5.2	4.2	-	790
<u>Synthesis Gas + 1.5 mole % <math>C_2H_4</math></u>					
2-4	0.1	4.6	3.4	32	1480
1-3	0.5	5.0	4.0	22	790
2-3	0.5	5.5	4.3	18	790

$$^a \frac{\text{moles } C_2H_4 \text{ in effluent/min} - \text{moles } C_2H_4 \text{ in feed/min}}{\text{moles } C_2H_6 \text{ in effluent/min}}$$