

```

C*****
C
C   CB(30,10) = Concentration in the bubble phase,
C               moles/cu.cm.
C               (Stage number, Component number)
C   CE(30,10) = Concentration in the emulsion phase,
C               moles/cu.cm.
C               (Stage number, Component number)
C   CC(30,10) = Concentration in the cloud phase,
C               moles/cu.cm.
C               (Stage number, Component number)
C   NSTAGE    = Number of the last stage
C   HSTAGE    = Height of the last stage,cm
C   IC        = number of components
C   HT(30)    = Height of each stage, cm
C               (Stage number)
C   UESN      = Last emulsion phase superficial gas
C               velocity, cm/s
C   UCSN      = Last cloud phase superficial gas
C               velocity, cm/s
C   UBSN      = Last bubble phase superficial gas
C               velocity, cm/s
C*****
C
C   SUBROUTINE CONPRT(CB,CE,CC,NSTAGE,HSTAGE,IC,HT,UESN,
C   +                UCSN,UBSN)
C
C   REAL CB(30,10),CE(30,10),CC(30,10),HT(30),CAVG(10)
C
C   Write out the bubble phase profiles
C
C   WRITE(6,100)
C 100 FORMAT(1X,'BUBBLE PHASE')
C   WRITE(6,110) (I,I=1,IC)
C 110 FORMAT(1X,' STAGE HEIGHT ',10('C',I3,' '),6X)
C   DO 10 I=1,NSTAGE
C       WRITE(6,120) I,HT(I),(CB(I,J),J=1,IC)
C 120 FORMAT(1X,I4,2X,F7.2,2X,20(E9.4,2X))
C   10 CONTINUE
C
C   Write out emulsion phase profiles
C
C   WRITE(6,130)
C 130 FORMAT(1X,///,2X,'EMULSION PHASE')
C   WRITE(6,110) (I,I=1,IC)
C   DO 20 I=1,NSTAGE
C       WRITE(6,120) I,HT(I),(CE(I,J),J=1,IC)
C 20 CONTINUE
C
C   Write out cloud phase profiles
C

```

```

        WRITE(6,140)
140  FORMAT(1X,///,2X,'CLOUD PHASE')
        WRITE(6,110) (I,I=1,IC)
        DO 20 I=1,NSTAGE
            WRITE(6,120) I,HT(I), (CC(I,J),J=1,IC)
        20  CONTINUE
C
C Calculate outlet gas composition
C
        DO 40 I=1,IC
            CAVG(I)=(CB(NSTAGE,I)*UBSN+CC(NSTAGE,I)*UCSN+
+                 CE(NSTAGE,I)*UESN)/(UBSN+UCSN+UESN)
        40  CONTINUE
C
C Write out this value
C
        WRITE(6,150)
150  FORMAT(///,2X,'GAS COMPOSITION AT OUTLET')
        WRITE(6,110) (I,I=1,IC)
        WRITE(6,160) (CAVG(I),I=1,IC)
160  FORMAT(16X,20(F9.4,2X))
        RETURN
        END
C*****
C
C Subroutine ENERGY
C
C This subroutine calculates the heat transfer properties
C of the reactor
C
C*****
C
C DP = Particle diameter, cm
C RKG = Thermal conductivity of gas, W/m*K
C CPS = Heat capacity of solids, kJ/kg*K
C DR = Reactor diameter, cm
C UD = Initial superficial gas velocity, cm/s
C VIS = Viscosity of gas, kg/cm*s
C DENS = Density of solids, kg/cu.cm.
C CPG = Heat capacity of gas, kJ/kg*K
C DENG = Gas density, kg/cu.cm.
C H = Expanded bed height, cm

```

```

C*****
C
C Program SLURRY
C
C This program calculates the concentration and
C temperature profiles in a slurry reactor using a
C modified finite difference technique.
C*****
C
C Declared Variables
C
C X(3) = Concentration of hydrogen in the liquid
C phase, dimensionless (C/Csat,c)
C (number of stage : 1 = next stage
C 2 = current stage
C 3 = last stage )
C
C Y(3) = Concentration of hydrogen in the gas phase,
C dimensionless (C/Co), (same index as X)
C
C T(3) = Temperature of liquid, dimensionless,
C (T/Tw), (same index as X)
C*****
C REAL X(3),Y(3),T(3)
C*****
C
C Common Variables
C
C DCOM: User supplied data describing the system
C
C ALPHA = Volume contraction factor for gas flow
C dimensionless
C
C U. = CO/H2 usage ratio, dimensionless
C
C RI = Inlet CO/H2 ratio, dimensionless
C
C RKFO = Preexponential factor, (s*percent
C catalyst in slurry)**-1
C
C DR = Reactor diameter, cm
C
C H = Reactor height, cm
C
C DP = Particle diameter, cm
C
C TW = Wall temperature, K
C
C UGD = Initial gas flow rate, cm/s
C
C WCAT = Weight percent catalyst in slurry
C
C DENCAT = Density of the catalyst, g/cm.cm.
C
C CPCAT = Heat capacity of catalyst, cal/g-C
C
C CCATM = Mean catalyst concentration, percent
C
C CPL = Heat capacity of the slurry liquid,
C cal/g-C
C
C CONL = Thermal conductivity of the slurry
C liquid, J/cm-s-C

```

P = Pressure, atm
 Y0 = Initial concentration of hydrogen in
 gas stream, mole fraction
 EA = Activation energy, kJ/mole

PCOM: Calculated parameters that are independant of
 bed height.

ALTWO = Modified contraction factor
 UG = Gas velocity, (U_g/U_{go}) dimensionless
 EG = Gas holdup, dimensionless
 DG = Diffusivity of hydrogen in the gas
 sq.cm./s
 BOG = Bordenstein number for gas phase, (See
 table __ in Barton, Design of Staged..
 Thesis), dimensionless
 BOL = Bordenstein number for liquid phase,
 dimensionless
 BOC = Catalyst settling Bordenstien number,
 dimensionless
 A = Gas-liquid interfacial area, 1/cm.
 RKF = Rate constant including stoichiometry
 same units as RKFO
 DA = Damkohler number, (See Barton 1986)
 DL = Diffusivity of hydrogen in the liquid,
 sq.cm./s
 E = Specific energy dissipation rate,
 sq.cm./cu.sec.
 GAMMA = Arrhenius number, dimensionless
 DHR = Reaction enthalpy, kJ/mole
 AH = specific heat transfer area, 1/cm

HCOM: Calculated parameters that depend on height

HE = Henry coefficient, cu.cm. kPa*ml/mol
 RKL = Liquid side mass transfer coefficient,
 cm/s
 RKS = liquid-solid mass transfer coefficient
 cm/s
 STG = Stanton number in gas phase
 dimensionless
 STL = Stanton number in liquid phase,
 dimensionless
 STH = Stanton number for heat transfer
 CCAT = Catalyst concentration, percent
 RNS = Liquid-solid mass transfer effective-
 ness factor, dimensionless

```

C      PE      = Peclet number
C      HT      = Heat transfer coefficient to wall
C      BE      = Dimensionless parameter, see Barton
C              1986
C*****
C      COMMON/DKOM/ALPHA,U,RI,RKFO,DR,H,DP,TW,UGD,WCAT,
C      +      DENCAT,CPCAT,CCATM,CPL,CONL,P,YO,EA
C
C      COMMON/PCOM/ALTWO,UG,EG,DG,BOG,BOL,BCC,A,RKF,DA,
C      +      DL,E,GAMMA,DHR,AH
C
C      COMMON/HCOM/HE,RKL,RKS,STG,STL,STH,CCAT,RNS,PE,HT,
C      +      BE
C
C Obtain initial data for the current reactor
C (See: Subroutine GETDAT)
C
C      CALL GETDAT(NSTEP,X,Y,T,YOUT,IP)
C
C Initialize the current height and set the height step
C size
C
C      CH=0.0
C      DZ=1.0/NSTEP
C
C Calculate the parameters that relate to the current bed
C from the initial data. (See: Subroutine PARAM)
C
C      CALL PARAM(YOUT)
C
C Step through the entire bed.
C
C      DO 30 I=1,NSTEP
C
C Update the current height
C
C      CH=CH+DZ
C
C Calculate the height dependant parameters. (See:
C Subroutine HPAR)
C
C      CALL HPAR(T(2),CH,Y(2),I)
C
C Calculate liquid concentration ( Subroutine XCALC),
C gas concentration (Subroutine YCALC), and temperature
C profile (Subroutine TCALC)
C

```

```

      CALL YCALC (STG, UGO, UG, AL TWO, YO, X, Y, T, DZ)
      CALL XCALC (BOL, STL, DA, RNS, CCAT, GAMMA, YO, X, Y, T,
+             DZ)
      CALL TCALC (PE, STH, BE, DA, RNS, CCAT, GAMMA, X, T, DZ)
C
C Print out current concentrations
C
      CALL REPORT (X, Y, T, I, IP, NSTEP)
C
C Adjust profile arrays for next step
C
      X(3)=X(2)
      X(2)=X(1)
      Y(3)=Y(2)
      Y(2)=Y(1)
      T(3)=T(2)
      T(2)=T(1)
C
      30 CONTINUE
      STOP
      END
C *****
C Subroutine GETDAT
C
C This subroutine obtains data on the properties of
C the bed.
C
C-----
C
C NSTEP = The number of stages the reactor is to be
C         divided into
C X(3)   = Liquid concentrations
C Y(3)   = Gas concentrations
C T(3)   = Temperatures
C YOUT   = Guesses outlet gas concentration
C IP     = Indicator parameter  IP = 1 :long report
C         IP = 0 :short report
C
C DCOM is apssed to this routine. See the main program
C for a description of the parameters.
C
C *****
C SUBROUTINE GETDAT (NSTEP, X, Y, T, YOUT, IP)
C
C COMMON/DCOM/ALPHA, U, RI, RKFD, DR, H, DP, TW, UGO, WCAT,
+ DENCAT, CPCAT, CCATM, CPL, CONL, F, YG, EA
C
C Declare arrays

```

```

C
C      REAL X(3),Y(3),T(3)
C
C Open the input data file. This statement is highly
C dependant on the version of FORTRAN used. It is
C written for IBM Mirrosoft FORTRAN 7
C
C      OPEN(7,FILE='NSLUR.DAT',STATUS='OLD',
C          +   ACCESS='DIRECT',FORM='FORMATTED',RECL=80)
C
C Read in the parameters free format
C
C      READ(7,*) ALPHA,U,RI,RKFO,EA
C      READ(7,*) DR,H,DF
C      READ(7,*) TW,P,YO,UGO
C      READ(7,*) WCAT,DENCAT,CPCAT,CCATM
C      READ(7,*) CPL,CONL
C      READ(7,*) NSTEP
C      READ(7,*) (X(I),I=1,3)
C      READ(7,*) (Y(I),I=1,3)
C      READ(7,*) (T(I),I=1,3)
C      READ(7,*) YOUT
C      READ(7,*) IP
C      RETURN
C      END
C*****
C
C Subroutine Param
C
C This subroutine calculate the parameters required
C that are not dependant on height
C
C-----
C
C      YOUT = Guessed outlet concentration, dimension-
C            less.
C      Commons DCOM and PCOM are passed to the subroutine.
C see the main routine for a description of the para-
C meters.
C*****
C      SUBROUTINE PARAM(YOUT)
C
C      COMMON/DCOM/ALPHA,U,RI,RKFO,DR,H,DF,TW,UGO,WCAT,
C          +   DENCAT,CPCAT,CCATM,CPL,CONL,P,YO,EA
C
C      COMMON/PCOM/ALTWO,UG,EG,DG,BOG,BOL,BOC,A,RKF,DA,
C          +   DL,E,GAMMA,DHR,AH
C

```

```

C Set the constants to be used in the subroutine
C   G = gravitational acceleration, cm./s*s
C   R = gas constant, J/atm*K
C
C       G=980.669
C       R=0.008314
C
C Calculate the heat of reaction based on stoichiometric
C considerations
C
C       DHR=-(165.0+40*(U-0.5)/1.5)
C
C Calculate modified contraction factor . Accounts for
C initial reactant make up and catalyst usage ratio.
C
C       ALTWO=ALPHA*(1+U)/(1+RI)
C
C Calculate velocity based parameters based on bed
C average gas velocity. Average velocity based on
C guessed outlet composition
C
C       YAVG=(1+YOUT)/2.0
C       UGA=(1+ALTWO)/(1+ALTWO*YAVG)
C
C Gas hold up. Deckwer et.al., Ind.Eng.Chem. Process Des.
C Dev., 1980, 19, 699.
C
C       EG=0.053*POW(UGA, 1.1)
C
C Gas phase dispersion coefficient. Mangartz, 1980 in
C Deckwer, Ind.Eng.Chem.Proc.Des.Dev., 1982, 21, p. 241
C
C       DG=5.0E-4*(UGA/EG)*(UGA/EG)*(UGA/EG)*DR**1.5
C
C Calculate Bodenstein numbers based on their definitions
C
C       BOG=UGO*H/(DG*EG)
C       BOL=2.83*POW(UGA*UGA/(G*DR), 0.34)
C       IF (ABS(BOL).LT.1E-6) BOL=1E-6*BOL/A25(BOL)
C
C Interfacial area. Deckwer et.al., Ind.Eng.Chem.Proc.Des.
C Dev., 1980, 19, 699.
C
C       A=4.5*POW(UGA, 1.1)
C
C Rate constant taking into account stoichiometry
C
C       RKF=RKFD/(1+U)
C
C Damkohler number by definition

```



```

C
C      DA=RKF*(1-EG)*H/UGO
C
C      Liquid phase dispersion coefficient, Shah, Scaleup
C      in Chemical Process Industries, ed. Kabel, R., Wiley, 1982
C
C      DL=3.676*POW(UGA,0.32)*POW(DR,1.34)
C
C      Bordenstein number for liquid
C
C      BOL=UGO*H/(DL*(1-EG))
C
C      Energy dissipation rate, Sanger, Chem.Eng.J., 1981, 22,
C      p. 179
C
C      IF (UGA.LT.6) THEN
C          E=UGA*G
C      ELSE
C          E=5886.0
C      ENDIF
C
C      Froude number for calculation of solids settling rate
C
C      FR=UGA/SQRT(G*DR)
C
C      Specific heat transfer area and arrhenius number
C
C      AH=(2*3.14*DR*H)/(3.14*DR*DR*H)
C      GAMMA= EA/(R*(TW+273))
C      UG=1.0
C      RETURN
C      END
C*****
C
C      Subroutine HPAR
C
C      Subroutine to calculate the parameters that vary with
C      height.
C
C-----
C
C      T = Current temperature
C      Z = Current height
C      Y = Current gas phase concentration
C      I = Number of the current stage
C
C      The commons DCOM, PCOM, and HCOM are passed to this
C      subroutine. See the main routine for a description of
C      the parameters.

```

```

C
C*****
C      SUBROUTINE HPAR(T,Z,Y,I)
C
C      COMMON/DCOM/ALPHA,U,RI,RKFO,DR,H,DP,TW,UGO,WCAT,
C      +          DENCAT,CPCAT,CCATM,CPL,CONL,P,YO,EA
C
C      COMMON/PCOM/ALTWO,UG,EG,DG,BOG,BOL,BOC,A,RKF,DA,
C      +          DL,E,GAMMA,DHR,AH
C
C      COMMON/HCOM/HE,RKL,RKS,STG,STL,STH,CCAT,RNS,PE,HT,
C      +          BE
C
C      Set the constants need for the routine
C      G =
C      G = gravitational acceleration, cm./s*s
C      R = gas constant, J/atm-K
C
C      R=0.008312
C      G=980.669
C
C      Calcualte the Henry coefficeint, Peter, Z. Phys. Chem.,
C      1955,5,p.114
C
C      HE=2.297E7*EXP(-1.2326+583/(T*TW+273))
C
C      Calculate the liquid density, (Fischer-Tropsch product)
C      Satterfield, Chem. Eng. Sci.,1980,35, p.195
C
C      DENL=0.758-0.555E-3*((T*TW)-100)
C
C      Liquid viscosity. Deckwer et.al., Ind.Eng.Chem.Proc.Des.
C      Dev.,1980,19,699.
C
C      VISL=0.052*EXP(-6.905+3266/(T*TW+273))
C
C      Calculate average physical properties of slurry
C
C      VCAT=(DENL*WCAT)/(DENCAT-WCAT*(DENCAT-DENL))*WCAT
C      DENAVG=VCAT*DENCAT+(1-VCAT)*DENL
C      VISAVG=VISL*(1+4.5*VCAT)
C
C      Liquid-gas mass transfer coeffiecient, Satterfield,
C      Chem. Eng. Sci.,1980,35, p.195
C
C      RKL=0.1165*POW(DENAVG/VISAVG*EXP(-4570/
C      +          (T*TW+273)),0.333)
C
C      Stanton number fromtheir definitions
C
C      STG=(RKL*A*H*R*(TW+273))/(UGO*HE)
C      STL=RKL*A*H/UGO

```

```

C
C Calculate the effectiveness factor, solid liquid mass
C transfer coefficient based on Sanger, (see above)
C
  AS=6.0*WCAT*(1-EG)*DENAUG/(DP*DENCAT)
  RKS=EXP(DF,4)*POW(DENL,3)/POW(VISL,3)
  RKS=2+RKS*POW((VISL/(DENL*DL)),0.333)*0.545
  RKS=(DL*RKS)/DP
  RNSO=RKF*CCATM*EL/(RKS*AS)
  RNS=1/(1+RNSO*EXP(-GAMMA/T))
C
C Calculate catalyst concentration, Kato, J.Chem.Eng.Jpn.
C 1972,5,p.112
C
  CCAT=CCATM*BOL/(1-EXP(-BOL))*EXP(-BOL*Z)
C
C Calculate average quantities needed for Deckwer, 1980,
C correlation for heat transfer coefficient.
C
  CPAVG=WCAT*CFCAT+(1-WCAT)*CPL
  DISAX=DL*DENAUG*CPAVG
  DIV2=(1.0-EG)*DISAX
  PE=UGO*DENAUG*CPAVG*H/((1-EG)*DISAX)
  CONAVG=CONL*(2*CONL+CONCAT-2*VCAT*(CONL-CONCAT))
  CONAVG=CONAVG/(2*CONL+CONCAT+VCAT*(CONL-CONCAT))
  HT=(UG*UG*UG)*DENAUG/(G*VISAVG)*(VISAVG*CPAVG/
+  CONAVG)*(VISAVG*CPAVG/CONAVG)
  HT=POW(HT*(VISAVG*CPAVG/CONAVG),-0.25)
  HT=0.1*DENAUG*CPAVG*CPAVG*UG*HT
C
C Stanton number
C
  STH=HT*AH*H/(UGO*DENAUG*CPAVG)
C
C Dimensionless parameter
C
  BE=DHR*P*YD/(DENAUG*CPAVG*HE*(TW+273))*153
C
C Gas velocity,
C
  IF(1.EQ.1) THEN
    UG=1.0
  ELSE
    XH=(YD-UG*Y)/(YD)
    UG=1+ALPHA*((1+U)/(1+RI))*XH
  ENDIF
  RETURN
  END

```

```

C *****
C
C Subroutine YCALC
C
C This subroutine calculates the gas phase concentration
C based on material balance
C
C *****
      SUBROUTINE YCALC(STG,UGO,UG,AL TWO,YO,X,Y,T,DZ)
      REAL X(3),Y(3),T(3)
      T1=DZ*STG*T(2)*(Y(2)-X(2)*YO)
      Y(1)=Y(2)-T1
      RETURN
      END
C *****
C
C Subroutine XCALC
C
C This subroutine calculates the liquid phase composition
C based on a material balance on a small but finite area
C
C *****
      SUBROUTINE XCALC(BOL,STL,DA,RNS,CCAT,GAMMA,YO,X,Y,
+
      T,DZ)
      REAL X(3),Y(3),T(3)
      T1=1.0/(DZ*BOL)*(X(3)-X(2))
      T2=DZ*STL*(Y(2)/YO-X(2))
      T3=DZ*DA*RNS*CCAT*EXP(-GAMMA/T(2))*X(2)
      X(1)=X(2)-DZ*BOL*(T1+T2-T3)
      RETURN
      END
C *****
C
C Subroutine TCALC
C
C This subroutine calculates the temperature based on an
C energy balance
C
C *****
      SUBROUTINE TCALC(PE,STH,BE,DA,RNS,CCAT,GAMMA,X,T,
+
      DZ)
      REAL T(3),X(3)
      V1=1.0/(DZ*PE)*(T(3)-T(2))
      V2=DZ*STH*(T(2)-1)
      V3=BE*DA*RNS*CCAT*EXP(-GAMMA/T(2))*X(2)
      T(1)=T(2)+PE*DZ*(V1-V2+V3)
      RETURN
      END

```

```

C*****
C
C Subroutine REPORT
C
C This subroutine lists the current concentrations.
C
C*****
C      SUBROUTINE REPORT(X,Y,T,I,IP,NSTEP)
C      REAL T(3),X(3),Y(3)
C
C if a short report was indicated list only the final
C three concentrations
C
C      IF((IP.EQ.1).AND.(I.LE.NSTEP-3)) GOTO 20
C      IF(I.NE.1) GOTO 10
C      WRITE(6,100)
100  FORMAT(' I          T          X          Y')
C      10 CONTINUE
C      WRITE(6,110) I,T(1),X(1),Y(1)
110  FORMAT(1X,I3,3F10.4)
C      20 CONTINUE
C      RETURN
C      END
C*****
C
C Function POW
C
C This function raises any number to any power. It was
C written to the inability of the intrinsic function to
C handle negative numbers.
C
C*****
C      BASE = The number to be raised to a power
C      POWER = The number to be used as the power
C
C*****
C      FUNCTION POW(BASE,POWER)
C
C If the base is a positive number set SIGN=1.0 so that
C the answer
C will be positive.
C
C      IF (BASE.EQ.0.0) THEN
C          POW=0.0
C          RETURN
C      ENDIF
C      IF (BASE.GT.0.0) THEN
C          A=POWER*ALOG(BASE)

```

```
        SIGN=1.0  
    ELSE .
```

C

C If the base is negative and the power is even then the
C answer will be positive. If the base is negative and
C the power is not even the answer is to be negative.

C

```
        REM=(POWER/2.0)-INT(POWER/2.0)  
        A=POWER*ALOG(ABS(BASE))  
        IF(REM.EQ.0.0) THEN  
            SIGN=1.0  
        ELSE  
            SIGN=-1.0  
        ENDIF  
    ENDIF  
    POW=SIGN*EXP(A)  
    RETURN  
END
```

```

C*****
C
C Program COMB
C
C   This program calculates the heat required by the
C combustor and the temperature of the combustor.
C
C*****
C
C   Common block
C
C       QP   = Heat load of the pyrolyzer, cal
C       AE   = External heat transfer area, sq.cm.
C       TE   = External temperature, K
C       AI   = Heat transfer area between combustor
C             and pyrolyzer, sq.cm.
C       TP   = Pyrolyzer temperature, K
C       CS   = Heat capacity of the solid material,
C             cal/g K
C       DENS = Density of the solids, g/cu.cm.
C       CG   = Heat capacity of the gas, cal/g K
C       DENG = Density of the gas, g/cu.cm.
C       VIS  = Viscosity of the gas,
C       RKG  = Thermal conductivity of the gas,
C       DP   = Partical diameter, cm
C       EMF  = Void fraction at minimum fluidization.
C       DR   = Reactor diameter, cm.
C
C*****
C   COMMON QP, AE, TE, AI, TP, CS, DENS, CG, DENG, VIS, RKG, DP,
C   +      EMF, DR
C
C   Open the data file. This statement is dependant on the
C the FORTRAN version used. The statement listed is for
C a IBM Microsoft FORTRAN
C
C       OPEN (5, FILE='COMB.DAT', STATUS='OLD', ACCESS='DIRECT',
C   +       FORM='FORMATTED', RECL=80)
C
C   Obtain the initial parameters. (See: Subroutine
C PARAM)
C
C       CALL PARAM(VGC, VGP, HMFC, HC, HMFP, HP, VS)
C
C   Calculate the internal (Subroutine RINTER) and external
C (Subroutine EXTER) heat transfer coefficients

```

```

C
  UE=EXTER(VGC,HC,HMFC)
  UI=RINTER(VGC,VGP,HC,HP,HMFC,HMFP)
E
C Calculate the required combustor temperature to
C provide required heat to pyrolyzer at the required
C temperature.
C
  TC=TP+QP/(UI*AI+CS*DENS*VS)
C
C Calculate the heat losses from the combustor.
C Q1=heat lost through wall
C Q2=heat lost in gas.
C
  Q1=UE*AE*(TC-TE)
  Q2=CG*DENS*VGC*TC
C
C Sum for total heat requirment
C
  Q=Q1+Q2+QP
C
C Write out result
C
  WRITE(0,100) TC,Q
  100 FORMAT(' T Q ',2E12.4)
  STOP
  END
C*****
C
C.Subroutine Param
C
C This subroutine reads in the needed data from the
C input file.
C*****
C
C          VGC = Superficial velocity of the gas
C              in the combustor, cm/s
C          VGP = Superficial velocity of the gas
C              in the pyrolyzer, cm/s
C          HMFC = Height of the combustor bed at
C              minimum fluidization, cm
C          HMFP = Height of the pyrolyzer bed at
C              minimum fluidization, cm
C          HP  = Height of the pyrolyzer, cm
C          HC  = Height of the combustor, cm

```



```

C          VS = Velocity of solids circulation
C
C The common block is passed to the subroutine. See the
C main routine for a description of the parameters in the
C common.
C
C*****
C          SUBROUTINE PARAM(VGC,VGP,HMFC,HC,HMFP,HP,VS)
C
C          COMMON QP,AE,TE,AI,TP,CS,DENS,CG,DENG,VIS,RKG,
+            DP,EMF,DR
C
C          READ(S,*) DC,TE,DR,TP
C          READ(S,*) QP
C          READ(S,*) CS,DENS,VS
C          READ(S,*) CG,DENG,VGC,VGP
C          READ(S,*) HMFC,HC,HMFP,HP
C          READ(S,*) VIS,RKG,DP,EMF
C          AE=DC*3.1416*HC
C          AI=DR*3.1416*HP
C          RETURN
C          END
C*****
C
C Function EXTER
C
C This function calculates the external heat transfer
C coefficient
C
C*****
C          VG = Velocity of gas in the combustor, cm/s
C          H = Total bed height, cm
C          HMF = Height of bed at minimum fluidization, cm
C
C The common block is passed to the function. See the
C main routine for a description of the parameters.
C
C*****
C          FUNCTION EXTER(VG,H,HMF)
C
C          COMMON QP,AE,TE,AI,TP,CS,DENS,CG,DENG,VIS,RKG,DP,
+            EMF,DR
C
C HEW1= Resistance to heat transfer by natural convection
C off the outside of the reactor.

```

```

C HEW2= Resistance from the fluidized bed to the wall
C
HEW1=(0.067544*0.59/DR)*(0.702*0.4462E9*TE*(DR**3))**0.25
HEW2=FLUID(VG,H,HMF)
EXTER=1.0/(1.0/HEW1+1.0/HEW2)
RETURN
END
C*****
C
C Function RINTER
C
C This function calculates the coefficient for the
C inner wall.
C*****
C
C          VGC = Superficial velocity of the gas
C              in the combustor, cm/s
C          VGP = Superficial velocity of the gas
C              in the pyrolyzer, cm/s
C          HMFC = Height of the combustor bed at
C              minimum fluidization, cm
C          HMFP = Height of the pyrolyzer bed at
C              minimum fluidization, cm
C          HP   = Height of the pyrolyzer, cm
C          HC   = Height of the combustor, cm
C
C The common block is passed to the subroutine. See the
C main routine for a description of the parameters in the
C common.
C*****
C          FUNCTION RINTER(VGC,VGP,HC,HP,HMFC,HMFP)
C
C          COMMON QP,AE,TE,AI,TP,CS,DENS,CG,DENG,VIS,RKE,DP,
C          +      EMF,DR
C
C HEW1 = Resistance on the combustor side of the wall
C HEW2 = Resistance on the pyrolyzer side of the wall
C
HEW1=FLUID(VGC,HC,HMFC)
HEW2=FLUID(VGP,HP,HMFP)
RINTER=1.0/(1.0/HEW1+1.0/HEW2)
RETURN
END

```

```

C*****
C
C Function FLUID
C
C   This function calculates the heat transfer
C resistance of a wall in contact with a fluidized bed.
C
C*****
C
C   VG = Velocity of the gas, cm/s
C   H  = Total bed height, cm
C   HMF = Bed height at minimum fluidization, cm
C
C   The common block is passed to the subroutine. See the
C main routine for a description of the parameters in the
C common.
C
C*****
C   FUNCTION FLUID (VG, H, HMF)
C
C   COMMON QP, AE, TE, AI, TP, CS, DENS, CG, DENG, VIS, RKG, DP,
C   +      EMF, DR
C
C   Look up the parameter Si used in the correlation
C
C   SI=SITBL (DP, DENS, VG, VIS)
C
C   HF=1.0-((1.0-EMF)*HMF/H)
C   AT=(1.0+7.5*EXP(-0.44*(H/DR))*(CG/CS))
C   BT=(DP/RKG)/((1-HF)*CS*DENS/(CG*DENG))
C   FLUID=(SI*AT)/BT
C   RETURN
C   END
C*****
C
C Function SITBL
C
C   This function determines the parameter Si
C
C*****
C
C   DP  = Partical diameter, cm
C   DENG = Density of the gas, g/cu.cm.
C   VG  = Gas velocity, cm/s
C   VIS = Viscosity of the gas,

```

```
C*****  
      FUNCTION SITBL(DP,DENG,VG,VIS)  
C  
      RE=DP*DENG*VG/VIS  
      RELOG=ALOG(RE)  
      IF(RELOG.GT.-0.66) GOTO 10  
      A=1.08  
      B=-2.99  
      GOTO 50  
10  IF(RELOG.GT.0.0) GOTO 20  
      A=0.91  
      B=-2.99  
      GOTO 50  
20  IF(RELOG.GT.0.9) GOTO 30  
      A=0.64  
      B=-3.10  
      GOTO 50  
30  IF(RELOG.GT.1.48) GOTO 40  
      A=0.25  
      B=-2.71  
      GOTO 50  
40  A=0.0  
      B=-2.3  
50  SILOG=A*RELOG+B  
      SITBL=10**SILOG  
      RETURN  
      END
```