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LIQUID-PHASE METHANOL PROCESS DEVELOPMENT UNIT: INSTALLATION, OPERATION, AND SUPPORT STUDIES

Technical Progress Report No. 2

For the Period 1 January 1982 - 31 March 1982

Contractor

AIR PRODUCTS AND CHEMICALS, INC. Allentown, PA 18105

and

DOE/PC/30019--T2

DE82 012725

Subcontractor to APCI

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ABSTRACT

This was the second period of Contract performance. During this period approval was obtained for the unified design concept, advanced schedule for relocation of the LPM pilot plant, and advanced procurement of long lead delivery equipment items. The LaPorte LPMeOH PDU Process Flowsheet developed further and the Engineering Flowsment evolved to the Revision OA preliminary issue. Eight cases of point-by-point heat and mass balances were released. Process equipment specifications were issued for 30 of the 33 equipment items. Mechanical specifications were issued for 16 equipment items. Quotations were received for the 2 long lead delivery items, the Feed/Recycle Compressor and the Slurry Circulation Pumps; technical evaluations of these bids are underway. Semifinal equipment arrangement and plot plan drawings were prepared. The Preliminary Hazards Review was conducted and the subsequent Design Hazards Review was initiated. A request for exemption from construction and operating permit requirements was submitted to the Texas Air Control Board. Progress was made on the specification of the Data Acquisition System. In the laboratories, APCI established the priority for compositions of new methanol powder catalysts to be prepared. Construction of the APCI Gas Phase Screening Reactor and Stirred Autoclave Reactor continued on schedule. Progress was made in evaluating the rotential modification of the Deckwer liquid phase Fisher-Tropsch model to describe LPMeOH performance. In the CSI laboratories, a 550-hour liquidfluidized run was completed successfully in the Lab PDU. Preliminary results indicate that the new catalyst tested is more attrition resistant than any prior liquid-fluidized catalyst candidate. Testing of in-situ catalyst reduction procedures continued in the Stirred Autoclave Reactor with successful results which led CSI to file a Record of Invention form for a potential invention covering this process. Specifications and quotations for major equipment items in the CSI liquid-entrained PDU were completed and received. The first of the two lab slurry pumps arrived. A preliminary plan for cold flow hydrodynamic modeling was completed. DOE approved submission of the Task 2 deliverable report on 1 June 1982 in order to increase the accuracy of the program cost estimate. The 1 June deliverable report will incorporate and take advantage of the research achievements and efforts currently underway at APCI and CSI.



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PROJECT DESCRIPTION:

On 28 September 1981, Air Products and Chemicals, Inc. (APCI) began a 42-month contract with the U.S. Department of Energy (DOE): "Liquid Phase Methanol (LPMeOH) Process Development Unit: Installation, Operation and Support Studies." This project is aimed to further develop the LPMeOH process invented by Chem Systems Inc. (CSI). Chem Systems is performing as a subcontractor to Air Products.

A DOE-owned, skid mounted pilot plant will be transferred from Chicago, refurbished, expanded for service as the LPMeOH Process Development Unit (PDU), and then relocated and commissioned at Air Products' LaPorte, Texas facility. Air Products will supply synthesis feed gas to the LPMeOH PDU and operate the unit for a planned 24-month period. Chem Systems is performing the major portion of the laboratory support R&D and is providing withical management for the project. Air Products is providing overall program management and is responsible for engineering design, construction, and operation.

The program is divided into 11 major tasks which are phased to allow progress review and approval to proceed. The 11 major tasks are:

- 1. Program Planning
- 2. Engineering and Design Specifications
- 3. Equipment Procurement
- 4. LPM Pilot Plant Relocation/Inspection
- 5. LaPorte LPMeOH PDU Renovation, Installation and Shakedown
- 6. Liquid-Fluidized Operation
- 7. Laboratory Support Program
- 8. Conversion of the LaPorte LPMeOH PDU from Liquid-Fluidized to Liquid-Entrained Mode
- 9. Shakedown of the Liquid-Entrained Mode of Operation
- 10. Liquid-Entrained Operation
- 11. Project Evaluation

The tasks are phased as follows:

<u>Phase</u>	<u>Tasks</u>	Schedule		
I II III IV V	1,2,4,7,11 3,4,5 6 8 9,10	l June 1982 l March 1983 l January 1984	L - 28 March 1985 (Months 1-42 2 - 1 April 1983 (Months 9-18 3 - 1 June 1984 (Months 18-32 4 - 1 April 1984 (Months 28-30 4 - 1 March 1985 (Months 31-41)

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OBJECTIVES:

The overall objective of this program is to demonstrate the technical feasibility of the Liquid Phase Methanol (LPMeOH) process at the Process Development Unit (PDU) scale of operation.

On a per task basis, objectives are to:

Task 1 - Program Planning

Establish a Project Work Plan presenting in detail all activities which will be performed for the successful completion of the program.

Task 2 - Engineering and Design Specifications

- a) Conduct a process engineering/design review and safety examination of the existing Liquid Phase Methanation (LPM) pilot plant at its present location in Chicago, Illinois;
- b) Obtain permits to install and operate the LPMeOH PDU at LaPorte, Texas;
- c) Develop detailed plans and specifications for the repair, modification, and expansion of the existing LPM unit to enable liquid-fluidized (ebullated bed) and, subsequently, liquid-entrained (slurry) methanol production; and
- d) Develop a deactivation plan for the LaPorte LPMeOH PDU.

Task 3 - Equipment Procurement

Purchase, lease, or obtain from DOE inventories the equipment and systems specified in Task 2.

Task 4 - LPM Pilot Plant Relocation/Inspection

Transfer the existing LPM pilot plant from its present location in Chicago to a vendor's facility for inspection.

Task 5 - LaPorte LPMeOH PDU Renovation, Installation, and Shakedown

- Renovate the LPM pilot plant to become the LaPorte LPMeOH PDU, according to the specifications developed in Task 2;
- b) Prepare the LaPorte site;
- c) Transfer and install the LPMeOH PDU at LaPorte;
- d) Nake interconnections and test components; and
- e) Conduct an integrated run without catalyst.

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Task 6 - Liguid-Fluidized Operation

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Operate in the liquid-fluidized (ebullated bed) mode to:

- a) Assess the effect of reactor configuration/internals;
- b) Identify catalysts which in short runs have acceptable activity and attrition characteristics;
- c) Perform process variable scans to determine the effects of temperature, pressure, space velocity, catalyst loading, circulating oil flowrate, and feed gas composition; and
- Perform a 45-day continuous run to demonstrate short-term process operability, principally at a single set of conditions.

Task 7 - Laboratory Support Program

- a) Conduct literature surveys, develop a bibliography of pertinent references, and maintain liaison with others working on related liquid-entrained (slurry) systems.
- b) Develop procedures for in-situ reduction of commercial powdered methanol catalysts slurried in oil, vapor phase reduction of commercial granular materials which can subsequently be slurried, and simultaneously screen commercial catalysts and develop data for modeling the liquid-entrained reaction;
- c) Synthesize new liquid-entrained catalysts;
- Screen new liquid-entrained catalysts in a gas phase fixed bed reactor, in a liquid-entrained stirred autoclave reactor, and in the Chem Systems' Fairfield laboratory PDU;
- Construct and operate a cold flow model unit to study the hydrodynamics of the gas-slurry reactor;
- f) Modify the existing Chem Systems' Fairfield laboratory PDU to allow liquid-entrained as well as liquid-fluidized operation;
- g) Operate the modified CSI lab PDU to perform process variable scans; and
- Support the LaPorte LPMeDH PDU liquid-fluidized and liquidentrained operating modes, principally by screening catalysts.

Task 8 - Conversion of the LaPorte LPMeOH PDU from Liquid-Fluidized to Liquid-Entrained Mode

Perform necessary process adjustments, alterations, and minor operational tests to facilitate the conversion of the PDU from the liquid-fluidized (ebullated bed) to the liquid-entrained (slurry) mode.

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Task 9 - Shakedown of the Liquid-Entrained Operation

Test components, conduct an integrated run with an inert powder, and conduct an integrated short run with a liquid-entrained methanol catalyst.

Task 10 - Liquid-Entrained Operation

- a) Conduct short runs with promising liquid-entrained catalysts;
- b) Perform process variable scans to determine the effects of various operating conditions; and
- c) Perform a 45-day continuous run to demonstrate short-term process operability.

Task 11 - Project Evaluation

- a) Evaluate data from the LaPorte LPMeOH PDU and the laboratories to develop models;
- Evaluate alternative reactor designs and the two liquid phase operating modes;
- c) Perform detailed process evaluations for commercial-size plants;
- Develop plans for a larger scale demonstration of the LPMeOH process; and
- e) Report on program activities.

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RESULTS:

Task 1 - Program Planning

This task is complete. No activity.

Task 2 - Engineering and Design Specifications

- 2.1* APC1 Management Activities
- 2.1.1 Project Management -

Specifications for dismantling the LPM pilot plant for relocation from Chicago were completed and released. Bids were received and a technical evaluation completed for this contract, and purchase approval has been requested of the DOE.

Specifications for shop inspection of the LPM pilot plant equipment in the Houston area have been completed and technically approved by the DDE. Receipt of bids is scheduled for 21 April 1982.

LaPorte commercial facility flowsheets were marked-up to illustrate the eleven piping tie-ins required for feed gases and utilities to the LPMeOH PDU. Instructions for further detailing of these tie-ins to the LPMeOH PDU battery limit were transmitted in coordination of Design Engineering activity.

DOE excess capital equipment and excess property lists for the Synthoil plant were reviewed to identify potential items for use in the Liquid Phase Methanol Program. A more detailed review and physical inspection of this equipment will be conducted on 21 April 1982.

A review of the Preliminary Hazards Review Report was conducted and a final draft is being developed. A Design Hazards Review Team was organized and assembled to conduct a detailed analysis of the plot plan, flowsheet, shutdown logic, solids handling systems, catalyst reduction and product storage.

Based on current schedules for receipt of vendor quotations for new equipment items and for inspection of the LPM equipment, a request was made to the DOE to revise the submittal date of the Phase I deliverable report that will include a revised estimate of the overall program. A revision from 1 May 1982 to 1 June 1982 was approved by the DOE, to enhance the usefulness of the estimate data.

2.1.2 Economic Evaluation - Work was started on revising an internal Project Scope Report that will consolidate the necessary data for detailed estimating by each performing group within APCI.

* Refers to Work Breakdown Structure Elements.

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- 2.1.3 Communications No Significant Activity.
- 2.1.4 Permit Fees No Activity.
- 2.2 CSI
- 2.2.1 CSI Assistance to APCI Chum Systems provided APCI with review and comment on preliminary flowsheets for the LaPorte LPMeOH PDU. A marked-up flowsheet showing suggested process corrections, control points' and data acquisition points was transmitted to APCI. This mark-up was reviewed in a meeting at APCI on 19-20 January 1982. Plans for dismantling the LPM pilot plant were also reviewed at this meeting including procedures, equipment lists, and skid and piping break points. Chem Systems also participated in the Process Hazards Review held at APCI on 15 March 1982.
- 2.2.2 Data Acquisition System Specification - The LaPorte LPMeOH PDU flowsheets were reviewed to determine and verify the required data acquisition and sampling points on the unit. Calculations to reduce these data points into an operational format were outlined in order to estimate the size of the data acquisition computer. Preliminary quotations and leasing arrangements, as well as catalog information, were received from several vendors on items required in the analytical (i.e., gas chromatographs, analytical balances, interfaces, etc.) as well as the computational (computers, data loggers, printers, etc.) sections of the data acquisition unit. On the basis of this information a preliminary estimate was prepared and the buy/lease option evaluated for the data logger/microcomputer option of the data acquisition system. These results were reviewed with APCI in Allentown on 25 March 1982, where the associated costs and leasing arrangements of the minicomputer option were presented. As a result it was agreed, in principle, to specify the minicomputer system as the leading option for use in data acquisition, provided CSI can maintain complete control and responsibility for the data acquisition task at LaPorte. Final selection of this option is dependent upon confirmation of system and project criteria discussed in the 25 March meeting. In addition, the preliminary configuration and cost estimate for the analytical portion of the data acquisition system was developed. A list of acceptable vendors has been established and final specification sheets are currently being developed as a prelude to formal equipment bid solicitation.
- 2.3 APCI Design
- 2.3.1 Integration -

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Process Flowsheet

The Process Flowsheet, Revision P1, dated 5 January 1982 was attached and described in Technical Progress Report No. 1. Since that time the following change considerations have developed:

1. Elimination of Pressure Leaf Filter (22.55)

A more detailed review of the LaPorte LPMeOH PDU shutdown and the Pressure Leaf Filter operating conditions revealed the following:

- The solids loading is too high for a pressure leaf filter.
- Upon shutdown, the PDU must be quickly evacuated of the catalyst/oil slurry, otherwise settled catalyst sludge will build up and cause numerous blockages. Catalyst settling in lab slurry samples implies there may be 15 minutes in which to begin evacuation, and 30 to 60 minutes available to complete the transfer. (Calculations are required to better determine these times.)
- The oil must be cooled below 180°F (80°C) for conventional pressure leaf filtration. Standard filters use rubber gasket materials and filter aid materials contain some entrapped moisture which could cause foaming when mixed with hot oil.

It is now recommended that the slurries be pressure transferred to the Slurry Preparation Tank (28.30) for temporary holding prior to gravity transfer t. Tote Bins for final disposal. The Tote Bins may be used to decant the slurries to yield a reuseable oil supernatent. Controlled oxidation of catalysts may be performed in the Tote Bins to permit safer handling and direct disposal to a secure landfill. The need and the methods for catalyst oxidation are under review. (A plan to evaluate the pyrophoric nature of spent catalyst/oil slurry is noted in Task 11.4.)

2. Alternative Water Addition Location

In the Revision P1 Process Flowsheet, water addition is shown upstream of the Three Phase Separator (23.10). An alternative route has been added to allow water addition to the top of a small packed section in the vapor outlet of the Three Phase Separator. This capability allows some scrubbing of methanol from the purge/recycle gas. Low methanol content in the recycle gas is desirable in order to accurately measure net methanol production in the reactor.

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3. Catalyst Reduction Vessel (02.81) - (On Hold)

Chem Systems continues to make significant progress in the stirred autoclave tests to optimize in-situ catalyst reduction/activation conditions (see Task 7.2.2). Evidence is mounting that the separate Catalyst Reduction Vessel is not required. Data is still needed on other catalysts to confirm more general abilities to achieve in-situ reduction.

4. <u>Potential Elimination of Spare Slurry Circulation Pump</u> (10.50 B)

The flowsheet for the LaPorte LPMeOH PDU has indicated two Slurry Circulation Pumps (10.59 A & B) since the initial proposal to the DOE for the LPMeOH Program. The proposal considered these pumps to each be 100% design capacity such that an installed spare would be available on standby during LaPorte PDU operation. This dual pump installation was justified originally by considering that the costs associated with a single pump failure leading to the loss of even one LaPorte PDU run would more than outweigh the cost for an additional pump.

Progressive development of the LaPorte LPMeOH PDU design has revealed that three key points of this original justification are questionable:

- Recent developmental experience with hot, high suction pressure, centrifugal, slurry pumps has lead to the commercial availability of equipment that may be considered to have acceptable reliability for the LaPorte LPMeOH PDU operating program.
- Failure of the Slurry Circulation Pump will not necessarily lead to loss of a PDU run since the Slurry Preparation Tank (28.30) will now be used to maintain the slurry in suspension and at temperature.
- Due to difficult technical problems associated with the installation of a stand-by pump in this service, the incremental costs for a dual pump installation over a single pump installation may be several times greater than originally estimated.

In the final analysis it is considered desirable to maintain the slurry circulation loop in the simplest, most direct flowing arrangement, from both operational reliability and safety standpoints. Therefore, a detailed evaluation is in progress to evaluate the suitability of a single Slurry Circulation Pump installation for the LaPorte LPMeOH FDU.

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A Simplified Process Flowsheet for the LaPorte LPMeOH PDU is given in Exhibit 2.3.1-1. This simplified version complements the Revision P1 issue of the Process Flowsheet by providing a clear, smaller-size schematic of the main process lines and equipment. Heat and mass balance points are also given on this flowsheet.

Engineering Flowsheet

A Revision 0 Engineering Flowsheet for the LaPorte LPMeOH 7DU was issued on 10 March 1982. This was subsequently marked up during the Design Hazards Review to produce a Revision 0A edition. A preliminary Revision 0A Engineering Flowsheet is attached as Exhibit 2.3.1-2. This preliminary flowsheet has just issued for internal APCI review and has not yet been approved and signed-off. The preliminary flowsheet does show the current state of development of the P&ID. The next level of development of the Engineering Flowsheet is the Revision 1 issue, which will be submitted in the June 1982 Phase I deliverable report to the DOE.

Heat and Mass Balances

The final design heat and mass balances for the eight (8) design cases, four (4) for the liquid-fluidized mode and four (4) for the liquid-entrained mode, were completed and released in January 1982. The operating conditions for the eight (8) design cases which include the maximum and minimum methanol production cases for both modes of operation as well as four (4) "normal" operating cases are given in Exhibits 2.3.1-3 and 2.3.1-4. The detailed point by point heat and mass balances for the design cases were developed using APCI's process simulator program and are enclosed as Exhibit 2.3.1-5. The key stream numbers for the heat and mass balance are shown in Exhibit 2.3.1-1, the Simplified Process Flowsheet for the LaPorte LPMeOH PDU.

Process Equipment Design

During this quarter, process equipment specifications were prepared and issued for 32 equipment items in the LaPorte LPMeOH PDU. One of these items (Pressure Leaf Filter 22.55) was subsequently voided, and two items are considered as one (O1.10/O1.20 Feed/Recycle Compressor is a multiservice machine) by Project Engineering. Therefore, 30 of 33 valid process equipment specifications are complete at this time. Of these 30 process specifications, 5 exist as revised specifications resulting from engineering feedback. The three remaining equipment items are the Reactor (27.10), the Slurry Preparation Tank (28.30), and

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the Catalyst Reduction Vessel (02.81). The Reactor is the existing reactor vessel (R-101) in the LPM pilot plant; the process specification is being delayed pending further analysis of the need for internals in the liquid-fluidized (ebullated bed) and liquid-entrained (slurry) modes. The Slurry Preparation Tank specification is scheduled for issue by 25 June 1982. As noted above, the Catalyst Reduction Vessel is on-hold pending additional experimental confirmation that this vessel is not required.

Some process design characteristics of key equipment items in the LaPorte LPMeOH PDU are provided in this report as follows:

1. Slurry Circulation Pumps (10.50 A & B)

The process equipment specification is attached as Exhibit 2.3.1-6.

2. Feed/Recycle Compressor (01.10/01.20)

The process equipment specification is attached as Exhibits 2.3.1-7A and 2.3.1-7B.

3. <u>Slurry Heat Exchanger (21.20)</u>

The process equipment specification is attached as Exhibit 2.3.1-8.

4. <u>Reactor (27.10)</u>

A schematic of the reactor and some key operating parameters are given in Exhibits 2.3.1-9A and 2.3.1-9B.

<u>Hazards Review</u>

The Preliminary Hazards Review was completed. The subsequent Design Hazards Review progressed to analyze specific hazards and to document conclusions and recommendations relevant to each item. The "What If?" method of analysis was used to review the Engineering Flowsheet, Revision 0, dated 10 March 1982. As a result of this review the following hazards were recommended for quantification by Fault Tree analysis:

	Description of Hazard	Recomm	uendation
1.	Potentially pyrophoric, hot, oil/catalyst slurry,		lse administrative rocedures to assure

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exposed to air.

2. Run-away reaction.

tight shutoff prior to maintenance on standby equipment in the slurry mode.

- 1b. Monitor errosion rates in equipment and piping.
- 1c. Use administrative controls to prevent overfill of Tote Bins for spent slurry disposal.
- 2a. Provide alarms for low nitrogen flow or high H₂ concentration, specifically for reduction gas supply in liquidfluidized catalyst preparation.
- 2b. Utilize administrative control to eliminate severe consequences of temperature rise upon loss of slurry circulation during in-situ reduction.
- 2c. Develop understanding of catalyst activity and potential for oil cracking on temperature excursions.
- 3. Major release from 3a. Provide adequate pressure Methanol Tank. relieving devices.
 - 3b. Provide high liquid level alarm.

Fault trees on the above items will be completed and quantified upon release of the Revision OA Engineering Flowsheet and the preliminary shutdown logic diagrams resulting from the "What If?" review.

Environmental Permit Action

A request for exemption from construction and operating permit requirements was submitted to the Texas Air Control

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Board (TACB) on 17 March 1982. It is believed that the PDU facility will not make a significant contribution of air contaminants to the atmosphere. The request to TACB included a report on the emission sources and quantities. The emission sources are the flare stack, storage tank vents, pressure leaf filter purge, and fugative hydrocarbons. The continuous process vents of hydrocarbons and CO along with emergency or relief valve vents will be sent to a single smokeless flare designed for complete combustion. Working losses from the storage tanks along with controlled fugative hydrocarbon emissions are estimated to total about 14 T/Y.

The water discharge (treated rainwater runoff from the process area) will be directed to the existing fire pond at APCI's commercial facilities at LaPorte. This water discharge increment is being included in renewal applications for APCI's overall water discharge permit at LaPorte.

Permits will not be required by APCI for handling of hazardous wastes on site. However, cradle-to-grave accounting will be required on all used catalyst/oil preparations requiring disposal.

Methanol product will be disposed of as a fuel and therefore is exempt from EPA regulation.

2.3.2

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Equipment - Exhibit 2.3.2-1 summarizes engineering specification activity for the process equipment items in the LaPorte LPMeOH PDU. Process specifications have been issued for 30 of the 33 equipment items. Mechanical specifications have been issued for 16 items, including 15 of the new equipment items (18 total new items). Quotations have been received on the 2 long lead delivery items (01.10/01.20 Feed/Recycle Compressor and 10.50 A & B Slurry Circulation Pumps) and technical evaluations are underway. Requests for purchase approval for these latter items are expected to be submitted to the DOE by 30 April 1982.

2.3.3 Site/Structural - A site visit was made to LaPorte to verify conditions for tie-in pipe racks, roads and underground road crossing designs.

2.3.4 Piping -

A site visit was made to LaPorte to verify existing piping systems for tie-in. Upon return, design drawings were prepared detailing the required tie-in consturction. These drawings will be utilized for the preparation of take-off estimates to be incorporated into the 1 June 1982 deliverable report.

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Semi-final equipment arrangement and plot plan drawings were prepared based on information from the Design Hazards Review. These drawings and the Revision OA Engineering Flowsheet will form a basis for the LaPorte LPMeOH PDU renovation and installation estimates to be incorporated into the 1 June 1982 deliverable report.

2.3.5 Electrical -

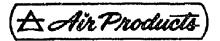
Specifications' have been prepared for switchgear additions to the LaPorte commercial facility that would provide a source of 600 kVA service for the LPMeOH PDU.

Two alternate specifications have been prepared for motor control for the LPMeOH PDU to allow evaluation between matching and line up with the existing LPM pilot plant motor control, and total new purchase of motor control equipment.

- 2.3.6 Instrumentation Support was provided in the development of control loop requirements on the Revision O and Revision OA Engineering Flowsheets.
- Task 3 Equipment Procurement

No Activity.

- Task 4 LPM Pilot Plant Relocation/Inspection
- 4.1 APCI Management Activities
- 4.1.1 Warehousing No Activity.
- 4.1.2 Traffic Services No Activity.
- 4.2 CSI Management Activities
- 4.2.1 On 11 February 1982, a meeting was held at IGT in Chicago, Illinois to inspect the LPM pilot plant with regard to its relocation to a fabricator shop in Texas. A Chem Systems representative was on hand for discussions with IGT personnel and to answer questions pertaining to the pilot plant. Chem Systems also reviewed the APCI specifications for dismantling the pilot plant.
- 4.3 Field Engineering A site inspection was conducted by an APCI field instrument technician on the LPM pilot plant instrumentation. Several loops were energized, and pneumatic valves stroked to establish a list of reuseable instrument items for incorporation into the detailed ship inspection plans.
- 4.4 LPM Pilot Plant Relocation



- 4.4.1 Disassembly A technical evaluation of bids was conducted and purchase approval has been sought from the DOE for award of this contract. Site activity in Chicago is expected during May 1982.
- 4.4.2 Inspection No Activity.
- 4.4.3 Rehabilitation No Activity.
- Task 5 LaPorte LPMeOH PDU Renovation, Installation, and Shakedown

No Activity.

Task 6 - Liquid-Fluidized Operation

No Activity.

Task 7 - Laboratory Support Program

- 7.1 APCI R&D
- 7.1.3 Catalyst Screening and Testing -

APCI Stirred Autoclave (Bench Scale Slurry) Reactor Set-Up

Major items ordered for construction of the 1000 mL Stirred Autoclave Reactor were delivered. Items which were ordered and not delivered as of this writing include:

- 1. Fittings and valves from Autoclave Engineers, Inc. (1 lot).
- 2. Pressure transducers and demodulators (3 ea.).
- 3. Multipoint chart recorder (1 ea.).
- 4. Pressure regulator (1 ea.).
- 5. Gas inlet flow integrators.
- 6. Miscellaneous solenoid valves and fittings.

The construction of the main control panel began, with cut-out holes for missing instrumentation items made from dimensions supplied by the manufacturers. The 1000 mL Stirred Autoclave Reactor was moved into the operations cell and plumbing operations will begin during April 1982. The reactor construction is proceeding on schedule; back-ordered items should not affect the schedule if promised shipping dates are met.

The operation cell area, which was newly constructed, was completed and was checked-cut for proper ventillation with smoke bombs. The area is monitored with recently installed carbon monoxide alarms. The principal lab area is monitored at 4 points. The gas supply lines are located external to the lab and are monitored at 3 points for carbon monoxide. With the final check on the cell operation area ventillation and the installation of the CO monitor, the lab area is now operational.



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High-pressure piping of inlet CO and H₂ gases from the external gas supply area was completed and leak²checked. The high pressure piping for inert and CO, gas supplies was completed; however, the gas cylinder manifold has not been installed. Work on this manifold is scheduled at a later date.

APCI Gas Phase Screening Reactor

Final specifications for this unit were given to Chemical Data Systems, Inc. and construction of this unit began at CDS's facility. Monitoring of progress continued and shipment of the completed unit is expected by 30 April 1982. Exhibit 7.1.3-1 shows a simplified schematic of the unit along with critical measurements and capacities.

7.1.4 Catalyst Preparation -

The methanol catalyst literature search to cover the program needs was initiated and is nearly complete. Discussions with APCI's Corporate Development Department and other Process Systems Group personnel have indicated that one-pound quantities of catalyst in the 45-75 micron range will be provided for testing. The first five catalysts for the program will be prepared for delivery before 30 May 1982. The catalysts will be characterized as to pore size, surface area, analytical composition, and bulk density, although only the composition and particle size distribution will be controlled in the initial preparations.

The preparation priority, from high to low, with respect to composition type is:

- 1. Supported Cu0/Zn0, Cu0/Mg0, Cu0/Zn0/Ceria.
- 2. Cu0/Ceria (Ce⁺³ and Ce⁺⁴), Cu0/Ceria/Alumina.
- 3. $Cu0/Mo0_3$ or $Cu0/W0_3$ types.
- 4. Raney alloys of Cu plus Zn and aluminum and copper plus cerium and aluminum.

Copper-thorium alloys have been dropped from consideration at present. This is due to the practical problems associated with handling radioactive materials. Copper-cerium and/or copper-lanthanum alloys may be recommended as substitutes after further analysis.

Mixed heterogeneous-homogeneous catalyst systems have been ruled out due to potential metal carbonyl volatility problems.

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7.2 CSI R&D

7.2.1 Literature Review -

Cold Flow Hydrodynamics of Three-Phase Systems

The following paragraphs discuss some of the literature reviewed prior to scoping a system for cold flow modeling of the LPMeOH process.

The performance of a chemical reactor with respect to conversion and selectivity depends on the intrinsic kinetics of the various chemical reactions, various physical rate processes such as interphase transfer, and inter and intra particle heat and mass transfer. The effects of these physical rate processes on the reaction performance have been shown to depend on the dynamics of the various phases involved. While there are numerous publications about backmixing in liquid-gas bubble columns and in solid-fluid systems (References 1-5), much less material has been published on three-phase ebullated bed/liquid entrained systems (References 5-8).

Experimental data on Peclet numbers due to axial dispersion in chemical reactors are also very limited. Most of the work has been limited to single phase packed bed reactors. Moreover, data on such systems are only reliable when applied to systems resembling those of the experimental studies (Reference 9).

At the present time, an extensive effort is being directed toward the measurement and evaluation of backmixing in multiphase systems through residence time distribution (RTD) studies (References 10-11). One major problem encountered is that separate RTD measurements are required to evaluate the mixing characteristics of each phase. Although there are numerous methods available to obtain RTDs in complex multiphase systems, measurement problems have been encountered by all recent investigators. Flow maldistribution of the phases can especially impede evaluation of RTD data.

7.2.2 CSI Stirred Autoclave Tests -

The program for optimizing in-situ catalyst reduction techniques for catalyst powders suspended in inert hydrocarbon liquids continued during this quarterly period. To date, seven runs have been completed including five in-situ reduction conditions, one replicate run and a base case. vapor-phase reduction condition.

1. Description of Stirred Autoclave Reaction System

A process schematic of the CSI lab Stirred Autoclave System is shown in Exhibit 7.2.2-1. The heart of the system is a two-liter autoclave equipped with a top entering

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magnedrive agitator assembly and water cooled by an automatic temperature controller. The autoclave is a Model AFP-2005 from Autoclave Engineers. The agitator has a 3/8-inch diameter hollow shaft with two 3/16-inch diameter draft tube inlet holes located ten inches above the 1-1/4-inch diameter impeller. The system is set up in such a way that feed gas, reduction gas and make-up oil can be introduced under controlled pressure and flow conditions. The reactor effluent passes through a shell and tube heat exchanger before it enters the vapor-liquid separator. Auxiliary equipment on the V/L separator allow for sampling of vapor and liquid streams and measurements of flows, temperature and pressure.

2. Catalyst Reduction Test Procedures

This section contains potentially patentable material and has therefore been issued in the Supplement to the Technical Progress Report, marked "Not For Publication".

3. Run Procedures and Preliminary Results

This section contains potentially patentable material and has therefore been issued in the Supplement to the Technical Progress Report, marked "Not For Publication".

4. Calculation Methods

The feed gas contained approximately 15 mole percent of argon as an internal standard for calculation purposes. The calculated data include vapor hourly space velocity (VHSV), hydrogen and carbon oxides conversions, selectivity and methanol productivity.

The VHSV is calculated as follows:

$$VHSV = \frac{V_e}{W_C} \times \frac{Ar_e}{Ar_f} \times \frac{273.15}{273.15 + Te} \times \frac{Pe}{101.35}$$
(Eq. 1)

$$Where: VHSV = Space Velocity in 1'hr^{-1}.kg^{-1}$$

$$V_e = Volume flow of effluent, 1/hr (at STP)$$

$$Ar_e = Mole percent argon in effluent$$

$$Ar_f = Mole percent argon in feed$$

$$W_C = 0xided catalyst charge, kg$$

$$Te = Effluent Temperature, °C$$

$$Pe = Effluent Pressure, kPa$$

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The percentage conversions of feed gas components (H_2 , CO and CO_2) are calculated as follows:

 $C_{i} = \frac{I_{f} - (I_{e} \times \frac{Ar_{f}}{Ar_{e}})}{I_{f}} \times 100$ (Eq. 2) Where C_{i} = Percent conversion of component I I_{f} = Mole percent of I in freed gas I_{e} = Mole percent of I in effluent gas I = H₂, CO or CO₂

If the feed gas has a low CO, concentration (less that three percent), then net CO, will be produced, and the percent selectivity to CO_2 (S_{CO_2}) can be calculated as follows:

$$S_{CO_2} = \frac{\begin{pmatrix} D_e & x & \frac{Ar_f}{Ar_e} \end{pmatrix} - D_f}{M_f - \begin{pmatrix} M_e & x & \frac{Ar_f}{Ar_e} \end{pmatrix}} \times 100 \quad (Eq. 3)$$

Where D = Mole percent of carbon dioxide M = Mole percent of carbon monoxide Ar = Mole percent of argon Subscript e refers to reactor effluent Subscript f refers to reactor feed

The methanol productivity is calculated as follows:

$$M_p = \frac{VHSV}{22.4 \times 100} \times (M_f \times C_M + D_f \times C_D)$$
 (Eq. 4)

Where: M_p = calculated methanol productivity; gmol/hr/kg oxidized catalyst.

When a low CO, content feed gas is used, part of the CO is converted to CO, as well as to methanol. For this case, the selectivity to CO, would have to be subtracted from the term in the parenthesis in Equation (4) in order to calculate the methanol productivity.

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7.2.5 Cold-Flow Model -

The initial scoping of equipment requirements and experimental techniques was conducted in order to determine costs and timing associated with cold flow hydrodynamic modeling of the LPMeriH process.

A cold flow hydrodynamic unit was designed which could be operated as either a liquid-fluidized reactor or a liquidentrained reactor. In the liquid-fluidized mode, the process liquid velocity is controlled over a narrow range in order to fluidize a fixed quantity of catalyst particles within the confines of the reactor. For liquid-entrained operations, smaller catalyst particles are intentionally suspended in the process liquid and are circulated throughout the liquid circulation loop. The process flows and physical dimensions of the hydrodynamic unit broadly resemble that of the LaPorte LPMeOH PDU. A conceptual process flow diagram of the cold flow hydrodynamic unit is shown in Exhibit 7.2.5-1.

It is anticipated that the hydrodynamic test unit would be constructed of materials that are compatible with a range of organic solvents. The process liquids will be selected to have properties similar to those of the hot process liquids. Solvents of differing physical properties would be used in the determination of the density, viscosity and surface tension effects on the hydrodynamic character of the process fluid.

1. Process Equipment

In the liquid-entrained gas/liquid upflow configuration, gas and slurry are co-fed to the bottom of Las reactor (TW-100). Gas is introduced through a suitable distribution device while the slurry is introduced below the gas distributor. Catalyst particle size and process liquid flows would be selected so as to intentionally suspend the catalyst in the process liquid and circulate the solids throughout the liquid circulation loop. By design, the catalyst solids and process liquids must remain a homogeneous mixture everywhere within the liquid circulation loop. Gas/solids/liquids are taken overhead out of the reactor to the V/L separator (VT-100) where phase separation between gas and slurry phases occurs. The separated slurry phase is recirculated to the reactor inlet through a pump (CP-100). The gas phase passes through a demister (VT-101) to de-entrain any liquid droplets. The gas can then be vented or recycled back to the compressor (GC-100). The gas compressor would be equipped with a water cooled aftercooler (HE-100). The gas then flows into a surge tank in order to damp out pressure (or flow) fluctuations prior to passing to the reactor gas distribution system.

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Reactor

The reactor used for the hydrodynamic study would be constructed of a combination of flange-connected glass and metal sections. The column dimensions (identical to the LaPorte LPMeOH PDU reactor) will be 0.56 meters inside diameter by 4.6 meters long. The reactor piping connections at the top and bottom will be flexible. The bottom metal spool piece is designed to support the entire cold flow reactor assembly. Each metal spool piece would be constructed so as to allow for the introduction of sample probes, pressure taps, and other instrumentation as required. The sample probes would be constructed and operated so as to obtain slurry concentration data along the radial and axial direction. A Plexiglass or Lexan shield would be used to enclose the glass column for personnel protection. Sections of the plastic shield would be made removable to allow access to the various sample and pressure taps. Finally, an x-ray source and detector will be mounted so as to traverse the length of the reactor. Alternately, a series of fixed source/detector pairs may be mounted along the vertical length to obtain the density profile.

Pumps and Compressors

A rotary screw air compressor with a water cooled aftercooler would be used for supplying gas. The present design requires a compressor capable of up to 2.8 m per minute at standard conditions and 790 kPa outlet pressure. The compressor discharges into a surge tank to damp out pressure and flow fluctuations.

Magnetically coupled centrifugal pumps will be selected for the slurry feed and circulation loop. These pumps are magnetically coupled to their motor so as to eliminate problems of liquid or gas leakage across a dynamic seal. In addition, these pumps do not require a seal flush flow. The present design requires a pump capable of 830 liters per minute maximum flow at 23 meters total dynamic head.

<u>Catalyst Recovery Filter</u>

A plate and frame filter press is included in the design to be used in determining solids holdup within the column. Additional use would be made of the filter in recovering "used" catalyst upon completion of testing.

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Vessels

The slurry feed tank (VT-102) was sized at 1100 liters to hold the entire contents of the cold flow hydrodynamic test unit. It is baffled at 90° and supplied with an agitator to maintain the catalyst slurry in suspension. Liquid inventory can be monitored by placing the unit on a weigh cell or by using a DP cell. If a DP cell is used, an inert purge gas must be supplied to the high side of the cell to prevent plugging by catalyst. A slurry feed pump (CP-102) is used to transfer the slurry to the main test unit circulating loop.

The slurry preparation tank (VT-103) has a capacity of 400 liters and was sized for slurry addition and makeup in multiple batches. It is also baffled at 90° and supplied with an agitator. Inventory control would be accomplished by placing the unit on a weight cell. Slurry is transferred from the vessel to the feed tank or the main circulation loop through the slurry transfer pump (CP-101).

2. Experimental Techniques

Test methods for determining hydrodynamic system characteristics can be categorized as being either external or internal monitoring techniques. External techniques are preferential in that they do not interfere with established flow patterns. Internal methods involve the insertion of devices through the test cell wall, consequently inducing flow disturbances downstream of the sample location.

External Methods

Sonic probes and gamma-ray scan techniques have been used to obtain data on the average bulk density in multiphase systems. Gamma-ray techniques make use of differential absorption of radiation by various materials. Being an external technique, it is an excellent method for determining the average density of a multiphase system without creating a flow disturbance. A movable density gauge could traverse the length of the reactor and give point bed density measurements directly. These measurements combined with fluidized bed height measurements give a direct evaluation of the relative liquid, gas and solid phase volume fraction.

Sonic techniques are alternate external methods for determining densities of multiphase systems, using sound rather than radiation. In single-phase systems,

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phase-time and dual-path sonic probes (which measure sonic impedance) can be used to determine density. These devices can also be used in two-phase, liquidsolid slurry systems, provided that the sonic impedance of the two-phase mixture is a very weak function of slurry concentration. These devices cannot be used when a bulk gas phase is present because discrete gas bubbles give rise to interfering sonic reflections. It can measure vertical bubble rise velocity or slurry velocity.

• Internal Methods

Several tracer testing methods are known for determining residence time distributions, flow rates and relative phase volumes in multiphase reactors. The techniques employed involve use of a tracer component with an internal or external monitoring device. External detection systems are preferred as they will not interfere with established flow patterns.

In general, flow patterns can be studied by injecting a tracer into a vessel inlet stream and observing the subsequent concentration profile at the outlet. At steady state, methods used consist of injecting a continuous tracer into the inlet of a studied interval and measuring the upstream concentration. For large diameter columns, problems are encountered in obtaining a homogeneous dispersion of the tracer. Further, attempts to obtain an average sample profile across the column can be difficult without disturbing the original flow patterns within the column. When continuous sample withdrawal is employed, sample time effects may distort the measured response. Unsteady state methods of measuring residence time distributions consists of injecting a momentary tracer pulse at the reactor inlet and measuring the response function at the outlet. Pulse injection methods are preferred to step or frequency response methods since inputs requiring large quantities of tracer are impractical on large units. Pulse injection techniques are simple, inexpensive, and require only small quantities of tracer material.

In performing a tracer study, proper tracer selection is extremely important. The hydrodynamic response must be characteristic of the flowing phase and not a function of the tracer component. Any tracer employed should be miscible and have physical properties similar to the bulk fluid phase. The tracer must not be transferrable to the other phases of the system. All tracers under consideration should be accurately

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detectable in low concentrations to minimize disturbances in the established reactor flow patterns.

To enable tracer detection in fast moving streams, the data recording equipment must offer exceptional sensitivity with a minimal detection response time. For simplicity and accuracy, the response of this equipment should be linear.

Gas, liquid or solid tracers can be injected into a flow system to determine the responses for each phase. For the gas phase, a tracer gas injected into a multi-phase reactor would have its concentration measured by a thermal conductivity or infrared absorption cell. Alternately, a radioisotope is substituted. In using gas phase tracers, absorption into the liquid phase precludes an accurate determination of the gas phase mixing and holdup without an independent measurement of tracer content in other phases. The differing rise velocities of individual bubbles further complicate the detector response. Because of these inherent difficulties in using gas phase tracers, only qualitative data concerning gas phase mixing are available in the literature.

The use of liquid tracers are well accepted industrial practices. Problems associated with their use are the familiar ones of sampling induced errors when internal techniques are used. External techniques employed include the use of dyes coupled with high speed photography and radioactive tracer methods. Unfortunately, photographic techniques relying on photochromatic dyes or particle luminescence cannot be used if the color change is obsured by the catalyst particles. In larger diameter columns wall effects can also obscure the events from photographic interpretation.

For the solid phase, a magnetic tracer can sometimes be used. The concentration of a solid phase tracer may be measured by a capacitance probe if the dielectric constant of the tracer material is substantially different than that of the solid phase. In general, for solid phases, a suitable radioactive tracer is often the most convenient to use. If proper precautions are observed, a radioactive tracer has a distinct advantage over other tracers in that the tracer detection devices can be mounted externally. In this way, no disturbances in the established flow patterns resulting from the presence of probes or sampling devices are encountered. The use of a radioactive tracer permits the time distribution function of a

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rapidly moving phase to be accurately determined, since scintillation detectors can be interfaced with high speed recorders or with multi-channel analyzers with data storage capabilities.

7.2.6

CSI Lab PDU Modifications

The request to purchase the first of two slurry pumps was approved. Meanwhile, all responses on the RFQ for fabrication of vessels and skid equipment for the CSI lab PDU were received and evaluated. It was decided, however, at a meeting held in Fairfield on 25 February with APCI personnel not to hire a contractor to build a complete skid-mounted unit. Instead, only major equipment items, such as process vessels and heat exchangers, will be fabricated outside with the majority of engineering, skid design and assembly handled by CSI in-house. This change has been necessitated to allow more project flexi-bility, lower overall costs and improved scheduling. Work began on the assembly of a technical package which will serve as sufficient documentation for required purchases of equipment or services. This package will contain process flowsheets, heat and material balances and a description of the liquidentrained CSI Lab PDU. The process flowsheets will eventually evolve into complete engineering flowsheets. This package when assembled will accompany any requests for approval sent to APCI/DOE.

- 7.2.7 CSI Lab PDU Experimental Program This subtask will not be initiated until the CSI Lab PDU modifications are completed.
- 7.2.8 LaPorte LPMeOH PDU Support -

Overview

United Catalysts Inc. has developed under EPRI support (Reference 12) a methanol synthesis catalyst for the liquid-fluidized (ebullated bed) mode. This material represents a catalyst candidate with potentially better attrition resistance than any catalyst tested under the prior EPRI contract (Reference 13). A 10 lb sample of this catalyst (CSI Identification Number R71/OF12-02) was shipped to CSI's Fairfield Research Center for evaluation in a test in the CSI Lab PDU. The catalyst was charged to the reactor on 16 February 1982 and was reduced utilizing a vapor-phase reduction technique over a three-day period. Two days of testing concentrated on the three-phase fluidization properties of the catalyst suspended in Witco mineral oil, prior to the actual synthesis test. The catalyst was brought on-stream with a 2/1 H_o/CO feed gas, and operating conditions were maintained constant for a period of about 370 hours.

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During this period, CO conversion and settled catalyst bed height were monitored. Fines generation, as determined by pressure drop buildup in the oil filters and decrease in settled bed height, was higher in the first two days on-stream time than during the later part of the run. Both factors were lower than experienced previously with another catalyst (FX2/ IF15-02) tested under a previous EPRI contract (Reference 13). A measure of the attrition resistance characteristics of the catalyst will be obtained upon inspection and post-mortem analysis of the catalyst recovered from the reactor at the conclusion of the run.

During the Lab PDU operation, a process variable scan was also made to study the effect of temperature, space velocity, pressure and synthesis gas composition on catalyst activity and productivity to methanol.

CSI Liquid-Fluidized Lab PDU Description

The CSI Lab PDU reactor is 0.092 m I.D. x 2.13 m high, and the catalyst bed height can be varied from 0.6 to 1.5 meters. The detailed engineering design of the CSI Lab POU has been presented elsewhere (Reference 14). The premixed synthesis gas feed is delivered to the laboratory in a tube trailer. A gas compressor is used to feed the gas to the reactor. In this manner, the pressure in the tube trailer can be reduced to 2170 kPa before a new supply is required. Two compressors are provided to allow flexibility in feed gas rate. Product methanol and small amounts of vaporized oil are condensed out of the product gas/vapor stream. Phase separation occurs at ambient temperature with a typical residence time in the product separator of one The oil is recycled back to the process oil circulating hour. loop. The product gases, following analysis, are sent to an incinerator. Sufficient instrumentation is provided for automatic control and monitoring from a remote control room. The system is designed for pressure up to 7000 kPa and temperatures up to 400°C. All necessary gas streams are connected to a common manifold and are constantly purged to reduce sampling time lags. The selected gas stream may be directed to each chromatograph column, in turn, to analyze for components of interest.

Preliminary Analysis of Short-Term Attrition Test

After the CSI Lab PDU was pressure tested, the reactor was loaded with fresh oxided catalyst (R71/OF12-02) and reduced over a three-day period. The system was put on-stream at conditions similar to those used in the previous EPRI-funded test made in November, 1978: 250°C reactor temperature, 7000 kPa and 3000 hr VHSV (Reference 13). These conditions were held constant for 370 hours before process variable scans proceeded. The complete run chronology is shown in Exhibit 7.2.8-2.

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At the onset of the run, CO conversion was 34 percent and then dropped linearly to the 28 percent level within 100 hours. During this time period, the settled catalyst bed height decreased to 93 percent of its initial height. For the remaining time, 270 additional hours, the CO conversion hovered at the 28 percent level while the settled catalyst bed height decreased to 81 percent of its initial height. These results are shown graphically in Exhibit 7.2.8-1.

The next 70 hours of running time were utilized in performing a process variable scan. The preliminary results of these tests are shown in Exhibit 7.2.8-3. At the termination of these scans (440 total hours on-stream time), the settled bed height had dropped to 78 percent of its initial height. Setting the system back to the initial run conditions gave a slightly lower CO conversion (27.5 percent) than the value just prior to the start of the variable scan.

With 460 hours logged on the catalyst, a short scan was performed using a low CO₂ (1.5 percent) content $2/1 H_2/CO$ feed gas. This synthesis gas resulted in essentially the same CO conversion as the 10 percent CO₂ gas with the exception that a small percentage of CO had apparently shifted to CO₂.

The synthesis gas used for the initial conditions was put back on-line resulting in a CO conversion of 27.5 percent. The settled catalyst bed height at this point was 75 percent of its initial height. After a total of 555 hours on-stream time, the settled catalyst bed height was 73 percent of the inital height and CO conversion was 27 percent. A short test using a 0.6/1 H_0/CO feed was then performed before the unit was shut down.

The unit will be disassembled to recover the catalyst and then cleaned up and placed in a stand-by condition. Catalyst and oil samples will be analyzed. The analysis of the non-hydrocarbon liquid products is not complete at this time but indicates a 96±1 weight percent methanol content with the remainder being Witco 40 oil, water and a small amount of higher alcohols ethanol through hexanols.

Task 8 - Conversion of the LaPorte LPMeOH PDU from Liquid-Fluidized to Liquid-Entrained Mode

No Activity.

Task 9 - Shakedown for Liquid-Entrained Operation

No Activity.

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Task 10 - Liquid-Entrained Operation

No Activity.

- Task 11 Project Evaluation
- 11.1 APCI Management Activities
- 11.1.1 Project Management -

The Project Status Reports, Format 5 Reports, and quarterly Technical Progess Report No. 1 were coordinated.

An arrangement was made to provide closer liaison between APCI design engineers and CSI's laboratory personnel following review of CSI's requisitioning material for a skidded assembly for modification of the Laboratory PDU to permit liquid-entrained operation. The specification, design, and erection of this unit remains in CSI's subcontract scope; however, APCI will take a more active role in engineering assistance and specification review. A rough project plan was worked out to establish requirements for future purchase requests by CSI in this area.

A meeting among APCI, CSI and DDE was held in Pittsburgh on 18 March 1982 to clarify procurement and approval procedures. A brief presentation was made by APCI and CSI on the program status.

- 11.1.2 Economic Evaluation No Activity.
- 11.1.3 Travel and Living APCI and CSI met on several occasions in Allentown and Fairfield and once in Pittsburgh. APCI's Operations Manager from LaPorte attended meetings in Allentown and Chicago. Two trips were made to Chicago by APCI and CSI personnel to review LPM pilot plant relocation specifics.
- 11.2 CSI Activities
- 11.2.1 Data Evaluation Information from the CSI Lab Stirred Autoclave and the CSI liquid-fluidized PDU runs was evaluated and reported under the corresponding subtasks. Thorough analysis of data from both of these units will continue into the next reporting period.
- 11.2.2 Design and Economics No Activity.
- 11.2.3 Process Scaleup No Activity.
- 11.2.4 Reporting Monthly Project Status Reports, management reports and the first quarterly Technical Progress Report were issued. Work was completed on a paper for presentation. A meeting was

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held at PETC on 18 March 1982 to discuss current project status and equipment review/purchase procedures. Work began on updating the CSI Project Work Plan including schedule, manpower and costs. This will be part of the 1 June deliverable to DOE from APCI.

- 11.3 APCI Design
- 11.3.1 Integration -

APCI reviewed and technically approved CSI's first Laboratory PDU slurry pump purchase. A technical difference exists between recommendations of the International Coal Refining Co. and Lawrence Pump Co. regarding the most appropriate seal arrangement for this application. Due to the experienced position Lawrence has with various pilot plant operations in hot, high pressure, slurry service these recommendations are being given thoughtful consideration.

Technical review and approval were given by APCI on CSI specifications for pressure vessels and a slurry heat exchanger required for modification of CSI's Laboratory PDU for liquidentrained operation.

- 11.4 APCI R&D Activities
- 11.4.1 Corporate Development Department ~ Input was provided to the Monthly Status Reports and Technical Progress Report No. 1. Meetings were held with the CSI Fairfield laboratory staff to strengthen the technical liaison between the research organizations.
- 11.4.2 Process Systems Group R&D -

Preliminary Viscosity and Density Data

In support of the LaPorte LPMeOH PDU design effort, preliminary viscosity measurements of Vitco 40 oil/MC-2 catalyst slurry were carried out using a Brookfield LVT viscometer with an ultra low viscosity adapter attachment and spindle. The variables included:

Temperature	-	67°F to 482°F (19 to 250°C)
Slurry Concentration	-	0 wt%, 12 wt% and 25 wt%

Immediately before measurement for slurries, the U.L. adapter was removed and shaken vigorously to ensure a uniform solids suspension during the viscosity measurement. Preliminary results indicated that 25 wt% slurry viscosity showed a strong shear-rate dependence. These results are suspect from several points of view. The data are currently being evaluated and the full report and conclusions will be included in the next quarterly

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report. In addition to the viscosity data, the density, the volume % and % value change of 12 wt% and 25 wt% slurry were measured at $71-72^{\circ}F(22^{\circ}C)$.

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Pyrophoric Nature of Spent Catalyst

An experimental plan was developed to assess the pyrophoric nature of oil/catalyst slurries. Three types of experiments have been considered:

- Qualitative observation of oil/catalyst slurries in an open air environment (hood).
- Differential Thermal Analysis (DTA) of oil/catalyst slurries (1-5 mg) to determine quantitatively the timing and the temperature at which auto-ignition would occur.
- 3. Heat of combustion measurements of oil/catalyst slurries (1 g sample) to verify the theoretical calculations for the largest possible energy release.

This plan is ready for circulation within APCI for review and comment.

Fundamental Model for LPMeOH

Progress was made in exploring fundamental modeling of the LPMeOH reactor and reaction kinetics. A computer model written by Professor W. D. Deckwer of Universitat Hannover (West Germany) for Fischer-Tropsch synthesis in a slurry phase reactor was tested. (This computer program is not generally available to the public but was made available by Professor Deckwer under a private agreement with APCI. It is planned to report results from the computer model; the software programming will not be reported without prior agreement with Professor Deckwer.) The Deckwer model is well described in Reference 15. The computer program was made operational and the results of computations published in Reference 15 were duplicated. The strategy is now being developed to model the LPMeOH fluidized (ebuilated bed) and entrained (slurry) reactors by modifying the rate expressions, modifying the mass balances to allow both solids and liquid to flow in and out the reactor, and by incorporating appropriate hydrodynamic parameters at high liquid velocities.

Liquid Phase Reactor Patents

A preliminary patent search on 3-phase slurry reactor designs was made regarding possible infringements of the LaPorte LPMeOH PDU reactor design on the prior patents. The search revealed that the current simple reactor designs at LaPorte probably do not infringe any prior patent because the prior 3-phase reactor patents are largely process-oriented.

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Input was provided to the Monthly Status Reports and the Technical Progress Report No. 1. Meetings were organized and held with the CSI Fairfield laboratory staff to enhance technical communications.

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ATTACHMENTS

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	2.3.1-5
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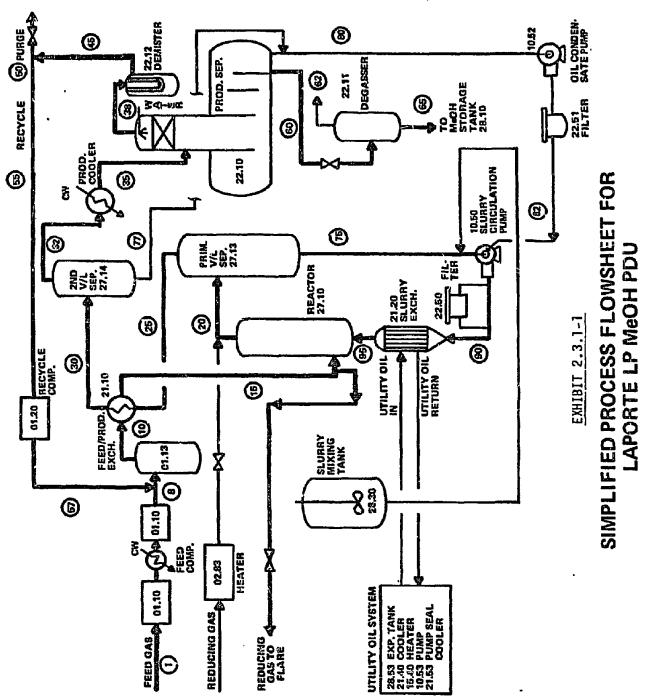
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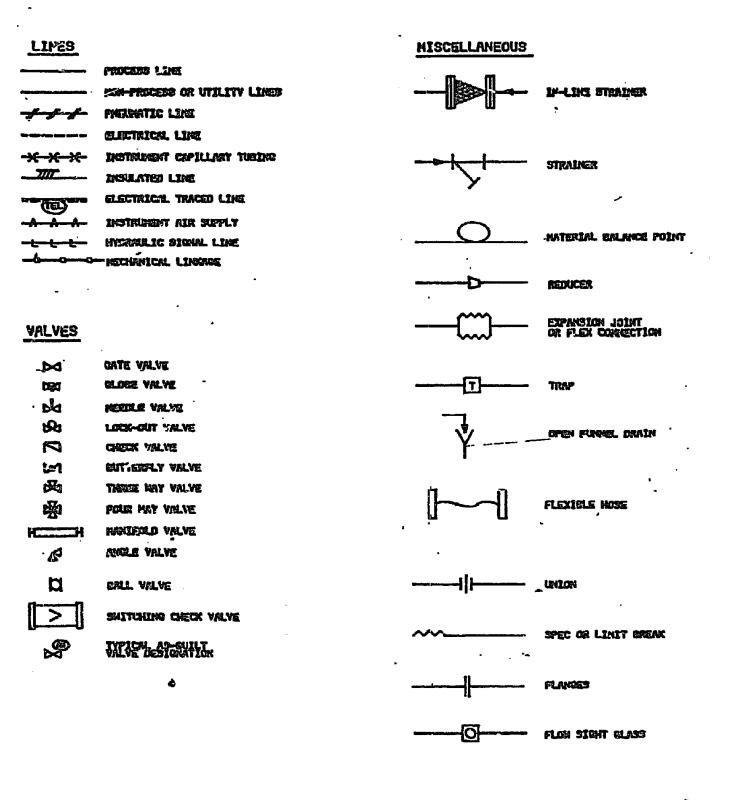
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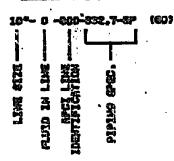
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BOLS AND ABBREVIATIONS

LINE DESIGNATION



FLUID ABBREVIATIONS

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AR	ACIO ENS
KAP -	AIR PURES
AR	PEONATIS
Elenn	BOILE: PESS KATER
	METHANK
C 44	COOLING WATER
0	BOHTMEN
ČS.	OISTATL SELFIDE
	SPILLENT
F9	
FO	Feed Gay Fuel Cil
G2.	GLYCEL
M	NTROCEN
IA	INSTRUMENT ALC
IFF	244 LUENT
K	CAROERCATE
L	LUCRICATING DIL
LOL	LEAN OIL
KEA	MEA .
R	NITROCON
ñr	en philippa
0	DAYDEN
P 0	PRODUCT GAS
5H	POTAGLE HATER
R	ARCON
87 9	REDUCTION CAS
RCL.	riq; oil
8	Stern
SL.	SLUDOG
8190	6740
S Y	SLURRY
uo	UTILITY OIL
Va	VENT CAS
HAS.	HASTE ACTIVATED
	SLUZAR
NO	WASTE OIL
We	HASTE NATER

PIPING MATERIALS

AU.	ALMING: MLCY
CP .	Grand Pipe
6T -	eras Ture
C9	CALYMNIZED
CI	CAST IRON
62°	COPPER PIPE
C3	Candon Steel
650	CAREON STEEL (DAYCON)
C?	COPPER TURE
TAB.	INSTRUMENT AIR SUPPLY
39	Stainliss steel
'YA	TUNCED BLLOY LAPLE
VC	VITRIPIER CLAY

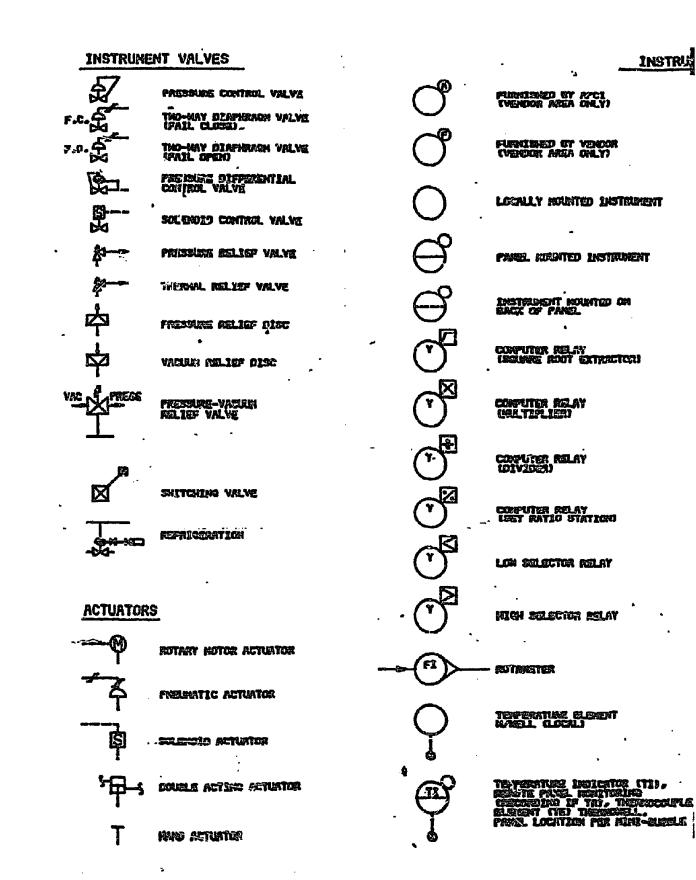
CSO GALVANZZED

MISC. ABBREVIATIONS

6903	NYDROCHARGE REALYER
0.23	ATTROUGH ANALYZER
1023	CITCEN ANELYZER
L/H	RUTO-RAUSSI STATION
C.8.	COLD 201 -
c.ø.	CRCES OVER
F.C.	FAIL CLOSE
R.G.	FIELD
1 0.,	FAIL OPEN
0.9.	CAS SAUTLE
i.PT.	
1.3.	INSIDE
1/2	CANADAT TO PRECATIC TRANSDUCER
	LOWER COPLOSIVE LIMIT
	LICK OPPN
L.PT.	
L.9.	LIGUID SAFELE
0.9.	
	PREDSTAR TAP
8.8.	SET POINT
9-5 7-3.	TO STACK
1.3. U.\$.	UTILITY STATION
V.8. V.8.	Vacian Greater
.e.	ADDIE CRICED
	rich is concept
U.Q.	
u.a.	
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INST F.O R: ACTUAT **~** ፕ ኑዋ

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RICER

INSTRUMENT IDENTIFICATION INDEX

		FLAST	LETTER	T		UCCEEDING LE	TIME
		MEASURED VARIAGLE	MODIFIER	Γ	Paddiae		PAT:
fixed restriction origics	1	AUNLYD18	1	┢╴	ALASSA	+	
	L	BURNER				<u> </u>	
	C	CONCUCTIVITY		Γ	·	CONTROL	
, orifice		DENSITY	DIFFERMINAL			1	+
	E	VOLTADE			ELENENT	<u> </u>	
Vertial	F	RAH	RATIO.	 		<u> </u>	
VETTOMA	0	ONUQINO		┢	GLART		
	H	HAND		-			
	1	ELECTRICAL			INDICATE	<u> </u>	HIGH
FITOT TUBE	1	POWER	BCAN		ANDALAID		
•	K	TINE					
ANALYZER	E	LEVEL	······································		LIGHT		LEGH
Sandarya a granta	H	HRIDITY					
	18	DERODICY					MICOL
uas chromatosrafh	0			-	ORIFICE		
- "	, [P	PRESSURE			FOINT		
	a	QUANTITY	INTEGRATE	ar yang s			
CALORINETER	F	MOLORCTIVITY			650280		_
Instrument	. 3	876ED	SAFETY	-		SMITCH	<u>+</u>
instructur Bistic Direzan	T	TEXTERNIURS				TRACENIT	+
	U	RET			ALTIFUNCTION		
Conflitter DATA LOGOER	V	VISCOSITY				VALVE	Processor 1
	H	1001			MELL.		
PRESS. TAP-PLU20ED	X	SCLENOID		-1			<u> </u>
-	Y	VIERATION				RELAY	
· · · · · · · · · · · · · · · · · · ·	12	POSITION		\neg		ORIVE	
			المحود ورجا				L .

NOTES:

and .

(21	For any additional instrument identification and streaks. Forthe TD The 12A structure. Courteen 15.1. of the flowment grave.	
(2)	New Instructure 72.5 Instruct Control Control Control Film The Placement Control	6
(3)	ect-for velys with intersel controllor by-for velys with defaunte controllor 8-13 The latter for screened variable	e
(4)	AL AT MARE CONNTING TO PLANNELS ONS LINES SHELL CONTON TO GAR. DES. STD. STO.9	

PANEL LECEND

3) - Hain Control Panel -

3 01.10 MO 01.37 PHEL UPCI - FLONSHEET LEC

9 01.10 AND 01.20 PARE. (VEDCOR)

AWALYZER PRIVEL

PERMIT

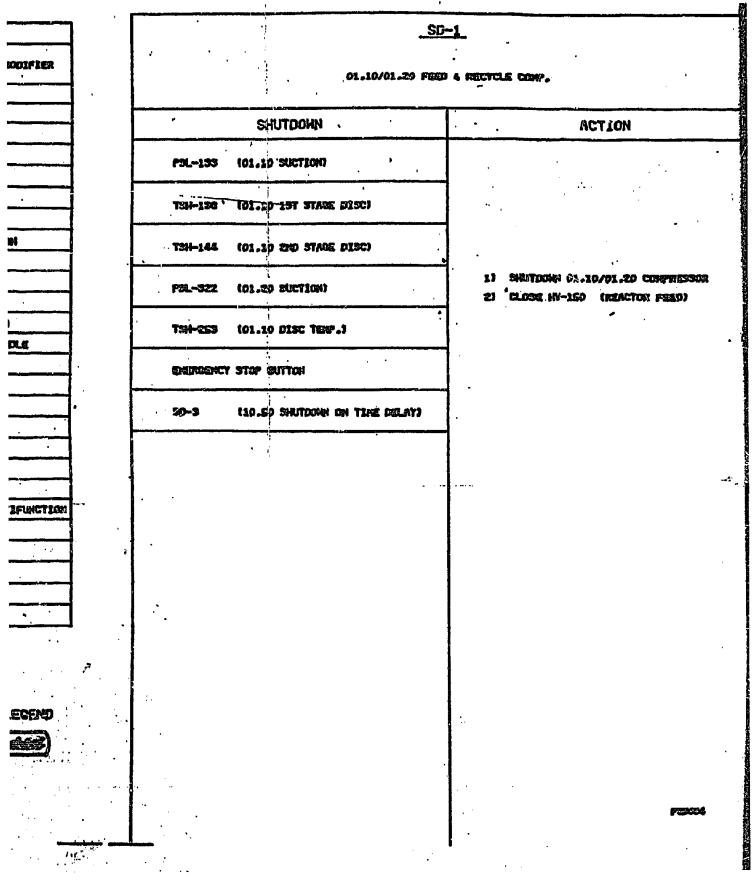


TRUMENTS

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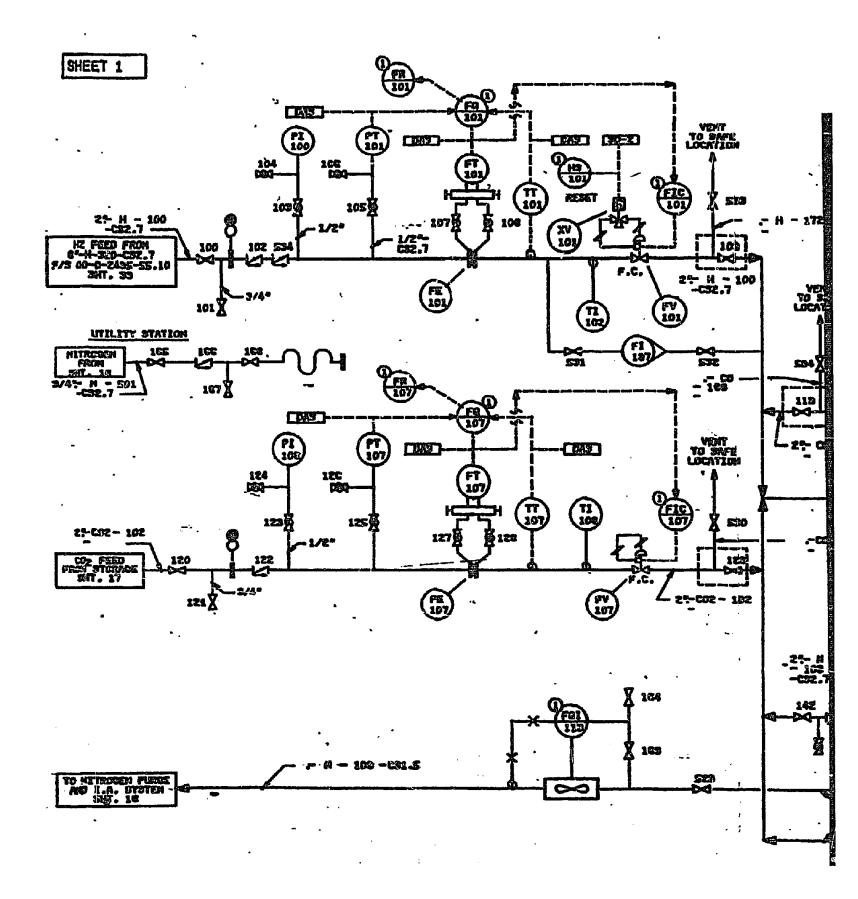
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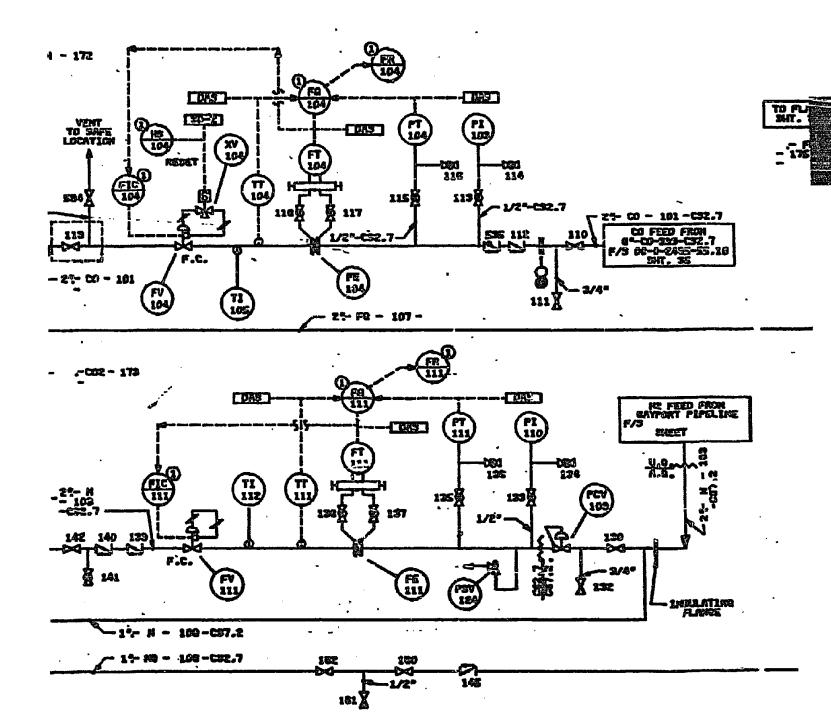


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			·					
		•	Shutdown	•		ACTION		الكواب ما المحمد الأرابي ا
-		ENERGENCY	TRIP		(1) (3	CL055 FV-101 CR2 FEED	•	:
		TSH4-120	(HICH REACTOR TEPP)		ຸ ສ)	CLOSE FV-101 CR2 FUED) CLOSE FV-104 (CJ FNED) TLOSE FV-118 (CH4 FUED)	••	
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			SHUTDOWN			ACTION		
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	<u>SD-4</u>	
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Shutoohn	ACTION	· ·
PSL-274 (LON GARLER FLUID PRESS.)	1) CLOSE PV-181	
Posl-173 (PURP DIFF. PRESS.)	21 3/2-3	
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	<u>SD5</u>	
SHUTDOHN LSLL-515 T22.11 LOH (SVEL)	ACTION	
Shutdohn		
SHUTDOWN	ACTION	

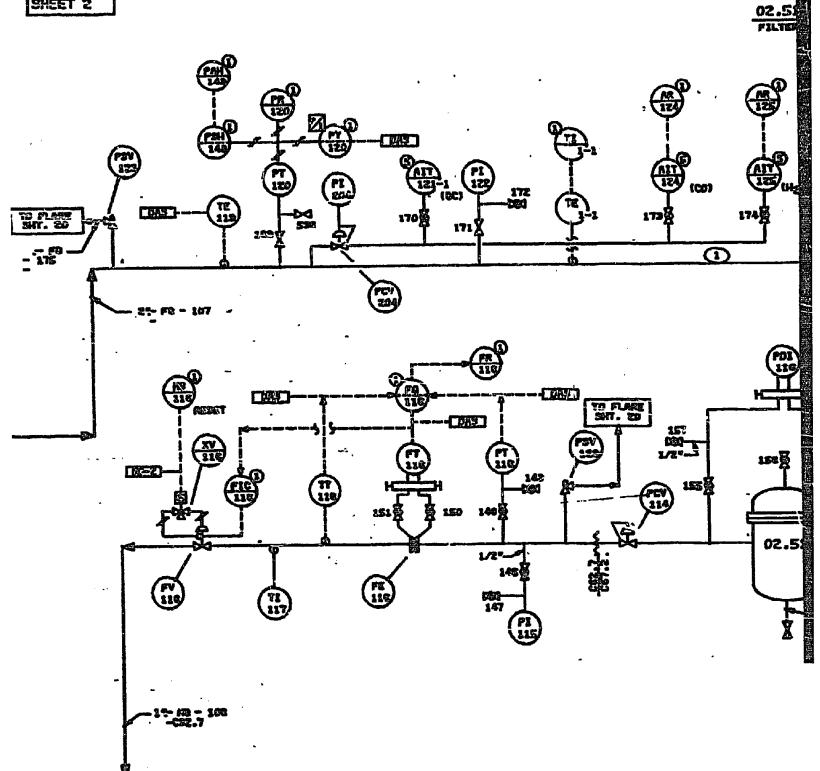


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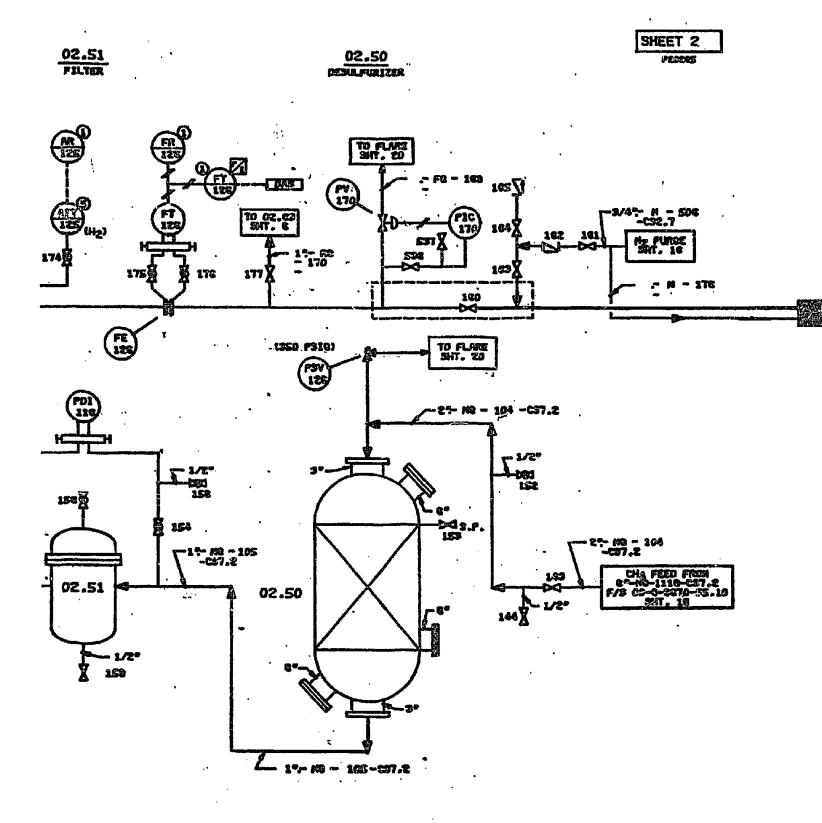
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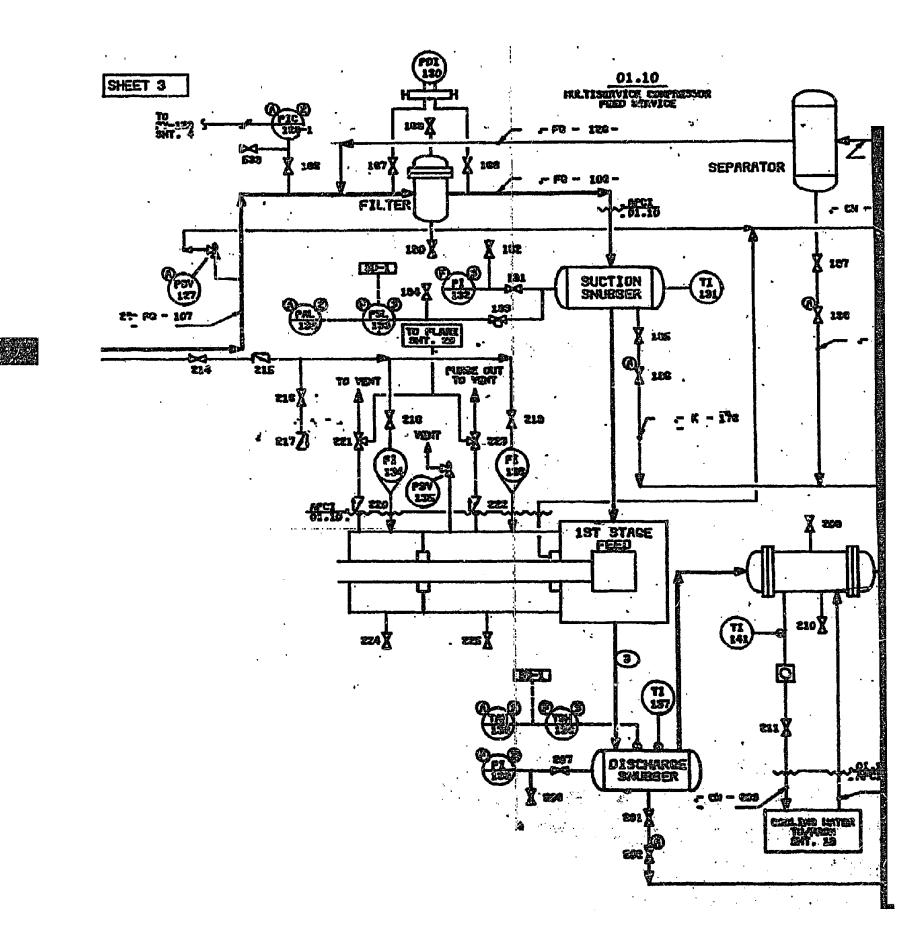
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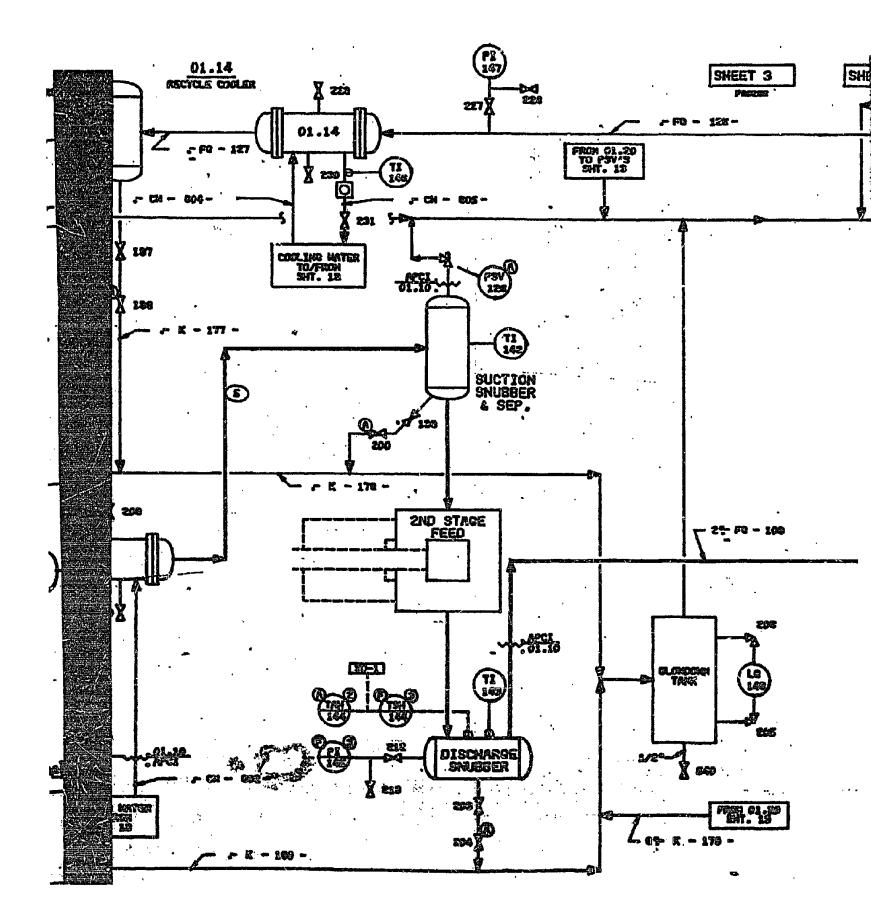


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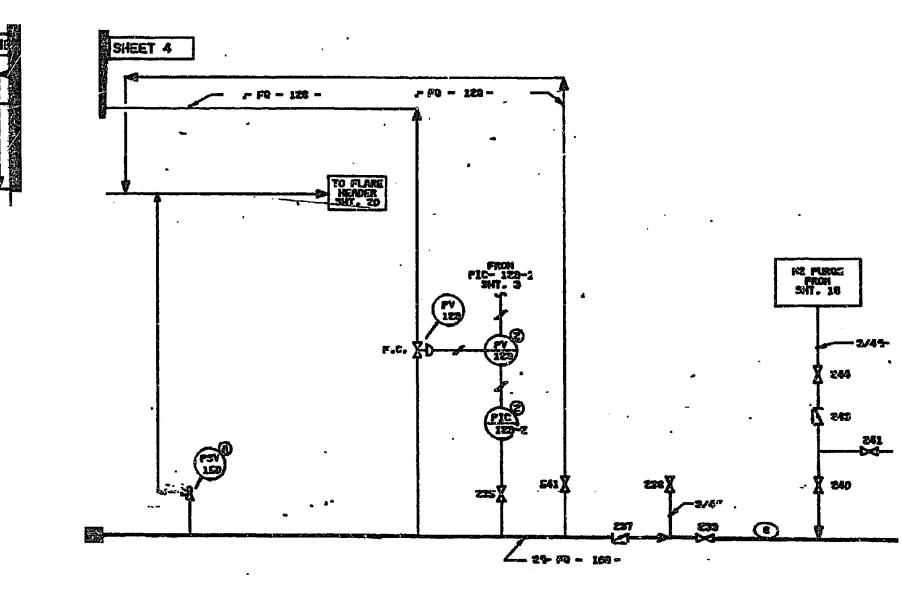
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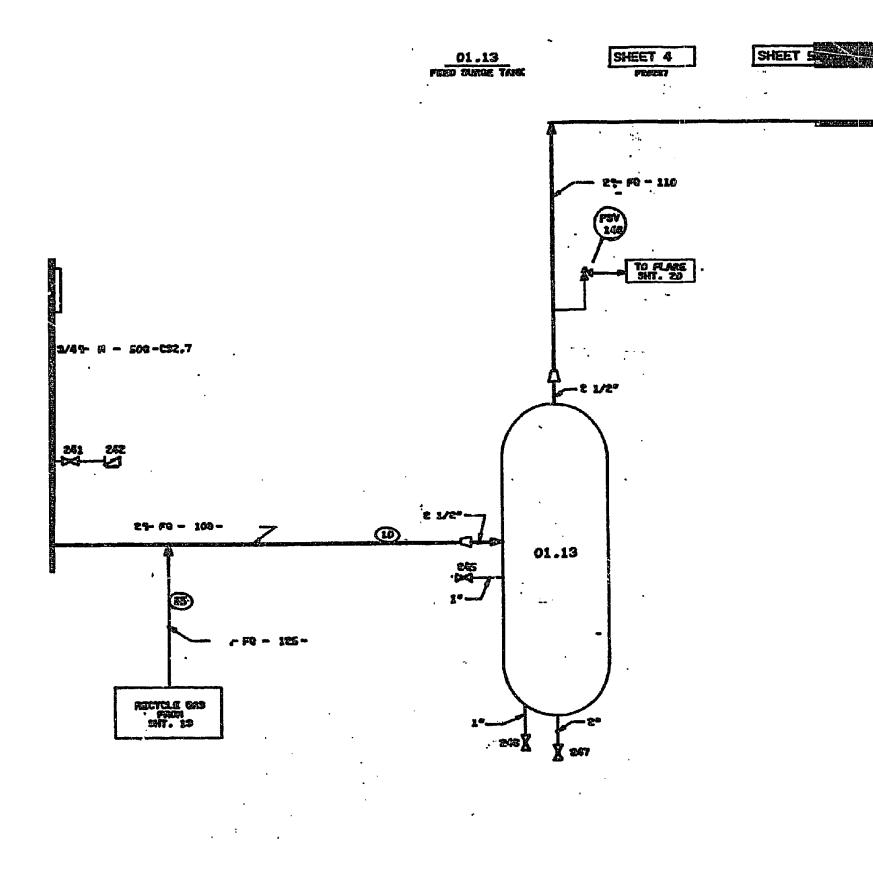


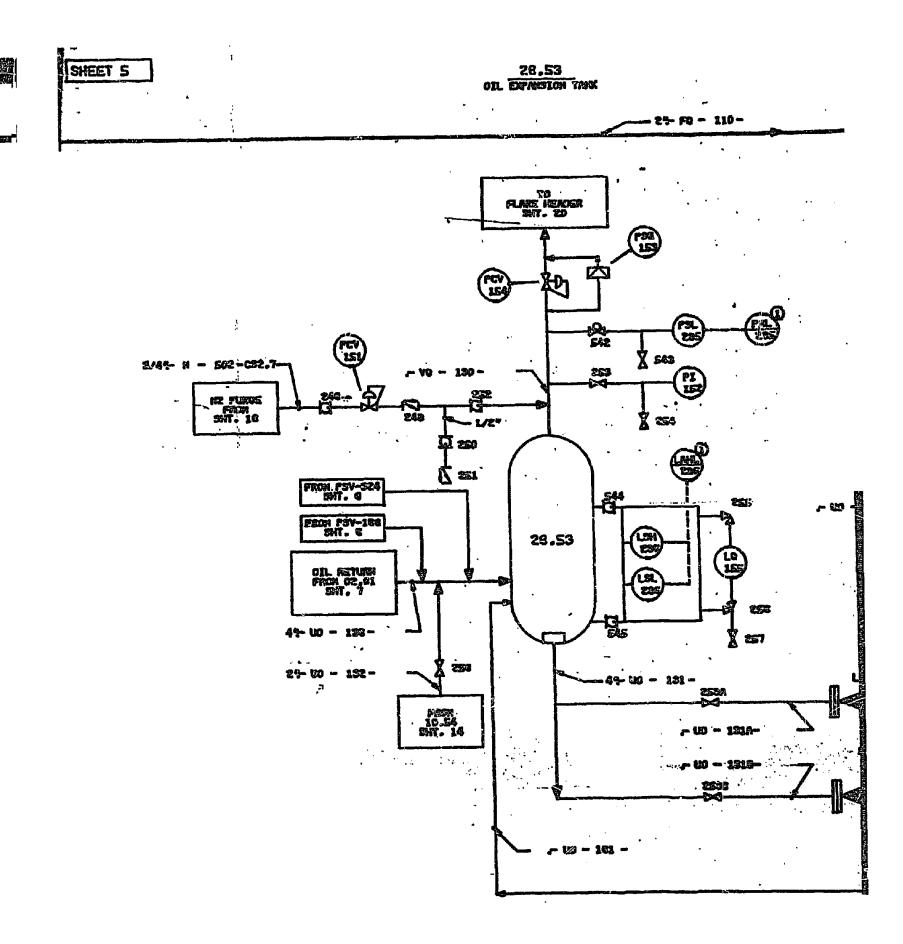


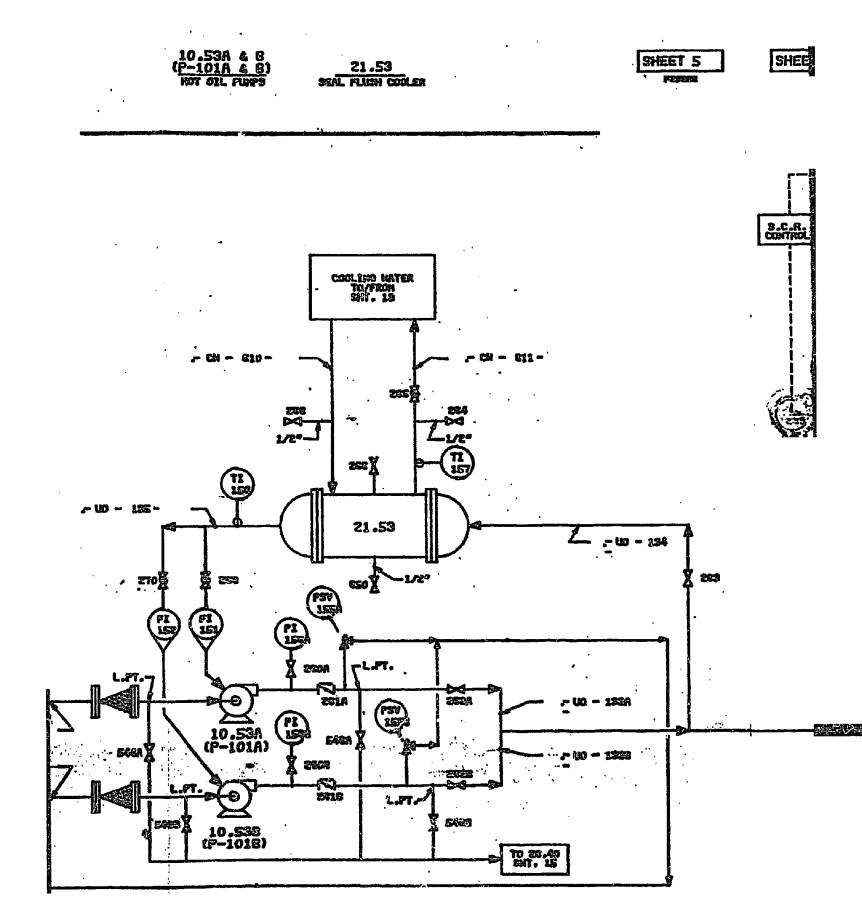


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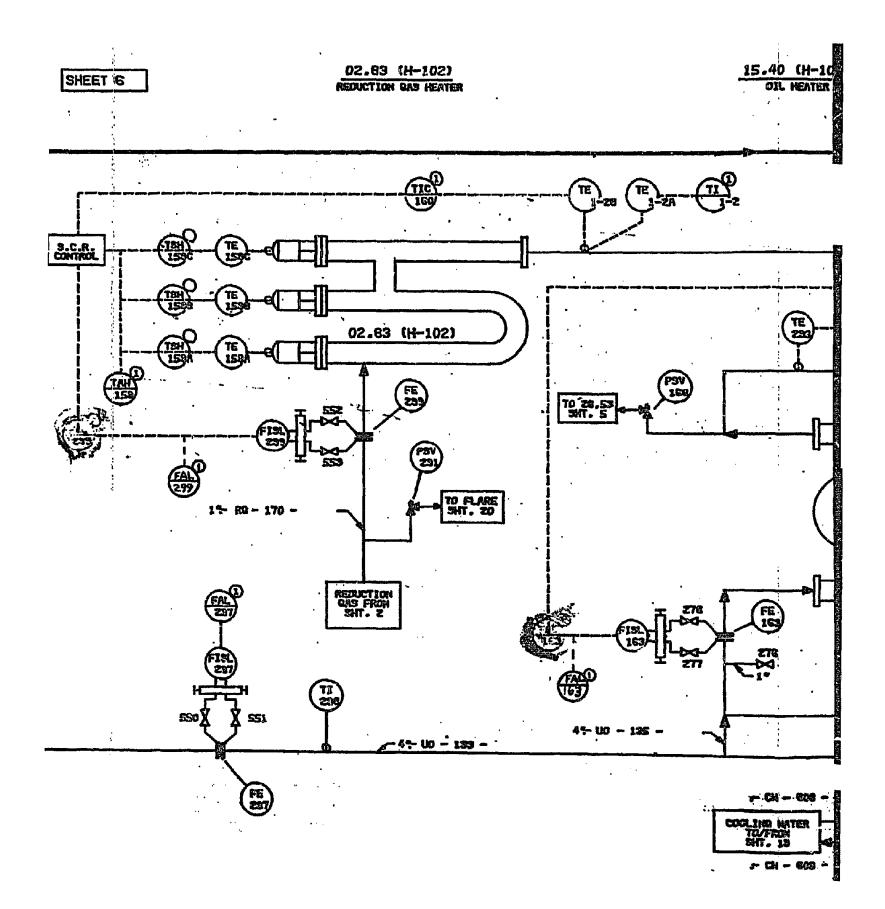


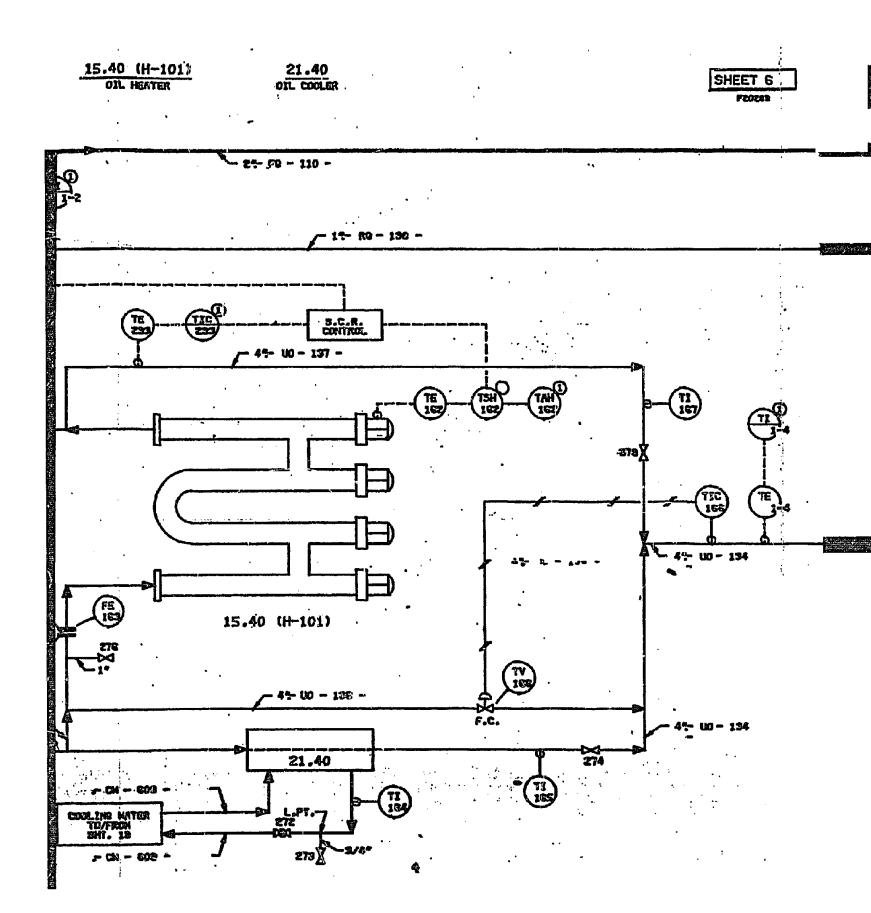




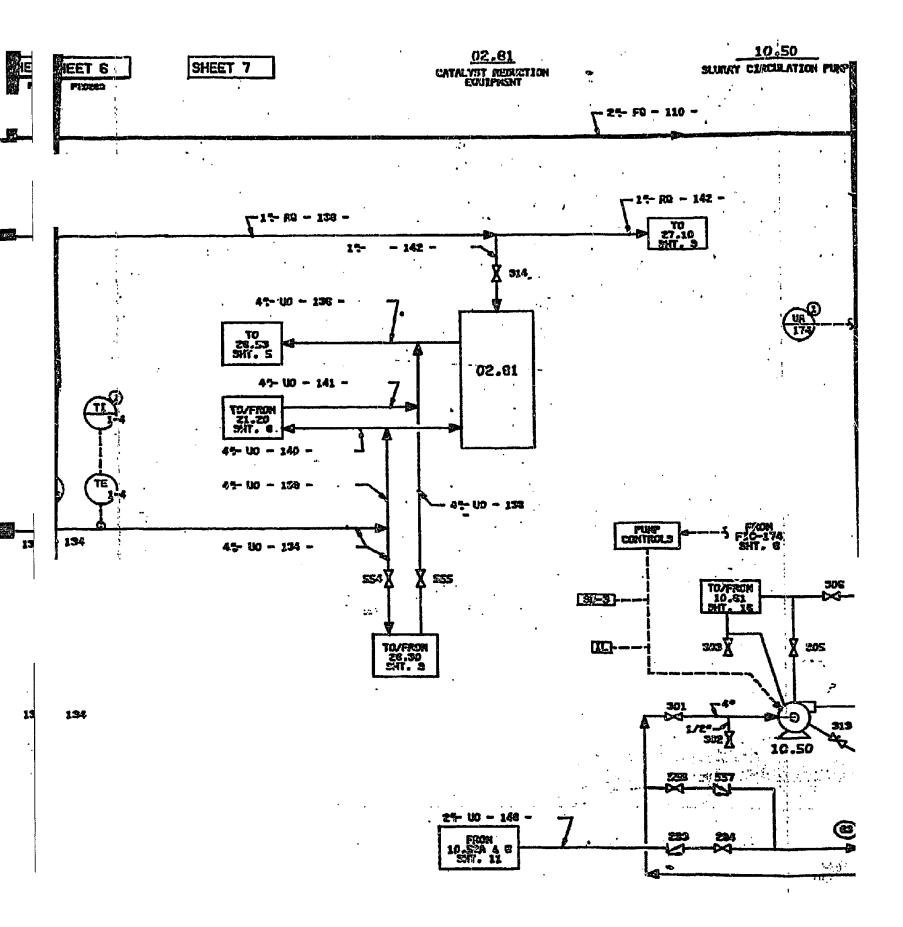


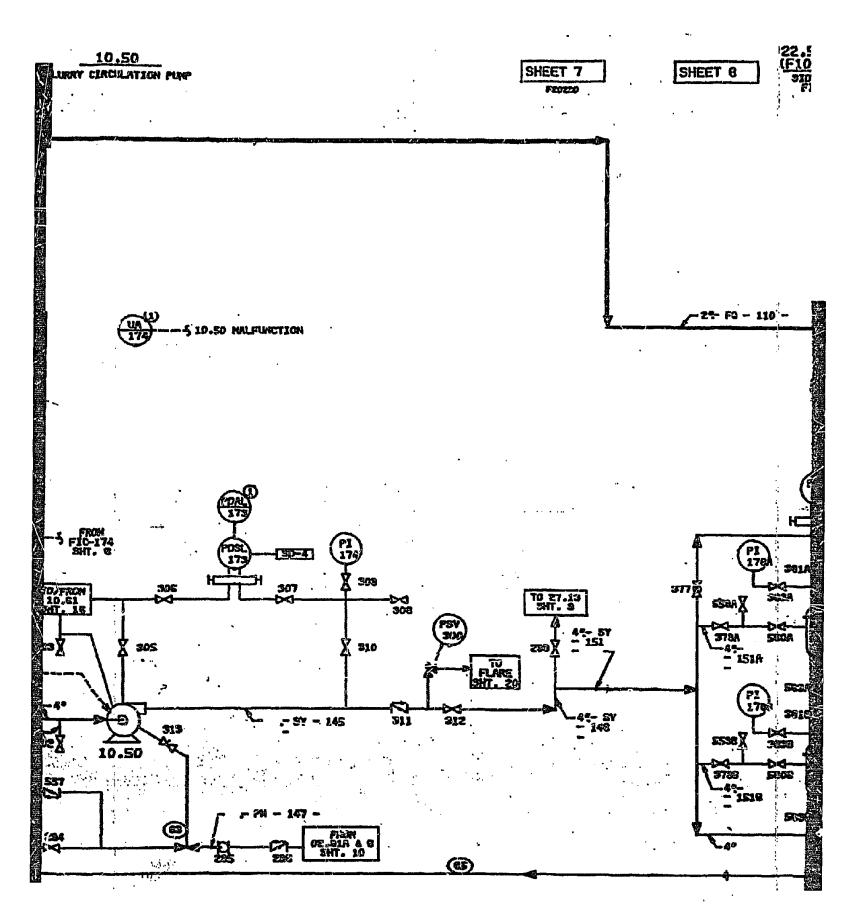
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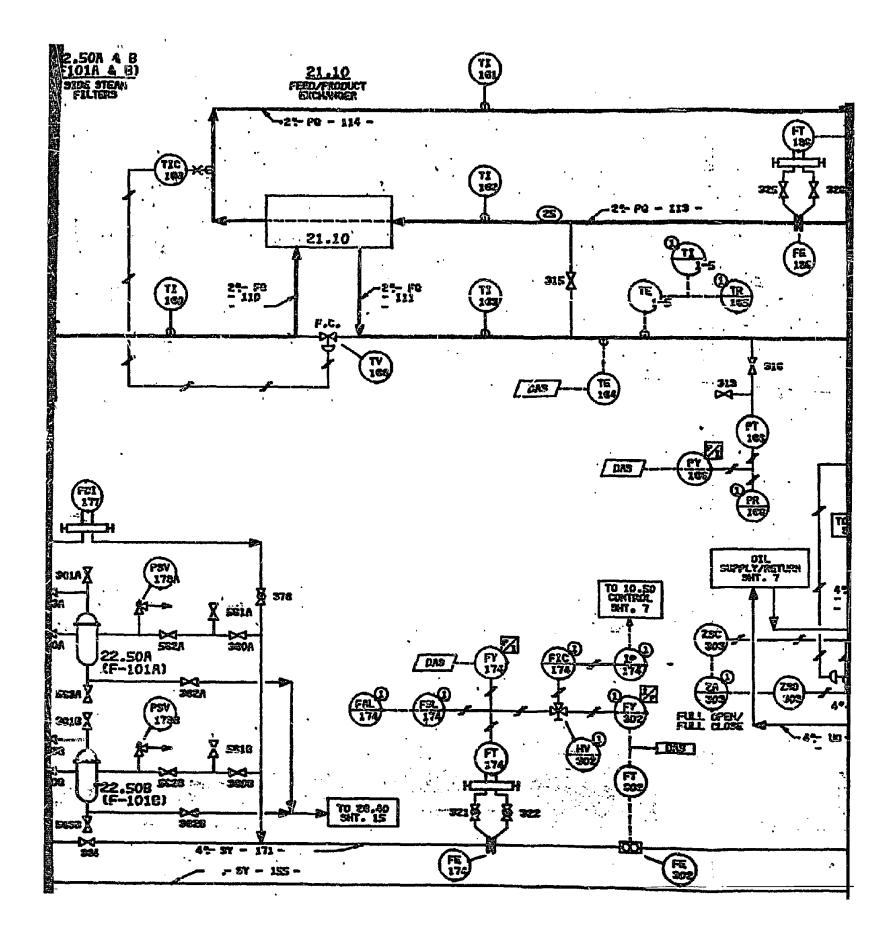


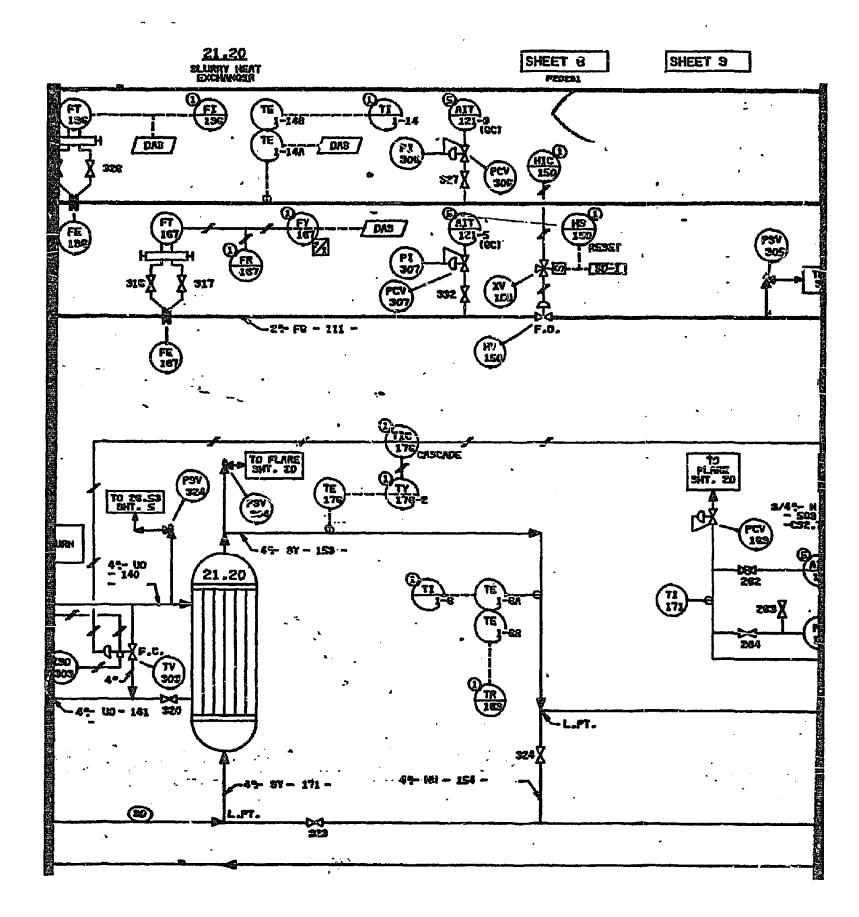


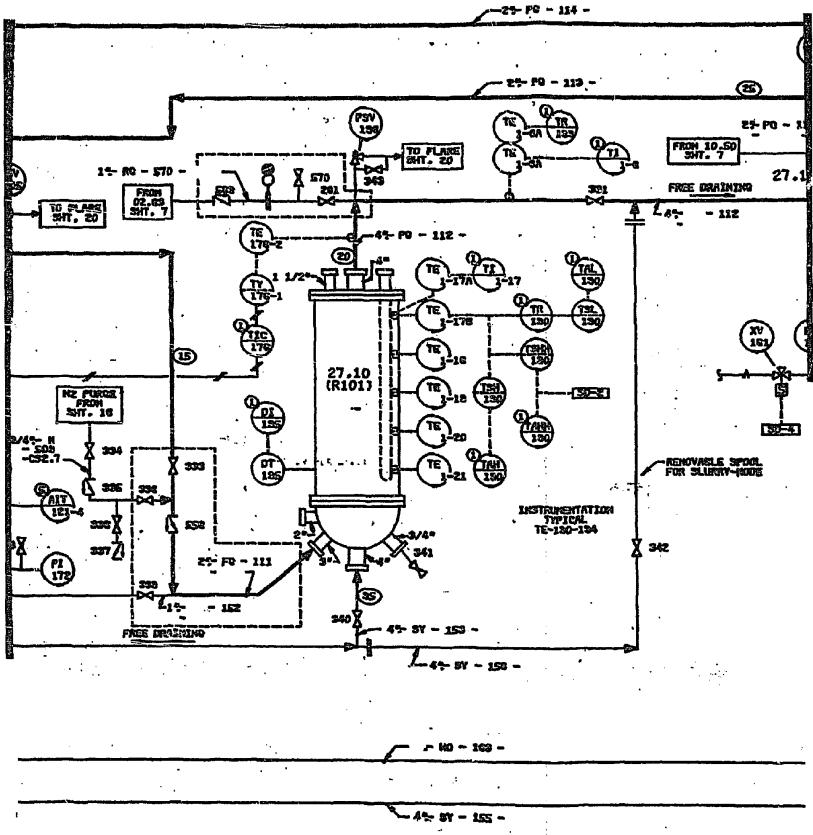
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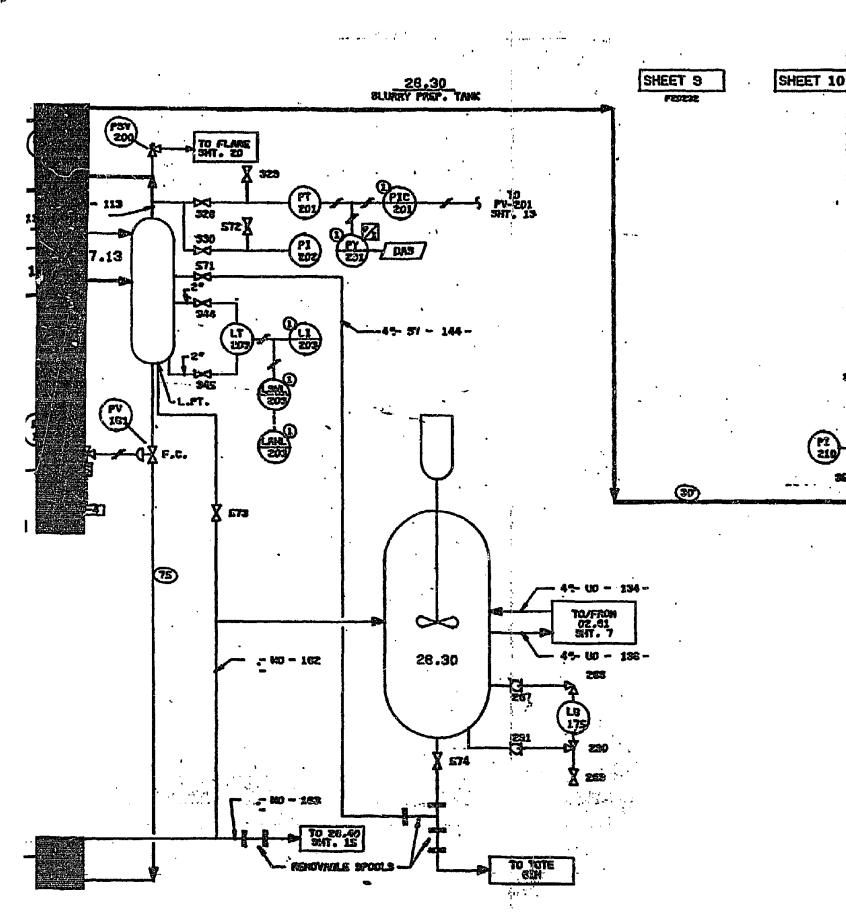




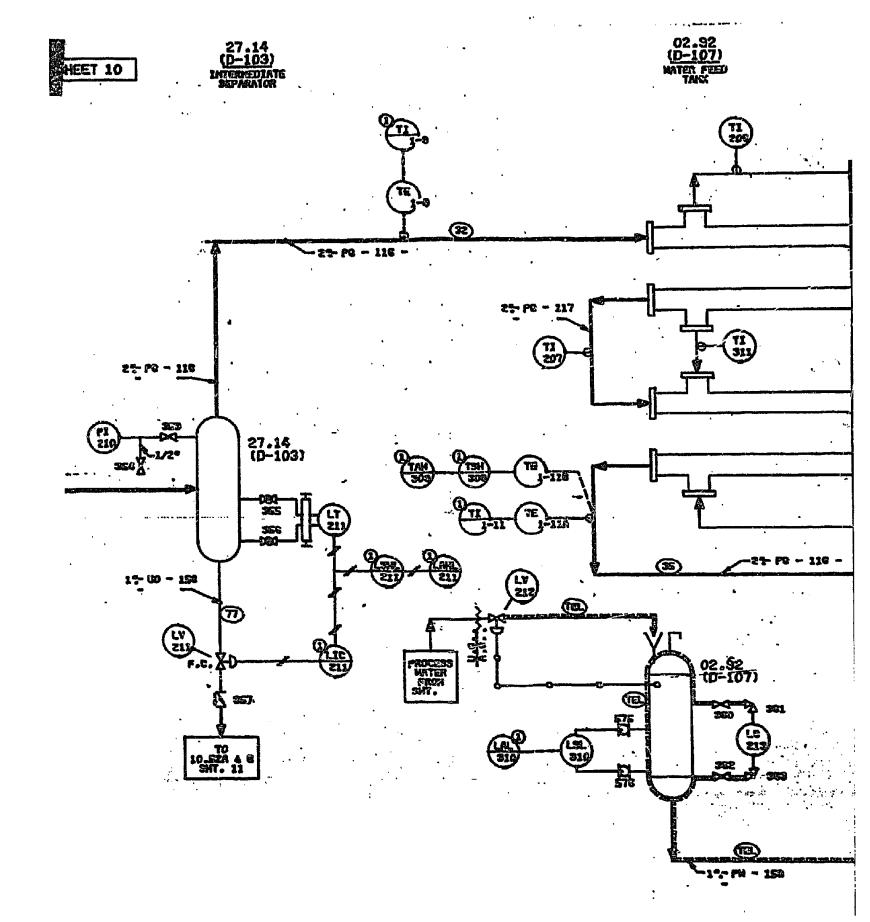






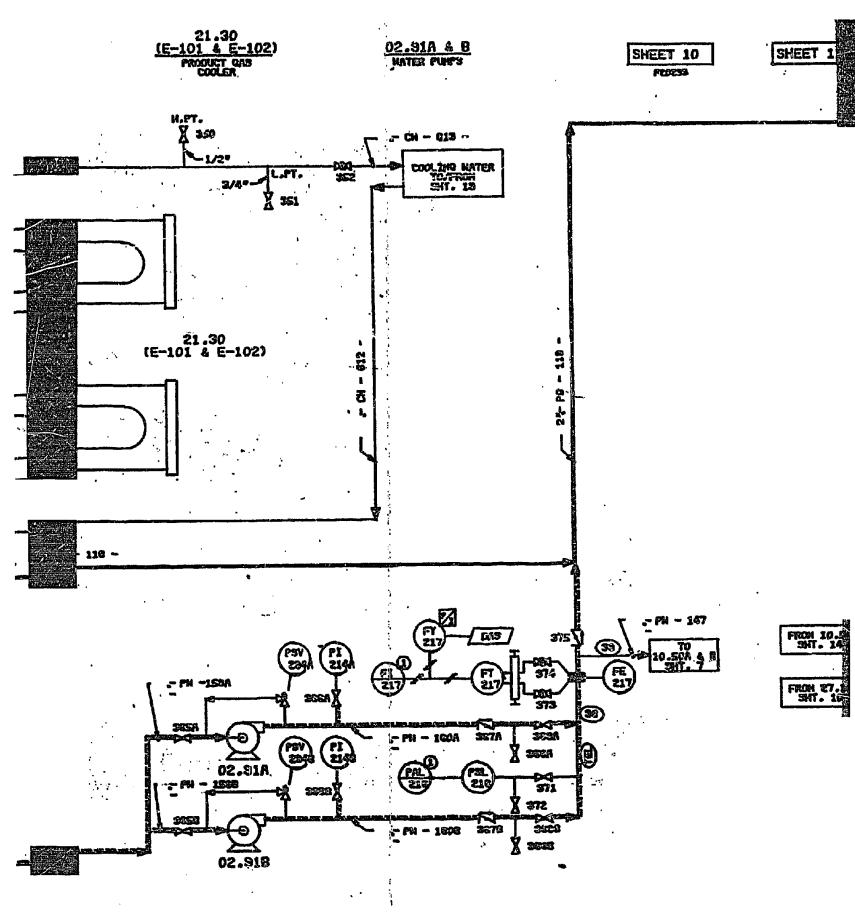


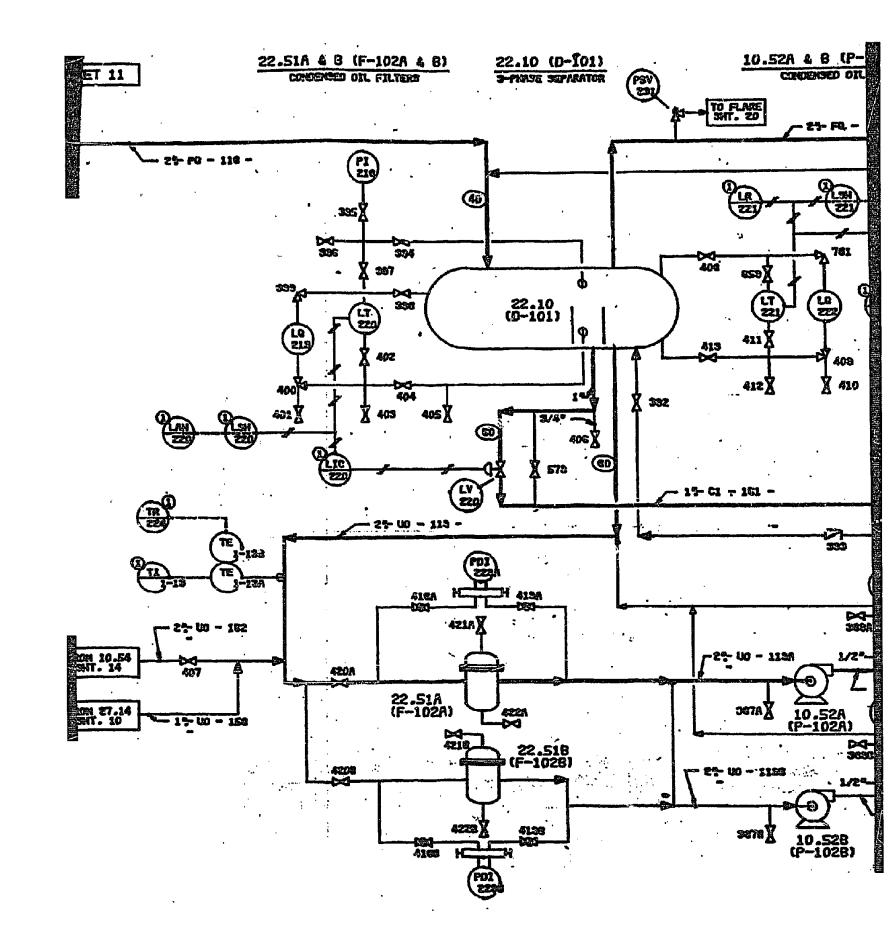
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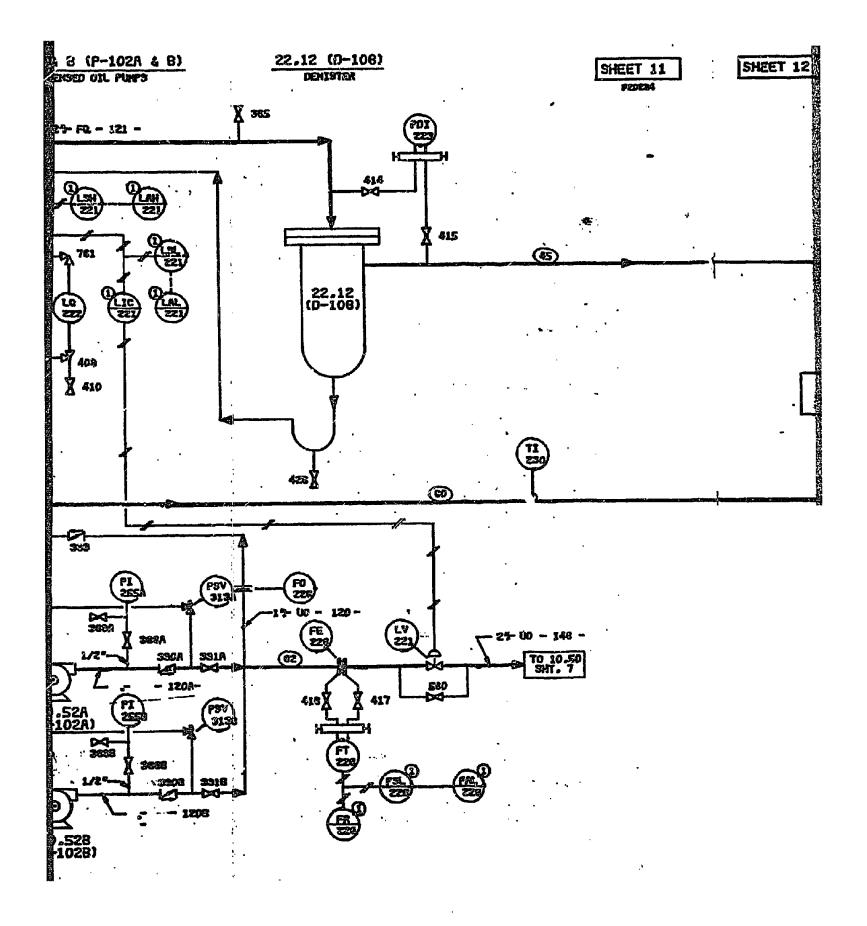


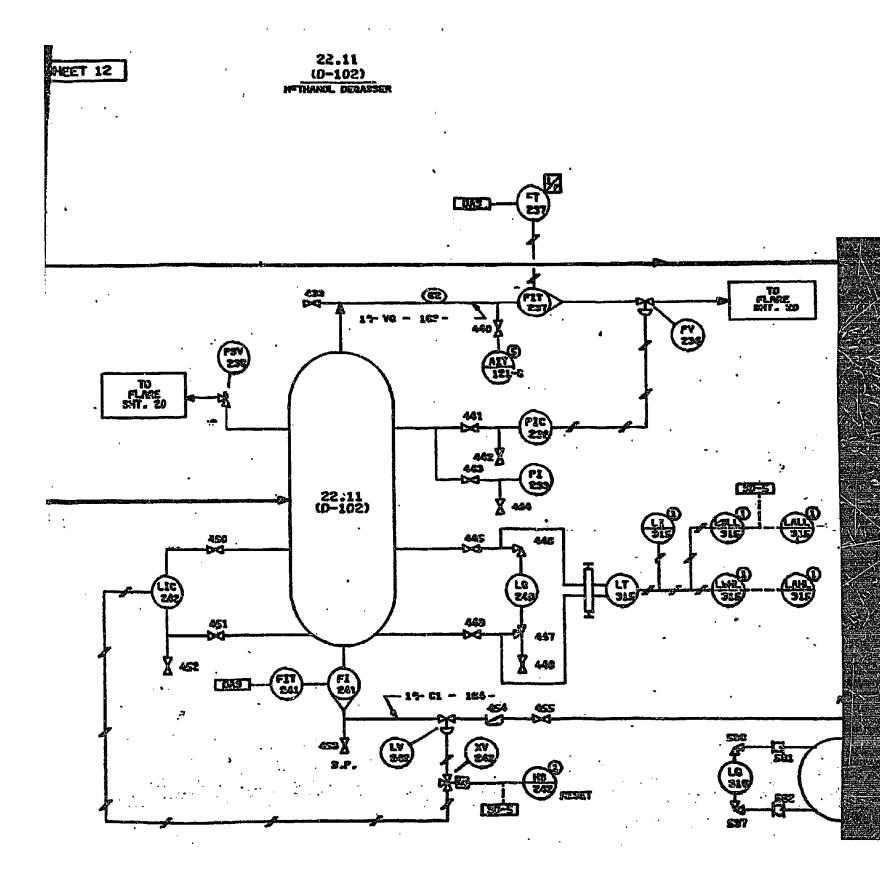
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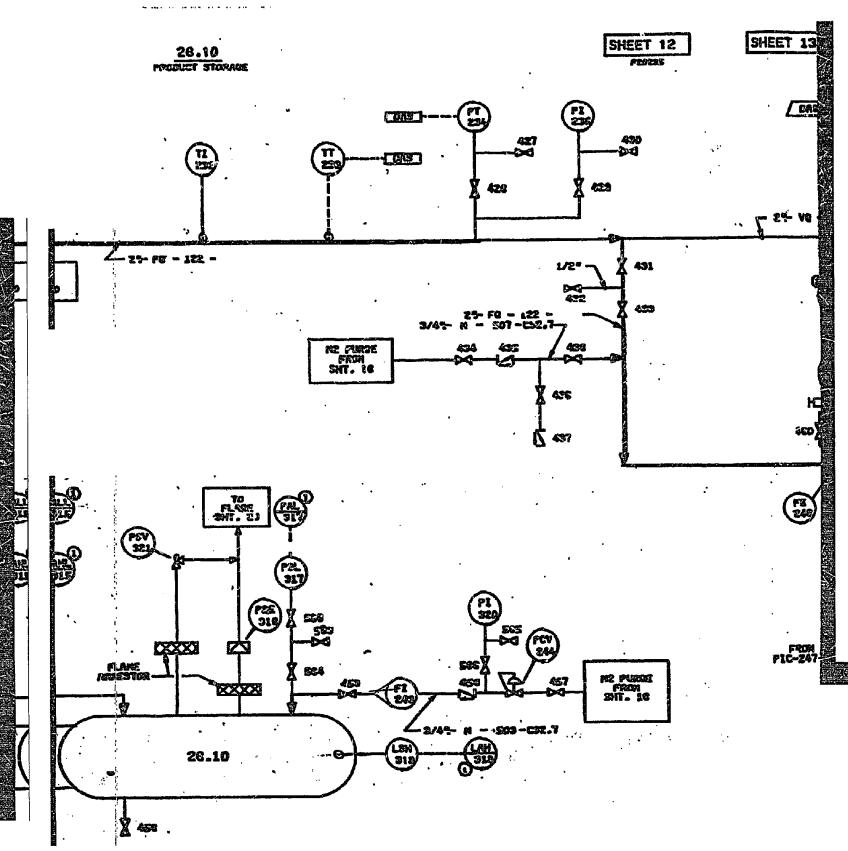
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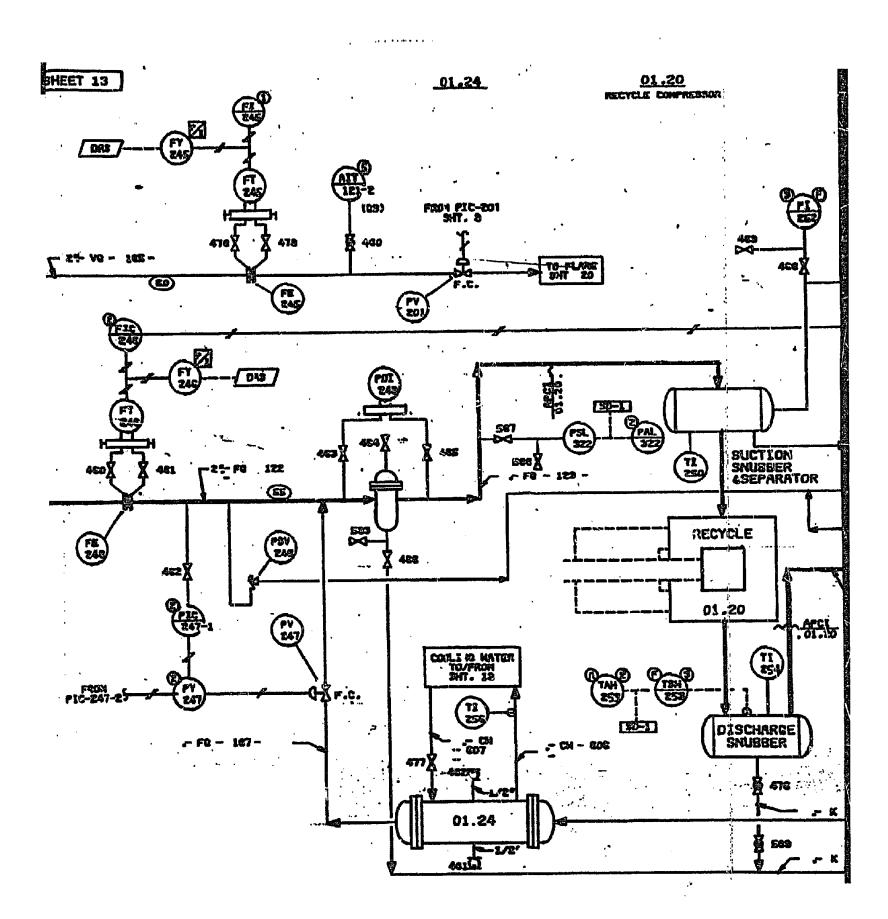


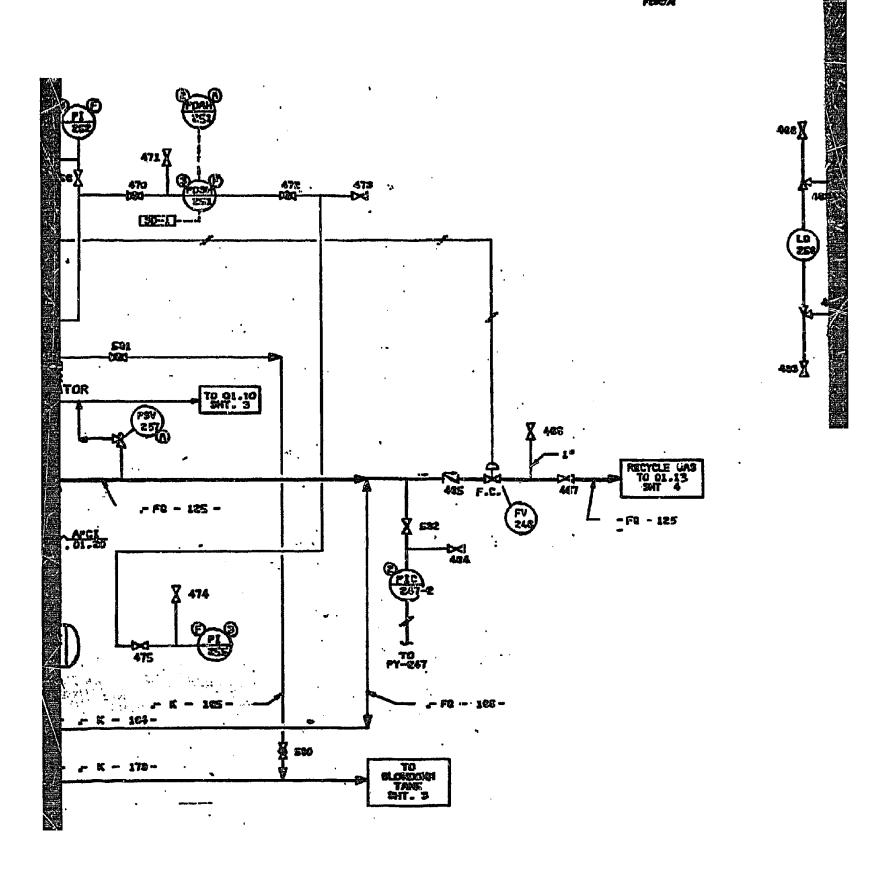






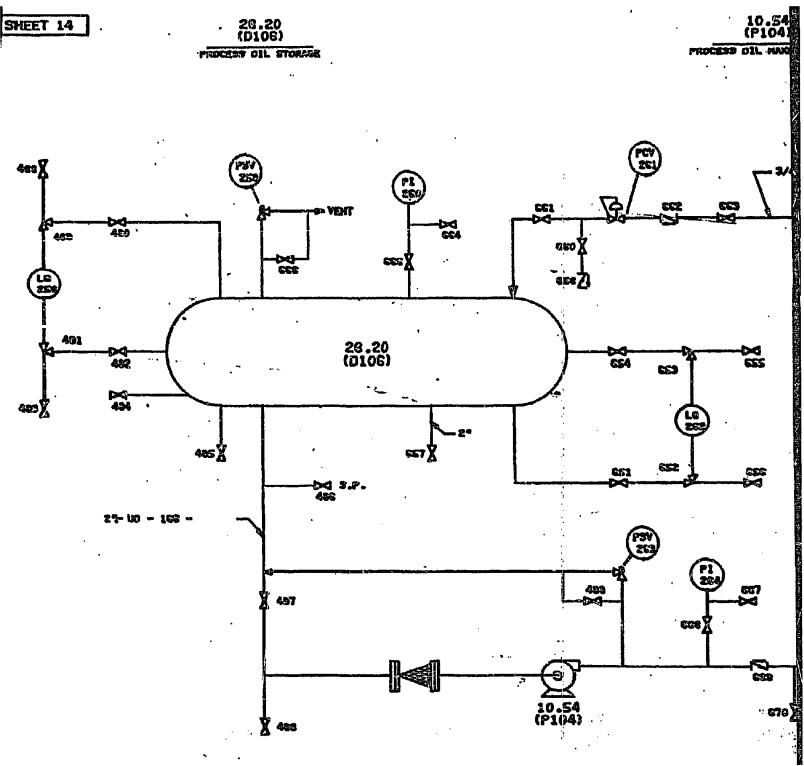
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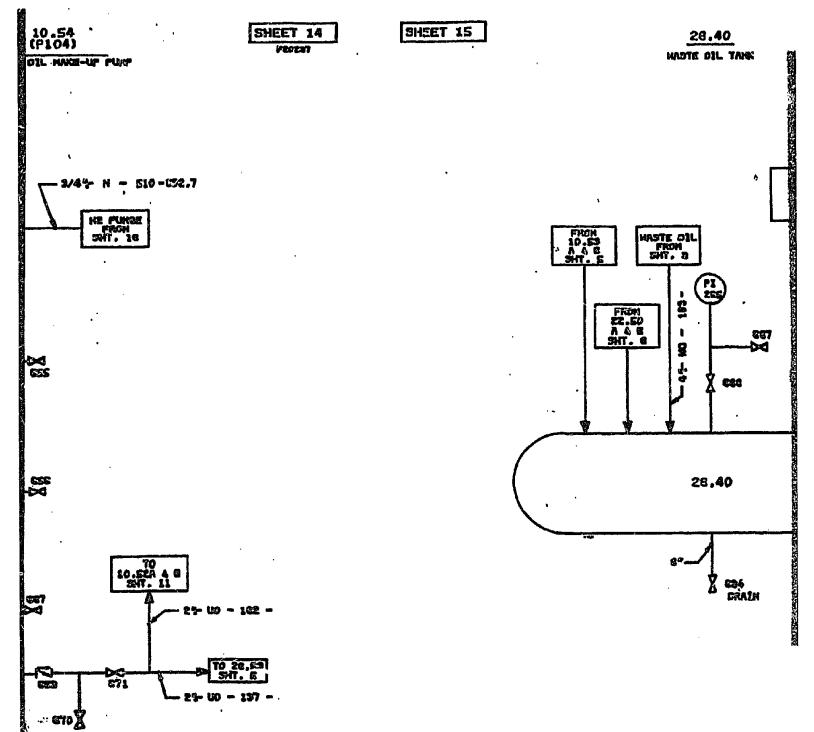


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SHEET 1

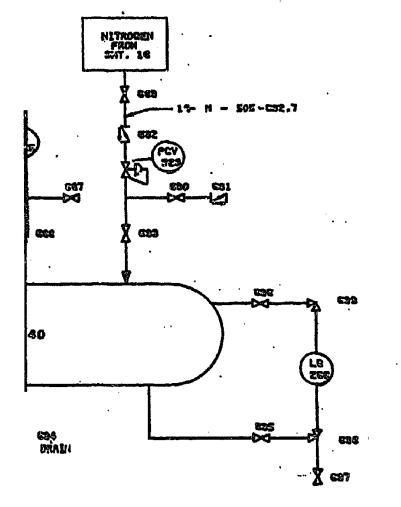


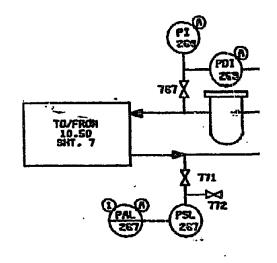
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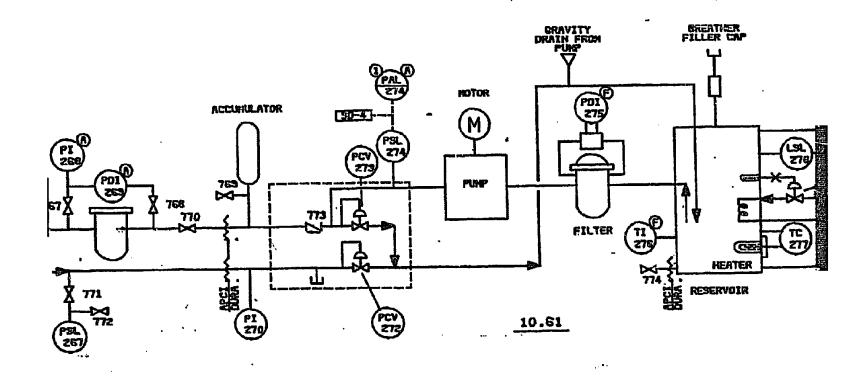
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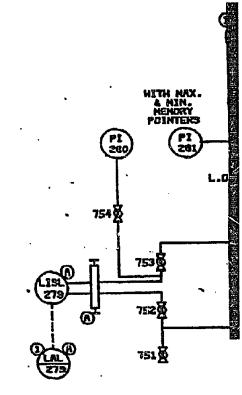
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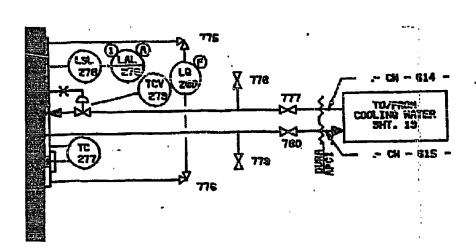
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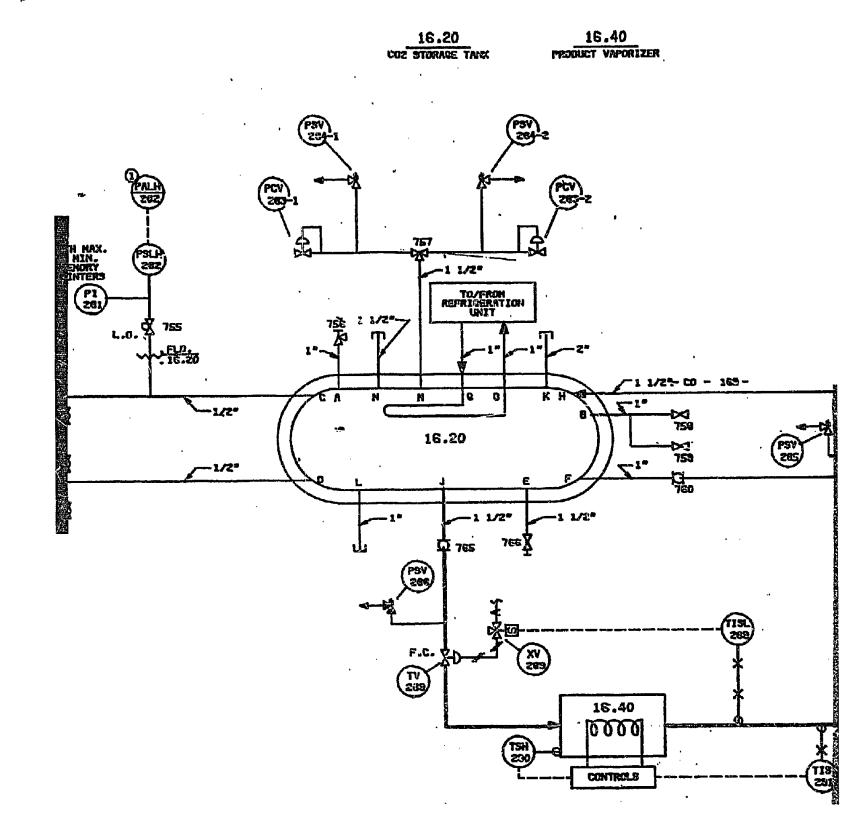




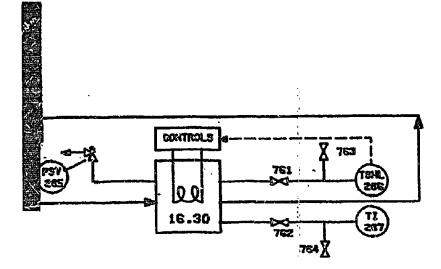
SHEET 17

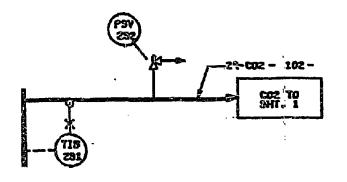


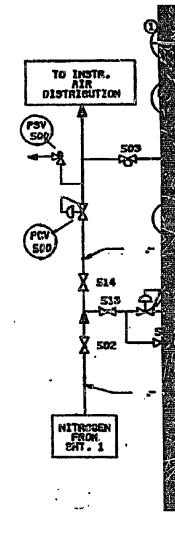




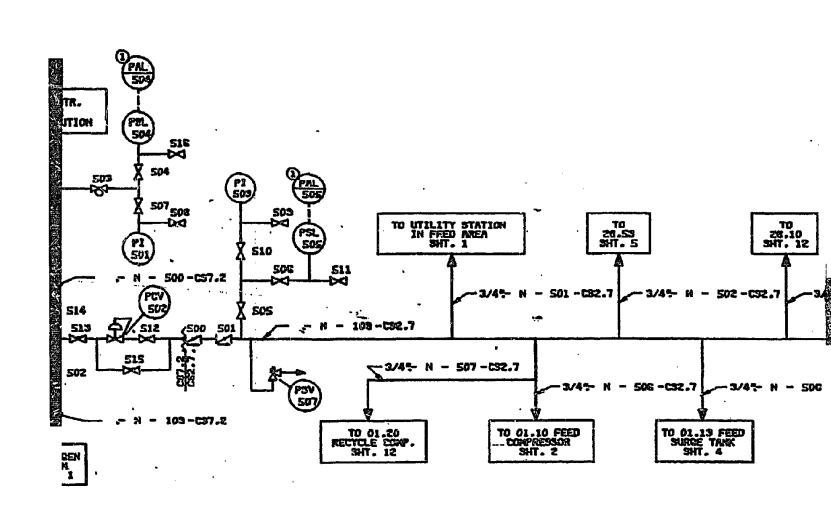






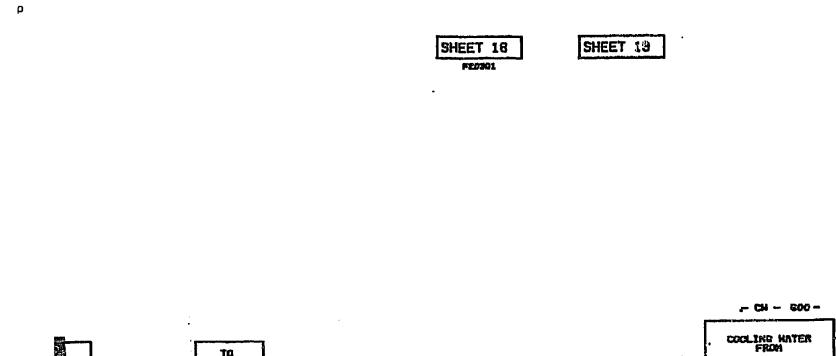


NITROGEN PURGE AND INSTR. AIR SYSTEM



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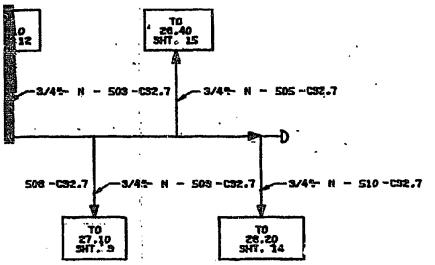


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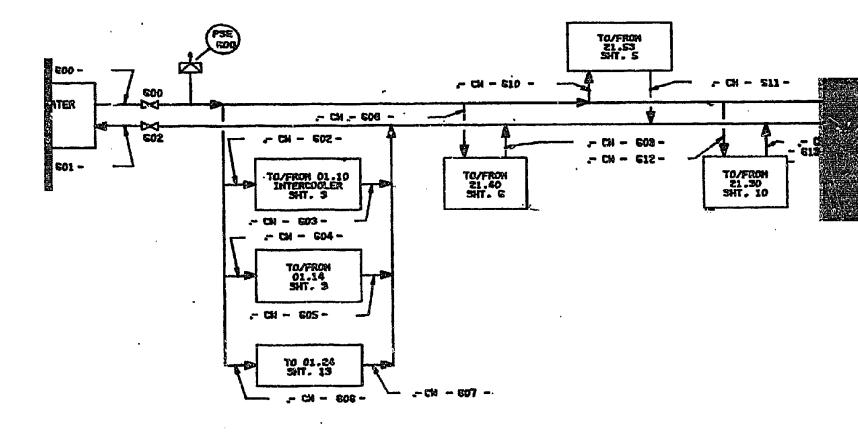


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COOLING WATER SYSTEM

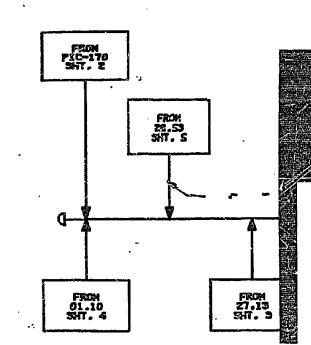
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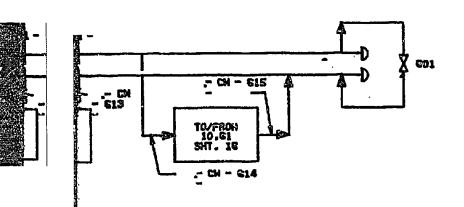




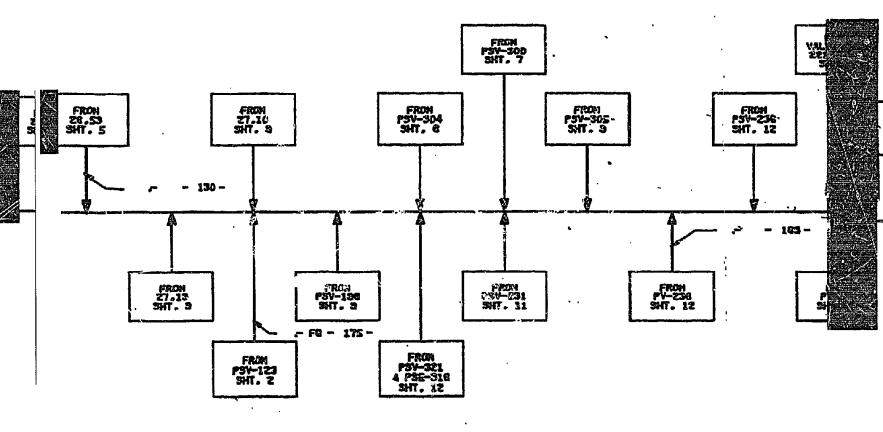


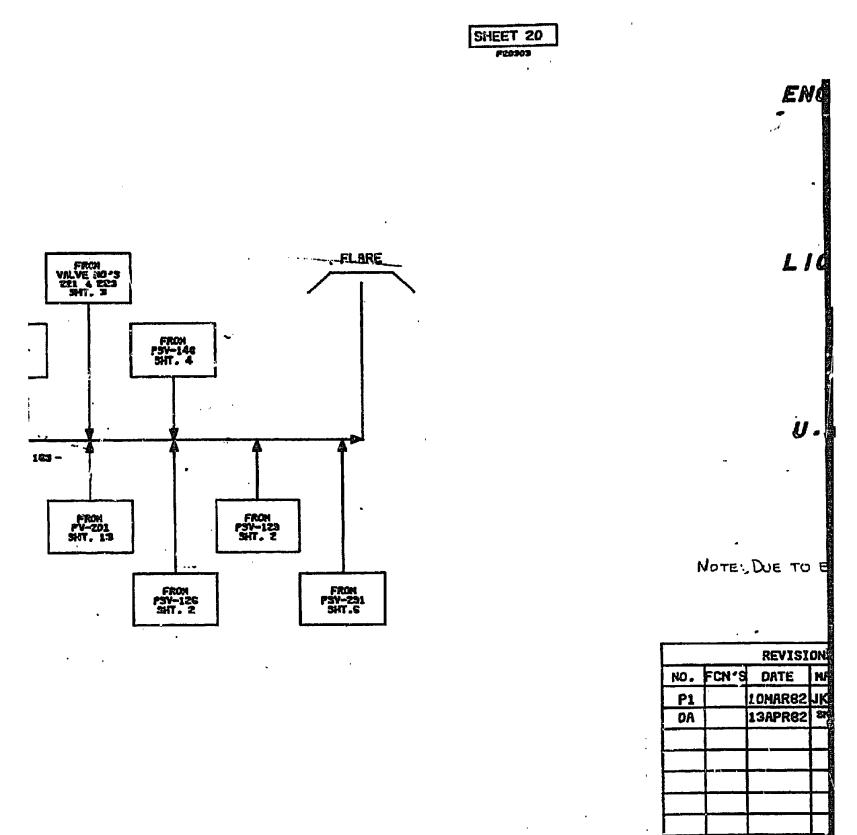
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ENGINEERING FLONSHEET

87-7-1533

LIQUID PHASE METHANOL

FOR

PRELIMINARY

U.S. DEPT. OF ENERGY (D.O.E.)

LAPORTE, TEXAS

NOTE , DUE TO EXTENSIVE CHANGES THRU-OUT FIS, REV. OA IS NOT CIRCLED



		REVISI	ons					APPROVED		
NO.	FCN'S	DATE	HADE	снк•р	PROCESS	START-UP	OPER.	CHF.ENC.	PROJECT	SAFET
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EXHIBIT

Design Cases for Liquid-Fluidized Mode: Operating Conditions for LaPorte LPMeOH PDU

	10	10	-	
Produce Produce Produce	6.5	2.6	с. С.	0,5
Purss Product Flow Rate 1b-Fol/hr SI/D	-	10	8	8.
Recycle Floa 15-Yol/hr	194	125	78	20
Fresh / Feed Ib-Hol/hi	53	30	46	41
Reactor Liq./Yapor Fresh Feed Linesr Velocity Feed b-Mol/hr ft/sec b-Mol/hr	0.16/0.26	0.16/0.22	0.16/0.18	0.16/0.13
Reactor Feed 1b-Hol/hr	247	155	124	Ð
Select.	0	•	5	ſ
ء 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	8	63	12	12
select.	3 8	86	83	83
xco, conv. (Single Pass)	en	5	G	°.
LCO Conv. (Single Pass)	25	20	01	1
Catalyst Loading kg/l	·. 1	,	•	1
Catalyst Catalyst Bed. Ht. Loading (ft kg/l	~	7	٢	1
Leep.	230	250	250	2/0
Press, psig	900	- 700	700	500
Space Velocity 1/hr kg	4,000	2,500	2,000	1,000
Space · Velocity Press, Temp. Case Nd. 1/hr kg psig °C	FB-4930.8 4,000	FL-375d.8 2,500	FK-2750.6 2,000	FK-1570.3 1,000

20 April 1982

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Case No.	Space Velocity Press, Teamp, B 1/hr kg psig °C	Press, psig	1emp. °C	XCO X(Catalyst Catalyst Conv. Co Bed, Ht. Loading (Single (Si ft kg/l pass) pa	Catalyst Loading kg/1	XCO Conv. (Single pass)	\$C0, Con9. (Single pass)	K CHJOH Select.	XCO, X X X Cano. X X X (Single CH ₃ OH C ₂ H ₅ OH CO ₂ pass) Select. Select.	% CO2 Selečt.	Reactor Feed 1b-Mul/hr	Reactor Liq./Yapor Fresh I Feed Linear Yelocity1b-Mol/hr 1 t//sec	Fresh Feed 1b-Mo1/hr	Recycle Furge Product Flow Flow Rate 1b-Kol/hr 1b-Kol/hr ST/D	Purge I Flow 1b-Mol/hr	ReOH Rate Site
EB-X954.8	EB-X954.8 10,000	005	250	•	. 4 .0	30	ę	3 8	2	Ģ	350	G.20/0.40	ħ	273	0.5	9.7
EL-6752.7 6,000	6,000	200	250	·	0.2	24	2	98	8	a	107	0.16/0.15	27	80	10	2.3
EK-4752.7 4,000	4,000	700	250	·	0.2	12	C	83	12	ъ	72	0.16/0.10	22	50	10	1.6
EK-2571.0 2,000	2,000	500	270	٠	0.1	7	0	83	12	Ω	18	0.16/0.04	18	٥	11	0.2

EXHEBIT 2.3.1-4

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Desion Cases for Liquid-Entrained Mode: Operating Conditions for LaPorte LPMeOH PDU •

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20 April 1982

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EXHIBIT 2.3.1-5

Point-by-point Heat and Mass Balances

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18JAN.82 PAGE 14:30:35	44 13 45 13 45 10 45 50 585 57 585 57 585 595 585 505 491 17, 55 505 491 29 515 2999 29 515 2998 20 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5
533	44 15 44 15 555615.00 535.00 535.00 535.00 535.00 1.681300 1.681300 1.681300 5359999 29,13599999 29,13599999 29,13599999 29,13599999 29,13599999 29,13599999 29,13599999 29,13599999 1,100000000 1,100000000 1,100000000 1,100000000
ВОЧНЕLL 87-7-1553	<pre>10 172.52 -5517937.00 -5517937.00 -5517937.00 2.151783 172.55 -5517937 172.55 -551783999 502.399999 503.53182999 5.152959 5.152959 6.0006-02 1.10006-02 1.10006-02 1.10006-02 2.318778 2.318778 2.318778 2.318778 2.318778 2.318778 2.318778 2.318778 2.318778 2.318778 2.318778 2.318778 2.318788 2.318888 2.318788 2.318788 2.318788 2.318788 2.318788 2.318788 2.318788 2.318788 2.318788 2.3187888 2.318788 2.328788 2.328788 2.3287788 2.3287888 2.3287888 2.328788888 2.32878888 2.328788888 2.32878</pre>
SYNTHESIS 8-4930 84	#1.4 950 377.73 377.73 377.73 11.156242 11.156242 11.269170 11.269170 11.269170 11.269170 11.269170 11.269170 11.269170 125,790000 11.708005 125,790000 11.708005 125,790000 125,79900 125,79266 8.35556
5, INC CYCLE SYNTHESIS Ed Max Prodn: <u>F8-4930</u> Stream Summary	1 ,4 5 1 ,56 1 ,60 1 ,269 1 ,76 1 ,700000 1 ,700000 1 ,700000 1 ,700000 1 ,799000 1 ,799000 1 ,799258 5 ,80,249258 5 ,80,249258 5 ,80,249258 5 ,80,249258 5 ,80,249258
AIR PRODUCTS & CHEMICALS, LPMEOH FLUIDIZED/BALANCED	#1,4 3 372.47 372.47 372.47 372.47 372.47 374.0 11.26917000000000000000000000000000000000000
LPMEOH FU	44 1 190.00 190.00 150.00 11.269188 11.269188 11.569000 15.7900000 15.7900000 15.790000 15.790000 15.790000 15.790000 15.790000 15.790000 15.790000 15.790000 15.790000 15.790000 15.790000 15.790000 15.790000 15.790000 15.790000 15.7900000 15.7900000 15.7900000 15.7900000 15.79000000 15.79000000 15.79000000000000000000000000000000000000
STREAM SUMMARY Version 82.011-A	T STREAM NUMBER NOTES - BELOW F PRESSATE BELOW A TEMPERATURE DEG,F EMTHALPY BYCHER VAP. DEHSITY, IB/CHFT VAP. DEHSITY, IB/CHFT AVE. FALL MI BYCHER HYDROGEN MOLOXIDE CARBON MOLOXIDE NITHANC MATER MAT

STREAMS ARE ALL VAPOR

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STREAM SUMMARY Version 52.011-A	AIR PRO LPMEGH	IDUCTS & CHEMICAL! Fluidized/balanci	5, INC CYCL Ed Max Prodn: Stream Summ	E SYNTHESIS FB-4930 ARY	87-7-11 87-7-1	د 535	18JAH.82 PAGE 19 14:30:36
T ISTREAM NUMBER NOTES- BELOW T PRESSURE PSIA T RESSURE PSIA T DEW PRATURE DEG,F Enthalpy BEG,F Enthalpy BIU/HR Flow Wites Moles/HR Carbon Monoxide Carbon Monoxide Nitrigen Nitrigen Mater Mater Nitrigen Nitrigen Nitrige	20 44 20 415,00 415,00 418 -51497646.00 446.00 446.00 54.597828 54.59432515 55.531540 3.2128315 3.2128315 54.5931355 2.5433135 2.543315 2.543515 2.543515 2.543515 2.543515 2.545515 2.543515 2.545515 2.545515 2.545515 2.5455515 2.5455555 2.5455555 2.5455555 2.54555555 2.54555555 2.54555555 2.54555555555 2.5455555555555555555555555555555555555	25 910.00 910.00 910.00 18.49999 18.400757 26.5201757 26.5201755 26.5201755 26.5201755 26.5201755 26.5201755 26.5201755 26.5201755 26.5201755 26.5201755 26.5201755 27.5455 0.17255502 0.172555502 0.1725555502 0.17255555502 0.172555502 0.172555502 0.172555502 0.172555502 0.172555502 0.172555502 0.172555502 0.172555502 0.172555502 0.17255555502 0.172555555555555555555555555555555555555	44 39 900.00 9343983.00 13.440157 65.740157 65.7201559 28.7205602 2.1205602 2.1205602 1.132375 0.372459 0.372459	22 927 0303.00 18.015250 18.015250 55.50853.00 55.508594 55.508594 29.13194594 29.13194594 29.13194594 29.13194594 29.13194594 29.13194594 29.13194594 29.13194594 29.13194594 29.1101 20.1101 2	35 35 890.00 100.00 180.094879 58.712265 58.712265 58.712265 58.71233 28.511233 29.137088 21.132375 21.132375 21.142354 11.132375 21.142354 21.1423555 21.142355 21.1423555 21.1423555 21.1423555 21.1423555 21.1423555 21.1423555 21.1423555 21.1423555 21.1423555 21.14235555 21.1425555 21.14255555 21.14255555 21.1425555555555555555555555555555555555		45 45 110.50 110.50 15.567914 16.267914 16.267914 28.654510 28.656627 28.156852 29.100338 20.100338 20.100358 20.100358 20.100358 20.100358 20.100358 20.100358 20.100358 20.100
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1. STREAM SPECIFIED AS ALL VAPOR 2. Stream specified as all liquid 4. <u>"Aution</u>: two liquid phases not considered. "Results may be in Error.

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AIR PRODUCTS & CHEMICALS, INC -- CYCLE SYNTHESIS LPMEON FLUIDIZED/BALANCED MAX PRODN: FB-4930 SUMMARY

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87-7-1533

STREAM SUMMARY Version 82.011-a	AIR PRO LPMEOH	AIR PRODUCTS & CHEMICALS, LPMEOH FLUIDIZED/BALAHCEO	INC CYCLE SYNTHESIS Max Prodn: Fb-4930 Stream Sutmary	57NTHE5IS 3-4930 87	BONNELL 87-7-1533	53 3	15JAN.52 PAGE 14:30:36
T STREAM MUMBER NOTES - BELOW T PREFEXE PELOW L PREFEXE PEGIL ENTHALPY DEGIL ENTHALPY DEGIL ENTHALPY DEGIL ENTHALPY IBJUK LIQ2 DENSITY, IBJUK ANC MOL WITY, IBJUK FLOW RATES MOLE FLOW RATES MOLE CARBON PHONOTO	R 75 1514 75 1514 745 99 1515, F 445 99 1516, F 445 99 1516, F 455 99 1516, F 455 99 1513, 75 1513, 70 150, 70 150, 70 11105 75 1533, 70 11105 75 10, 5323, 1105 1531, 1105 1531, 1105 1531, 1105 1531, 1105 1532, 11105 1532, 111105 1532, 111	255355 259000 259000 259000 2595000 269000 269000 269000 269000 269000 269000 269000 2776 29100 29100 20000 201000 201000 201000 201000 2010000	77 800.00 269.09 -58546.35 39.297089 291.157700 201.157700 2.7900256-02 1.0363256-02 1.036356-02 1.036356-02 8.561356-05 8.5814576-05 8.5814576-05	78 885 .00 110.50 110.50 142.502156 194.607208 144.607200000000000000000000000000000000000	25.56 885.00 253.24 253.24 253.24 253.26 39.711136 199.711136 199.711136 1355286-02 1.355286-02 1.355286-02 1.159416-02 1.159416-02	83 918.00 918.00 253.40 253.40 39.519159 39.519159 19.511136 3.5563366-02 1.1553966-02 1.1553966-02 1.1254966-02 1.1254966-02	89 845.00 945.00 446.95 446.95 55.536100 204.751099 204.751099 205.72564 7.522946 6.8222946 7.522946
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STREAM SUMMARY Version 82.011-A

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CYCLE SYNTHESIS Summary	1,46 356.56 356.56 326.56 12.658406.06 12.658499 12.470467 12.659999 12.659999 1.650000 1.650000 1.650000 1.650000 1.650000 1.650000 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.
, INC CYGLE S FL-3750 Stream Summary	#1,4 #1,4 335,00 335,00 335,00 122,470467 12,6589999 12,450000 12,450000 12,65000 0,0 0,0 0,0 0,0 0,0 0,0 0,0
AIR PRODUCTS & CHEMICALS, INC LPMEOK FLUIDIZED/LURGI: <u>FL-3750</u> Stream	41,4 326.13 326.13 326.13 326.13 326.13 6.559997 12.670467 12.670467 12.659999 1.554999 1.564336 370.108963 370.108963 311.554336
AIR PRODU LPMEOH FL	11,4 160.00 160.00 160.00 160.00 12.470467 12.470467 12.470467 12.199997 12.199997 12.199997 11.550900 0.0 0.0 0.0 0.0 0.0 0.0 0.116955 20.116955
STREAM SUMMARY Version 82.011-A	T STREAM NUMBER MOTES - BELOUA T FRESSURE FSIA T FRESSURE FSIA T FRESSURE FSIA T FRESSURE FSIA FROM RATES MOLES/HR HYDROGEN METRADH DIOXIDE CARBON MONOXIDE METRADH METRADH METRADH METRADH METRADH METRADH METRADH METRADH METRADL MITCO 40 OIL MITCO 40 OIL

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STREAM SUMMARY Version 82.011-a	T ISTREAM NUMBER INDIES - BELGU INDIES - BELGU PRESSURE PEG.F A TEMPERATURE DEG.F ENTHALPY BUCHR AVE. MOL WT BUCHR AVE. MOL WTES MOLES/HR HYPROGEN NONXXIDE CARBON NONXXIDE CARBON NONXXIDE MATER MATE	ENTHALPY BTU/HR - LIQ. DENSITY,LB/CUFT - AVE. MOL WT FLGW RAYES MOLES/HZ CARBON DIOXIDE CARBON DIOXIDE CARBON DIOXIDE MITROGEN MATHANOL MITRO ETHANOL ETHANOL MITCO 40 OIL MITCO 40 OIL	ENTHALPY BTU/HR LIQ1 DEHSITY,LB/CUFT AVE, MOL UT FLUW RATES MOLES/HR HYDROGEN MONOXIDE Carbon Dioxide Kethane Nitrogen Matare Mitco 40 dil
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3	TOTAL LIQ. MOL/HR LD/HR	LI ENTHALPY BTU/HR LIQ2 DENSITY.LLCUFT LOW ROL LA LOW ROL LA LOW ROLS/HR LANENGEN MOLES/HR CARBON MONOXIDE CARBON MONOXIDE CARBON DIOXIDE NETHANE MATER MATE	V ENTHALPY BIU/HR A VAP: DENSITY,LB/CUFT DD FLOW RATES MOLES/HR HYDROGEN Carbon MDHOXIDE Carbon Dioxide Methang Hater Mattanol Hater Mattanol Flaanol Total Vapor Mol/HR Total Vapor Mol/HR Total Vapor Mol/HR

21JAN.82 PAGE 13:35:05	65 65 104.26 104.26 104.26 104.26 104.26 104.25 104.25 10.05
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STREAM SUMMARY Version 82.011-a	AIR PRO LPNEOH	EPRODUCTS & CITEMICAL IEON FLUIDIZED/LURGI	5, INC FL-3750	SYNTHESIS	7.R.TSAD 87-7-1533	AD 533	21JAN.82 1 13:35:05	PAGE 10
			INCALI JUMANIC	5				
T STREAM NUMBER 0 NDTES - BELOW		76 14	5		80 \$2,4 485 no	83 #2,4 710 00	- KO - K	5
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HYDROGEN CARBON MONOXIDE	4	7.19530E-03 2.86773E-03	2.87812E-02 1.14709E-02	6.85064E-03 2.99716E-03 4.012176-03	.56318E-D .44681E-D	3.56318E-02 1.44681E-02 1.84107E-02	16.6209 6.3561 7.5569	226
METHANE NITROGEN	140	2.49824E-03 2.31603E-04	9.99296E-03 9.26410E-04	3.96408E-05	.12366E-0	1.30570E-02 1.12366E-03	6.9535	82
WATER Methanol Ethanol Mitco 40 Jil	2.9.9	5.11224E-11 2.62218E-03 8.52677E-05 0.102551	2.04490E~10 1.04887E-02 3.41071E-34 0.410203	5.3363E-11 1.77319E-03 4.99228E-05 0.101836	Z-578866-10 1.22619E-02 3.90995E-04 0.512038	2.578865-18 1.226195-02 3.909936-04 0.512038	2.5/850E-10 5.385400 9.95473E-02 215.802170	2992
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			STREAM SUMMARY	RY				
T STREAM NUMBER O NOTES - BELOU T PRESSUE T PRESATURE DEG.F L ENTMALPY L ENTMALPY LIQ. DEMSITY.LB/CUFT AVE. MOL WIL	90 42,4 745,00 745,00 482,70 -355,413785 -35,413785 216,930008	95 84 735.00 738.14 -36044400.00 35.594376 216.930005						
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TOTAL FLOW MOLVHR LB/HR	251.372940 54530.332031	251.372940 54530.332031						
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REAM SUMMARY AIR FRODUCTS & CHEMICALS, INC CYCLE SVATHESIS I.R. 1540 21444.62 RESIGN & 22.011-A LARE RODUCTS & CHEMICALS, INC CYCLE SVATHESIS 0.7-1533 13149:21 PAGE STREAM SUMMARY STREAM SUMMARY STREAM SUMMARY 0.7-1533 13149:21 13149:21 STREAM SUMMARY RESUME 0.5 5 0.5 515.67 0.5 13149:21 1314	T I STREAM NUMBER T FRESSURE PERTAURE PSIA T PRESSURE PSIA T TEMPERTURE DEG,F LIQ2 DENSITY,LB/CUFT LIQ2 DENSITY,LB/CUFT AVE. MOL WT NONOXIDE CARBOH DIOXIDE CARBOH DIOXIDE CARBOH DIOXIDE CARBOH DIOXIDE NITRANC	2572 710.0 710.0 710.0 710.0 710.0 710.0 710.0 12.07249 16.57249 16.57249 16.57249 16.57249 16.57249 16.57249 16.57249 16.57249 16.57249 16.59951 16.59555 16.59951 1	76 700.000 700.000 700.400 700.000 -15300.440 -153205 10.282776 216.9028 5.6532295 -0.3005 1.020875 -0.30056 -0.5 -0.20026 19.527191 LTQ	77 79 79 70 70 70 70 70 70 216 96 95 27 76 76 76 76 76 76 76 76 76 76 76 76 76	78 685.00 111.00 685.00 685.00 685.00 685.09 449.450944 449.450944 649.450944 649.450944 219.465149 1.205426-03 1.205426-03 1.205426-03 1.205416-05 1.0152556-03 1.02556-03 1	42.45 685.00 265.80 265.80 685.00 265.80 217.903966 217.903966 217.903966 1.863966-02 2.131966-02 2.131966-02 2.939966-02 2.939966-02 2.939966-02 2.939966-02 2.939966-02 2.939966-02 2.939966-03 2.939966-03 2.939966-03 2.9383993 2.9383993 2.9383966-03 2.9383993 2.9383993 2.9383966-03 2.9383993 2.9383993 2.9383966-03 2.9383993 2.9383966-03 2.9383993 2.9383966-03 2.9383966-03 2.9383966-03 2.9383966-03 2.9383966-03 2.9383966-03 2.9383966-03 2.9383966-03 2.9383966-03 2.9383966-03 2.9383966-03 2.9383966-03 2.9383666-03 2.9383966-03 2.9383966-03 2.9383966-03 2.9383966-03 2.9383966-03 2.9383966-03 2.9383966-03 2.9383966-03 2.9383966-03 2.9383966-03 2.9383966-03 2.9383966-03 2.9383966-03 2.9383966-03 2.9383966-03 2.93839666-03 2.93839666-03 2.93839666-03 2.93839666-03 2.938396666666666666666666666666666666666	265.66 710.00 265.66 710.00 265.66 41.012793 41.012793 61.012793 710.00 2017793 5.1509065-02 2.5150905-02 2.5150905-02 2.5150905-02 2.5150905-03 2.515005-03	69 745.00 745.00 35950~00.00 35.534506 35.634506 12.090334 16.600800 0.885319 0.885319 1.0528191 4.825711 1.052812 215.753830 215.7538530 215.7538550 215.7538550 215.753850 215.753850 215.753850 215.7538550 215.7538500 215.753850 215.7538500 215.7558500 215.7558500 215.7558500 215.7558500 215.75585000 215.75585000000000000000000000000000000000	
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	T STREAM NUMBER NOTES - BELOW NOTES - BELOW T PRESSURE PSIA FRHALPY BILVHR LIQ. DENSITY,LB/CUFT FLOW RATES MOLES/H., HYDROGEN MOHOXTDE CARBON DIOXIDE NITRIGEN NATER NITRIGEN NATER NITRIGEN NATER NITRIGEN NATER NITRIGEN NATER NATER NITRIGEN NATER	4.54 4.54 585 585 585 585 565 15,533 16,605 16,605 16,605 16,605 16,605 16,605 16,7705 215,77							

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v.H.EISENH 87-7-1533	11.40 550.00 551.00 551.01 251.01 251.01 13.54545 37.134996 37.134999 37.134999 37.134999 1.000006-02 1.000006-02 1.000006-02 1.55.162356
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5, INC CYCLE 5 M PRODN: <u>FK-1570</u> Stream Survary	11,4 252.00 252.00 252.00 120,034 15,05934 16,050034 16,050034 16,050034 16,050050 10,00 10,000 10,000 10,000 110000 110000 110000 110000 110000 110000 110000 110000 110000 110000 1110000 1110000 1110000 1110000 1110000 1110000 1110000 1110000 1110000 1110000 1110000 1110000 1110000 1110000 1110000 1110000 1110000 1110000 1110000 1110000 1110000 1110000 1110000 1110000 1110000 1110000 1110000 1110000 1110000 1110000 1110000 1110000 1110000 1110000 1110000 1110000 1110000 1110000 1110000 1110000 1110000 1110000 1110000 1110000 1110000 1110000 1110000 1110000 1110000 1110000 1110000 1110000 1110000 1110000 1110000 1110000 1110000 1110000 1110000 1110000 1110000 1110000 1110000 1110000 1110000 1110000 1110000 1110000 1110000 1110000 1110000 1110000 1110000 1110000 1110000 1110000 1110000 1110000 1110000 1110000 1110000 1110000 1110000 1110000 1110000 1110000 1110000 1110000 1110000 1110000 1110000 1110000 1110000 1110000 1110000 1110000 1110000 1110000 1110000 1110000 1110000 1110000 1110000 1110000 1110000 1110000 1110000 1110000 1110000 1110000 1110000 1110000 1110000 1110000 1110000 1110000 1110000 1110000 11100000 11100000 11100000 11100000 1110000000000
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AIR PRODU LPMEOH FL	1,4 10,6 100,00 100,00 0,44639 16,050034 16,050034 16,050034 16,050034 16,050034 0,0 0,0 0,0 0,0 0,0 0,0 0,0 0,0 0,0 0,
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STREAM SUMMARY Version 82.021-a	STREAM NUMBER HOTES - BELOW FRESSULE FREFERENCE ENFERENCE PEGFF DEW POINT PEGFF DEW POINT PEGFF DEW POINT DEGFF I OW RATES MOLES/HR HARD MOUNTDE CARBON DIOXIDE CARBON DIOXIDE RITROGEN METHAND MITCO 90 OIL WITCO 90 OIL WITCO 90 OIL	ENTHALFY BIU/HR LIG, DENSITY,LB/CUFT FLOW, MOL WT FLOW, MALES MOLES/HR HYDROGEN MATER MATE	ENTILALPY BIU/HR LIQ1 DENSITY,1B/CUFT LIQ1 RATES HOLES/HR HYDROGEN CARBON MOHOXIDE CARBON MOHOXIDE METAMAG MATER MATER MATER MATER MATER MATER MATER MATER MATER MATER MATER MATER MATER
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LI SIREAM SUMMARY	2-133-130 LOTOLA	T [STREAM HUMBER 0 [NOTES - BELQX 1 [Pressure PSIA 1 [Tressure Dec,F 1 [Dev Point Dec,F	8080LE PT DEGAF ENTRALPY BIU/HR LIQL DENSITY.LB/CUFT LIQL DENSITY.LB/CUFT VAC. DENSITY.LB/CUFT VAC. MOL 4T	FLON RATES MOLES/IR Hydrogen Cardon Pondxide Carbon Dioxide	METHANE MITROGEN MATER METHANOL ETHANOL MITCO 40 DIL	TOTAL FLOW MOLVHR 18/HR Actual CFM	

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T STREAM NUMBER O HOTES - BELOW T FRESURE DEG,F L TEMPERATURE DEG,F L BUBBLE PT DEG,F L BUBBLE PT DEG,F L TQ DENSITY,LB/CUFT LIQ2 DENSITY,LB/CUFT FLOW RATES MOLES/HR			STREAM SUMMARY	RY				
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T STREAM NUMBER NOTES - BELGUM T PRESSURE BELGUM T TEMPERATURE PEIA ENHALPY BTU/HR LIC. DENSITY.LB/CUFT AVE. MDL MT BTU/HR LUC. BTU/HR FLOW RATES MOLES/HR HYDROGEN MOLES/HR HYDROGEN MOLES/HR MATER MATER MATER MATER MATER MATER MATER MOL HANG MATER MATER MOL HANG MOL HR MOL HANG MOL HR MOL	#2,40 #2,40 545.00 545.00 545.00 545.00 545.72 8.466772 8.466772 1.401579 1.421389 1.421389 1.421389 1.421389 2.15.539401 2.15.539401 2.15.533401 2.15.53315 2.15.533401 2.15.533401 2.15.53315 2.15.533401 2.15.53315 2.15.53515 2.15.55515 2.15.555515 2.15.55515 2.15.5555555555	44 95 45 535 00 535 00 535 535 535 00 233 55 55 55 55 55 55 55 55 55 55 55 55 5						

27.37 CPU SECONDS CYCLE SYNTHESIS RUN TIME : ρ

4. CAUTION: TWO LIQUID PHASES NOT CONSIDERED. "RESULTS MAY BE IN ERROR.

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	22JAN.82 PAGE 12:47:19	18 18 19 19 19 19 10 17 17 17 17 17 17 17 17 17 17	
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Case EB-X954

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STREAM SUMMARY Version 82.021-A	STREAM NUMBER NOTES - BELOW PRESSURE PSIA PRESSURE PSIA PEW POINT DEG.F ENTALPY BTU/HR ENTALPY BTU/HR FLOM RATES MOLES/HR FLOM RATES MOLES/HR FLOM RATES MOLES/HR FLOM RATES CARBON DIOXIDE CARBON DIOXIDE MATTER MA	ENTHALPY BTUTHR LIQ. DENSITY, LB/CUFT AVE. MOL WT ML BS/CUFT AVE. MOL WT ML BS/CUFT AVE. MOL WT ML BS/CUFT AVE AND MINOXIDE CARBON MUNOXIDE CARBON MUNOXIDE MUTOXIDE MUNOXIDE	ENTHALPY BTU/HR LIGI DENSITY,LB/CUFT AVE. MOL WI FLOW RATES MOLES/HR Hydrody Monoxide Carbon Monoxide Carbon Dioxide Methane Nitrogen Kater Methand
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22JAH.82 PAGE 54 12:47:19	4 4 65 1 20.00 104.19 -2974003.00 -2974003.00 -20 30.475159	2.463496-03 5.53546E-03 5.53546E-03 5.53686E-02 5.788175 7.788175 2.48175 2.195898 2.19584E-02 2.19584E-02	28.243912 860.737549 0.0	LIQ
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TOTAL LIQ, MOLYHR LBYHR	ENTHALPY BTU/HR VAP. DEHSITY,LB>CUFT VAP. DEHSITY,LB>CUFT FLOE RAIL MT FLOE RAIL MT FLOE RAIL MOHES/HR CARBON BOHDXIDE CARBON BIOXIDE METHANG MATER MATER MATER MATER MATER MATER MATER MATER MATER MATER MATER MATER MATER MATER	TOTAL VAPOR MOLVHR LOVHR Actual CFM

T.R.TSA0 87-7-1533

21JAN.82 PAGE 12 15:29:10

AIR PRODUCTS & CHEMICALS, INC -- CYCLE SYNTHESIS LPMEOM ENTRAINED/LURGI: EL-6752 STREAM SUMMARY STREAM SUMMARY Version 82.021-A

4, 95 735.00 775.00 775.00 775.00 755.02 55.628566 6.146519 5.615254 1.85665-10 9.615254 1.615254 1.615254 1.615254 1.615254 1.615254 2.15.116109 2.15.816024	545551.613235 545551.347656 LIQ
42,4 42,4 455,50 455,60 455,60 455,60 15,052528 16,052228 16,05256 16,16653 16,0581 1,616653 1,616653 1,616653 1,616651 1,83656610 1,6166519 1,61913 2,61861913 1,61161913 1,61161913 1,6116131 1,61161313 1,61161313 1,61161313 1,61161313 1,61161313 1,6116131 1,61161511 1,6116151515151 1,611615151515555555555	251.613235 54555.347656 LIQ
T STREAM NUMBER N HDTES - BELOW T FREESURE BELOW F51A F1 PREESURE DEG.F ENTHALPY BIU/HR L ENTHALPY BIU/HR AVE. MOL WI AVE. MOL WI HAVE. MOL WI FLOW RATES MOLES/HR FLOW RATES MOLES/HR FLOW RATES MOLES/HR HAVE CARBON DONOTOF CARBON DONOTOF CARBON DIOXIDE NATER MATER MATER MATER MATER MATER MATER MATER MATER MATER MATER MATER MATER MATER MATER MATER	TOTAL FLOW MOLVHR Lavhr

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NOTES

1. STREAM SPECIFIED AS ALL VAPOR 2. Stream Specified As all Liquid 4. <u>cauiloy</u>" two Liquid Phases Hot Considered. "Results May de In Error.

34.15 CPU SECONDS CYCLE SYNTHESIS RUN TIME :

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21 JAN.82 PAGE 15:41:04	21 25 21 25 25 25 25 25 25 25 25 25 25
51 3	15 742-00 742-00 742-00 742-00 1456.00 1.456.00 1.456.00 1.456.00 1.640005-02 2.40005-02 2.40005-02 2.400005-02 2.400005-02 2.400005-02 2.400005-02 2.400005-02 2.400005-02 2.40005-02 2.40005-02 2.40005-02 2.40005-02 2.40005-02 2.40005-02 2.40005-02 2.400005-02 2.400005-02 2.400005-02 2.40005-02 2.40005-02 2.40005-02 2.40005-02 2.40005-02 2.40005-02 2.40005-02 2.40005-02 2.40005-02 2.400005-02 2.500005-0200000000000000000000000000000
T.R.T540 \$7-7-1533	10 136.00 136.00 136.00 135.00 13.01995 1.95016 1.66006-02 2.400006-02 2.400006-02 2.400006-02 2.400006-02 2.400006-02 1.556527 1.556527
SYNTHESIS RY	1,4 1,50.09 1,50.09 1,50.09 1,269641 1,269641 1,269641 1,269641 1,269641 1,269641 1,269641 1,269641 1,269641 1,577000 1,000 1,5770000 1,577000 1,577000 1,577000 1,5770000 1,577000 1,577000 1,577000 1,577000 1,577000 1,577000 1,577000 1,577000 1,577000 1,577000 1,577000 1,577000 1,577000 1,5770000 1,5770000 1,5770000 1,57700000 1,57700000000 1,57700000000000000000000000000000000000
5, IHG CYCLE 5 : <u>EK-4752</u> : STREAM SUMMARY	11,4 126.00 126.00 126.00 126.00 126.999 11.577000 12.570000 12.570000 12.570000 12.570000 12.570000 12.570000 12.570000 12.570000 12.570000 12.570000 12.570000 12.570000 12.570000 12.5700000 12.5700000 12.5700000 12.57000000 12.57000000000000000000000000000000000000
AIR PRODUCIS & CHEMICALS, INC CYCLE SYNTHESIS LPMEOH ENTRAINED/KT GAS: <u>EK-4732</u> Siream Summ.ry	1 ,45 1 ,45 1 ,55 1 ,57700 1 ,577000 1 ,5770000 1 ,5770000 1 ,5770000 1 ,57700000000000000000000000000000000000
AIR PROD LPMEOH E	<pre>*1.4 1.5.00 150.00 150.00 150.00 0.3855.25 0.3855.25 0.3855.25 14.7999 14.7999 14.7999 14.7999 14.7999 14.7999 14.7999 15.231978 15.231978 15.231936 15.231936</pre>
STREAM SUMMARY Version 32.021-a	T [STREAM NUMBER MOTES - BELOW T PRESSURE PERFERENCE DEW POINT DEG.F DEW POINT DEG.F NUMENDERSTYLEVCNT AVE. MOL WITYLEVCNT AVE. MOL WITYLEVCNT AVE. MOL WITYLEVCNT AVE. MOL WITYLEVCNT AVE. MOL WITYLEVCNT AVE. MOL WITSCH METHANC METHANCL MITROGEN METHANOL ETHANOL ETHANOL TOTAL FLOW MOLVHR TOTAL FLOW MOLVHR TOTAL FLOW MOLVHR

STREAMS ARE ALL VAPOR

Case EK-4752

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T.R.T5A0 87-7-1533	35 690-00 110.00 110.00 125.25.26.72 21.56.726.72 35.654.72 1.64.5134 1.64.5134 3.56.265 6.06.055-65 6.06.055-65 6.224.651 5.325.0565 5.325.0565 5.325.0565 5.325.0565 5.325.0565 5.325.0565 5.325.0565 5.325.0565 5.325.0565 5.325.0565 5.325.0565 5.325.0565 5.325.055 5.325 5.325 5.325 5.325 5.325 5.355 5.5555 5.555 5.5555 5.5555 5.5555 5.5555 5.5555 5.5555 5.55555 5.55555 5.55555 5.555555	6.16557 6.82299	-42/201-05 35.526917 35.526917 5.680549E-02 1.94416E-02 5.70115E-02 5.70115E-02 5.28070707070000000000000000000	-421759.94 -421759.94 -47.856501 -286127-02 5.496127-02 1.996126-02 1.906126-02 1.902136-02 5.701136-02 5.701136-02
SYNTHESIS Ly	32 32 291.22 291.22 291.22 291.22 291.22 291.22 291.22 291.22 291.22 291.22 291.22 291.22 291.22 291.22 36.64153 36.64153 36.64153 36.65 6.0680555902 6.0680555902 6.2553451 7.2753451	0 H 0		
5, INC CYCLE 5 : EK-4752 STREAN SUMMARY	44 46 700.03 700.23 -2473911.00 21.982906 35.889906 35.889906 35.889906 35.889906 35.28076 6.86805E-02 6.86805E-02 6.256136 9.235090	14	4,6481.24 4,6481.24 4,6481.24 4,0481.25 1,66781.55 1,66781.55 1,67881.55 1,67881.55 1,77	
PRONUCTS & CHEMICALS, Eoh Entraihed/KT Gas:	6 25 6 25 6 25 6 10 710.00 710.00 710.00 710.00 88.69805.00 1.669855.00 1.6698556 0.0062807 0.2060155 0.2060			5 6 6 8 7 7 7 7 8 7 7 7 7 7 7 7 7 7 7 7 7
AIR FROM LPMEOH E	**************************************	315.47973 6016.08203	-15874368.79 25.587677 15.793287677 16.793289 16.793289 0.338450 0.338450 0.338450 0.338450 0.35882344 215.584778 215.584778 215.584778	
STREAM SUMMARY Version 82.021-a	STREAM NUMBER NOTES - BELOW PRESSURE PSIA TEMPERATURE PEG,F EHTHALPY BEU/HR AVE MOL WT BEU/HR PLOW RATES MOLES/HR HYDROGEN MOHOXIDE Carbon Dioxide Methane Mater Hater Mitrogen Mater Mitrogen M	TOTAL FLOW MOL/HR LB/HR	ENTHALPY BTUVIR LIQ. DENBITY,LB/CUFT AVE. WIL WT FLOW RATES MOLES/HR PROBON MONOXTDE CARBON MONOXTDE MATTR M	LIQ1 DENSITY, LBUCHR LIQ1 DENSITY, LBUCHR AVE. MOL HY FLOM RATES MOLES/HR FLOM RATES MOLES/HR CARBON MOHOXCDE CARBON MOHOXCDE CARBON DIOXCDE MATER MATER MATER MATER MATER MATER MATER
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	TOTAL LTQ. MOLVHR Total Ltq. Holvhr	T CONTRACT BTU/HR T LOC DEHSTY/LB/CUFT AVE AOL WT AVE AOL WT AVE AOL WT AVE AOL WT AVE AND WIGKTDE C ARBON MOHOXIDE C ARBON MOHOXIDE AFTHANDL METHANDL METHANDL TOTAL LTQ. MOL/HR TOTAL LTQ. LB/HR	V ENTHALPY BTU/HR -2 A YAP- DENSTY/LB/CUFT O FLOL WT ATES MOLES/HR R RYDROGEN MOLES/HR R CARBON MONXIDE CARBON MOUXIDE METHANG METHANGL METHANGL METHANGL METHANGL METHANGL METHANGL METHANGL METHANGL	TOTAL VAPOR MOL/HR Ib/Hr Actual GFM Actual GFM
141 142			an na kao kao kao kao	

21JAN.82 PAGE 10 15:41:04	45 65 46 65 108.15 108.15 108.15 4531158.15 4531158.15 4531158.15 4531158 10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.
533	4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4
T.8.75An 87-7-1533	60 109.95 109.95 109.95 109.95 109.200256 1091356 10.0256949 1.6231356-02 1.691355-02 1.691355-02 1.691355-02 1.691355-02 1.5313596-02 1.5313596-02 1.5313596-02 1.5313596-02 1.5313596-02 1.531359 1.177277 1.177277 1.177277 1.177277
CYCLE SYNTHESIS Surmary	157 151.07 151.07 151.07 151.07 15.79966 20.3559966 15.7900000 15.790000 15.790000 15.7900000 15.7900000 15.7900000 15.7900000 15.7900000 15.790000000 15.79000000000000000000000000000000000000
5, IHC CYCLE 5 : EK-4752 STREAM SUMMARY	•15 •15 •15 •15 •15 •15 •16 •10 •10 •10 •10 •15 •10 •15 •10 •15 •10 •15 •10 •15 •10 •15 •15 •15 •15 •15 •15 •15 •15 •15 •15
AIR PRODUCTS & CHEMICALS, INC LPMEOH EHTRAINED/KT GAS= EK-4752 Stream	54 64 54 685.00 685.00 0.0 0.0 0.0 0.0 0.0 0.0 22.255300 1.555401 1.555401 1.555401 1.555401 1.556500 1.555611 1.664375214 1.664375214 2.577465 2.577455 2.577465 2.577455 2.577455 2.5774555 2.5774555 2.57745555555555555555555555555555555555
AIR PROD LPMEDH E	50 53 53 53 53 53 53 53 54 53 54 54 54 54 54 54 54 54 54 54
STREAM SUMMARY Version 82.021-A	T STREAM NUMBER NOTES - BELOW T FRESSURE T FERFESURE T FERFESURE FSID BUBBLE PT DEG,F BUBBLE PT DEG,F BUBBLE PT DEG,F EUBBLE PT DEG,F LIQ DEHSITY,LB/CUFT LIQ DEHSITY,LB/CUFT VAP. DEHSITY,LB/CUFT AVE. MOL WT AVE. MOL WT AVE

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STREAM SUMMARY Version 82.021-A	AIR PROD LPMZOH E	DUCTS 1 CHEMICAL	5, IHC CYCLE : EK-4/52 Stream Summa	SYNTHESIS By	1.R.TSA(87-7-15)	533 1533	21JAN.82 PAGE 1 15:41:04
T İSTREAM NUMBER 0 İnotes = Belom 1 Pressure Psia	<u>ه</u> ؟	76 00.0	77 700.00	ه. :	80 82,4 685.00	42,4 710-00	84 84 755.00
TEMPERATURE DEG.F BUBBLE ?T DEG.F ENTHALP? BTU/HR AVE. MOL WT	481.99 481.99 -35862768.00 217.446823	291.22 291.22 -9158.22 216.245728	291.22 -36632.90 216.245697	3.6. 3	58.0 16.5 6203	58.1 05.7 6293	83.8 72.0 5618
	12.869812 16.621048 0.844998	2.48079E-03 3.45957E-03 2.96890E-04	9.92315E-03 1.35332-02 1.18756E-03	2.17204E-03 3.37232E-03 6.96947E-04	1.20952E-02 1.72106E-02 1.88451E-03	0.0	12.881907 16.638245 0.846883
METHANE MATROGER WATROGER MATHANOL ETHANOL MATTO 40 DIL	0.0 0.335755 2.235176-08 3.987540 2.852941 215.581741	0.0 6.103616-05 5.2803176-12 1.3303176-12 3.065766-03 4.570256-03	2.443855-04 2.1432855-04 2.1132805-04 5.323805-03 1.226305-03 1.226305-03	0.0 4.92040E-05 8.95540E-12 5.95540E-12 1.13745E-04 4.51145E-02	2.9535885-04 2.9535885-04 2.9535885-04 5.919368-01 1.340058-03 1.340058-03	2,935886-04 2,93586-04 2,933678-11 5,933678-11 5,933678-13 1,340056-03 1,340056-03	2.2356946 2.23156946 2.995659 0.850281 215.809662
	65953	0.05363	0.214553	0.052114 11.433830	0.266667 [.] 57.829895	0.266{57 57.829895	251.366501 54658.683594
L [ENTHALPY BTU/HR I [LIQ. DEHSITY,LB/CUFT Q [AVE. MOL H]	-35862763.00 35.51115 217.696823	-9158.22 40.375137 216.245632	-36632.90 40.375137 216.255636	-10183.68 49.200256 219.399338	-46816.57 41.146332 216.862030	-46884.44 41.147568 216.886734	-35859856.00 35.284213 217.446213
	16.12	2.48079E-03 3.45957E-03 2.75890E-04	9.923156-03 1.383836-03 1.187566-03		1.209526-02 1.72106E-02 1.88951E-03	60 (P H)	
METHANE MATER WATER METHANOL MATCO 40 DIL	0.0 0.335753 2.235775-00 3.8387941 215.858941 215.581741	0.0 6.10961E-05 5.28317E-05 3.0357E-03 3.05576E-03 4.57053E-02	2.44385E-04 2.113285E-04 5.32380E-03 1.22630E-03 1.22630E-03	0.0 4.92040E-05 8.5040E-05 5.95510E-04 1.137458-04 4.511458-02	2.95388E-04 2.95388E-04 2.91938E-11 5.91938E-03 1.34005E-03 1.227924	2.93596E-04 2.793596E-04 5.91755E-04 1.33995E-03 1.33995E-03	2.238046 2.2386046 0.86028 0.860281 215.809662
TOTAL LIQ. MOL/HR Lo/HR	251.09983	55	52	05211	0.264667 57.829895	0.266653 57.829178	251.366455 54658.683594
	0.0 0.0	0.0	0.0 0.0	-10183.68 44.427689 219.399338	0.0 0.0 0.0	0.0	8-0 0-0
I FLOW RATES HOLES/HR HYDRCGEN CAREON DIONIDE CAREON DIONIDE METHAND METHANDL METHANDL LETHANDL	6 566666666666666666666666666666666666		900000000 	2.17204E-03 5.37232E-03 6.9507FE-04 4.92040E-05 5.95510E-05 5.95510E-04 1.13455-04		000000000 000000000	922359980

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TOTAL LIQ. MULHR LB/HR	V ENTHALPY BIUCHE A VAP. DENSITY-LB/CUF; AVE. MOL WI AVE. MOL WI F LOW, RATES FOLES/HR CARBON MOHOXIDE CARBON MOHOXIDE CARBON MOHOXIDE CARBON MOHOXIDE MATER METHANOL LITEO 40 OIL LITEO 40 OIL LITEO 40 OIL TOTAL VAPOR MOL/HR ACTUAL CFM

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AIR PRODUCTS & CHEMICALS, INC CYCLE SYNTHESIS LPheoh Entrained/kt gas: EK-4752 Stream Summary	
DUCTS & CHEMIC Entrained/kt g	46 46 475.05 475.05 475.05 235.711426 235.711426 217.655905 12.885905 12.885905 12.885905 12.885905 10.547400 0.034600 2.7744261
AIR PRO LPMEOH	90 755,40 755,40 -3585948.00 25588747 217.459839 12.885908 12.885908 12.885908 0.834903 0.834903 0.834903 0.835960 2.77452515 2.77452515
STREAM SUMMARY Version 82.021-a	T [STREAM HUMBER D HODES - BELOW T PRESSURE PSIA PRESSURE PSIA L FRYPALLPY BULHR L ENTHALPY BULHR LIQ, DENSITY,LB/CUFT LIQ, DENSITY,LB/CUFT FLQW RALE MOLES/HR FLQW RALE MOLES/HR PLQW RALE MOLES/HR FLQW RALE MOLES/HR CARBON MOUXIDE CARBON MOUXIDE METHANE MATER MATEROEH WATEROEH

-36052464.00 355714420 25714420 114464359 1566634003 166634003 166634003 1647319 2.774426-11 355160 2.774426-11 3449048 2.15.817825 2.15.817825	251.355881 54659.808594
-358594870 555594870 217.459487 12.855948 12.855948 16.034903 0.847319 0.847319 0.847319 0.335160 2.774426-11 2.774426-11 2.7744265 3.5991665 2.57744265 2.57164655 2.57164255	251.355881 54659.808594
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STREAM SPECIFIED AS ALL VAPOR
 STREAM SPECIFIED AS ALL LIQUID
 Stream Specified as all liquid
 Cauiton: Two Liquid Phases and Considered. Tresults may be in Error.

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31.74 CPU SECONDS CYCLE SYNTHESIS RUN TIME :

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21JAN.82 PAGE 12 15:41:05

T.R.T5A0 87-7-1533

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20JAN.62 PAGE 12:44:29		254.468323 54746.281250 -33862640.00 228.341864 8.402276 1.57467 1.574677 1.557477 1.557477 2.15.71655 2.15.717655 2.15.71755 2.15.71755 2.15.71755 2.15.717555 2.15.717555 2.15.717555 2.15.7175555 2.15.71755555 2.15.71755555555555555555555555555555555	-558755.65 2.1652128 2.1652128 5.238514 9.581918 9.581918 9.581918 9.581918 9.581918 1.50458 4.31156-02 4.31156-02 4.31156-02 4.31156-02 5.137347 3.552781 5.1,998255 5.1,998255	
ISENHAU 533	4 4 4 4 4 4 4 4 4 4 4 4 4 4	M M M M M M M M M M M M M M M M M M M	-518125,44 50.77984 50.677984 50.634695 10.034695 10.036795 10.036795 10.036795 10.552765 10.552765 1.552765 1.552765 1.0506899 4.51266899 4.51266899 4.512645 3.11325458	
У.Н.ЕТ: 87-7-11	2010 2010	14 14 15 15 15 15 15 15 15 15 15 15 15 15 15	-518126,75 0.948408 15.449860 10.7990000 0.7990000 0.3550000 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0	07920-
5 SYHTIIESIS 1 <u>1</u> КТ		117-98 311-98 31-98 228 228 228 228 228 228 228 228 228 2	-545320.13 13.45554 13.459566 10.7390000 10.7390000 1.50000 1.50000 1.50000 1.50000 1.50000 1.00 1.	
S, INC CYCLE S M Prodn: <u>Ek-2571</u> Stream Summary	#1,45 242.0 120.0 6,3326.7 6,3326.7 120.0 6.83000 6.83000 6.83000 6.83000 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	331.2.984985 331.2.984985 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.	-567326.75 -5726.75 16.459860 16.830000 10.750000 10.750000 10.0 1.50000 1.500000 1.500000 1.500000 1.500000 1.5000000 1.5000000 1.500000000 1.5000000000000000000000000000000000000	77010.
IR PRODUJIS & CHEMICAL PMEOH ENTRAINED/K-T MI	E1,43 287.0 281.7 281.7 281.7 85000 1.3500000 1.3500000 1.3500000 1.3500000 1.3500000 1.3500000 1.350000000 1.35000000 1.350000000 1.35000000000000000000000000000000000000	17.984985 331.626315 6.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	-569209.56 0.678357 16.679860 16.690000 16.759000 0.759000 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	
AIR PROL LPMEOH E	11.4 100.0 100.0 100.0 100.0 100.0 100.0 179000 0.79000 0.79000 0.1 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	331.585985 331.620 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0	-569678.44 -569678.44 18.449869 18.449869 10.790000 10.790000 1.984985 17.984985 12.030315	20n¢n•2
STREAM SUMMARY Version 82.011-a	STREAM NUMB NDTEE - SEL NDTEE - SEL TEMPESURE DEW FUTHT AVE. NOL WITHOUT FLOW RATES Hydrogen METHANDL Carbon DI METHANDL MITROGEN UATER	TOTAL FLOW MOLVHR LBVHR ENTHALPY BTUVHR LTG. DENSITY-LBVCUFT AVE. MOLWT MOLET AVE. MOLWT MOLESVHR FLOW ATES MOLESVHR AVERAN MONZIDE CARBON DIOXIDE ATER MATE	ENTHALPY VAP. DEHSITY,LB/CUFT VAP. TOL WI FLOG RATES MOLES/HR HYDROGEN CARBON MONOXIDE CARBON MONOXIDE CARBON DIOXIDE RETHANUL WITROGEN MATER METHANUL ETHANUL WITCO 40 OIL WITCO 40 OIL MITCO 40 OIL MITCO 40 OIL	ALIUAL LEN
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Case EK-2571

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TREAM SUMMARY Ersion 82.011-A	AIR PRODU LPMEOH ER	NUCTS & CHEMICALS. ENTRAINED/K-1 MIN	5, INC CYCLE S H Prodn: EK~2571 Stream Summary	. SYNTHESIS 1 Ry	V.H.EIS 87-7-15	SENHAU 533	20JAH.82 PAGE 12:44:29
STREAM NUMBER NOTES - BELOW PRESSURE PSTA TEMPERATURE DEG,F DEW POINT DEG,F BRITALPY BTU/HR AVE. MOL WT FLOW RATES MOLES/HR CARBON MONOXIDE CARBON DIOXIDE METHANE	7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7	84 84 84 86 85 86 86 86 86 86 86 86 86 86 86 86 86 86	500.6 500.6 500.6 500.6 50.20 20.20 13.63332 13.633332 13.633332 13.633332 13.633332 13.633332 13.633332 13.633332 13.63533332 13.63533332 13.6353332 13.6353332 13.6353333332 13.6353332 13.63533332 13.6353332 13.6353332 13.635332 13.635333332 13.635333332 13.63533333332 13.63533333332 13.6353333333333333333333333333333333333		2,43 110.00 110.00 11378.69 11378.69 119989 10.0 1989 10.0 1989 10.0 1989 10.0 1989 10.0		- 55 - 55 - 55 - 11 - 15 - 15 - 15 - 15
NITEGEN Mater Methanol Ethanol Mitcd 40 dil Total Flow Mol/Hr LB/Hr	1.55618E-02 7.55270E-03 6.655255 4.42075E-02 6.741125 16.709625 367.504150	1.552708-02 7.552708-03 6.635257 4.42068-02 0.141125 16.709625 367.504150	7.55276E-02 7.55276E-02 4.592559E-02 1.11410E-02 16.566956 354.755127	7.5527664-02 7.5527664-02 4.461438 4.413746-02 3.713746-02 3.713765-02 341.305664	9.5000E-02 0.0 0.0 0.0 1.675858	1.2545956702 1.2545956703 9.194503 9.10181967703 1.6.0809845 5.16.080215	2.81(2)35-02 0.435695 3.43105-02 2.914555-03 17.477956 17.477956
ENTHALPY BTU/HR LIQ. DENSITY, LB/CUFT AVE. NUL WT FLDM RATES NOL ES/HR HYDRDGEN NORDGEN CARBON MDNOXIDE CARBON MDNOXIDE METIANE MATER MATER MATER MATER MATER MATER MATER MATER MATER MATER MATEN MATE	0 0 00 0000000000000000000000000000000	-24959.16 39.653020 229.552429 4.51576E-03 4.152070E-03 4.152070E-03 1.9267E-03 1.92657E-03 1.08567E-03 2.285567E-03 2.289567E-03 2.229926		-56140.00 48.0 48.6 48.6 2.188625 6.156958 6.156958 6.156958 1.779958 6.258658 6.258658 6.2584558 1.7128558 3.4177552 3.41775555 3.417755555555555555555555555555555555555	-11378.69 61.833420 13.019989 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.		-60137.52 50.119256 50.119256 50.1194664 2.848556-05 1.194866-05 3.827346-05 5.817266-05 5.817266-05 5.91426-02 2.91456-02 2.91456-02 2.914556-05
LB/HR LEATHALPY BTU/HR LEAT DENSITY.LB/CUFT AVE. MOL WT NLE/CUFT AVE. MOL WT NLE/CUFT AVE. MOL ES/HR HVDROGEN MATROGEN MATROGEN MATROGEN MATROGEN MATRO							2.411725 -60137.52 50.139236 50.139236 50.794656-05 7.976945-03 1.19885-03 1.19885-03 5.827346-06 8.827346-00 8.827346-00 8.827346-00 8.82

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6.0 0		
0.468773 16.1301?7	-7546.55 227.956403 227.956909 1.09084E-03 1.70677E-03 3.36453E-03 3.96453E-06 3.95453E-06 3.95453E-05 3.37077E-05 7.43109E-05 7.43109E-05 3.37077E-05 3.508172	-5591880.38 1.55880.38 1.5588791 5.432034 1.55859944 1.553598-02 1.553598-02 1.553598-02 9.24446-03 9.24446-03 9.24446-03 9.25671086-03 9.24446-03
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TOTAL LIG. MULYR Leater	L LEAZ DENSITY BTU/HR L LEAZ DENSITY LB/CUFT AVE. MOL MI LURZ DENSITY LB/CUFT AVE. MOL MI L CARBON MOHOXIDE CARBON MOHOXIDE CARBON MOHOXIDE CARBON MOHOXIDE CARBON MOHOXIDE CARBON MOHOXIDE CARBON MOHOXIDE CARBON MOHOXIDE MITROGEN MATER MATER MITCO 40 DIL TOTAL LIQ. MOL/HR	V ENTHALPY BTU/HR A VAP. DENSITY.LB/CUFT AVE. MOL WT AVE. MOL WT AVE. MOL WT HYDROGEN MYDROGEN NTROGEN METHANU MATER MATHANU ETHANU ETHANU ETHANU FITCO 40 DIL MITCO 40 DIL MITCO 40 DIL MICO 40 DIL MICO 40 DIL MICO 40 DIL

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• • • • • • • • • • • • • • • • • • •	0.154/93 35.493561
T STREAM NUMBER HOTES - BELOW HOTES - BELOW T FRESSURE DEG,F EUDIN HET DEG,F EUNHALPY BIU/HR EUNHALPY BIU/HR EUNHALPY BIU/HR EUNHALPY BIU/HR LIQO DENSITY, LS/CUFT LIQO DENSITY, LS/CUFT VAP DENSITY, LS/CUFT VAP DENSITY, LS/CUFT AVENDE METHANG CARBON DIOXIDE METHANG METHA	I ULAL FLUM RULYAK

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CYCLE SYNTHESIS RUN TIME : 29.41 CPU SECONDS

1. STREAM SPECIFIED AS ALL VAPOR 2. Stream specified as all liguid 4. <u>cauiton</u>: two liguid phases not considered. "Results may be in Error.

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20JAN.82 PAGE 9 12:44:29

V.H.EISENKAU 87-7-1533

AIR PRODUCTS & CHEMICALS, INC -- CYCLE SYNTHESIS LPMEOH ENTRAINED/K-T MIN PRODN: EK-2571

STREAM SUMMARY Version 82.011-A

STREAM SUMMARY

A Air Products

PAGE 1 of 2 DATE 1/29/82 Revised _____

CENTRIFUGAL PUMP SPECIFICATION SHEET

EXHIBIT 2.3.1-6

USTOMER APCI	
VENDOR By Elec. Mech. UNIT LP MeOH PDU	PROJECT ND. 87-7-1533
ENERAL INFORMATION Slurry Circulation Pump	
1. ITEM ND. 10,50 A & B	
2. No. REQUIRED Two (2) - one on stream &	one_spare
T 3. TYPE	
4. DUTY (CONTINUOUS, INTERMITTENT) Continuous	
5. SERVICE . To circulate hot oil and	hot oil-catalyst slurry
ROCESS INFORMATION Liquid Fluidized Mode	Liquid Entrained Mode
7, FLUID *Hydrocarbon Fluid & Dissolved Syngas+CH ₃ OH	Hydrocarbon Fluid-Catalyst
8. CORROSIVE COMPOUNDS	Slurry & Dissolved Syngas &CH ₂ O
9. Solids None	Metal oxides powder:~50/4%
10. TEMPERATURE, OPERATING, F 430~530	430~530
11. TEMPERATURE, MAXIMUM, °F 550	550
12. VAPOR PRESSURE, OPERATING @530°F, psia 5 sat'd w/	
13. SPECIFIC GRAVITY, OPERATING @480°F 0.63	0.89
14. SPECIFIC GRAVITY. 2 60°F D.8'	1.15
15. VISCOSITY, OPERATING @480°F CPS 0.7	1.0 Max. Slurry Conditions
16, VISCOSITY, a 60°F CPS 6	9
17. NORMAL FLOW - GPM 200	200
18. MAXIMUM FLOW GPM 250	250
19. Minimum Flow GPM 150	150
20. Solid Concentration Wt.% D	33 Max. (8% by vol. @ 100°F
HYDRAULIC INFORMATION	6% by vol. @ 480°F
1_21. NPSH REQUIRED By Elec. Mech.	By Elec. Mech.
22. NPSH AVAILABLE	
23, SUCTION PRESSURE PSI 495/695/895	495/695/895
24. DISCHARGE PRESSURE PSI 545/745/945	545/745/945
25. HEAD REQUIRED PSI 50 = 185 ft. 0 480°F	50 = 130 ft, 0 480°F
26, HEAD AVAILABLE PSI	
27. Avail. Condensed Oil for Seal Flush, GPM 0280°F, Min/Max, 0.1	/1 0.1/0.7
28.	
<u>CONSTRUCTION</u>	<u>الاستراحي والالاحرية من المحروم من المحروم المحروم المحروم المحروم المحروم المحروم المحروم المحروم المحروم ا</u>
29. MATERIAL OF CONSTRUCTION	
30. CONNECTIONS (INCLUDE FIG. RATING; 3-1/2" in/3-1/2"	cut or by vendor
31. PACKING AND/OR SEALS Seal flush requirement should be	minimized to less than U.I.GPM
32. IMPELLER TYPE if possible. The use of water a	s supplment seal flush should
33. STUFFING BOX only be considered as the last a	Iternative when other means to
34. SMOOTHERING GLAND provide adequate seal flush fail	Vendor should specify the
34. SMOUTHERING GLAND MOVING addite Section 1997	allowable solid loading,
36. particle size, etc.	
DRIVER	
37. TYPE Flectric Motor	
38 CURRENT CHARACTERISTICS	
39. MOTOR CLASS	
40. RPM & HORSEPOWER RATING	
41. BHP & REQUIRED CAPACITY	
42. MANUFACTURE & MODEL NO.	
43. *See attached Table 1	
44.	، بالمحمد المحمد الم

FORM 8243 (REV. 11/75)

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SPECIFIED BY T. R. Tsao 1/29/82

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SPECIFICATION SHEET

2 of 2 29 January 82

For Slurry Circulation Pump 30.50 A&B

EXHIBIT 2.3.1-6

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RELEASED FOR PROJECT

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CI Table 1 PROPERTIES OF WITCO #40 OIL

1. Composition - (72% paraffinic, 28% maphthenic)

Component	<u>x</u>
C14	5
C14-C15	15
C16-C17	20
C18-C19	25
C20-C21	20
>C21	15
Sulfur	1 ppm

- 2. Viscosity, Kinematic = 4.2 cSt 0100°F Saybolt = 40-43 SUS 0100°F
- 3. Vapor Pressure < 0.002 mm Hg @100°F
- 4. Specific Gravity = 0.810 @ 60°F Density = 0.810 g/cc @100°F
- 5. Initial Boiling Point = 471°F @ 1 atm.
- 6. Solubility in Methanol: 7.2 wt. % oil 0 0 wt. % H₂O in methanol and 120°F 2.9 wt. % oil 0 0 wt. % H₂O in methanol and 70°F 2.1 wt. % oil 0 5 wt. % H₂O in methanol and 120°F (Insoluable in Water)
- 7. M.W. = 268.5 1b./1b. mole
- 8. ASTM Pour Point = -35°F, maximum
- 9. Surface Tension = 32 dynes/cm. 0~68°F = 13 dynes/cm. 0~464°F
- 10. ASTM Cloud Point = +40°F, Maximum
- 11. Saybolt Color = +30
- 12. Odor or Taste-> None
- 13. U.V. Absorbance-> Passes FDA Requirements
- 14. USP Acid Test→ Passes

2					PAGE	1/2
AA	r Products)	COMPRESSOR	SPECIFICATION	N SHEET	DATE	29 January 1982
		EXH	IBIT 2.3.1-7A		REVISED	
CUSTOM	ER APCI					
VENDOR		1	UNIT LP MeOH PD	U I	PROJECT NO.	87-7-1533
	L INFORMATION		Feed Compressor			
1	ITEM NO.		01.10			
	ND. REQUIRED		one (1) Reciprocating Co		. ovpostod	
N3			Continuous	ompressor	expected	
<u> 4 </u>	SERVICE		Compress Dry Sy	nthesis (Gas (H2, CO,	CQ2, N2, CH4)
	S INFORMATION					
	FLUID		Synthesis Gas			
	COMPOSITION - MO	L X	(see page 2/2)			
8.	AVERAGE MOLECULA	R WEIGHT	(see page 2/2)			<u></u>
1	CORROSIVE COMPOU			0.111	<u> </u>	
_10,	RELATIVE HUMIDIT		7% (7x10-4LB H2		Gas, U.P. = 2	(/°F)
' <u>-11-</u>	SUCTION TEMPERAT	URE °F.	100 Norm., 125 150	<u>max.</u> 50	150	
12.	SUCTION PRESSURE Discharge Pressu	- PSIA		50**	950***	
13.	DISCHARGE PRESSU DISCHARGE TEMPER			<u> </u>		
15,	NORMAL SUCTION F				<u> </u>	
I	A. A.C.F.M.		S	ee page 2	2/2	
	B. POUNDS/HOUR					
<u> 16. </u>	STANDARD CUBIC F			0.40		
1-17.	COOLING WATER SU		90 Nor., 105 Ma		psiq [‡]	
18,	COOLING WATER RE	TURN °F.	120 Nor., 105 M	<u>lax. @ 10</u>	ps1q+	
and the second design of the s	NUCTION					
<u>20,</u>	TYPE OF COMPRESS	DR				•
21.	MATERIAL OF CONS					
22.	SUCTION CONNECTI		2-1/2" or by ve	ndor		
23.	DISCHARGE CONNEC	TIONS	2-1/2" or by ve	ndor/int	<u>erstage relie</u>	ef valve inlet flange
_24 .	TYPE OF LUBRICAT				2-1/2" with 4	150 psig design press
25.	COMPRESSOR SPEED		Tuteurezleu Pu			Fax 100% varials
<u>_26</u> , _27,	AFTERCOOLER REQU				obier design	for 100% recycle
	AFTERCOOLER SURF		Intercooler by	COMDress	or vendor: re	ecycle cooler by proce
29,	WATER REQUIRED G		By vendor **Coo	ling wat	er is a premi	ium
30,	Utility		Minimize coolin	g water	requirement	
	SORIES					
31.	FILTER		· · · · · · · · · · · · · · · · · · ·			
	CLEARANCE POCKET	s				
33.						
			·			
<u> </u>					<u> </u>	ها بالم انية بسيرينك ^{بري} م الربية في
DRIVER	2		·····		<u>. </u>	
37,	TYPE		Electric Motor			
38.	POWER CHARACTERI	STICS				
39.						
40,						on of recycle cooler
. 41.	MOTOR CLASS					at the max. discharge
42.	MOTOR TYPE					taimable when the
<u> </u>	POWER FACTOR M. G. SET	·····	the design pres			set at 1000 psig.
44.	<u>rt, 0, 361</u>		*For cases opera			<u></u>
START	ER	*	*For cases opera	iting at	700 psia	
46.	Түре	**	*For cases opera	ating at	900 psia	
47.			<pre>#Project should cooling water i</pre>	confirm	temp. and pr	essure of
<u>48.</u>			cooling water i	III Writin	Ig.	

FORM 8240 (REV. 2/76)

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T. R. Tsao 1/29/82

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EXHIBIT 2.3.1-7A

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LPMeOH PDU; FEED COMPRESSOR, 01.10

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87-7-1533

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	For Lurgi-type Reactor Feed, Mol %	For KT-type Reactor Feed, Mol %	For Balanced Fresh Feed, Mol %	N2 Mo1 %
H ₂	50 🛹 63	38 ~ 51	65 ~ 67	
co.	25 ~ 29	49 ~ 60	30 ~ 33	
C0 ₂	4~10	^い 0 ~ 2	0 ~ 3	
N ₂	0~15	0 ~ 1	0~~1	99.99
CH4	0 ~15	trace	trace	
0 ₂	trace	trace	trace	trace

	Lightest Mol %	Heaviest Mol %	Lightest Mol %	Heaviest Mol %	Lightest Mol %	Heaviest Mol %	
 Но	63	50	51	38	67	67	· _
co	29	25	49	60	33	29	-
C0 ₂	4	10	-	2	-	3	-
N2	4	15	-	-	-	1	99.99
СН4	-	-	-	-	-	-	
0 ₂	_ - -				_		Trace
Total	100	190	100	100	100	100	100 .
M.W.	12.3	16.6	14.7	18.5	10.6	11.1	28

Suction Flow Rate	Min	Nor	Max	Min	Nor	Max	Min	Nor	Max	Nor	Max
lb-mol/hr	18	60	100	18	40	55	18	50	80	20	30
A.C.F.M.	12	40	67	12	27	37	12	34	54	13	20
1b/hr	220	870	1660	265	660	1020	190	540	890	560	840
SCFM @ 1 at 70°F ‡	m. 116	387	644	116	258	354	116	322	516	129	193

#386.68 SCF/1b-mol

A	Air Products
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COMPRESSOR SPECIFICATION SHEET

PAGE <u>1/2</u> DATE <u>29 January 1982</u> REVISED

EXHIBIT 2.3.1-78 REFISE NUSTOMER APCI ENDOR BY Elec. Mech. UNIT LP MedM PDU PROJECT NO. 87-7-1533 ENDOR ATTAC DATA TAN ENDOR ATTAC DATA TAN ENDOR ATTAC DATA TAN ENDOR ATTAC DATA TAN ENDOR ATTACH DATA T	L-2 677	in Producto	COM ACOUNT SPEC			25 0010001 9 1502
NUSTOMER APCI ENDOR BY Elec. WIT LP MoUP PU PROJECT NO. 87-7-1533 MERKAAL INFORMATION 01.20 PAREMAN LINE MED. 01.20 P			EXHIBIT	2.3.1-7B	REVISED _	
FENDOR by Elec. Mech. UNIT LP MedW PDU PROJECT NO. 67-7-1533 1. TERM NO. D.20 Action Compressor Action Compressor Action Compressor 1. TTWE Recurred Compressor Expected 3. TYPE Recurred Synthesis Cas or Nitrogen 3. TYPE Continuous 3. SERVICE Continuous 3. TYPE Recurred Synthesis Cas or Nitrogen 4. DUTY Unconverted Synthesis Cas or Nitrogen 5. SERVICE Control Not Server Compressor 6. FLUID Unconverted Synthesis Cas or Nitrogen 7. COMPOSITION - MOLX (see page 2/2) 8. AVERAGE MOLECULAR WEIGHT (see page 2/2) 8. AVERAGE MOLECULAR WEIGHT 1002 Saturated w/H00 & CHQ0H 10. Suction Tenegratures 'F. 110 Norma, 125 Max. 11. Suction Tenegratures 'F. 110 Norma, 125 Max. 12. Suction Tenegrature 'F. 100 Norm., 105 Max. 0 43 psic 4 13. Discharder Temperature 'F. 90 Nor., 105 Max. 0 10 psigt 14. D. COLING WATER RETURE 'F. 90 Nor., 105 Max. 0 10 psigt 15. Standard Cubic FEET/MINUTE See page 2/2 16. Standard Cubic FEET/MINUTE 100 Norma 17. Cope Compressor 2-1/2" or by vendor 23. Discharder Construct/fink 2-1/2" or by vendor 24.	0.010100					
EXERGAL INFORMATION Recycle Compressor 1. TERM NO. 0.20 2. NO. REQUIRED one (1) 3. TYPE Reciprocating Compressor Expected 4. DUTY Constinuous 5. SERVICE Compress Recycle Gas FLUID Unconverted Synthesis Gas or Nitrogen 7. COMPOSITION - MOLX (see page 2/2) 8. AVERAGE MOLECULAR MERCHAIL (see page 2/2) . 9. CORROSIVE COMPOUNDS HP0, C02, CH30H 0 & CH30H 10. ReLATIVE HUMIDITY 100X Startafe MY00 & CH30H 11. SUCTION PRESENTE - PSIA 485* 665** 12. SUCTION REPERATURE *F. 100 Norm. 125 Max. 13. DISCHARGE TEMPERATURE *F. 100 Norm. 125 Max. 14. DISCHARGE TEMPERATURE *F. 100 Norm. 125 Max. 15. NORMAL SUCTION FLOW RATE		MEK AFLI D. Bu Floo Moch			DOD LEAT NO	97.7.1533
1. TIEM NO. 01,20 2. NO. REQURED one (1) 3. TYPE Reciprocating Compressor Expected 4. DUTY Continuous 5. SERVICE Compress Recycle Gas 7. COMPOSITION Unconverted Synthesis Gas or Nitrogen 7. COMPOSITION Unconverted Synthesis Gas or Nitrogen 7. COMPOSITION - MOLX (see page 2/2) 9. AVERAGE MOLECULAR MEIGHT (see page 2/2) 9. CORROSIVE COMPOUNDS HP0. CD2. CH3CHL & Higher Alcohols 10. RELATIVE HUMPIDITY 100X Saturated MH20 & CH3CHL 11. Suction Pressure - PSIA# 550 750 12. DISCHARGE TEMPERATURE *F. 100 Nor., 105 Max. 805** 13. DISCHARGE TEMPERATURE *F. 120 Nor., 105 Max. 0 10 psig# 14. COLLING WATER RETURN *F. 90 Nor., 105 Max. 0 10 psig# 15. NORMAL SUCTION FLOW RATE			UNTI	LP MEUN PUU	PRUJECI NU.	0/-/-1000
2. No. Recurrence one (1) 3. Type Reciprocating Compressor Expected 4. DUTY Continuous 5. SERVICE Combinious 6. FLUID Unconverted Synthesis Gas or Nitrogen 7. COMPOSITION - MOLX (see page 2/2) 8. AVERAGE MOLECULAR WEIGHT (see page 2/2) 9. CORROSIVE COMPONDS H20, CO2, CH30H, C2H50H & Higher Alcohols 10. RELATIVE HUMIDITY 100% Saturated w/H20 & CH30H 11. SUCTION TENERERTURE *F. 110 Morma, 125 Max. 12. SUCTION TERESTURE - PSIA 485* 655** 13. DISCHARGE PRESSURE - PSIA 485* 655** 14. DISCHARGE PRESSURE - PSIA 485* 550 15. NORMAS SUCTION FLOW RATE (see page 2/2) 16. STANDARG VUBIC ZHWINTE (see page 2/2) 17. COOLING WATER RETURN *F. 120 Nor., 105 Max. @ 43 psig 4 18. COLING WATER RETURN *F. 120 Nor., 105 Max. @ 43 psig 4 19. CP/CV ONSTRUCTION 20. Type of COMPRESSOR 2-1/2" or by vendor 21. DISCHARGE CONNECTIONS 2-1/2" or by vendor 22. SUCTION CONNECTIONS 2-1/2" or by vendor 23. DISCHARGE AREQUIRED Only required for the compressor recycle stream. Desin <td>JENER</td> <td></td> <td></td> <td>c compt casot</td> <td></td> <td></td>	JENER			c compt casot		
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S. SERVICE Compress Recycle Gas GROESS INFORMATION Unconverted Synthesis Gas or Nitrogen 7. COMPOSITION - MOLX (see page 2/2) 9. AVERAGE MOLECULAR WEIGHT (see page 2/2) 9. CORROSIVE COMPOUNDS H20, C02, CH30H, CH50H & Higher Alcohols 10. ReLATIVE HUMPIDITY 100% Saturated WH20 & CH30H 11. Suction Pressure - PSIA 4855 685** 12. Suction Pressure - PSIA* 550 750 13. Discharage Pressure - PSIA* 550 750 14. Discharage Temesrature *F. 100 Norm., 125 Max. 15. NORMAL SUCTION FLOW RATE (see page 2/2) 16. Stanbard Cubic FEET/MINUTE 100 Nor., 105 Max. @ 43 psig ± 17. COOLING WATER SUPPLY *F. 90 Nor., 105 Max. @ 10 psig ± 18. COOLING WATER SUPPLY *F. 90 Nor., 105 Max. @ 10 psig ± 19. CP/CV 20. Type OF COMPRESSOR 21. MATERIAL OF CONSTRUCTION 2-1/2" or by vendor 23. Discharage connections 2-1/2" or by vendor 24. Type DF LUBRICATION 2-1/2" or by vendor 25. COMPRESSOR SPEED 0nly required for the compressor recycle stream, Desi 26. AFTERCOOLER REQUIRED ONLY required for the compressor recycle stream, Desi 27. Type FLUBRICATION 2 28. AFTERCOOLER REQUIRED ONLY required for the compressor recycle stream, Desi 29. OWER REACE FFE By vendor, **Coo	4.					
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LPMeOH PDU; RECYCLE COMPRESSOR, 01.20 page 2 of 2

87-7-1533

EXHIBIT 2.3.1-7B

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‡ 386.68 s											29/

4386.68 SCF/1b-mol



EXHIBIT 2.3.1-8

VENDOR:

HEAT EXCHANGER SPECIFICATION SHEET

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	FORM 8304 (REV. 12/80)			•	PAGE 1 OF 2	
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		A	Cooler Or	OCESS DATA				
L	Service of Unit	Heater R	eboller Vap	orizer				
7.1 Number of Units Required DNA (1)								
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			IN	OUT	IN	OUT		
Ĺ	The Busie Point	°E	<u> </u>)0°F	Saturated	<u>Liquid</u>		
Ľ	Density, V/L	Lbs,/Cu, Ft,						
L	Viscosity, V/L	Ср						
	Molecular Weight, V/L	Lbs./Mole	<u> </u>					
	Specific Heat, V/L	8tu/Lb, ⁰ F						
	Thermal Conductivity, V	/L Blu FL/Hr, Sa.FL	Ę	l				
	Highest Operating Pressus	re, psia	<u> </u> !	00	95			
	Velocity, In/Out	Ft./Soc.		3.1*		5.7*		
ļ	Heat Transfer Cooff Class	n Bru/Hr. Sq. FL F	l lominal	50*	22 60 [:] *	<u>U"</u>		
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ł	Transfer Rate Clean, Btu Transfer Rate Service, Btu	WHr. So. Ft. ⁰ F	includes 40	% Process S	afety Factor)	43*		
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ł		ADD	TIONAL MECH	ANICAL DAT				
1	Additional Connections	Vents: Num		Size & F				
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		Rupture Di	scs: Number	Size & F	Reting			
	Finned or Extended Surf	ace: Type			Area Ratio Ao/A	V		
2	Surface or Bundle Mfr.	-		Model & Descript	len			
	Fin Count FP	i Fin Thio	<u>ik In</u>	Fin Mat	'l, Coatin			
۹.	Bundle Length In	Height	In Depth	In Face A	rea	Ft, ²		
5	Seal Type & Arrangemen	t (Describe)			· · · · · · · · · · · · · · · ·			
1	Tube Sheati					e 1		
2	Stationary	Material	Thickness Thickness	in	Corrosion Allowanc			
	P.oating	Matorial	THEROMS.	10.				
	Baffie Thickness	In.	Method of Faster	ing (Describe)				
	Baffle Spacer Mat'l.	Size	Tie Rod Mat'l.		Size			
	Partie Spart, West to							
	Diametrical Clearances							
	Bundle to Shell	in. Baffle t	o Shelt	In. Tub	e to Baffle Hole	In		
	Demister, Perforated Plate or Condensate Removal Device Type & Description:							
			·					
	Lifting Lugs	<u> </u>	Pali	17				
	Cleaning Requirements		<u> </u>					
	Shipping ()-automents				•			
	Exchanger Drawing Nun Detail Method & Rating		ficient					
	Detail Method of Calcul							
	Remarks	<u> </u>						
			SEE REMARKS	PAGE 3				
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HEAT EXCHANGER SPECIFICATION SHEET ADDITIONAL INFORMATION REQUIRED BY AIR PRODUCTS & CHEMICALS, INC.

FORM 6304-1 (REV. 12/80)

PAGE 2 OF 4

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L. W. Bonnell 3/22/82 T. R. Tsao 3/22/82

L. W. Bonnell 19 March 1982

EXHIBIT 2.3.1-8

21.20 Slurry Heat Exchanger Remarks

87-7-1533

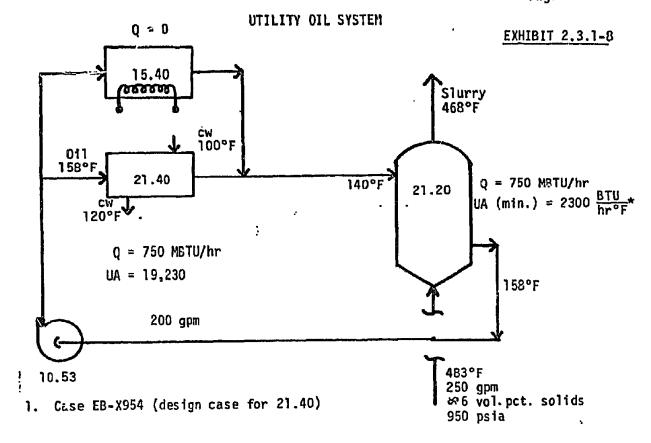
- 1. APCI Design Case: EK-2571 with 150 MBTU/hr. heat leak. 40 percent process duty safety factor has been applied.
- 2. Shell and Tube flowrate design ranges (gpm)

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	Min.	Normal	Max.
Shell (oil)	100	200	210
Tube (slurry)	200	200	260

- 3. Minimum tubeside velocities <u>must</u> be maintained between 5 and 10 ft/sec for above flow range.
- 4. Due to slurry service and erosion concerns, <u>one tube pass</u> strongly recommended, with vertical upflow of slurry in normal operation. Inlet (front) head should be <u>cone-shaped</u>, to eliminate dead spaces where solids can gather.
- 5. Data marked with an asterisk ("*") on pp. 1 & 2 are given for <u>estimate</u> <u>purposes only</u>, and do not constrain the vendor's design.
- 6. See p. 4 for sketch of 21.20 and utility oil system. 21.20 will function as both heater and cooler. Design Eng. and the vendor to ensure that exchanger is designed to handle large shell-to-tube temperature differences.
- 7. Catalyst particle size (typical): 60 microns



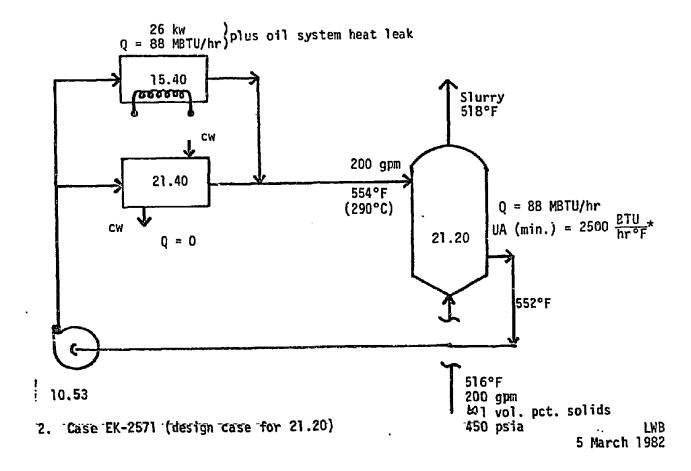


EXHIBIT 2.3.1-9A



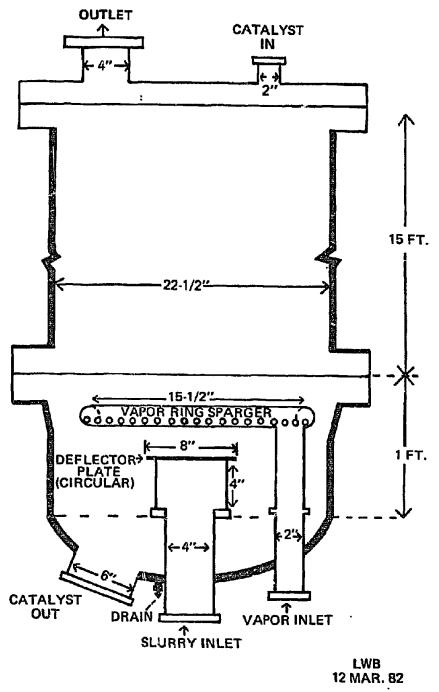


EXHIBIT 2.3.1-98

LaPorte LPMeOH Reactor Operating Parameters

:	<u>Case EB-X954</u> (Max. Production, Liquid-Entrained)	<u>Case FB-4930</u> (Max. Production Liquid Fluidized)
Superficial Vapor Velocity, ft/sec	0.39	0.26
Superficial Liquid Velocity, ft/sec	0.21	0.17
Space Velocity, acfh/ft ^{3*} Space Velocity, scfh/ft ³ Space Velocity, Std. liters/hr-kg cat oxi	93.6 3270 ide 9770	62.4 2300 3975
Catalyst Loading, 1b	909	1387
Catalyst Particle Size, inches Catalyst Particle Size, microns	0.0024 60	0.107 2718

*ft³ refers to reactor free volume.

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LWB 16 April 1982

EXHIBIT 2.3.2-1

Engineering Specification Activity for Process Equipment/LaPorte LPMeOH PDU

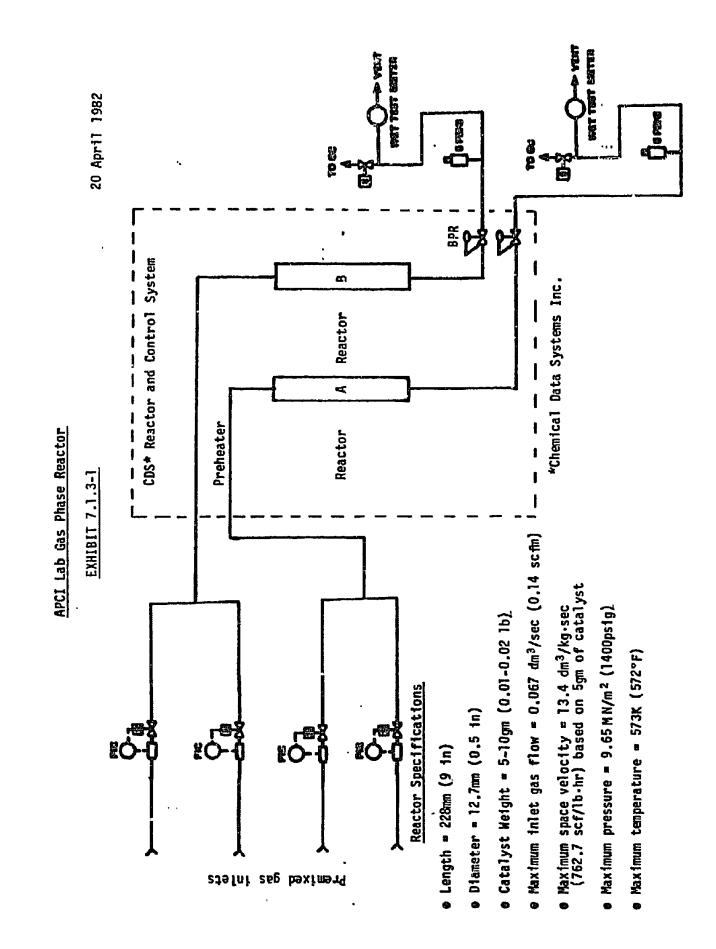
Equipment Item	Process <u>Specification</u>	Mechanical Specification	Quotations <u>Received</u>	Existing Equipment
01.10/01.20 Feed/Recycle	X (Note	1)		
Compressor	X	X	X	
01.13 Feed Surge Tank	X	X		
01.14 Feed Compressor Recycle				
Cooler) X	Х		
01.24 Recycle Compressor Recycle	•			
Cooler	Х	X		
02.50 Sulfur Trim Bed	X	X		
02.51 Sulfur Trim Bed Afterfilts	er X	Х		
02.81 Catalyst Reduction Vessel				
02.83 Reduction Gas Heater	X			X
02.91 A&B Water Pumps	X	Х		•
02.92 Water Feed Tank	X	••		X
10.50 A&B Slurry Circulation Pur	nps X	X	X	v
10.52 A&B Condensed Oil Pumps	X			X
10.53 A&B Hot Oil Pumps	X			X
10.54 Process Oil Make-up Pump	X			X
15.40 Oil Heater	X			X
21.10 Feed/Product Exchanger	X	X		
21.20 Slurry Heat Exchanger	X	X		м
21.30 Product Gas Cooler	X			X
21.40 Dil Cooler	x	X		
21.53 Hop Seal Flush Cooler	x	X		V (Nata 2)
22.10 Three-phase Separator	X X	X		X (Note 2) X
22.11 Methanol Degasser	x			X
22.12 Demister 22.50 A&B Side Stream Filters	â			Ŷ
22.51 A&B Condensed Oil Filters	x			x
27.10 Reactor	(Note 3)			Ŷ
27.13 Primary V/L Separator	X	X		~
27.14 Intermediate V/L Separato		~		Х
28.10 Product Storage Tank	X X	Х		**
28.20 Process Oil Storage Tank	x			Х
28.30 Slurry Preparation Tank	(Note 4)			
28.40 Maintenance Dump Tank	X			
28.53 Oil Expansion Tank	X	X		
Total Items = 33	Total = 30	Total = 16	Total = 2	Total = 15

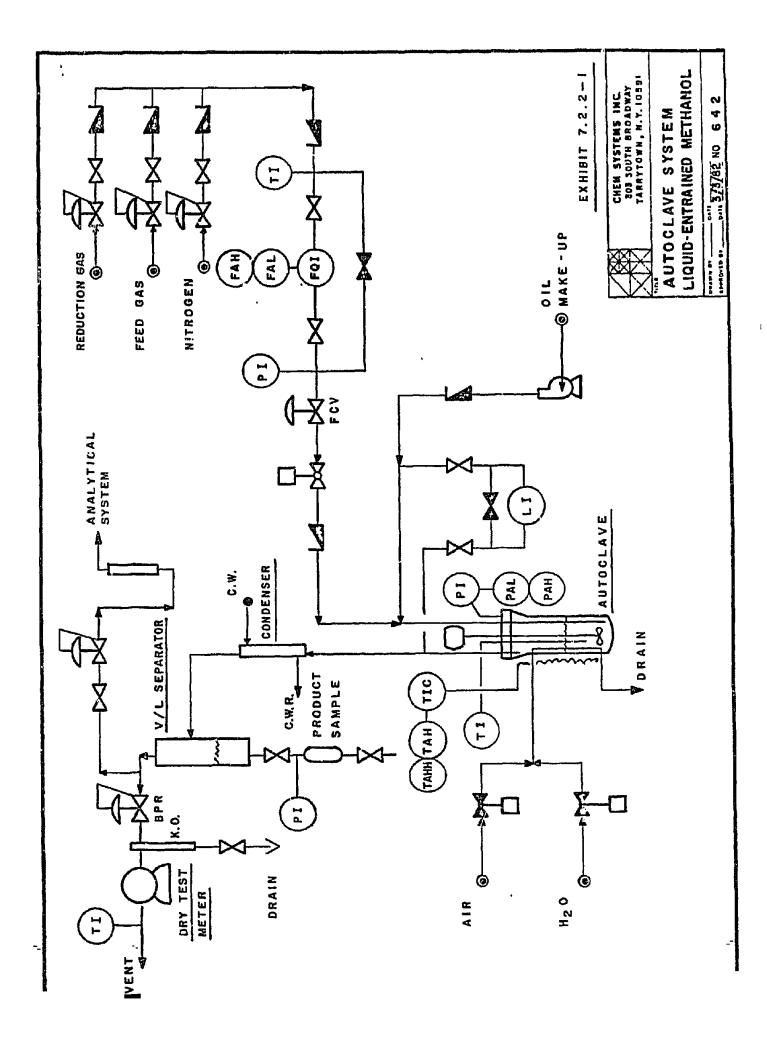
lotal 30

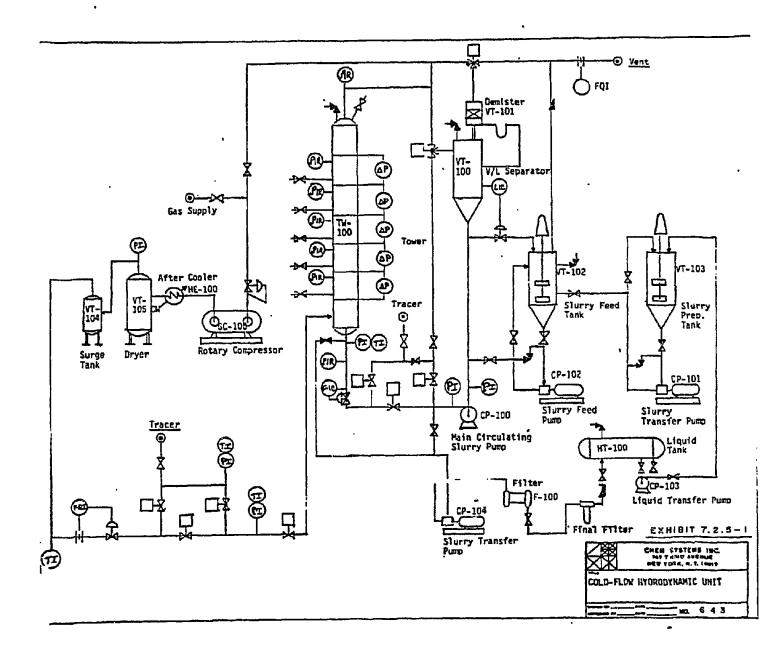
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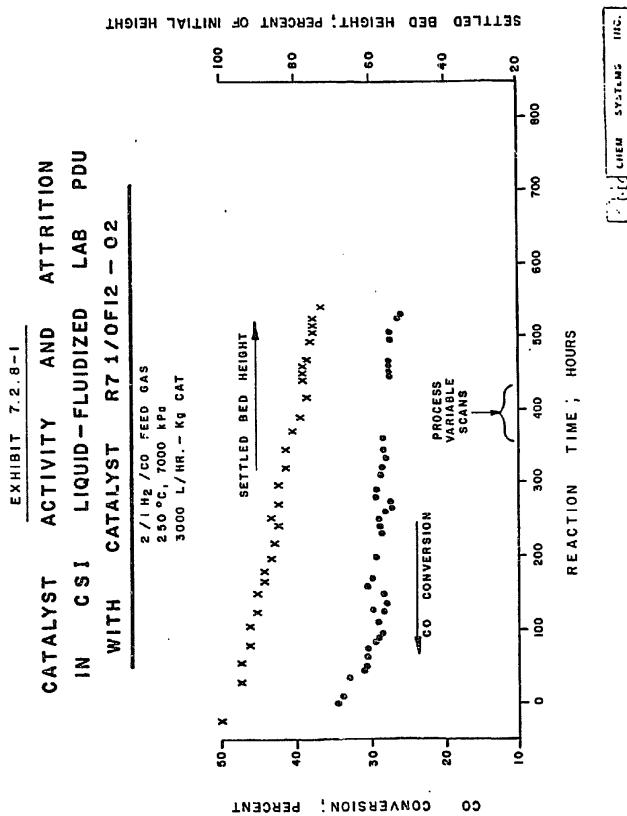
NOTES: (1) Two process specifications issued, counted here as one for multiservice machine.

- (2) Existing vessel D-101 considered marginally acceptable for use on LaPorte LPMeOH PDU. Evaluation of modification costs versus new
- (3) Process specification covering LaPorte LPMeOH reactor based on existing LPM vessel R-101, delayed pending determination of internals.
 (4) Slurry Preparation Tank required for liquid-entrained modifications only. Process specifications scheduled for 25 June 1982.









FRUJECT M. 546 PATE

CHEM SYSTEMS INC.

EXHIBIT 7.2.8-2

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CSI LIQUID-FLUIDIZED PDU RUN CHRONOLOGY

Page 1 of 2

WITH CATALYST R71/0F12-02

<u>Date</u>	Time	Cumulative Reaction Time (Hours)	Milestone
2/16/82	090 0 1600	0 0	4.4 Kg exided catalyst (R71/OF12-D2) loaded into reactor. 2% H2/N2 reduction gas in; catalyst heating to 180°C.
2/17/82		0	Reduction continuing
2/18/82		0	Two Al203-filled guard chambers put on-line.
2/19/82	0300 0430	0 0	First sight of H2 break through; a total of 45.0 gmol H2 has passed over catalyst at this point. Begin heating catalyst @ 10°C per hour to 240°C.
	1100	0	Catalyst at 2400C.
	1200	ŏ	Catalyst cooling to 200°C.
	1300	Ō	Oil circulating on reactor by-pass; heating to 200°C; pressurizing system to 3500 kPa with nitrogen.
	1630	0	Reactor filled w/Witco 40 oil.
	1830	0	Oil flow started through reactor; filters placed in-service.
2/20/82	0500	0	Oil through reactor @ 15 liters/min.
2/ 20/ 02	1000	0	Fluidization tests at various oil flow rates at 7000 kPa and 250°C.
	1630	0	Gas flow started through reactor.
	1745	0	Fluidization tests @ 15 liters/min oil and various gas flows started at 7000 kPa and 250°C.
	2100	0	Gas fluidization tests complete and establishment of run conditions.
2/21/82	0800	11	At steady-state conditions of 3000 VHSV, 7000 kPa, 250°C; draining 2L methanol product each hour; fluidized bed height taken every 4 hrs, and settled bed height taken every 24 hrs.
2/22/82	1800	45	Change filter.
2/23/82	1400	65	Change filter.
2/26/82	0230	125	Change filter.
2/28/82	9230	173	Change filter.
3/2/82	1400	233	Change filter.
3/5/82	0100	292	Cnange filter.
3/8/82	0500	368	Change filter.

CHEM SYSTEMS INC.

EXHIBIT 7.2.8-2 (Continued)

CSI LIQUID-FLUIDIZED PDU RUN CHRONOLOGY

Page 2 of 2

WITH CATALYST R71/OF12-02

Data	-	Cumulative Reaction Time	
Date	<u>Time</u>	<u>(Hours)</u>	Milestone
3/8/82	1315 1330 1400 1900	376 376 377 382	Switch oil pumps due to excessive leaking. Begin process variables scan. 7000 kPa, 250°C, 2000 VHSV, 2/1 H2/CO feed gas. 7000 kPa, 230°C, 2000 VHSV, 2/1 H2/CO feed gas.
3/9/82	0100 0700 1300 1400 1800	388 394 399 400 404	7000 kPa, 270°C, 2000 VHSV, 2/1 H ₂ /CO feed gas. 7000 kPa, 270°C, 4000 VHSV, 2/1 H ₂ /CO feed gas. Change filter. 7000 kPa, 250°C, 4000 VHSV, 2/1 H ₂ /CO feed gas. 7000 kPa, 230°C, 4000 VHSV, 2/1 H ₂ /CO feed gas.
3/10/82	0100 0600 1100 1700 2200	411 416 421 427 432	3500 kPa, 230°C, 4000 VHSV, 2/1 H ₂ /CO feed gas. 3500 kPa, 250°C, 4000 VHSV, 2/1 H ₂ /CO feed gas. 3500 kPa, 270°C, 4000 VHSV, 2/1 H ₂ /CO feed gas. 3500 kPa, 270°C, 2000 VHSV, 2/1 H ₂ /CO feed gas. 3500 kPa, 230°C, 2000 VHSV, 2/1 H ₂ /CO feed gas.
3/11/82	0600 1400 1500 2000	440 448 449 454	3500 kPa, 250°C, 1000 VHSV, 2/1 H ₂ /CO feed gas. Change filter. 3500 kPa, 250°C, 3000 VHSV, 2/1 H ₂ /CO feed gas. Back to original conditions of 7000 kPa, 250°C, 3000 VHSV, 2/1 H ₂ /CO feed gas.
3/ 12/82	1130 1800	469 476	Start low CO2-content 2/1 H2/CD feed gas @ 7000 kPa, 250°C, 3000 VHSV. 7000 kPa, 270°C, 3000 VHSV, low CO2 2/1 H2/CO feed gas.
3/13/82	0200 0800 1200 1800	484 490 494 500	7000 kPa, 270°C, 4000 VHSV, low CO ₂ 2/l H ₂ /CO feed gas. Change filter. 7000 kPa, 250°C, 4000 VHSV, low CO ₂ 2/l H ₂ /CO feed gas. Back to original with 2/l H ₂ /CO feed gas at 7000 kPa, 250°C, 3000 VHSV.
3/14/82	0500	511	Change filter.
3/15/82	1000 1100 1700 1800	540 541 547 548	2/1 H ₂ /CO feed off, K/T gas on-line. Start K/T run; 7000 kPa, 250°C, 3000 VHSV. End K/T run. Shutdown; feed gas switched to N ₂ ; all heats off; circulating through oil cooler on reactor bypass; depressurize system and seal flush over 2 hr period; pump off when oil at 200°F; cooling water left on overnight. overnight.

CHEM SYSTEMS INC.

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EXHIBIT 7.2.8-3

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CSI LIQUID-FLUIDIZED

PDU VARIABLE SCANS: PRELIMINARY RESULTS

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H ₂ /CO Feed			VHSV*	C	onversion	2
Gas	P, kPa	Temp., ^O C	L/Hr·Kg	<u>. CO</u>	<u>н</u> 2-	<u>co</u> 2_
2/1	7000	250	2000	33.1	34.6	3.3
2/1	7000	230	2000	31.1	33.6	6.1
2/1	7000	270	2000	29.8	30.0	1.5
2/1	7000	270	4000	23.8	24.2	4.5
2/1	7000	250	4000	24.1	24.5	5.3
2/1	7000	230	4000	20.3	21.4	6.B
2/1	3500	230	4000	9.4	10.3	1.9
2/1	3500	250	4000	10.2	10.5	1.7
2/1	3500	270	4000	8.7	9.7	2.3
2/1	3500	270	2000	12.8	13.2	2.3
2/1	3500	230	2000	17.3	21.5	5.2
2/1	3500	250	1000	17.4	18.2	0.7
2/1	3500	250	3000	11.9	13.2	3.0

*Based on weight of oxided catalyst (R71/OF12-02) charged at start of run