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LIQUID-PHASE METHANOL PROCESS DEVELOPMENT UNIT:
INSTALLATION, OPERATION, AND SUPPORT STUDIES

Technical Progress Report No. 2

For the Period 1 January 1982 - 31 March 1982

Contractor

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Allentown, PA 18105

and

DOE/PC/30019--T2

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Subcontractor to APCI

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ABSTRACT

This was the second period of Contract performance. During this period approval was obtained for the unified design concept, advanced schedule for relocation of the LPM pilot plant, and advanced procurement of long lead delivery equipment items. The LaPorte LPM₂OH PDU Process Flowsheet developed further and the Engineering Flowsheet evolved to the Revision OA preliminary issue. Eight cases of point-by-point heat and mass balances were released. Process equipment specifications were issued for 30 of the 33 equipment items. Mechanical specifications were issued for 16 equipment items. Quotations were received for the 2 long lead delivery items, the Feed/Recycle Compressor and the Slurry Circulation Pumps; technical evaluations of these bids are underway. Semi-final equipment arrangement and plot plan drawings were prepared. The Preliminary Hazards Review was conducted and the subsequent Design Hazards Review was initiated. A request for exemption from construction and operating permit requirements was submitted to the Texas Air Control Board. Progress was made on the specification of the Data Acquisition System. In the laboratories, APCI established the priority for compositions of new methanol powder catalysts to be prepared. Construction of the APCI Gas Phase Screening Reactor and Stirred Autoclave Reactor continued on schedule. Progress was made in evaluating the potential modification of the Deckwer liquid phase Fisher-Tropsch model to describe LPM₂OH performance. In the CSI laboratories, a 550-hour liquid-fluidized run was completed successfully in the Lab PDU. Preliminary results indicate that the new catalyst tested is more attrition resistant than any prior liquid-fluidized catalyst candidate. Testing of in-situ catalyst reduction procedures continued in the Stirred Autoclave Reactor with successful results which led CSI to file a Record of Invention form for a potential invention covering this process. Specifications and quotations for major equipment items in the CSI liquid-entrained PDU were completed and received. The first of the two lab slurry pumps arrived. A preliminary plan for cold flow hydrodynamic modeling was completed. DOE approved submission of the Task 2 deliverable report on 1 June 1982 in order to increase the accuracy of the program cost estimate. The 1 June deliverable report will incorporate and take advantage of the research achievements and efforts currently underway at APCI and CSI.



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PROJECT DESCRIPTION:

On 28 September 1981, Air Products and Chemicals, Inc. (APCI) began a 42-month contract with the U.S. Department of Energy (DOE): "Liquid Phase Methanol (LPMeOH) Process Development Unit: Installation, Operation and Support Studies." This project is aimed to further develop the LPMeOH process invented by Chem Systems Inc. (CSI). Chem Systems is performing as a subcontractor to Air Products.

A DOE-owned, skid mounted pilot plant will be transferred from Chicago, refurbished, expanded for service as the LPMeOH Process Development Unit (PDU), and then relocated and commissioned at Air Products' LaPorte, Texas facility. Air Products will supply synthesis feed gas to the LPMeOH PDU and operate the unit for a planned 24-month period. Chem Systems is performing the major portion of the laboratory support R&D and is providing technical management for the project. Air Products is providing overall program management and is responsible for engineering design, construction, and operation.

The program is divided into 11 major tasks which are phased to allow progress review and approval to proceed. The 11 major tasks are:

1. Program Planning
2. Engineering and Design Specifications
3. Equipment Procurement
4. LPM Pilot Plant Relocation/Inspection
5. LaPorte LPMeOH PDU Renovation, Installation and Shakedown
6. Liquid-Fluidized Operation
7. Laboratory Support Program
8. Conversion of the LaPorte LPMeOH PDU from Liquid-Fluidized to Liquid-Entrained Mode
9. Shakedown of the Liquid-Entrained Mode of Operation
10. Liquid-Entrained Operation
11. Project Evaluation

The tasks are phased as follows:

<u>Phase</u>	<u>Tasks</u>	<u>Schedule</u>	
I	1,2,4,7,11	28 September 1981 -	28 March 1985 (Months 1-42)
II	3,4,5	1 June 1982 -	1 April 1983 (Months 9-18)
III	6	1 March 1983 -	1 June 1984 (Months 18-32)
IV	8	1 January 1984 -	1 April 1984 (Months 28-30)
V	9,10	1 April 1984 -	1 March 1985 (Months 31-41)



OBJECTIVES:

The overall objective of this program is to demonstrate the technical feasibility of the Liquid Phase Methanol (LPM_{OH}) process at the Process Development Unit (PDU) scale of operation.

On a per task basis, objectives are to:

Task 1 - Program Planning

Establish a Project Work Plan presenting in detail all activities which will be performed for the successful completion of the program.

Task 2 - Engineering and Design Specifications

- a) Conduct a process engineering/design review and safety examination of the existing Liquid Phase Methanation (LPM) pilot plant at its present location in Chicago, Illinois;
- b) Obtain permits to install and operate the LPM_{OH} PDU at LaPorte, Texas;
- c) Develop detailed plans and specifications for the repair, modification, and expansion of the existing LPM unit to enable liquid-fluidized (ebullated bed) and, subsequently, liquid-entrained (slurry) methanol production; and
- d) Develop a deactivation plan for the LaPorte LPM_{OH} PDU.

Task 3 - Equipment Procurement

Purchase, lease, or obtain from DOE inventories the equipment and systems specified in Task 2.

Task 4 - LPM Pilot Plant Relocation/Inspection

Transfer the existing LPM pilot plant from its present location in Chicago to a vendor's facility for inspection.

Task 5 - LaPorte LPM_{OH} PDU Renovation, Installation, and Shakedown

- a) Renovate the LPM pilot plant to become the LaPorte LPM_{OH} PDU, according to the specifications developed in Task 2;
- b) Prepare the LaPorte site;
- c) Transfer and install the LPM_{OH} PDU at LaPorte;
- d) Make interconnections and test components; and
- e) Conduct an integrated run without catalyst.



Task 6 - Liquid-Fluidized Operation

Operate in the liquid-fluidized (ebullated bed) mode to:

- a) Assess the effect of reactor configuration/internals;
- b) Identify catalysts which in short runs have acceptable activity and attrition characteristics;
- c) Perform process variable scans to determine the effects of temperature, pressure, space velocity, catalyst loading, circulating oil flowrate, and feed gas composition; and
- d) Perform a 45-day continuous run to demonstrate short-term process operability, principally at a single set of conditions.

Task 7 - Laboratory Support Program

- a) Conduct literature surveys, develop a bibliography of pertinent references, and maintain liaison with others working on related liquid-entrained (slurry) systems.
- b) Develop procedures for in-situ reduction of commercial powdered methanol catalysts slurried in oil, vapor phase reduction of commercial granular materials which can subsequently be slurried, and simultaneously screen commercial catalysts and develop data for modeling the liquid-entrained reaction;
- c) Synthesize new liquid-entrained catalysts;
- d) Screen new liquid-entrained catalysts in a gas phase fixed bed reactor, in a liquid-entrained stirred autoclave reactor, and in the Chem Systems' Fairfield laboratory PDU;
- e) Construct and operate a cold flow model unit to study the hydrodynamics of the gas-slurry reactor;
- f) Modify the existing Chem Systems' Fairfield laboratory PDU to allow liquid-entrained as well as liquid-fluidized operation;
- g) Operate the modified CSI lab PDU to perform process variable scans; and
- h) Support the LaPorte LPMeOH PDU liquid-fluidized and liquid-entrained operating modes, principally by screening catalysts.

Task 8 - Conversion of the LaPorte LPMeOH PDU from Liquid-Fluidized to Liquid-Entrained Mode

Perform necessary process adjustments, alterations, and minor operational tests to facilitate the conversion of the PDU from the liquid-fluidized (ebullated bed) to the liquid-entrained (slurry) mode.



Task 9 - Shakedown of the Liquid-Entrained Operation

Test components, conduct an integrated run with an inert powder, and conduct an integrated short run with a liquid-entrained methanol catalyst.

Task 10 - Liquid-Entrained Operation

- a) Conduct short runs with promising liquid-entrained catalysts;
- b) Perform process variable scans to determine the effects of various operating conditions; and
- c) Perform a 45-day continuous run to demonstrate short-term process operability.

Task 11 - Project Evaluation

- a) Evaluate data from the LaPorte LPMeOH PDU and the laboratories to develop models;
- b) Evaluate alternative reactor designs and the two liquid phase operating modes;
- c) Perform detailed process evaluations for commercial-size plants;
- d) Develop plans for a larger scale demonstration of the LPMeOH process; and
- e) Report on program activities.



RESULTS:

Task 1 - Program Planning

This task is complete. No activity.

Task 2 - Engineering and Design Specifications

2.1* APCI Management Activities

2.1.1 Project Management -

Specifications for dismantling the LPM pilot plant for relocation from Chicago were completed and released. Bids were received and a technical evaluation completed for this contract, and purchase approval has been requested of the DOE.

Specifications for shop inspection of the LPM pilot plant equipment in the Houston area have been completed and technically approved by the DOE. Receipt of bids is scheduled for 21 April 1982.

LaPorte commercial facility flowsheets were marked-up to illustrate the eleven piping tie-ins required for feed gases and utilities to the LPMeOH PDU. Instructions for further detailing of these tie-ins to the LPMeOH PDU battery limit were transmitted in coordination of Design Engineering activity.

DOE excess capital equipment and excess property lists for the Synthoil plant were reviewed to identify potential items for use in the Liquid Phase Methanol Program. A more detailed review and physical inspection of this equipment will be conducted on 21 April 1982.

A review of the Preliminary Hazards Review Report was conducted and a final draft is being developed. A Design Hazards Review Team was organized and assembled to conduct a detailed analysis of the plot plan, flowsheet, shutdown logic, solids handling systems, catalyst reduction and product storage.

Based on current schedules for receipt of vendor quotations for new equipment items and for inspection of the LPM equipment, a request was made to the DOE to revise the submittal date of the Phase I deliverable report that will include a revised estimate of the overall program. A revision from 1 May 1982 to 1 June 1982 was approved by the DOE, to enhance the usefulness of the estimate data.

2.1.2 Economic Evaluation - Work was started on revising an internal Project Scope Report that will consolidate the necessary data for detailed estimating by each performing group within APCI.

* Refers to Work Breakdown Structure Elements.



- 2.1.3 Communications - No Significant Activity.
- 2.1.4 Permit Fees - No Activity.
- 2.2 CSI
- 2.2.1 CSI Assistance to APCI - Chem Systems provided APCI with review and comment on preliminary flowsheets for the LaPorte LPMeOH PDU. A marked-up flowsheet showing suggested process corrections, control points and data acquisition points was transmitted to APCI. This mark-up was reviewed in a meeting at APCI on 19-20 January 1982. Plans for dismantling the LPM pilot plant were also reviewed at this meeting including procedures, equipment lists, and skid and piping break points. Chem Systems also participated in the Process Hazards Review held at APCI on 15 March 1982.
- 2.2.2 Data Acquisition System Specification - The LaPorte LPMeOH PDU flowsheets were reviewed to determine and verify the required data acquisition and sampling points on the unit. Calculations to reduce these data points into an operational format were outlined in order to estimate the size of the data acquisition computer. Preliminary quotations and leasing arrangements, as well as catalog information, were received from several vendors on items required in the analytical (i.e., gas chromatographs, analytical balances, interfaces, etc.) as well as the computational (computers, data loggers, printers, etc.) sections of the data acquisition unit. On the basis of this information a preliminary estimate was prepared and the buy/lease option evaluated for the data logger/microcomputer option of the data acquisition system. These results were reviewed with APCI in Allentown on 25 March 1982, where the associated costs and leasing arrangements of the minicomputer option were presented. As a result it was agreed, in principle, to specify the minicomputer system as the leading option for use in data acquisition, provided CSI can maintain complete control and responsibility for the data acquisition task at LaPorte. Final selection of this option is dependent upon confirmation of system and project criteria discussed in the 25 March meeting. In addition, the preliminary configuration and cost estimate for the analytical portion of the data acquisition system was developed. A list of acceptable vendors has been established and final specification sheets are currently being developed as a prelude to formal equipment bid solicitation.
- 2.3 APCI Design
- 2.3.1 Integration -



Process Flowsheet

The Process Flowsheet, Revision P1, dated 5 January 1982 was attached and described in Technical Progress Report No. 1. Since that time the following change considerations have developed:

1. Elimination of Pressure Leaf Filter (22.55)

A more detailed review of the LaPorte LPMeOH PDU shutdown and the Pressure Leaf Filter operating conditions revealed the following:

- The solids loading is too high for a pressure leaf filter.
- Upon shutdown, the PDU must be quickly evacuated of the catalyst/oil slurry, otherwise settled catalyst sludge will build up and cause numerous blockages. Catalyst settling in lab slurry samples implies there may be 15 minutes in which to begin evacuation, and 30 to 60 minutes available to complete the transfer. (Calculations are required to better determine these times.)
- The oil must be cooled below 180°F (80°C) for conventional pressure leaf filtration. Standard filters use rubber gasket materials and filter aid materials contain some entrapped moisture which could cause foaming when mixed with hot oil.

It is now recommended that the slurries be pressure transferred to the Slurry Preparation Tank (28.30) for temporary holding prior to gravity transfer to Tote Bins for final disposal. The Tote Bins may be used to decant the slurries to yield a reuseable oil supernatant. Controlled oxidation of catalysts may be performed in the Tote Bins to permit safer handling and direct disposal to a secure landfill. The need and the methods for catalyst oxidation are under review. (A plan to evaluate the pyrophoric nature of spent catalyst/oil slurry is noted in Task 11.4.)

2. Alternative Water Addition Location

In the Revision P1 Process Flowsheet, water addition is shown upstream of the Three Phase Separator (23.10). An alternative route has been added to allow water addition to the top of a small packed section in the vapor outlet of the Three Phase Separator. This capability allows some scrubbing of methanol from the purge/recycle gas. Low methanol content in the recycle gas is desirable in order to accurately measure net methanol production in the reactor.



3. Catalyst Reduction Vessel (02.81) - (On Hold)

Chem Systems continues to make significant progress in the stirred autoclave tests to optimize in-situ catalyst reduction/activation conditions (see Task 7.2.2). Evidence is mounting that the separate Catalyst Reduction Vessel is not required. Data is still needed on other catalysts to confirm more general abilities to achieve in-situ reduction.

4. Potential Elimination of Spare Slurry Circulation Pump (10.50 B)

The flowsheet for the LaPorte LPMeOH PDU has indicated two Slurry Circulation Pumps (10.50 A & B) since the initial proposal to the DOE for the LPMeOH Program. The proposal considered these pumps to each be 100% design capacity such that an installed spare would be available on stand-by during LaPorte PDU operation. This dual pump installation was justified originally by considering that the costs associated with a single pump failure leading to the loss of even one LaPorte PDU run would more than outweigh the cost for an additional pump.

Progressive development of the LaPorte LPMeOH PDU design has revealed that three key points of this original justification are questionable:

- Recent developmental experience with hot, high suction pressure, centrifugal, slurry pumps has led to the commercial availability of equipment that may be considered to have acceptable reliability for the LaPorte LPMeOH PDU operating program.
- Failure of the Slurry Circulation Pump will not necessarily lead to loss of a PDU run since the Slurry Preparation Tank (28.30) will now be used to maintain the slurry in suspension and at temperature.
- Due to difficult technical problems associated with the installation of a stand-by pump in this service, the incremental costs for a dual pump installation over a single pump installation may be several times greater than originally estimated.

In the final analysis it is considered desirable to maintain the slurry circulation loop in the simplest, most direct flowing arrangement, from both operational reliability and safety standpoints. Therefore, a detailed evaluation is in progress to evaluate the suitability of a single Slurry Circulation Pump installation for the LaPorte LPMeOH PDU.



A Simplified Process Flowsheet for the LaPorte LPMeOH PDU is given in Exhibit 2.3.1-1. This simplified version complements the Revision P1 issue of the Process Flowsheet by providing a clear, smaller-size schematic of the main process lines and equipment. Heat and mass balance points are also given on this flowsheet.

Engineering Flowsheet

A Revision 0 Engineering Flowsheet for the LaPorte LPMeOH PDU was issued on 10 March 1982. This was subsequently marked up during the Design Hazards Review to produce a Revision 0A edition. A preliminary Revision 0A Engineering Flowsheet is attached as Exhibit 2.3.1-2. This preliminary flowsheet has just issued for internal APCI review and has not yet been approved and signed-off. The preliminary flowsheet does show the current state of development of the P&ID. The next level of development of the Engineering Flowsheet is the Revision 1 issue, which will be submitted in the June 1982 Phase I deliverable report to the DOE.

Heat and Mass Balances

The final design heat and mass balances for the eight (8) design cases, four (4) for the liquid-fluidized mode and four (4) for the liquid-entrained mode, were completed and released in January 1982. The operating conditions for the eight (8) design cases which include the maximum and minimum methanol production cases for both modes of operation as well as four (4) "normal" operating cases are given in Exhibits 2.3.1-3 and 2.3.1-4. The detailed point by point heat and mass balances for the design cases were developed using APCI's process simulator program and are enclosed as Exhibit 2.3.1-5. The key stream numbers for the heat and mass balance are shown in Exhibit 2.3.1-1, the Simplified Process Flowsheet for the LaPorte LPMeOH PDU.

Process Equipment Design

During this quarter, process equipment specifications were prepared and issued for 32 equipment items in the LaPorte LPMeOH PDU. One of these items (Pressure Leaf Filter 22.55) was subsequently voided, and two items are considered as one (01.10/01.20 Feed/Recycle Compressor is a multiservice machine) by Project Engineering. Therefore, 30 of 33 valid process equipment specifications are complete at this time. Of these 30 process specifications, 5 exist as revised specifications resulting from engineering feedback. The three remaining equipment items are the Reactor (27.10), the Slurry Preparation Tank (28.30), and



the Catalyst Reduction Vessel (02.81). The Reactor is the existing reactor vessel (R-101) in the LPM pilot plant; the process specification is being delayed pending further analysis of the need for internals in the liquid-fluidized (ebullated bed) and liquid-entrained (slurry) modes. The Slurry Preparation Tank specification is scheduled for issue by 25 June 1982. As noted above, the Catalyst Reduction Vessel is on-hold pending additional experimental confirmation that this vessel is not required.

Some process design characteristics of key equipment items in the LaPorte LPM₂OH PDU are provided in this report as follows:

1. Slurry Circulation Pumps (10.50 A & B)

The process equipment specification is attached as Exhibit 2.3.1-6.

2. Feed/Recycle Compressor (01.10/01.20)

The process equipment specification is attached as Exhibits 2.3.1-7A and 2.3.1-7B.

3. Slurry Heat Exchanger (21.20)

The process equipment specification is attached as Exhibit 2.3.1-8.

4. Reactor (27.10)

A schematic of the reactor and some key operating parameters are given in Exhibits 2.3.1-9A and 2.3.1-9B.

Hazards Review

The Preliminary Hazards Review was completed. The subsequent Design Hazards Review progressed to analyze specific hazards and to document conclusions and recommendations relevant to each item. The "What If?" method of analysis was used to review the Engineering Flowsheet, Revision 0, dated 10 March 1982. As a result of this review the following hazards were recommended for quantification by Fault Tree analysis:

<u>Description of Hazard</u>	<u>Preliminary Recommendation</u>
1. Potentially pyrophoric, hot, oil/catalyst slurry,	1a. Use administrative procedures to assure



exposed to air.

tight shutoff prior to maintenance on stand-by equipment in the slurry mode.

- 1b. Monitor erosion rates in equipment and piping.
- 1c. Use administrative controls to prevent overfill of Tote Bins for spent slurry disposal.
- 2. Run-away reaction.
 - 2a. Provide alarms for low nitrogen flow or high H₂ concentration, specifically for reduction gas supply in liquid-fluidized catalyst preparation.
 - 2b. Utilize administrative control to eliminate severe consequences of temperature rise upon loss of slurry circulation during in-situ reduction.
 - 2c. Develop understanding of catalyst activity and potential for oil cracking on temperature excursions.
- 3. Major release from Methanol Tank.
 - 3a. Provide adequate pressure relieving devices.
 - 3b. Provide high liquid level alarm.

Fault trees on the above items will be completed and quantified upon release of the Revision OA Engineering Flowsheet and the preliminary shutdown logic diagrams resulting from the "What If?" review.

Environmental Permit Action

A request for exemption from construction and operating permit requirements was submitted to the Texas Air Control



Board (TACB) on 17 March 1982. It is believed that the PDU facility will not make a significant contribution of air contaminants to the atmosphere. The request to TACB included a report on the emission sources and quantities. The emission sources are the flare stack, storage tank vents, pressure leaf filter purge, and fugative hydrocarbons. The continuous process vents of hydrocarbons and CO along with emergency or relief valve vents will be sent to a single smokeless flare designed for complete combustion. Working losses from the storage tanks along with controlled fugative hydrocarbon emissions are estimated to total about 14 T/Y.

The water discharge (treated rainwater runoff from the process area) will be directed to the existing fire pond at APCI's commercial facilities at LaPorte. This water discharge increment is being included in renewal applications for APCI's overall water discharge permit at LaPorte.

Permits will not be required by APCI for handling of hazardous wastes on site. However, cradle-to-grave accounting will be required on all used catalyst/oil preparations requiring disposal.

Methanol product will be disposed of as a fuel and therefore is exempt from EPA regulation.

- 2.3.2 Equipment - Exhibit 2.3.2-1 summarizes engineering specification activity for the process equipment items in the LaPorte LPMeOH PDU. Process specifications have been issued for 30 of the 33 equipment items. Mechanical specifications have been issued for 16 items, including 15 of the new equipment items (18 total new items). Quotations have been received on the 2 long lead delivery items (01.10/01.20 Feed/Recycle Compressor and 10.50 A & B Slurry Circulation Pumps) and technical evaluations are underway. Requests for purchase approval for these latter items are expected to be submitted to the DOE by 30 April 1982.
- 2.3.3 Site/Structural - A site visit was made to LaPorte to verify conditions for tie-in pipe racks, roads and underground road crossing designs.
- 2.3.4 Piping -

A site visit was made to LaPorte to verify existing piping systems for tie-in. Upon return, design drawings were prepared detailing the required tie-in construction. These drawings will be utilized for the preparation of take-off estimates to be incorporated into the 1 June 1982 deliverable report.



Semi-final equipment arrangement and plot plan drawings were prepared based on information from the Design Hazards Review. These drawings and the Revision OA Engineering Flowsheet will form a basis for the LaPorte LPM₂OH PDU renovation and installation estimates to be incorporated into the 1 June 1982 deliverable report.

2.3.5 Electrical -

Specifications have been prepared for switchgear additions to the LaPorte commercial facility that would provide a source of 600 kVA service for the LPM₂OH PDU.

Two alternate specifications have been prepared for motor control for the LPM₂OH PDU to allow evaluation between matching and line up with the existing LPM pilot plant motor control, and total new purchase of motor control equipment.

2.3.6 Instrumentation - Support was provided in the development of control loop requirements on the Revision 0 and Revision OA Engineering Flowsheets.

Task 3 - Equipment Procurement

No Activity.

Task 4 - LPM Pilot Plant Relocation/Inspection

4.1 APCI Management Activities

4.1.1 Warehousing - No Activity.

4.1.2 Traffic Services - No Activity.

4.2 CSI Management Activities

4.2.1 On 11 February 1982, a meeting was held at IGT in Chicago, Illinois to inspect the LPM pilot plant with regard to its relocation to a fabricator shop in Texas. A Chem Systems representative was on hand for discussions with IGT personnel and to answer questions pertaining to the pilot plant. Chem Systems also reviewed the APCI specifications for dismantling the pilot plant.

4.3 Field Engineering - A site inspection was conducted by an APCI field instrument technician on the LPM pilot plant instrumentation. Several loops were energized, and pneumatic valves stroked to establish a list of reuseable instrument items for incorporation into the detailed ship inspection plans.

4.4 LPM Pilot Plant Relocation



- 4.4.1 Disassembly - A technical evaluation of bids was conducted and purchase approval has been sought from the DOE for award of this contract. Site activity in Chicago is expected during May 1982.
- 4.4.2 Inspection - No Activity.
- 4.4.3 Rehabilitation - No Activity.

Task 5 - LaPorte LPMeOH PDU Renovation, Installation, and Shakedown

No Activity.

Task 6 - Liquid-Fluidized Operation

No Activity.

Task 7 - Laboratory Support Program

- 7.1 APCI R&D
- 7.1.3 Catalyst Screening and Testing -

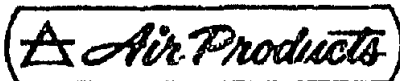
APCI Stirred Autoclave (Bench Scale Slurry) Reactor Set-Up

Major items ordered for construction of the 1000 mL Stirred Autoclave Reactor were delivered. Items which were ordered and not delivered as of this writing include:

1. Fittings and valves from Autoclave Engineers, Inc. (1 lot).
2. Pressure transducers and demodulators (3 ea.).
3. Multipoint chart recorder (1 ea.).
4. Pressure regulator (1 ea.).
5. Gas inlet flow integrators.
6. Miscellaneous solenoid valves and fittings.

The construction of the main control panel began, with cut-out holes for missing instrumentation items made from dimensions supplied by the manufacturers. The 1000 mL Stirred Autoclave Reactor was moved into the operations cell and plumbing operations will begin during April 1982. The reactor construction is proceeding on schedule; back-ordered items should not affect the schedule if promised shipping dates are met.

The operation cell area, which was newly constructed, was completed and was checked-out for proper ventilation with smoke bombs. The area is monitored with recently installed carbon monoxide alarms. The principal lab area is monitored at 4 points. The gas supply lines are located external to the lab and are monitored at 3 points for carbon monoxide. With the final check on the cell operation area ventilation and the installation of the CO monitor, the lab area is now operational.



High-pressure piping of inlet CO and H₂ gases from the external gas supply area was completed and leak-checked. The high pressure piping for inert and CO₂ gas supplies was completed; however, the gas cylinder manifold has not been installed. Work on this manifold is scheduled at a later date.

APCI Gas Phase Screening Reactor

Final specifications for this unit were given to Chemical Data Systems, Inc. and construction of this unit began at CDS's facility. Monitoring of progress continued and shipment of the completed unit is expected by 30 April 1982. Exhibit 7.1.3-1 shows a simplified schematic of the unit along with critical measurements and capacities.

7.1.4 Catalyst Preparation -

The methanol catalyst literature search to cover the program needs was initiated and is nearly complete. Discussions with APCI's Corporate Development Department and other Process Systems Group personnel have indicated that one-pound quantities of catalyst in the 45-75 micron range will be provided for testing. The first five catalysts for the program will be prepared for delivery before 30 May 1982. The catalysts will be characterized as to pore size, surface area, analytical composition, and bulk density, although only the composition and particle size distribution will be controlled in the initial preparations.

The preparation priority, from high to low, with respect to composition type is:

1. Supported CuO/ZnO, CuO/MgO, CuO/ZnO/Ceria.
2. CuO/Ceria (Ce⁺³ and Ce⁺⁴), CuO/Ceria/Alumina.
3. CuO/MoO₃ or CuO/WO₃ types.
4. Raney alloys of Cu plus Zn and aluminum and copper plus cerium and aluminum.

Copper-thorium alloys have been dropped from consideration at present. This is due to the practical problems associated with handling radioactive materials. Copper-cerium and/or copper-lanthanum alloys may be recommended as substitutes after further analysis.

Mixed heterogeneous-homogeneous catalyst systems have been ruled out due to potential metal carbonyl volatility problems.



7.2 CSI R&D

7.2.1 Literature Review -

Cold Flow Hydrodynamics of Three-Phase Systems

The following paragraphs discuss some of the literature reviewed prior to scoping a system for cold flow modeling of the LPMeOH process.

The performance of a chemical reactor with respect to conversion and selectivity depends on the intrinsic kinetics of the various chemical reactions, various physical rate processes such as interphase transfer, and inter and intra particle heat and mass transfer. The effects of these physical rate processes on the reaction performance have been shown to depend on the dynamics of the various phases involved. While there are numerous publications about backmixing in liquid-gas bubblic columns and in solid-fluid systems (References 1-5), much less material has been published on three-phase ebullated bed/liquid entrained systems (References 6-8).

Experimental data on Peclet numbers due to axial dispersion in chemical reactors are also very limited. Most of the work has been limited to single phase packed bed reactors. Moreover, data on such systems are only reliable when applied to systems resembling those of the experimental studies (Reference 9).

At the present time, an extensive effort is being directed toward the measurement and evaluation of backmixing in multiphase systems through residence time distribution (RTD) studies (References 10-11). One major problem encountered is that separate RTD measurements are required to evaluate the mixing characteristics of each phase. Although there are numerous methods available to obtain RTDs in complex multiphase systems, measurement problems have been encountered by all recent investigators. Flow maldistribution of the phases can especially impede evaluation of RTD data.

7.2.2 CSI Stirred Autoclave Tests -

The program for optimizing in-situ catalyst reduction techniques for catalyst powders suspended in inert hydrocarbon liquids continued during this quarterly period. To date, seven runs have been completed including five in-situ reduction conditions, one replicate run and a base case, vapor-phase reduction condition.

1. Description of Stirred Autoclave Reaction System

A process schematic of the CSI lab Stirred Autoclave System is shown in Exhibit 7.2.2-1. The heart of the system is a two-liter autoclave equipped with a top entering



magnedrive agitator assembly and water cooled by an automatic temperature controller. The autoclave is a Model AFP-2005 from Autoclave Engineers. The agitator has a 3/8-inch diameter hollow shaft with two 3/16-inch diameter draft tube inlet holes located ten inches above the 1-1/4-inch diameter impeller. The system is set up in such a way that feed gas, reduction gas and make-up oil can be introduced under controlled pressure and flow conditions. The reactor effluent passes through a shell and tube heat exchanger before it enters the vapor-liquid separator. Auxiliary equipment on the V/L separator allow for sampling of vapor and liquid streams and measurements of flows, temperature and pressure.

2. Catalyst Reduction Test Procedures

This section contains potentially patentable material and has therefore been issued in the Supplement to the Technical Progress Report, marked "Not For Publication".

3. Run Procedures and Preliminary Results

This section contains potentially patentable material and has therefore been issued in the Supplement to the Technical Progress Report, marked "Not For Publication".

4. Calculation Methods

The feed gas contained approximately 15 mole percent of argon as an internal standard for calculation purposes. The calculated data include vapor hourly space velocity (VHSV), hydrogen and carbon oxides conversions, selectivity and methanol productivity.

The VHSV is calculated as follows:

$$VHSV = \frac{V_e}{W_C} \times \frac{Ar_e}{Ar_f} \times \frac{273.15}{273.15 + T_e} \times \frac{P_e}{101.35} \quad (\text{Eq. 1})$$

- Where:
- VHSV = Space Velocity in l·hr⁻¹·kg⁻¹
 - V_e = Volume flow of effluent, l/hr (at STP)
 - Ar_e = Mole percent argon in effluent
 - Ar_f = Mole percent argon in feed
 - W_C = Oxided catalyst charge, kg
 - T_e = Effluent Temperature, °C
 - P_e = Effluent Pressure, kPa



The percentage conversions of feed gas components (H₂, CO and CO₂) are calculated as follows:

$$C_i = \frac{I_f - \left(I_e \times \frac{Ar_f}{Ar_e} \right)}{I_f} \times 100 \quad (\text{Eq. 2})$$

Where C_i = Percent conversion of component I
 I_f = Mole percent of I in feed gas
 I_e = Mole percent of I in effluent gas
 I = H₂, CO or CO₂

If the feed gas has a low CO₂ concentration (less than three percent), then net CO₂ will be produced, and the percent selectivity to CO₂ (S_{CO₂}) can be calculated as follows:

$$S_{CO_2} = \frac{\left(D_e \times \frac{Ar_f}{Ar_e} \right) - D_f}{M_f - \left(M_e \times \frac{Ar_f}{Ar_e} \right)} \times 100 \quad (\text{Eq. 3})$$

Where D = Mole percent of carbon dioxide
 M = Mole percent of carbon monoxide
 Ar = Mole percent of argon
 Subscript e refers to reactor effluent
 Subscript f refers to reactor feed

The methanol productivity is calculated as follows:

$$M_p = \frac{VHSV}{22.4 \times 100} \times (M_f \times C_M + D_f \times C_D) \quad (\text{Eq. 4})$$

Where: M_p = calculated methanol productivity; gmol/hr/kg oxidized catalyst.

When a low CO₂ content feed gas is used, part of the CO is converted to CO₂ as well as to methanol. For this case, the selectivity to CO₂ would have to be subtracted from the term in the parenthesis in Equation (4) in order to calculate the methanol productivity.

7.2.5

Cold-Flow Model -

The initial scoping of equipment requirements and experimental techniques was conducted in order to determine costs and timing associated with cold flow hydrodynamic modeling of the LPM₂H process.

A cold flow hydrodynamic unit was designed which could be operated as either a liquid-fluidized reactor or a liquid-entrained reactor. In the liquid-fluidized mode, the process liquid velocity is controlled over a narrow range in order to fluidize a fixed quantity of catalyst particles within the confines of the reactor. For liquid-entrained operations, smaller catalyst particles are intentionally suspended in the process liquid and are circulated throughout the liquid circulation loop. The process flows and physical dimensions of the hydrodynamic unit broadly resemble that of the LaPorte LPM₂H PDU. A conceptual process flow diagram of the cold flow hydrodynamic unit is shown in Exhibit 7.2.5-1.

It is anticipated that the hydrodynamic test unit would be constructed of materials that are compatible with a range of organic solvents. The process liquids will be selected to have properties similar to those of the hot process liquids. Solvents of differing physical properties would be used in the determination of the density, viscosity and surface tension effects on the hydrodynamic character of the process fluid.

1. Process Equipment

In the liquid-entrained gas/liquid upflow configuration, gas and slurry are co-fed to the bottom of the reactor (TW-100). Gas is introduced through a suitable distribution device while the slurry is introduced below the gas distributor. Catalyst particle size and process liquid flows would be selected so as to intentionally suspend the catalyst in the process liquid and circulate the solids throughout the liquid circulation loop. By design, the catalyst solids and process liquids must remain a homogeneous mixture everywhere within the liquid circulation loop. Gas/solids/liquids are taken overhead out of the reactor to the V/L separator (VT-100) where phase separation between gas and slurry phases occurs. The separated slurry phase is recirculated to the reactor inlet through a pump (CP-100). The gas phase passes through a demister (VT-101) to de-entrain any liquid droplets. The gas can then be vented or recycled back to the compressor (GC-100). The gas compressor would be equipped with a water cooled aftercooler (HE-100). The gas then flows into a surge tank in order to damp out pressure (or flow) fluctuations prior to passing to the reactor gas distribution system.



- Reactor

The reactor used for the hydrodynamic study would be constructed of a combination of flange-connected glass and metal sections. The column dimensions (identical to the LaPorte LPMeOH PDU reactor) will be 0.56 meters inside diameter by 4.6 meters long. The reactor piping connections at the top and bottom will be flexible. The bottom metal spool piece is designed to support the entire cold flow reactor assembly. Each metal spool piece would be constructed so as to allow for the introduction of sample probes, pressure taps, and other instrumentation as required. The sample probes would be constructed and operated so as to obtain slurry concentration data along the radial and axial direction. A Plexiglass or Lexan shield would be used to enclose the glass column for personnel protection. Sections of the plastic shield would be made removable to allow access to the various sample and pressure taps. Finally, an x-ray source and detector will be mounted so as to traverse the length of the reactor. Alternately, a series of fixed source/detector pairs may be mounted along the vertical length to obtain the density profile.

- Pumps and Compressors

A rotary screw air compressor with a water cooled aftercooler would be used for supplying gas. The present design requires a compressor capable of up to 2.8 m³ per minute at standard conditions and 790 kPa outlet pressure. The compressor discharges into a surge tank to damp out pressure and flow fluctuations.

Magnetically coupled centrifugal pumps will be selected for the slurry feed and circulation loop. These pumps are magnetically coupled to their motor so as to eliminate problems of liquid or gas leakage across a dynamic seal. In addition, these pumps do not require a seal flush flow. The present design requires a pump capable of 830 liters per minute maximum flow at 23 meters total dynamic head.

- Catalyst Recovery Filter

A plate and frame filter press is included in the design to be used in determining solids holdup within the column. Additional use would be made of the filter in recovering "used" catalyst upon completion of testing.



- Vessels

The slurry feed tank (VT-102) was sized at 1100 liters to hold the entire contents of the cold flow hydrodynamic test unit. It is baffled at 90° and supplied with an agitator to maintain the catalyst slurry in suspension. Liquid inventory can be monitored by placing the unit on a weigh cell or by using a DP cell. If a DP cell is used, an inert purge gas must be supplied to the high side of the cell to prevent plugging by catalyst. A slurry feed pump (CP-102) is used to transfer the slurry to the main test unit circulating loop.

The slurry preparation tank (VT-103) has a capacity of 400 liters and was sized for slurry addition and makeup in multiple batches. It is also baffled at 90° and supplied with an agitator. Inventory control would be accomplished by placing the unit on a weight cell. Slurry is transferred from the vessel to the feed tank or the main circulation loop through the slurry transfer pump (CP-101).

2. Experimental Techniques

Test methods for determining hydrodynamic system characteristics can be categorized as being either external or internal monitoring techniques. External techniques are preferential in that they do not interfere with established flow patterns. Internal methods involve the insertion of devices through the test cell wall, consequently inducing flow disturbances downstream of the sample location.

- External Methods

Sonic probes and gamma-ray scan techniques have been used to obtain data on the average bulk density in multiphase systems. Gamma-ray techniques make use of differential absorption of radiation by various materials. Being an external technique, it is an excellent method for determining the average density of a multiphase system without creating a flow disturbance. A movable density gauge could traverse the length of the reactor and give point bed density measurements directly. These measurements combined with fluidized bed height measurements give a direct evaluation of the relative liquid, gas and solid phase volume fraction.

Sonic techniques are alternate external methods for determining densities of multiphase systems, using sound rather than radiation. In single-phase systems,



phase-time and dual-path sonic probes (which measure sonic impedance) can be used to determine density. These devices can also be used in two-phase, liquid-solid slurry systems, provided that the sonic impedance of the two-phase mixture is a very weak function of slurry concentration. These devices cannot be used when a bulk gas phase is present because discrete gas bubbles give rise to interfering sonic reflections. It can measure vertical bubble rise velocity or slurry velocity.

• Internal Methods

Several tracer testing methods are known for determining residence time distributions, flow rates and relative phase volumes in multiphase reactors. The techniques employed involve use of a tracer component with an internal or external monitoring device. External detection systems are preferred as they will not interfere with established flow patterns.

In general, flow patterns can be studied by injecting a tracer into a vessel inlet stream and observing the subsequent concentration profile at the outlet. At steady state, methods used consist of injecting a continuous tracer into the inlet of a studied interval and measuring the upstream concentration. For large diameter columns, problems are encountered in obtaining a homogeneous dispersion of the tracer. Further, attempts to obtain an average sample profile across the column can be difficult without disturbing the original flow patterns within the column. When continuous sample withdrawal is employed, sample time effects may distort the measured response. Unsteady state methods of measuring residence time distributions consists of injecting a momentary tracer pulse at the reactor inlet and measuring the response function at the outlet. Pulse injection methods are preferred to step or frequency response methods since inputs requiring large quantities of tracer are impractical on large units. Pulse injection techniques are simple, inexpensive, and require only small quantities of tracer material.

In performing a tracer study, proper tracer selection is extremely important. The hydrodynamic response must be characteristic of the flowing phase and not a function of the tracer component. Any tracer employed should be miscible and have physical properties similar to the bulk fluid phase. The tracer must not be transferrable to the other phases of the system. All tracers under consideration should be accurately



detectable in low concentrations to minimize disturbances in the established reactor flow patterns.

To enable tracer detection in fast moving streams, the data recording equipment must offer exceptional sensitivity with a minimal detection response time. For simplicity and accuracy, the response of this equipment should be linear.

Gas, liquid or solid tracers can be injected into a flow system to determine the responses for each phase. For the gas phase, a tracer gas injected into a multi-phase reactor would have its concentration measured by a thermal conductivity or infrared absorption cell. Alternately, a radioisotope is substituted. In using gas phase tracers, absorption into the liquid phase precludes an accurate determination of the gas phase mixing and holdup without an independent measurement of tracer content in other phases. The differing rise velocities of individual bubbles further complicate the detector response. Because of these inherent difficulties in using gas phase tracers, only qualitative data concerning gas phase mixing are available in the literature.

The use of liquid tracers are well accepted industrial practices. Problems associated with their use are the familiar ones of sampling induced errors when internal techniques are used. External techniques employed include the use of dyes coupled with high speed photography and radioactive tracer methods. Unfortunately, photographic techniques relying on photochromatic dyes or particle luminescence cannot be used if the color change is obscured by the catalyst particles. In larger diameter columns wall effects can also obscure the events from photographic interpretation.

For the solid phase, a magnetic tracer can sometimes be used. The concentration of a solid phase tracer may be measured by a capacitance probe if the dielectric constant of the tracer material is substantially different than that of the solid phase. In general, for solid phases, a suitable radioactive tracer is often the most convenient to use. If proper precautions are observed, a radioactive tracer has a distinct advantage over other tracers in that the tracer detection devices can be mounted externally. In this way, no disturbances in the established flow patterns resulting from the presence of probes or sampling devices are encountered. The use of a radioactive tracer permits the time distribution function of a



rapidly moving phase to be accurately determined, since scintillation detectors can be interfaced with high speed recorders or with multi-channel analyzers with data storage capabilities.

7.2.6 CSI Lab PDU Modifications

The request to purchase the first of two slurry pumps was approved. Meanwhile, all responses on the RFQ for fabrication of vessels and skid equipment for the CSI lab PDU were received and evaluated. It was decided, however, at a meeting held in Fairfield on 25 February with APCI personnel not to hire a contractor to build a complete skid-mounted unit. Instead, only major equipment items, such as process vessels and heat exchangers, will be fabricated outside with the majority of engineering, skid design and assembly handled by CSI in-house. This change has been necessitated to allow more project flexibility, lower overall costs and improved scheduling. Work began on the assembly of a technical package which will serve as sufficient documentation for required purchases of equipment or services. This package will contain process flowsheets, heat and material balances and a description of the liquid-entrained CSI Lab PDU. The process flowsheets will eventually evolve into complete engineering flowsheets. This package when assembled will accompany any requests for approval sent to APCI/DOE.

7.2.7 CSI Lab PDU Experimental Program - This subtask will not be initiated until the CSI Lab PDU modifications are completed.

7.2.8 LaPorte LPMeOH PDU Support -

Overview

United Catalysts Inc. has developed under EPRI support (Reference 12) a methanol synthesis catalyst for the liquid-fluidized (ebullated bed) mode. This material represents a catalyst candidate with potentially better attrition resistance than any catalyst tested under the prior EPRI contract (Reference 13). A 10 lb sample of this catalyst (CSI Identification Number R71/OF12-02) was shipped to CSI's Fairfield Research Center for evaluation in a test in the CSI Lab PDU. The catalyst was charged to the reactor on 16 February 1982 and was reduced utilizing a vapor-phase reduction technique over a three-day period. Two days of testing concentrated on the three-phase fluidization properties of the catalyst suspended in Witco mineral oil, prior to the actual synthesis test. The catalyst was brought on-stream with a 2/1 H₂/CO feed gas, and operating conditions were maintained constant for a period of about 370 hours.



During this period, CO conversion and settled catalyst bed height were monitored. Fines generation, as determined by pressure drop buildup in the oil filters and decrease in settled bed height, was higher in the first two days on-stream time than during the later part of the run. Both factors were lower than experienced previously with another catalyst (FX2/1F15-02) tested under a previous EPRI contract (Reference 13). A measure of the attrition resistance characteristics of the catalyst will be obtained upon inspection and post-mortem analysis of the catalyst recovered from the reactor at the conclusion of the run.

During the Lab PDU operation, a process variable scan was also made to study the effect of temperature, space velocity, pressure and synthesis gas composition on catalyst activity and productivity to methanol.

CSI Liquid-Fluidized Lab PDU Description

The CSI Lab PDU reactor is 0.092 m I.D. x 2.13 m high, and the catalyst bed height can be varied from 0.6 to 1.5 meters. The detailed engineering design of the CSI Lab PDU has been presented elsewhere (Reference 14). The premixed synthesis gas feed is delivered to the laboratory in a tube trailer. A gas compressor is used to feed the gas to the reactor. In this manner, the pressure in the tube trailer can be reduced to 2170 kPa before a new supply is required. Two compressors are provided to allow flexibility in feed gas rate. Product methanol and small amounts of vaporized oil are condensed out of the product gas/vapor stream. Phase separation occurs at ambient temperature with a typical residence time in the product separator of one hour. The oil is recycled back to the process oil circulating loop. The product gases, following analysis, are sent to an incinerator. Sufficient instrumentation is provided for automatic control and monitoring from a remote control room. The system is designed for pressure up to 7000 kPa and temperatures up to 400°C. All necessary gas streams are connected to a common manifold and are constantly purged to reduce sampling time lags. The selected gas stream may be directed to each chromatograph column, in turn, to analyze for components of interest.

Preliminary Analysis of Short-Term Attrition Test

After the CSI Lab PDU was pressure tested, the reactor was loaded with fresh oxidized catalyst (R71/OF12-02) and reduced over a three-day period. The system was put on-stream at conditions similar to those used in the previous EPRI-funded test made in November, 1978: 250°C reactor temperature, 7000 kPa and 3000 hr⁻¹ VHSV (Reference 13). These conditions were held constant for 370 hours before process variable scans proceeded. The complete run chronology is shown in Exhibit 7.2.8-2.

At the onset of the run, CO conversion was 34 percent and then dropped linearly to the 28 percent level within 100 hours. During this time period, the settled catalyst bed height decreased to 93 percent of its initial height. For the remaining time, 270 additional hours, the CO conversion hovered at the 28 percent level while the settled catalyst bed height decreased to 81 percent of its initial height. These results are shown graphically in Exhibit 7.2.8-1.

The next 70 hours of running time were utilized in performing a process variable scan. The preliminary results of these tests are shown in Exhibit 7.2.8-3. At the termination of these scans (440 total hours on-stream time), the settled bed height had dropped to 78 percent of its initial height. Setting the system back to the initial run conditions gave a slightly lower CO conversion (27.5 percent) than the value just prior to the start of the variable scan.

With 460 hours logged on the catalyst, a short scan was performed using a low CO₂ (1.5 percent) content 2/1 H₂/CO feed gas. This synthesis gas resulted in essentially the same CO conversion as the 10 percent CO₂ gas with the exception that a small percentage of CO had apparently shifted to CO₂.

The synthesis gas used for the initial conditions was put back on-line resulting in a CO conversion of 27.5 percent. The settled catalyst bed height at this point was 75 percent of its initial height. After a total of 555 hours on-stream time, the settled catalyst bed height was 73 percent of the initial height and CO conversion was 27 percent. A short test using a 0.6/1 H₂/CO feed was then performed before the unit was shut down.

The unit will be disassembled to recover the catalyst and then cleaned up and placed in a stand-by condition. Catalyst and oil samples will be analyzed. The analysis of the non-hydrocarbon liquid products is not complete at this time but indicates a 96±1 weight percent methanol content with the remainder being Witco 40 oil, water and a small amount of higher alcohols - ethanol through hexanols.

Task 8 - Conversion of the LaPorte LPMcOH PDU from Liquid-Fluidized to Liquid-Entrained Mode

No Activity.

Task 9 - Shakedown for Liquid-Entrained Operation

No Activity.



Task 10 - Liquid-Entrained Operation

No Activity.

Task 11 - Project Evaluation

11.1 APCI Management Activities

11.1.1 Project Management -

The Project Status Reports, Format 5 Reports, and quarterly Technical Progress Report No. 1 were coordinated.

An arrangement was made to provide closer liaison between APCI design engineers and CSI's laboratory personnel following review of CSI's requisitioning material for a skidded assembly for modification of the Laboratory PDU to permit liquid-entrained operation. The specification, design, and erection of this unit remains in CSI's subcontract scope; however, APCI will take a more active role in engineering assistance and specification review. A rough project plan was worked out to establish requirements for future purchase requests by CSI in this area.

A meeting among APCI, CSI and DOE was held in Pittsburgh on 18 March 1982 to clarify procurement and approval procedures. A brief presentation was made by APCI and CSI on the program status.

11.1.2 Economic Evaluation - No Activity.

11.1.3 Travel and Living - APCI and CSI met on several occasions in Allentown and Fairfield and once in Pittsburgh. APCI's Operations Manager from LaPorte attended meetings in Allentown and Chicago. Two trips were made to Chicago by APCI and CSI personnel to review LPM pilot plant relocation specifics.

11.2 CSI Activities

11.2.1 Data Evaluation - Information from the CSI Lab Stirred Autoclave and the CSI liquid-fluidized PDU runs was evaluated and reported under the corresponding subtasks. Thorough analysis of data from both of these units will continue into the next reporting period.

11.2.2 Design and Economics - No Activity.

11.2.3 Process Scaleup - No Activity.

11.2.4 Reporting - Monthly Project Status Reports, management reports and the first quarterly Technical Progress Report were issued. Work was completed on a paper for presentation. A meeting was



held at PETC on 18 March 1982 to discuss current project status and equipment review/purchase procedures. Work began on updating the CSI Project Work Plan including schedule, manpower and costs. This will be part of the 1 June deliverable to DOE from APCI.

11.3 APCI Design

11.3.1 Integration -

APCI reviewed and technically approved CSI's first Laboratory PDU slurry pump purchase. A technical difference exists between recommendations of the International Coal Refining Co. and Lawrence Pump Co. regarding the most appropriate seal arrangement for this application. Due to the experienced position Lawrence has with various pilot plant operations in hot, high pressure, slurry service these recommendations are being given thoughtful consideration.

Technical review and approval were given by APCI on CSI specifications for pressure vessels and a slurry heat exchanger required for modification of CSI's Laboratory PDU for liquid-entrained operation.

11.4 APCI R&D Activities

11.4.1 Corporate Development Department - Input was provided to the Monthly Status Reports and Technical Progress Report No. 1. Meetings were held with the CSI Fairfield laboratory staff to strengthen the technical liaison between the research organizations.

11.4.2 Process Systems Group R&D -

Preliminary Viscosity and Density Data

In support of the LaPorte LPM₂OH PDU design effort, preliminary viscosity measurements of Witco 40 oil/MC-2 catalyst slurry were carried out using a Brookfield LVT viscometer with an ultra low viscosity adapter attachment and spindle. The variables included:

- Temperature - 67°F to 482°F (19 to 250°C)
- Slurry Concentration - 0 wt%, 12 wt% and 25 wt%

Immediately before measurement for slurries, the U.L. adapter was removed and shaken vigorously to ensure a uniform solids suspension during the viscosity measurement. Preliminary results indicated that 25 wt% slurry viscosity showed a strong shear-rate dependence. These results are suspect from several points of view. The data are currently being evaluated and the full report and conclusions will be included in the next quarterly



report. In addition to the viscosity data, the density, the volume % and % volume change of 12 wt% and 25 wt% slurry were measured at 71-72°F (22°C).

Pyrophoric Nature of Spent Catalyst

An experimental plan was developed to assess the pyrophoric nature of oil/catalyst slurries. Three types of experiments have been considered:

1. Qualitative observation of oil/catalyst slurries in an open air environment (hood).
2. Differential Thermal Analysis (DTA) of oil/catalyst slurries (1-5 mg) to determine quantitatively the timing and the temperature at which auto-ignition would occur.
3. Heat of combustion measurements of oil/catalyst slurries (1 g sample) to verify the theoretical calculations for the largest possible energy release.

This plan is ready for circulation within APCI for review and comment.

Fundamental Model for LPMeOH

Progress was made in exploring fundamental modeling of the LPMeOH reactor and reaction kinetics. A computer model written by Professor W. D. Deckwer of Universitat Hannover (West Germany) for Fischer-Tropsch synthesis in a slurry phase reactor was tested. (This computer program is not generally available to the public but was made available by Professor Deckwer under a private agreement with APCI. It is planned to report results from the computer model; the software programming will not be reported without prior agreement with Professor Deckwer.) The Deckwer model is well described in Reference 15. The computer program was made operational and the results of computations published in Reference 15 were duplicated. The strategy is now being developed to model the LPMeOH fluidized (ebullated bed) and entrained (slurry) reactors by modifying the rate expressions, modifying the mass balances to allow both solids and liquid to flow in and out the reactor, and by incorporating appropriate hydrodynamic parameters at high liquid velocities.

Liquid Phase Reactor Patents

A preliminary patent search on 3-phase slurry reactor designs was made regarding possible infringements of the LaPorte LPMeOH PDU reactor design on the prior patents. The search revealed that the current simple reactor designs at LaPorte probably do not infringe any prior patent because the prior 3-phase reactor patents are largely process-oriented.



Input was provided to the Monthly Status Reports and the Technical Progress Report No. 1. Meetings were organized and held with the CSI Fairfield laboratory staff to enhance technical communications.



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ATTACHMENTS

- Exhibits 2.3.1-1
- 2.3.1-2
- 2.3.1-3
- 2.3.1-4
- 2.3.1-5
- 2.3.1-6
- 2.3.1-7A
- 2.3.1-7B
- 2.3.1-8
- 2.3.1-9A
- 2.3.1-9B
- 2.3.2-1
- 7.1.3-1
- 7.2.2-1
- 7.2.5-1
- 7.2.8-1
- 7.2.8-2
- 7.2.8-3

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E. P. Holley
Project Manager

Handwritten signature of J. Klosek in cursive script.

J. Klosek
Program Manager

ATTACHMENTS

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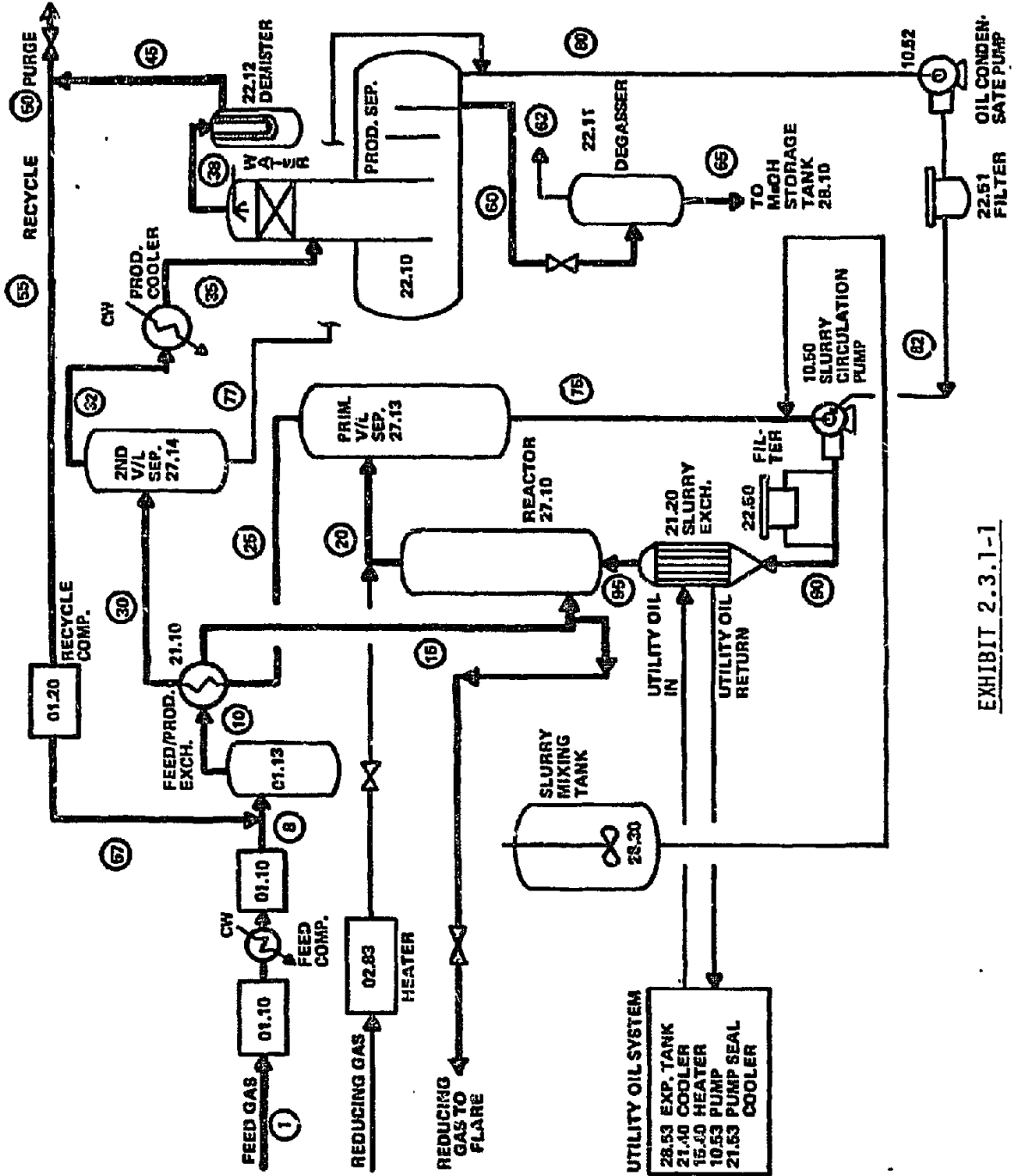












EXHIBIT 2.3.1-1














SIMPLIFIED PROCESS FLOWSHEET FOR LAPORTE LP MeOH PDU

STANDARD













LINES

	PROCESS LINE
	NON-PROCESS OR UTILITY LINES
	PNEUMATIC LINE
	ELECTRICAL LINE
	INSTRUMENT CAPILLARY TUBING
	INSULATED LINE
	ELECTRICAL TRACED LINE
	INSTRUMENT AIR SUPPLY
	HYDRAULIC SIGNAL LINE
	MECHANICAL LINES

VALVES

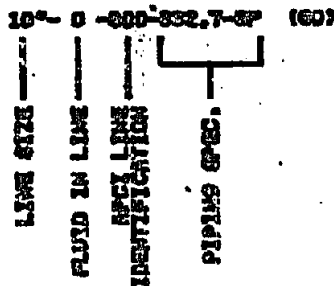
	GATE VALVE
	GLOBE VALVE
	NEEDLE VALVE
	LOCK-OUT VALVE
	CHECK VALVE
	BUTTERFLY VALVE
	THREE WAY VALVE
	FOUR WAY VALVE
	MANIFOLD VALVE
	ANGLE VALVE
	BALL VALVE
	SWITCHING CHECK VALVE
	TYPICAL AIR-CULT VALVE DESIGNATION

MISCELLANEOUS

	IN-LINE STRAINER
	STRAINER
	MATERIAL BALANCE POINT
	REDUCER
	EXPANSION JOINT OR FLEX CORRECTION
	TRAP
	OPEN FUNNEL DRAIN
	FLEXIBLE HOSE
	UNION
	SPEC OR LIMIT BREAK
	FLANGES
	FLOW SIGHT GLASS

BOLS AND ABBREVIATIONS

LINE DESIGNATION



FLUID ABBREVIATIONS

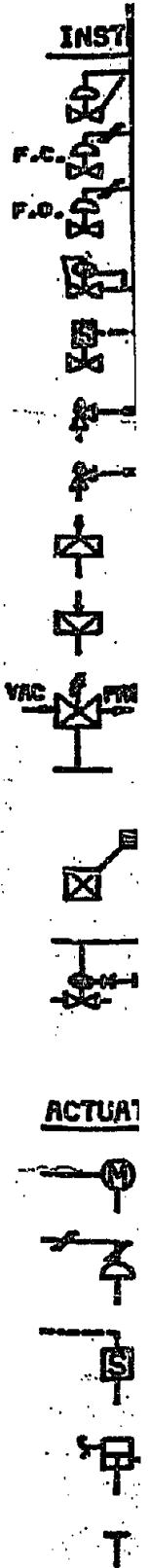
A	AIR
AG	ACID GAS
AP	AIR PURGE
AR	ARGON
BFW	BOILER FEED WATER
CI	METHANOL
CM	COOLING WATER
D	DISTILLATE
DS	DISTILL. SULFIDE
EP	EFFLUENT
FG	FEED GAS
FO	FUEL OIL
GL	GLYCOL
H	HYDROGEN
IA	INSTRUMENT AIR
INF	INFLUENT
K	CONDENSATE
L	LUBRICATING OIL
LOL	LEAN OIL
MEA	MEA
N	NITROGEN
NAP	NAPHTHA
O	OXYGEN
PG	PRODUCT GAS
FW	POTABLE WATER
R	ARGON
RG	REDUCTION GAS
ROL	RICH OIL
S	STEAM
SL	SLUDGE
SG	SG
SY	SLURRY
UD	UTILITY OIL
VG	VENT GAS
WAS	WASTE ACTIVATED SLUDGE
WO	WASTE OIL
WH	WASTE WATER

PIPING MATERIALS

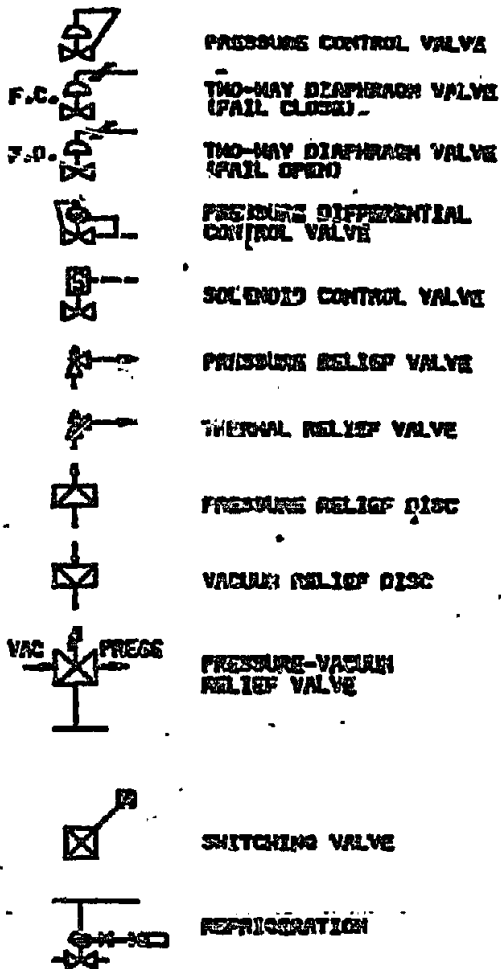
AA	ALUMINUM ALLOY
BP	BRASS PIPE
BT	BRASS TUBE
CG	GALVANIZED
CI	CAST IRON
CP	COPPER PIPE
CS	CARBON STEEL
CSO	CARBON STEEL (OXYGEN)
CT	COPPER TUBE
IAB	INSTRUMENT AIR SUPPLY
SS	STAINLESS STEEL
TA	TUNGSTEN ALLOY (WPL)
VC	VITRIFIED CLAY
CSG	GALVANIZED

MISC. ABBREVIATIONS

CA	HYDROCARBON ANALYZER
CAZ	NITROGEN ANALYZER
COZ	OXYGEN ANALYZER
A/N	AUTO-NORMAL STATION
C.S.	COLD BOX
C.O.	CROSS OVER
F.C.	FAIL CLOSE
F.O.	FIELD
F.O.	FAIL OPEN
G.S.	GAS SAMPLE
H.P.T.	HIGH POINT
I.S.	INSIDE
I/P	CURRENT TO PNEUMATIC TRANSDUCER
L.E.L.	LOWER EXPLOSIVE LIMIT
L.O.	LOCK OPEN
L.P.T.	LOW POINT
L.S.	LIQUID SAMPLE
N.H.	NANGLE
O.S.	OUTSIDE
P.T.	PRESSURE TAP
S.P.	SET POINT
T.S.	TO STACK
U.S.	UTILITY STATION
V.S.	VACUUM BREAKER
A.G.	ABOVE GROUND
U.G.	UNDER GROUND
B.L.B.	BUILDING

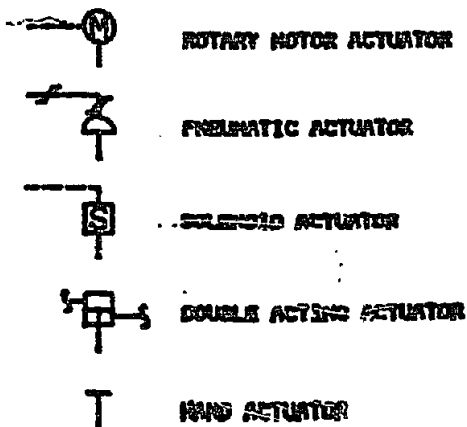


INSTRUMENT VALVES

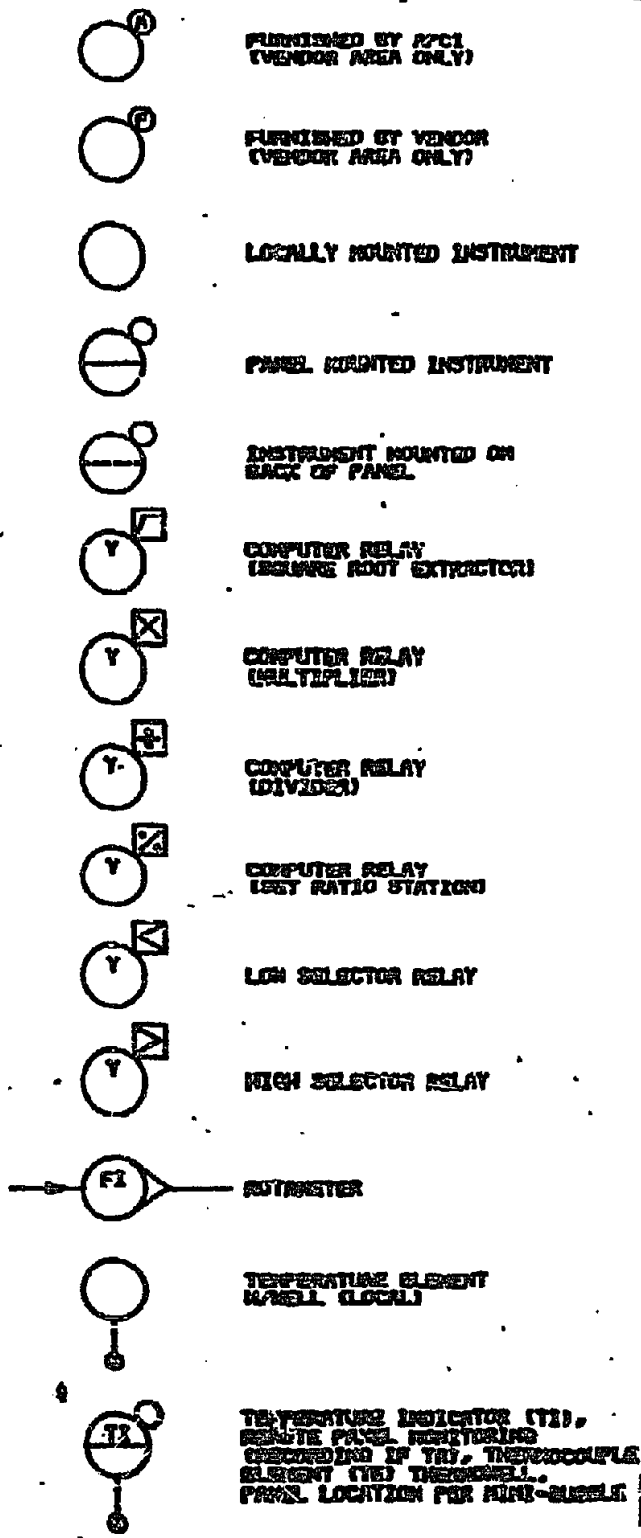


ACTUATORS

INDEX

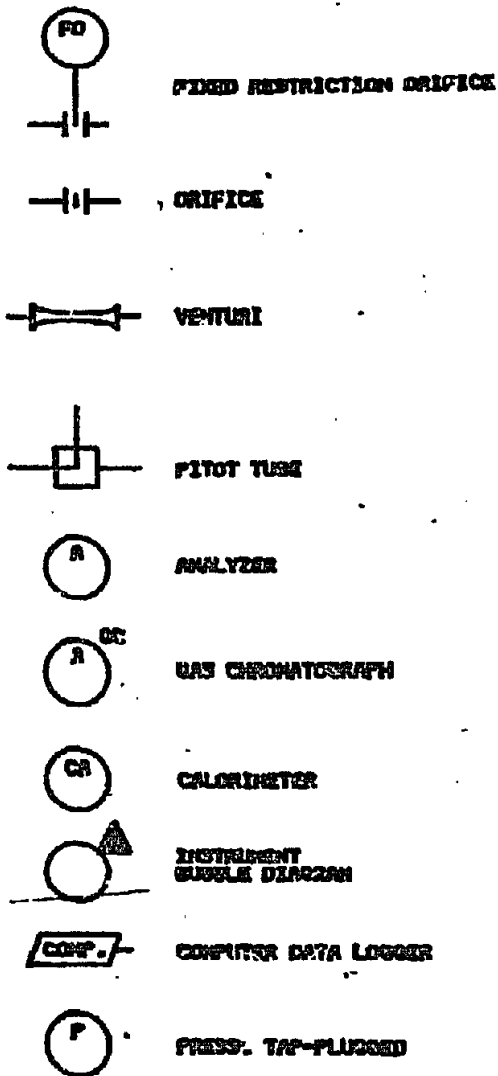


INSTRUMENTS



INSTRUMENT IDENTIFICATION INDEX

INSTRUMENTS



	FIRST LETTER		SUCCEEDING LETTERS		
	MEASURED VARIABLE	MODIFIER	PASSIVE FUNCTION	OUTPUT FUNCTION	FC
A	ANALYSIS		ALARM		
B	BURNER				
C	CONDUCTIVITY			CONTROL	
D	DENSITY	DIFFERENTIAL			
E	VOLTAGE		ELEMENT		
F	FLOW	RATIO			
G	GAUGING		GLASS		
H	HAND				HIGH
I	ELECTRICAL		INDICATE		
J	POWER	SCAN			
K	TIME				
L	LEVEL		LIGHT		LOW
M	HUMIDITY				MIDDLE
N	EMERGENCY				
O			ORIFICE		
P	PRESSURE		POINT		
Q	QUANTITY	INTEGRATE			
R	RADIOACTIVITY		RECORD		
S	SPEED	SAFETY		SWITCH	
T	TEMPERATURE			TRANSMIT	
U	ULTRAVIOLETS		MULTIFUNCTION	MULTIFUNCTION	MULTIF
V	VISCOSITY			VALVE	
W	WEIGHT		WELL		
X	SOLENOID				
Y	VIBRATION			RELAY	
Z	POSITIVE			DRIVE	

NOTES:

- (1) FOR ANY ADDITIONAL INSTRUMENT IDENTIFICATION AND SYMBOLS, REFER TO THE ISA SYMBOLS, SECTION 26.1, OR THE FLOW-SHEET GROUP.
- (2) NEW INSTRUMENT TAGS SHOULD BE ORIGINATED FROM THE FLOW-SHEET GROUP.
- (3) BOP FOR VALVE WITH INTEGRAL CONTROL, BY-PASS VALVE WITH SEPARATE CONTROLLER B- IS THE LETTER FOR MEASURED VARIABLE.
- (4) ALL RE-PIPE CONNECTIONS TO FLAMMABLE GAS LINES SHALL CONFORM TO ENR. DES. STD. 570.8

PANEL LEGEND

- ① MAIN CONTROL PANEL
 - ② 01.10 AND 01.20 PANEL (APCS)
 - ③ 01.10 AND 01.20 PANEL (VENTURI)
 - ④ ANALYZER PANEL
- FLOW-SHEET LEG**
-
- FIGURE

FILE
LE

<u>SD-2</u>	
SHUTDOWN	ACTION
EMERGENCY TRIP	1) CLOSE FV-101 (R2 FEED) 2) CLOSE FV-104 (C3 FEED) 3) CLOSE FV-116 (C4 FEED)
TSM-100 (HIGH REACTOR TEMP)	

02002
00

<u>SD-3</u>	
SHUTDOWN	ACTION
S/D-4	1) S/D-1 2) S/D 10.50
10.50 PUMP LOW AMP CUTOUT	

02002

<u>SD-4</u>	
SHUTDOWN	ACTION
PCL-274 (LOW CARRIER FLUID PRESS.)	17 CLOSE PV-181 21 3/P-3
PSL-173 (PUMP DIFF. PRESS.)	

SH

IN
C
P/S

NT
3/8

<u>SD-5</u>	
SHUTDOWN	ACTION
LSL-315 (22.11 LOW LEVEL)	17 CLOSE XV-242

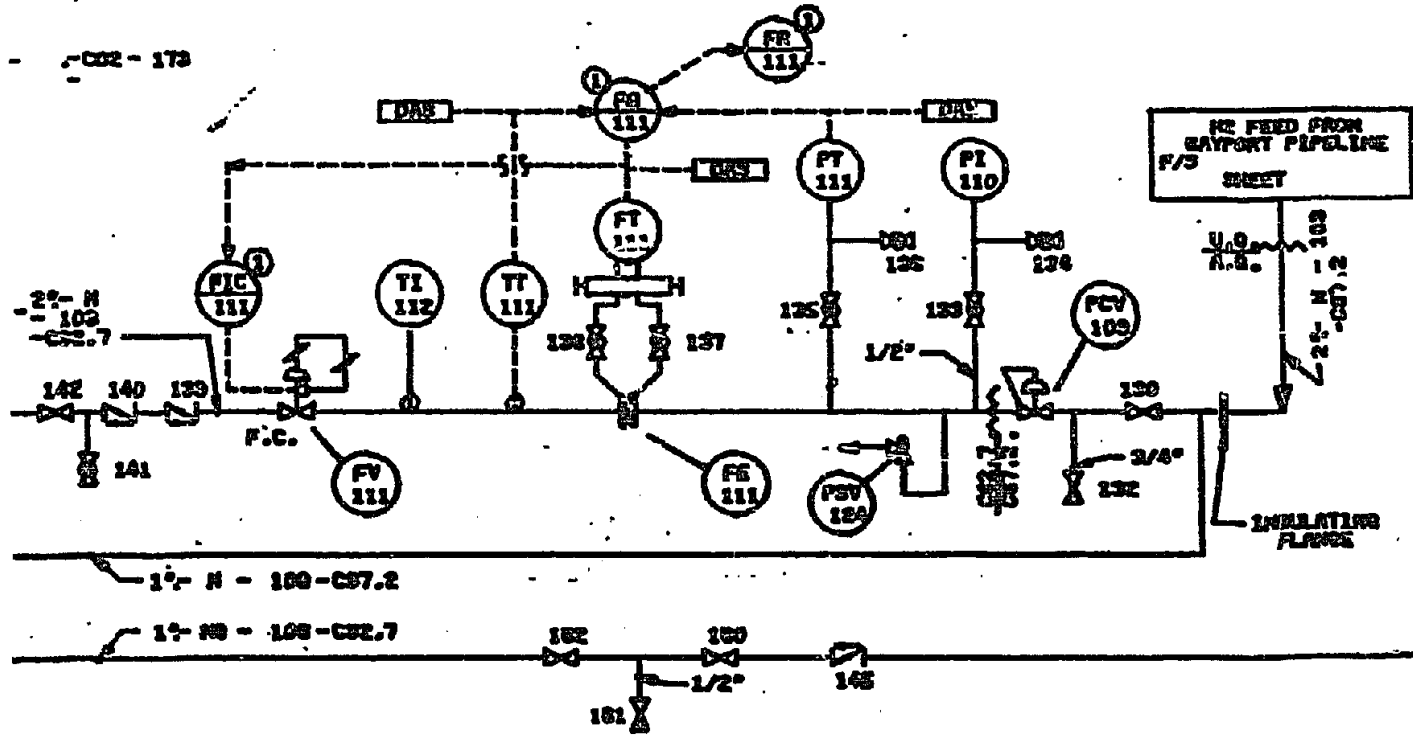
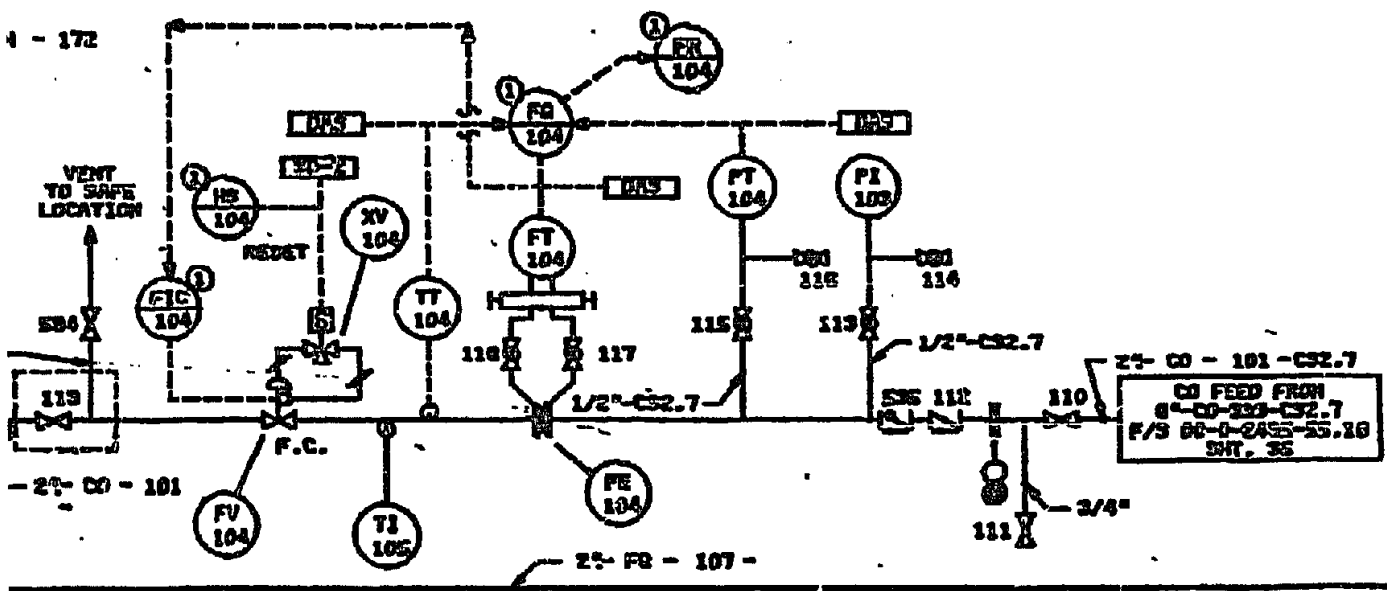
2
C
PRES

TO

FIGURE

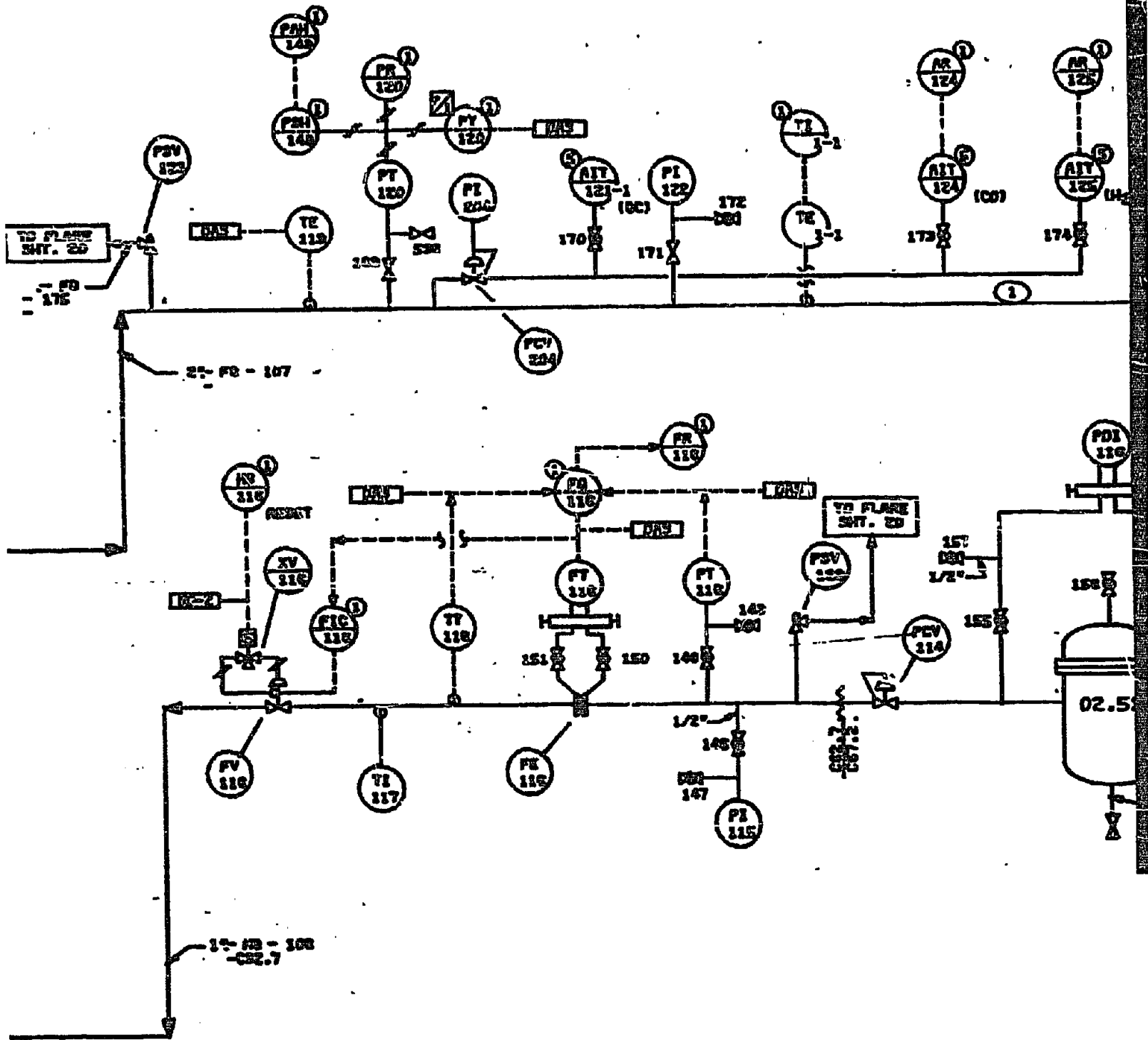
SH

TO FL
SMT.
- 175



SHEET 2

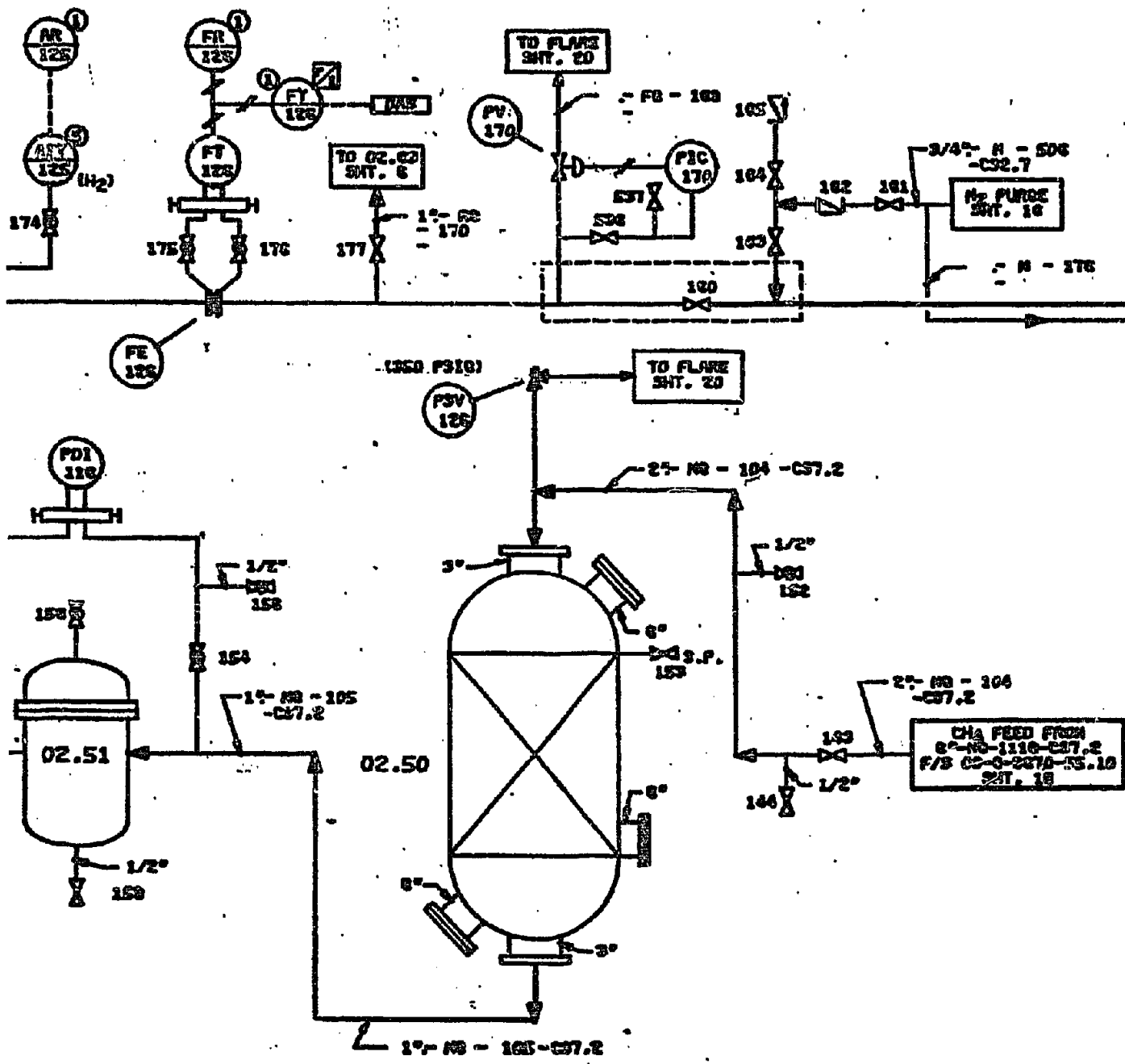
02.5
FILTER



02.51
FILTER

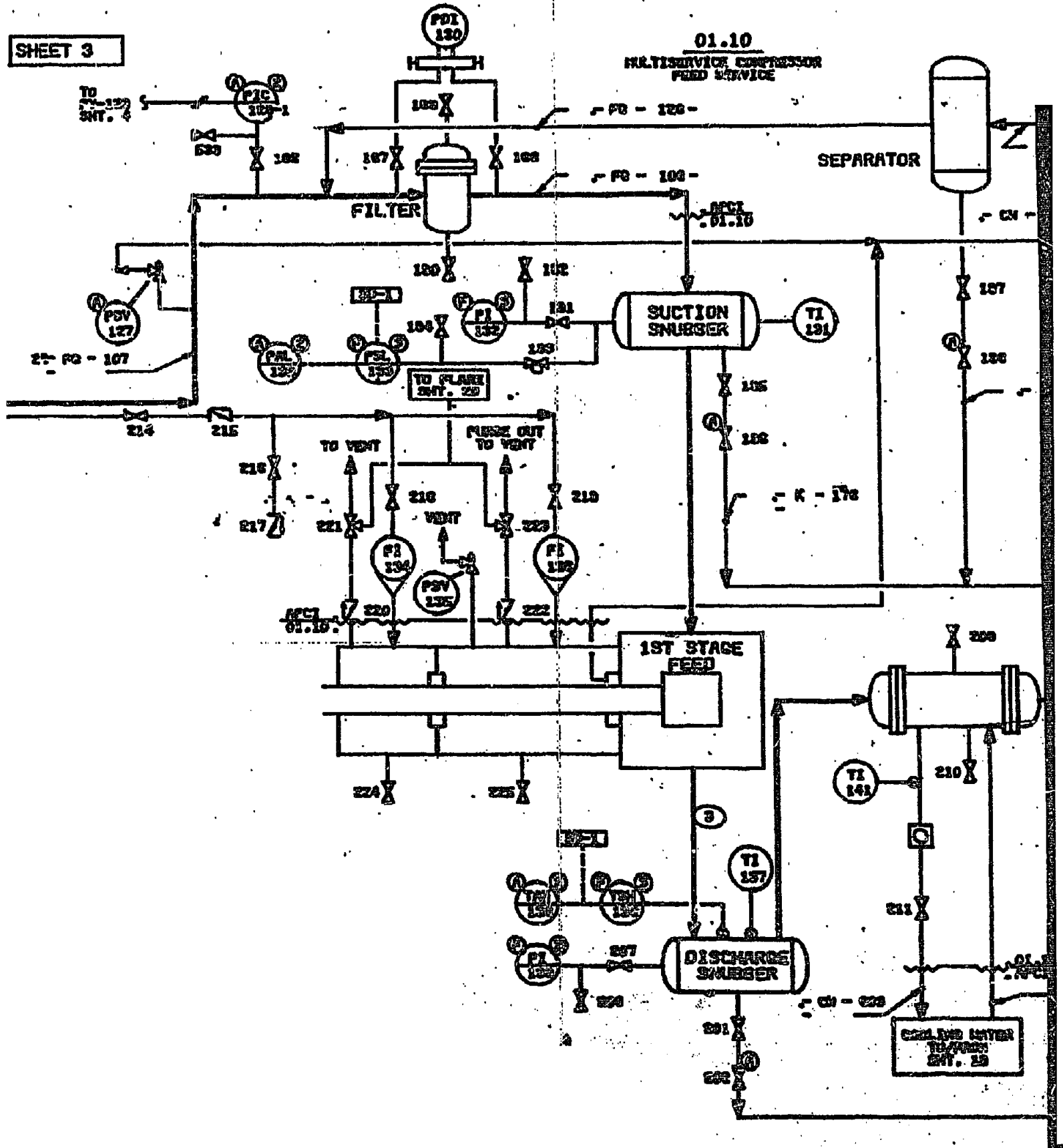
02.50
DESULFURIZER

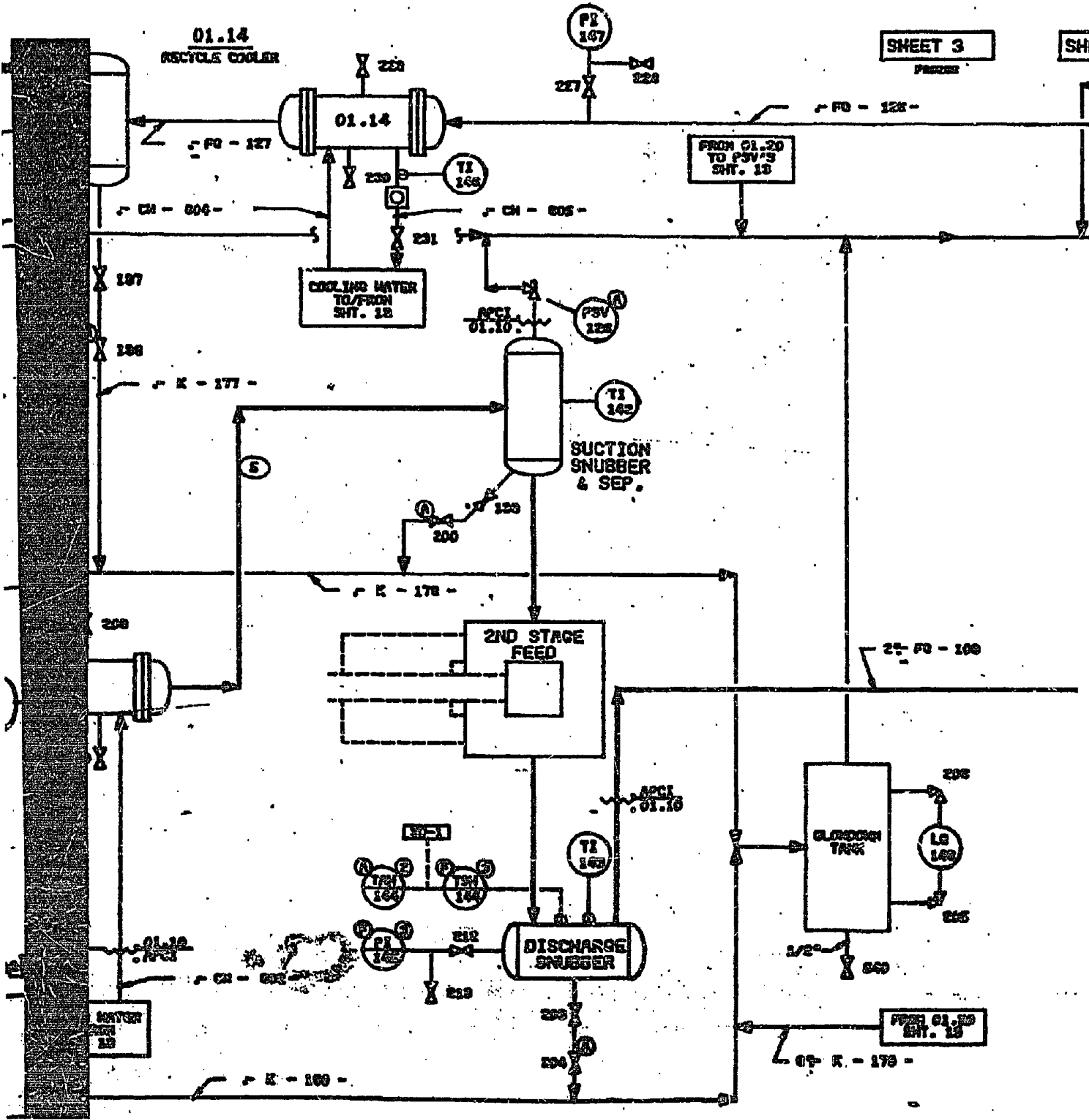
SHEET 2
P20085



SHEET 3

01.10
MULTISERVICE COMPRESSOR
FEED SERVICE

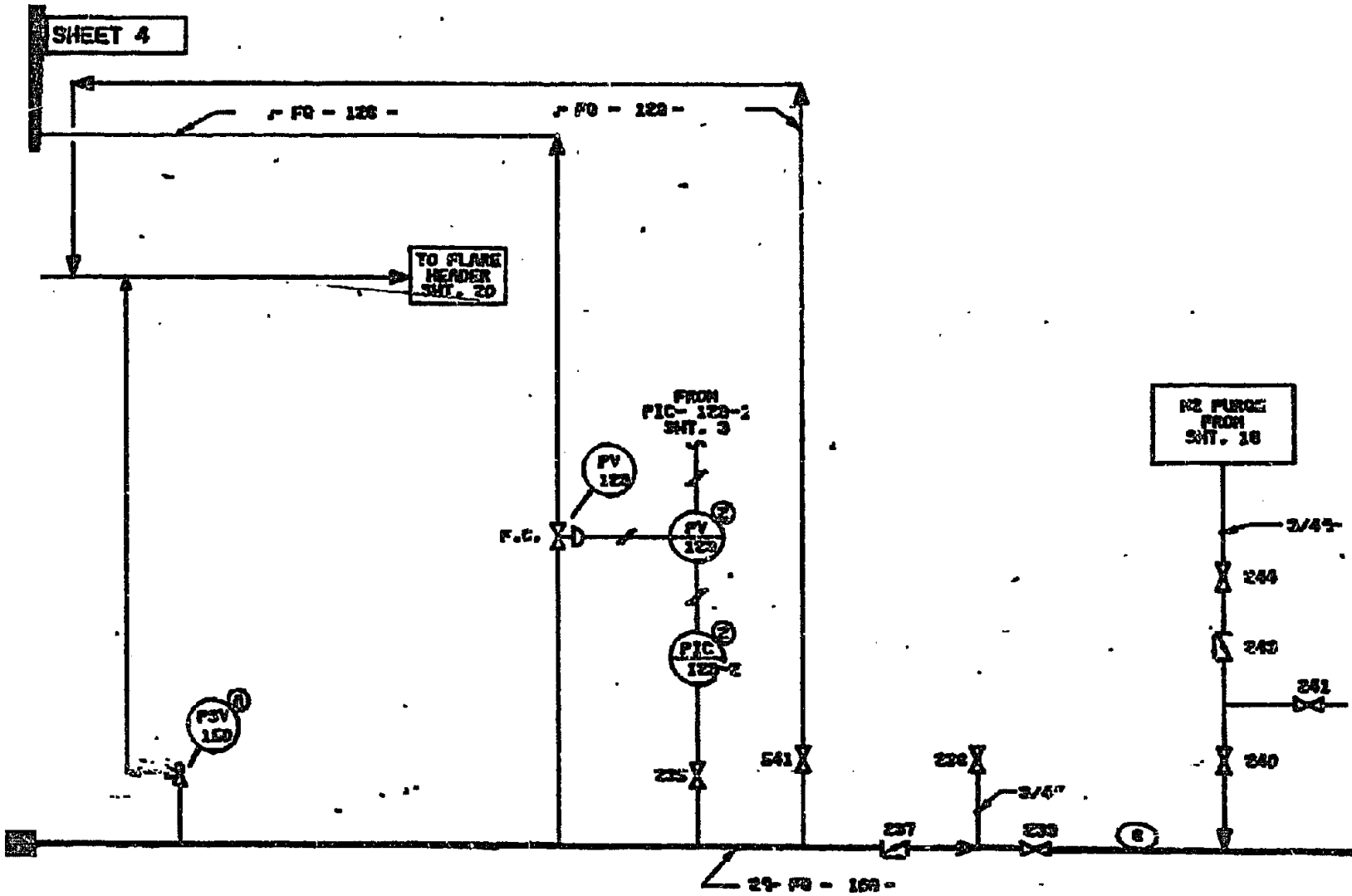




SHEET 3

SH. 13

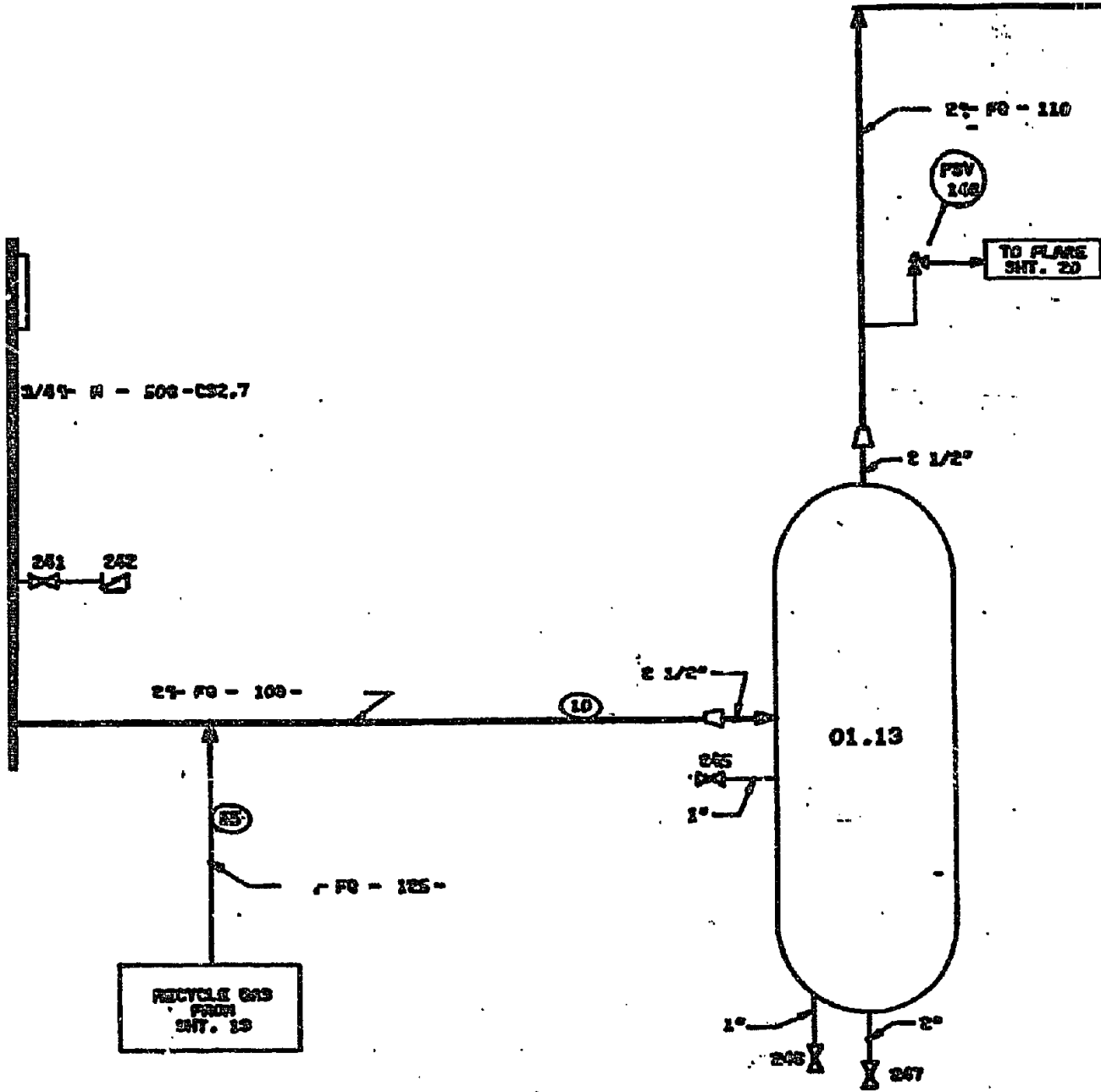
SHEET 4

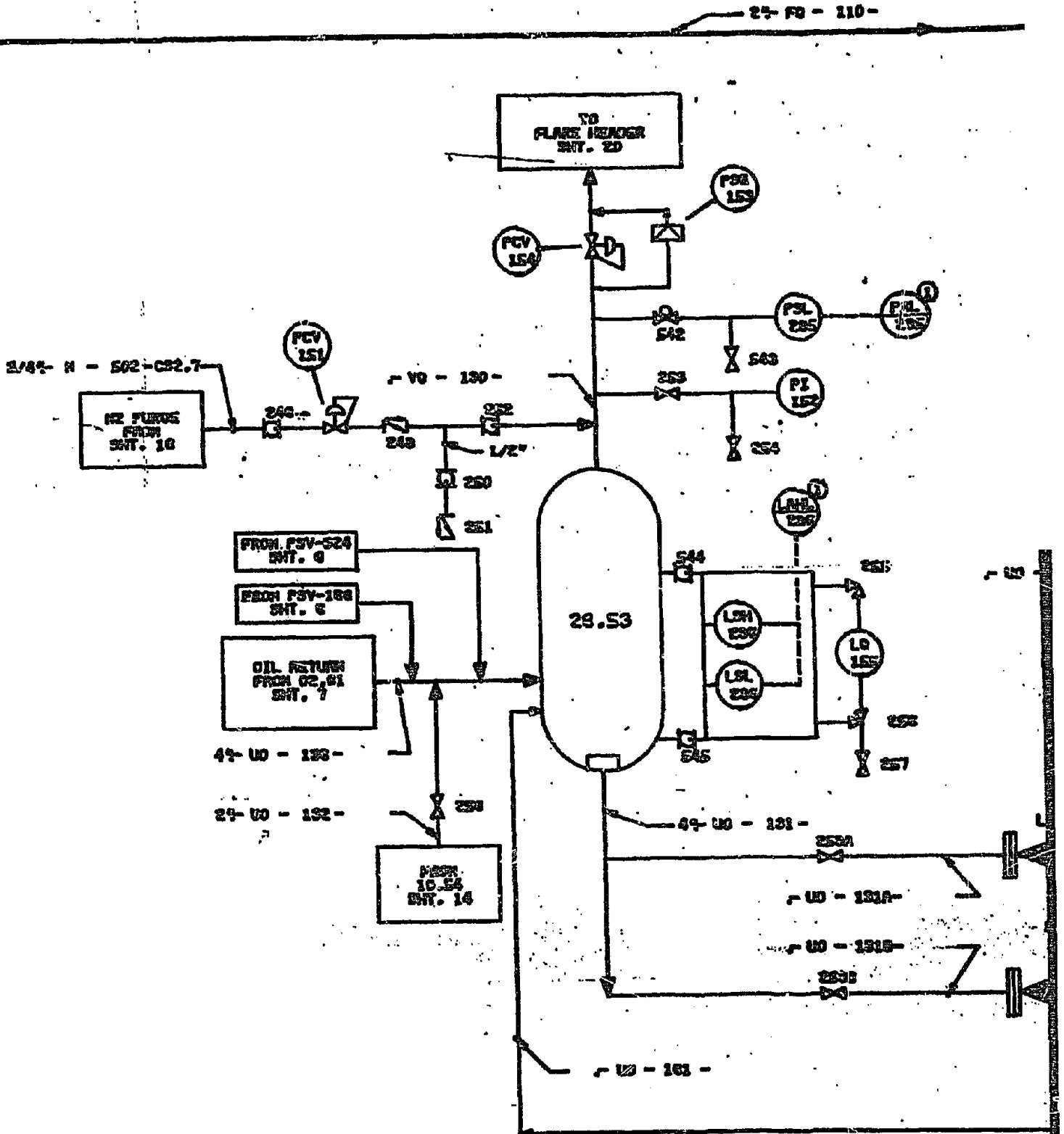


01.13
FRESH DUDGE TANK

SHEET 4
FIGURE 7

SHEET 5



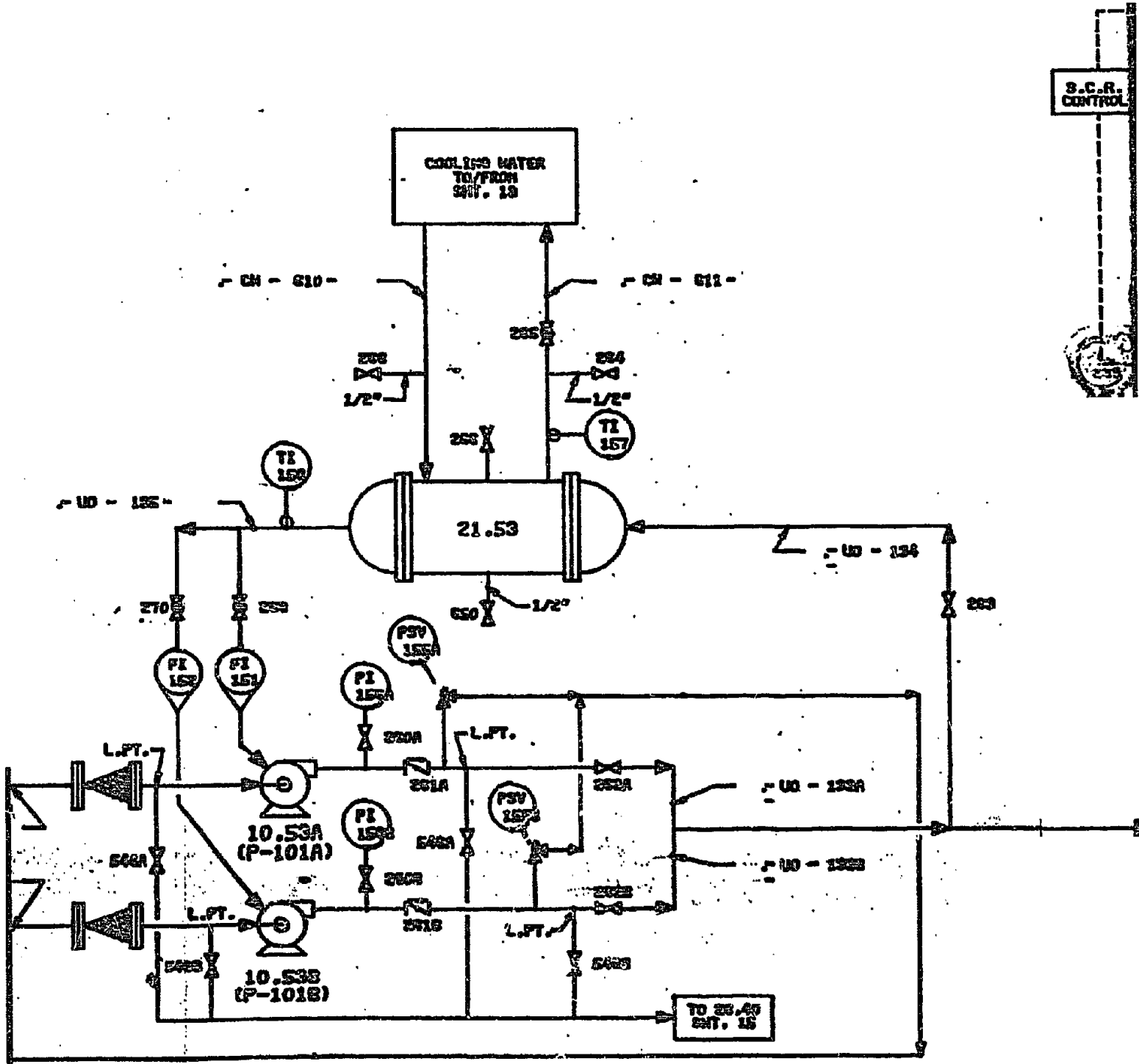


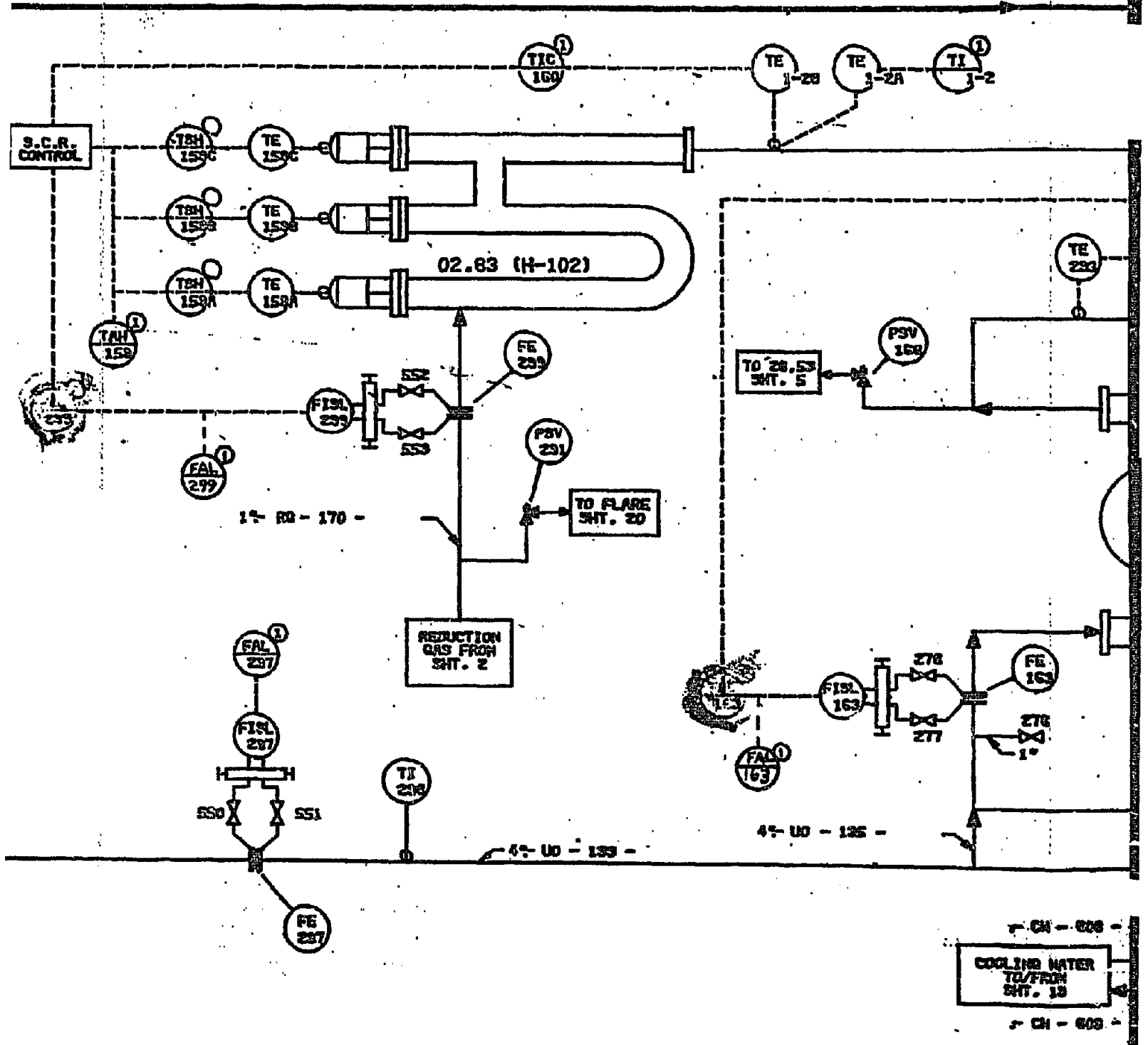
10.53A & B
(P-101A & B)
HOT OIL PUMPS

21.53
SEAL FLUSH COOLER

SHEET 5
P25024

SHEET

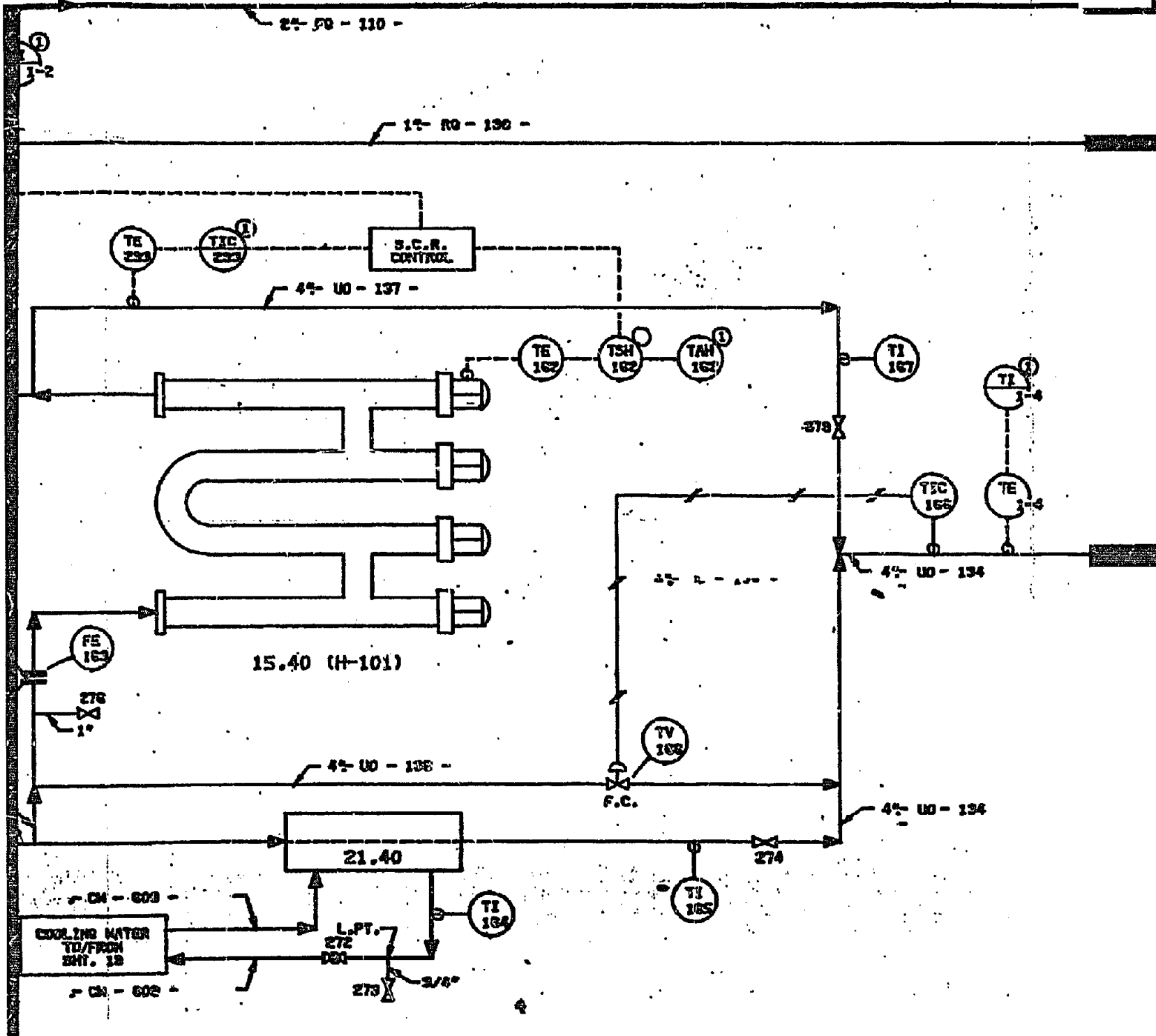




15.40 (H-101)
OIL HEATER

21.40
OIL COOLER

SHEET 6
PROCESS



p

10.50

MURRY CIRCULATION PUMP

SHEET 7

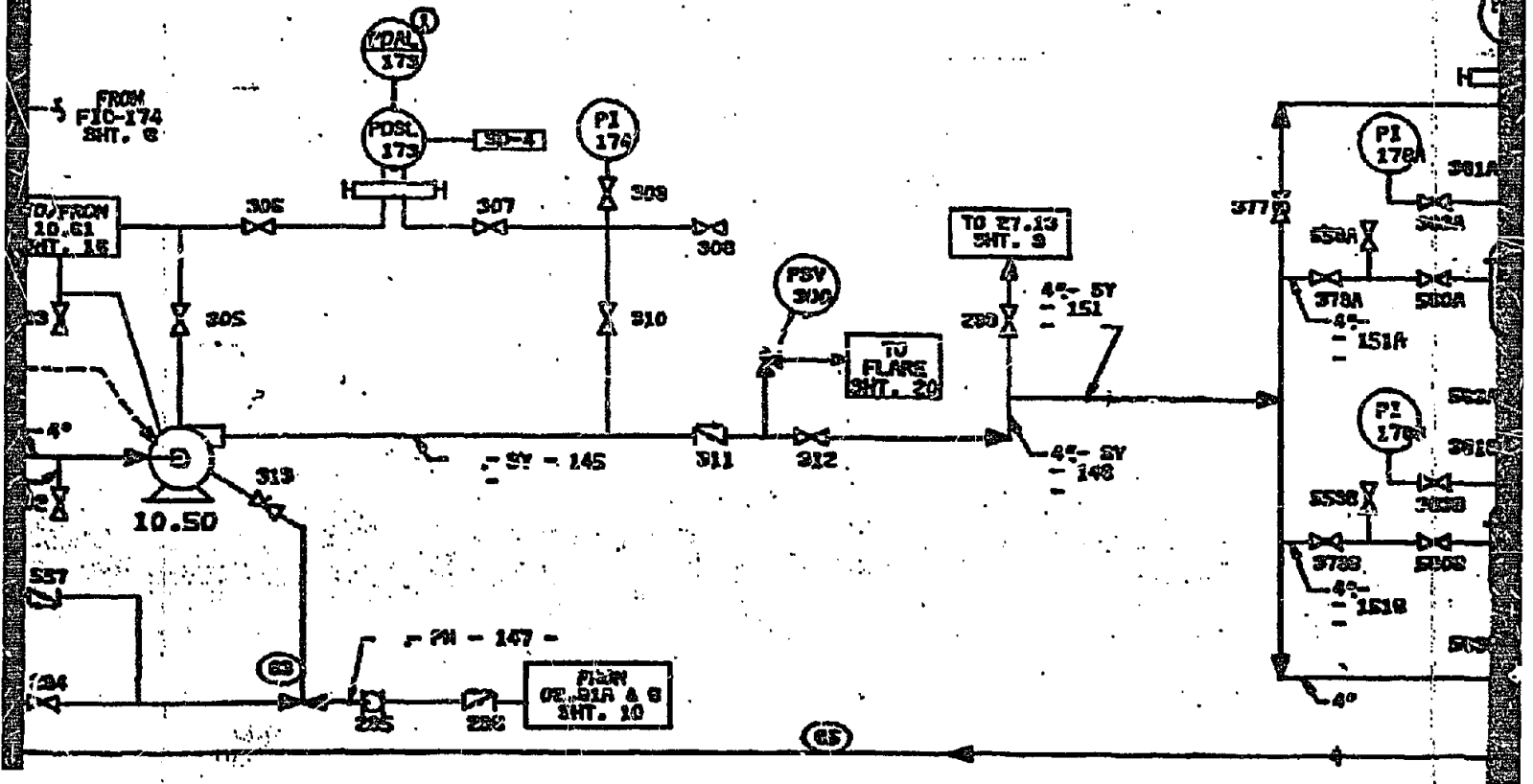
FE0220

SHEET 8

22.5
(F10
310
F1)

UA 174 (3) 10.50 MALFUNCTION

2" FG - 110 -



PI 174
OP. 31A & B
SHT. 10

TO 27.13
SHT. 9

TO FLARE
SHT. 20

PI 178A 381A
 378A 380A
 4" 151A
 PI 178B 381B
 378B 380B
 4" 151B

2" FG - 147 -

4" 5T - 145

4" 5T - 151

4" 5T - 148

TO/FROM
10.61
SHT. 15

FROM
FIC-174
SHT. 6

PDS 173

PDS 173

PI 174

PSV 310

10.50

65

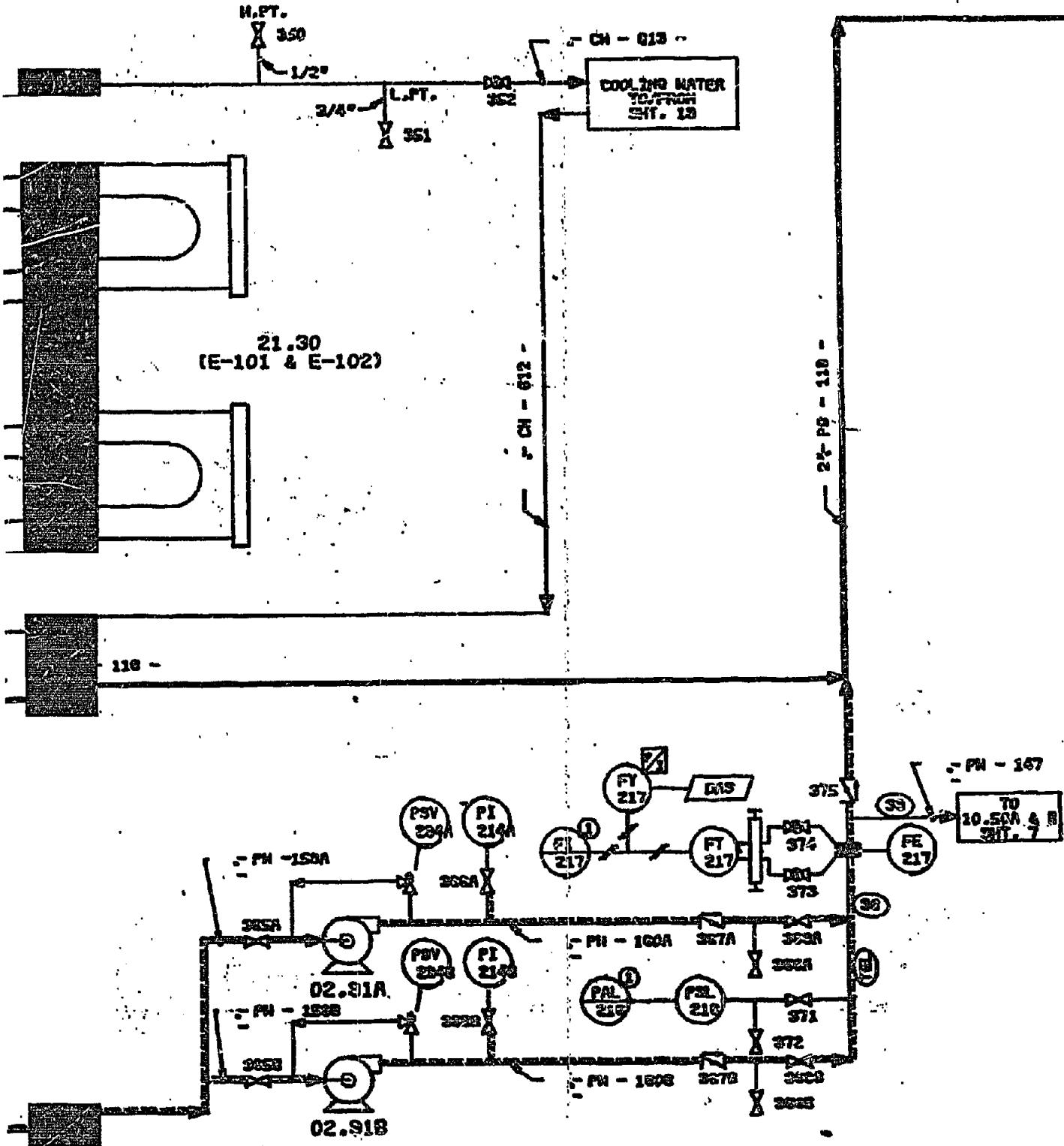
65

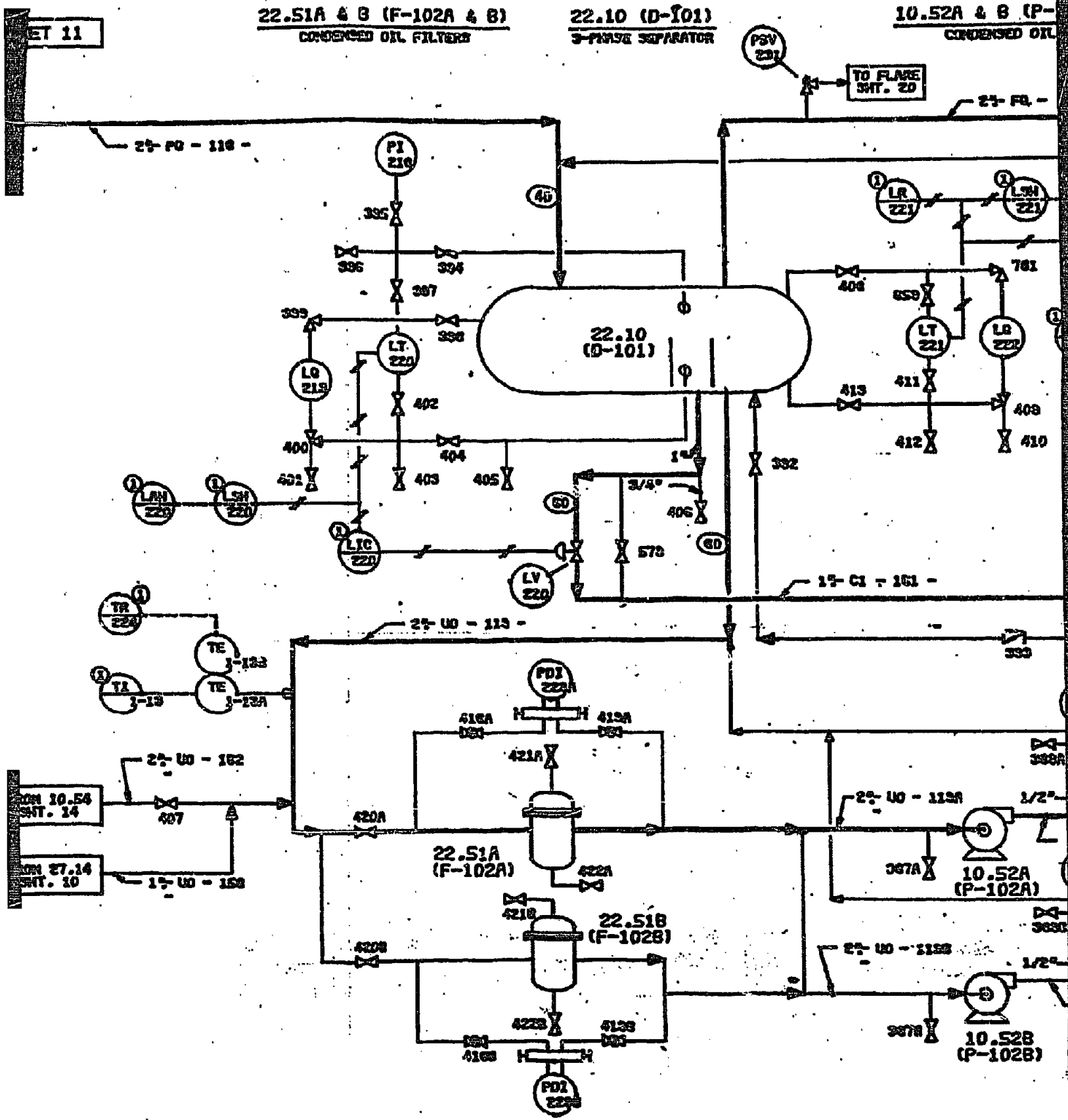
21.30
(E-101 & E-102)
PRODUCT GAS
COOLER

02.91A & B
WATER PUMPS

SHEET 10
PFD23A

SHEET 1



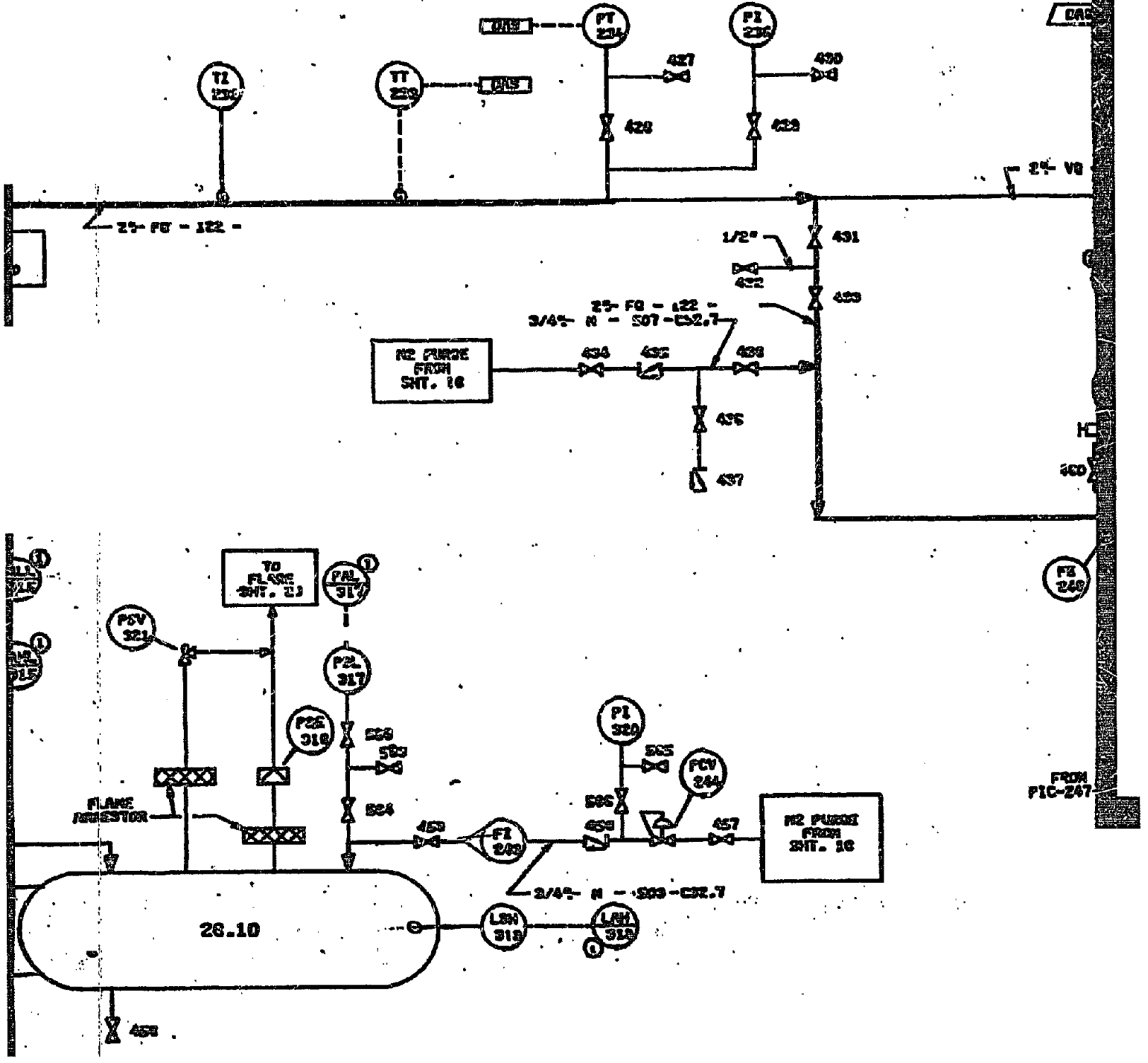


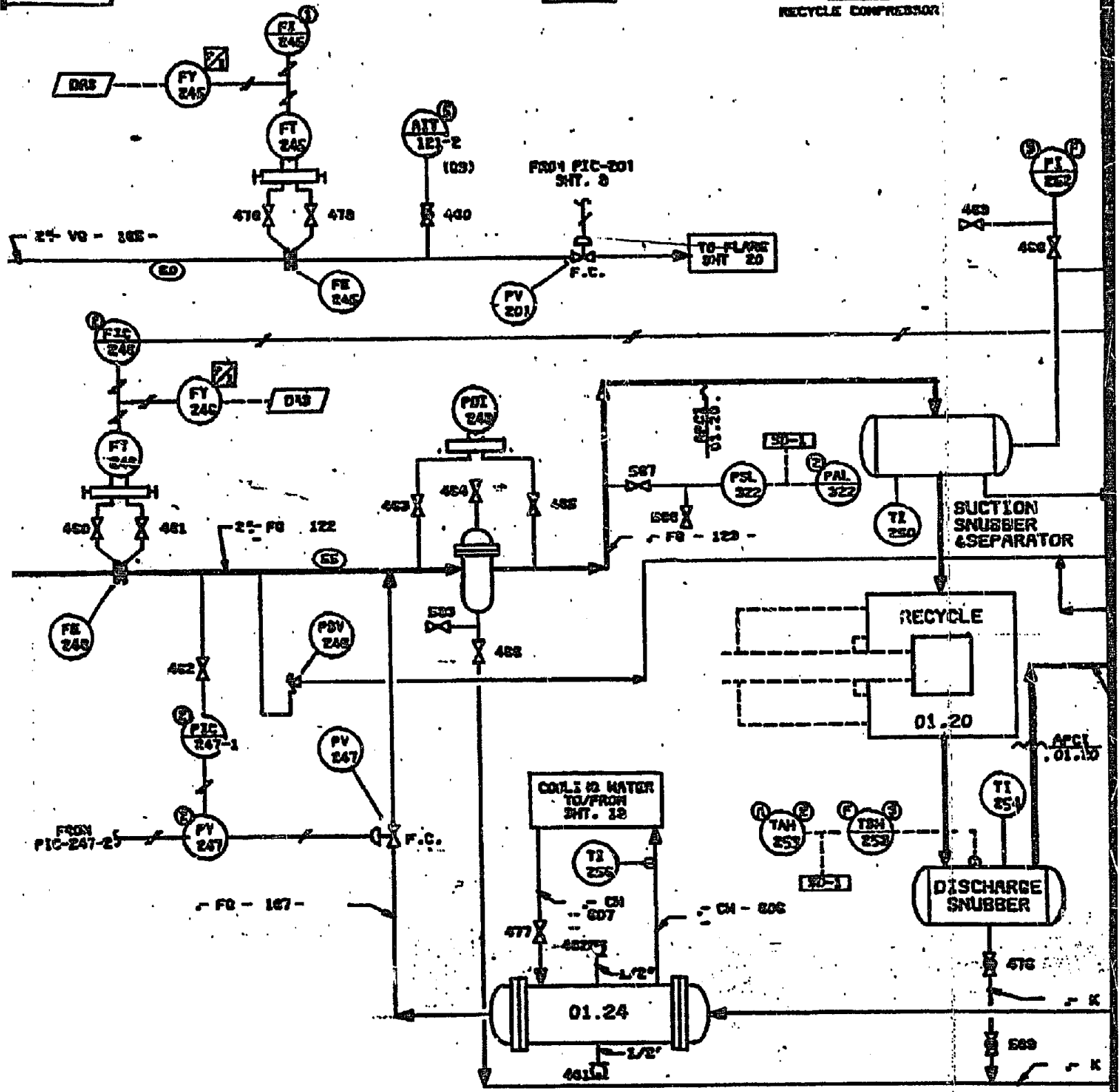
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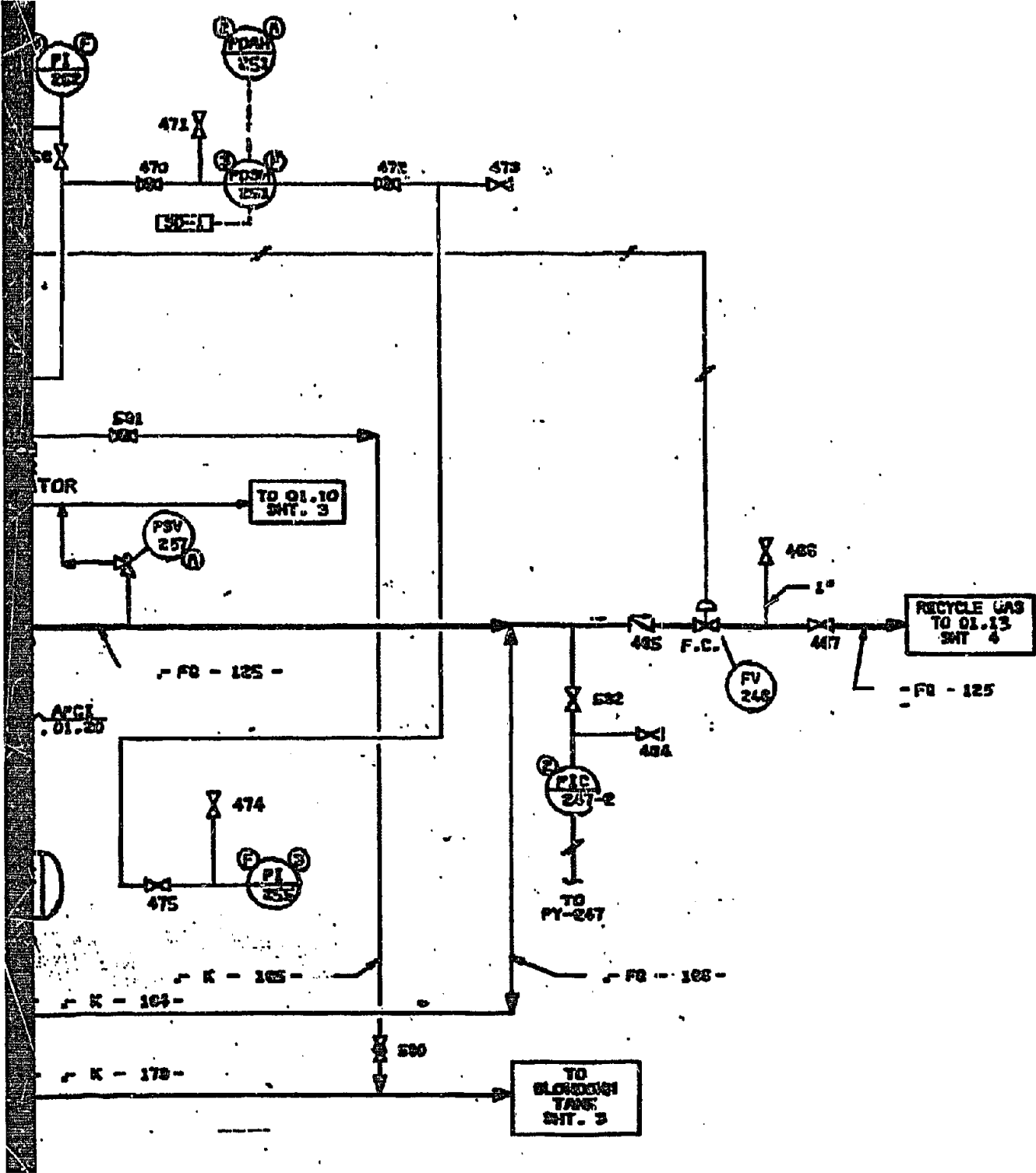
26.10
PRODUCT STORAGE

SHEET 12
P26215

SHEET 13







10.54
(P104)

SHEET 14
P20227

SHEET 15

28.40
WASTE OIL TANK

OIL MAKE-UP PUMP

3/4" N - 510-032.7

HE FLUID
FROM
SHT. 10

X

X

X

TO
20.52A & B
SHT. 11

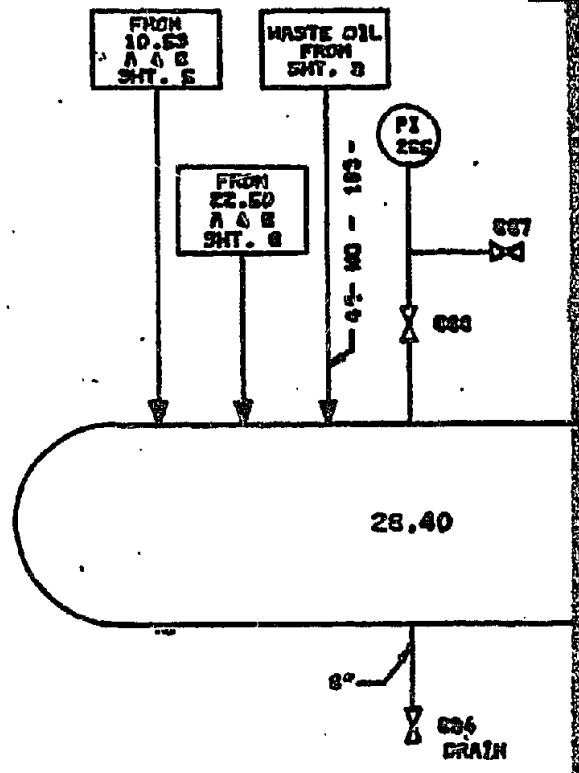
27-UD-102

TO 28.53
SHT. 6

25-UD-137

X

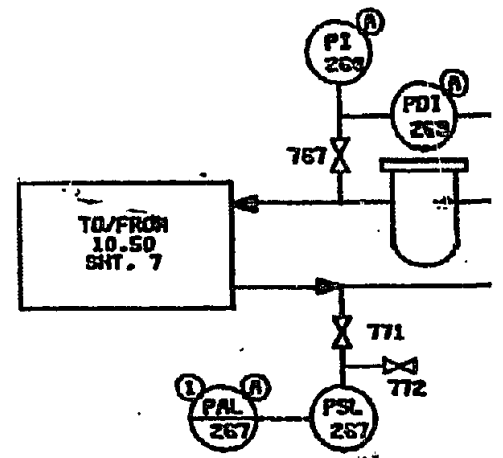
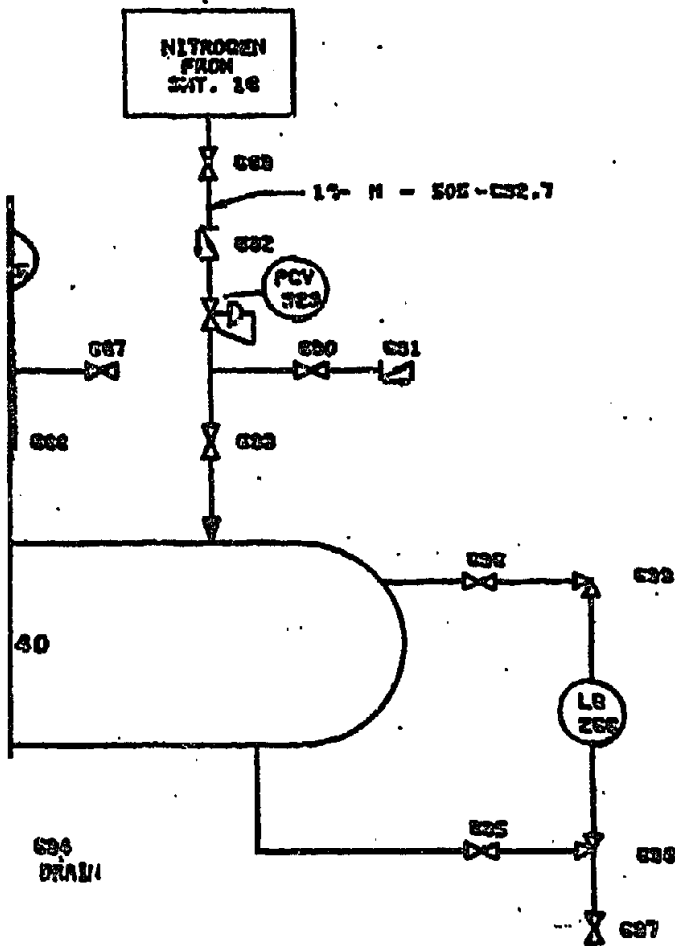
X



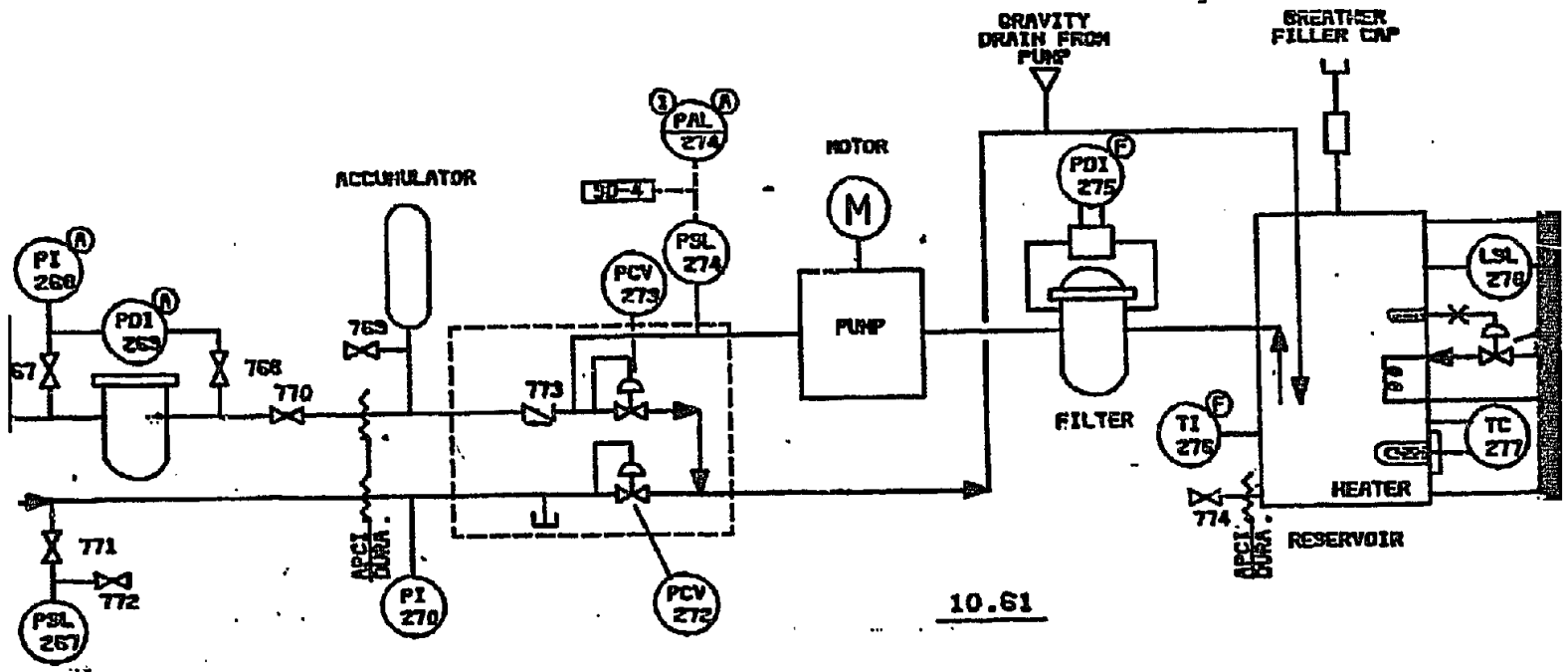


SHEET 15
FC2230

SHEET 16

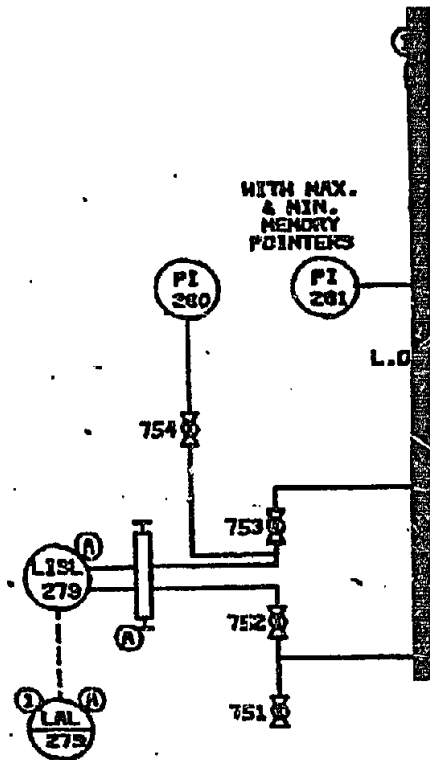
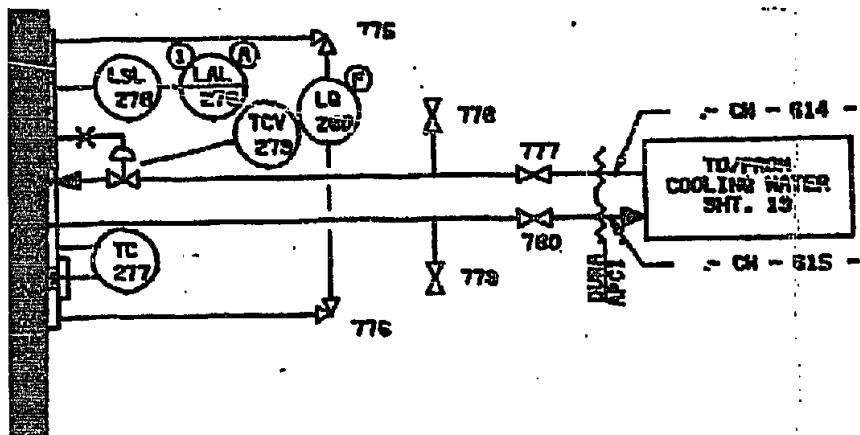


10.61
BARRIER FLUID SYSTEM



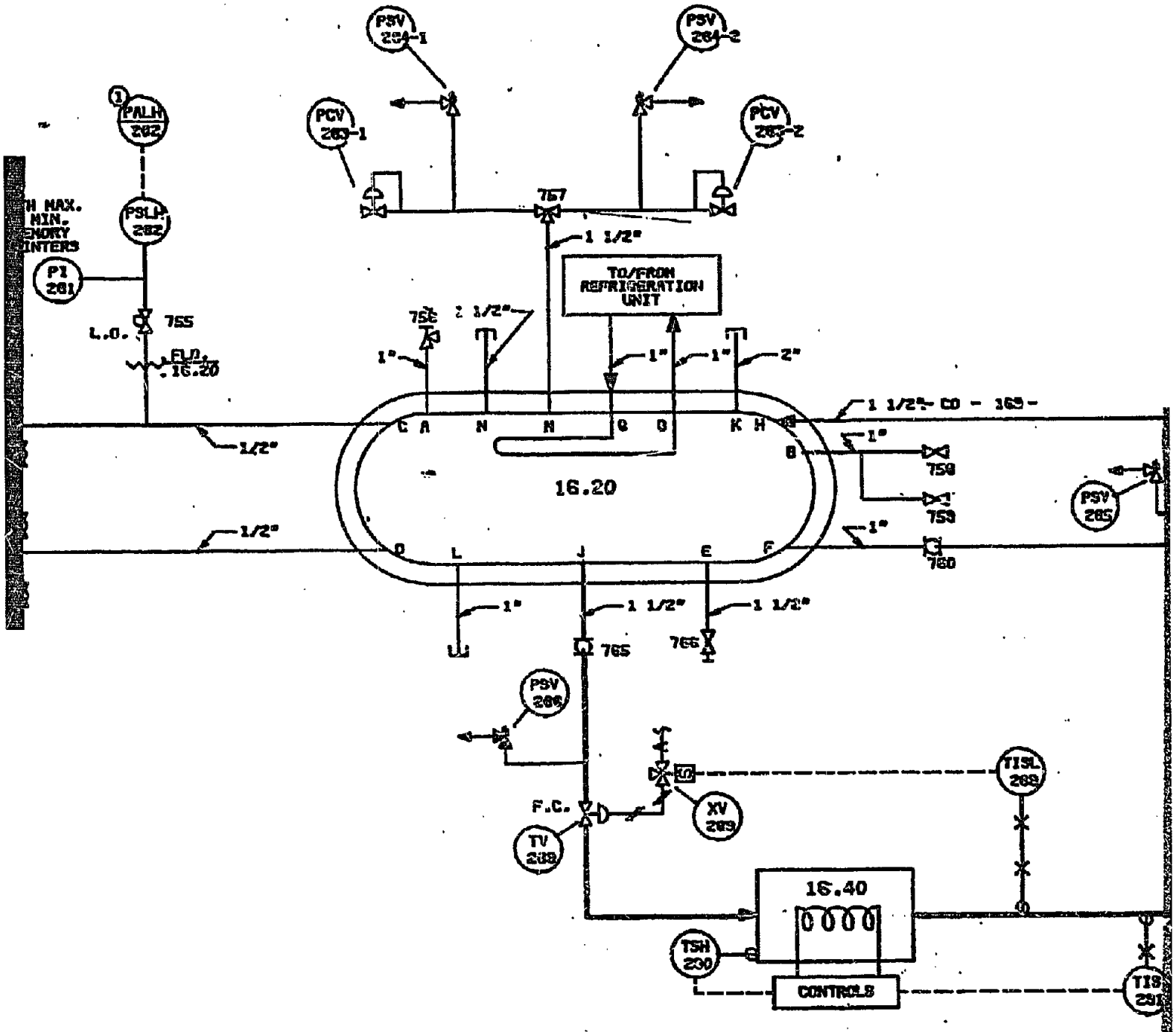
SHEET 16
FD228

SHEET 17



16.20
CO2 STORAGE TANK

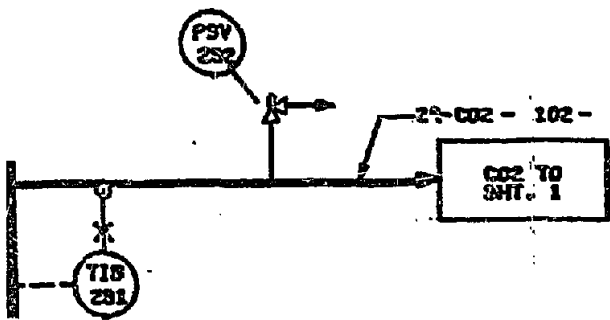
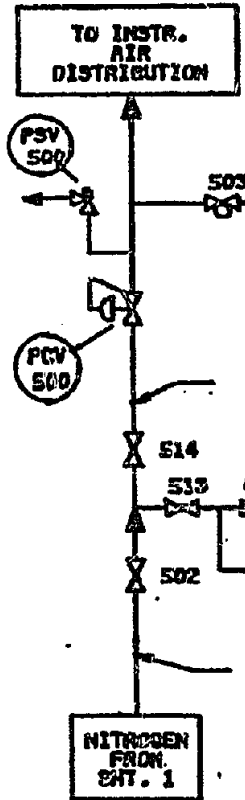
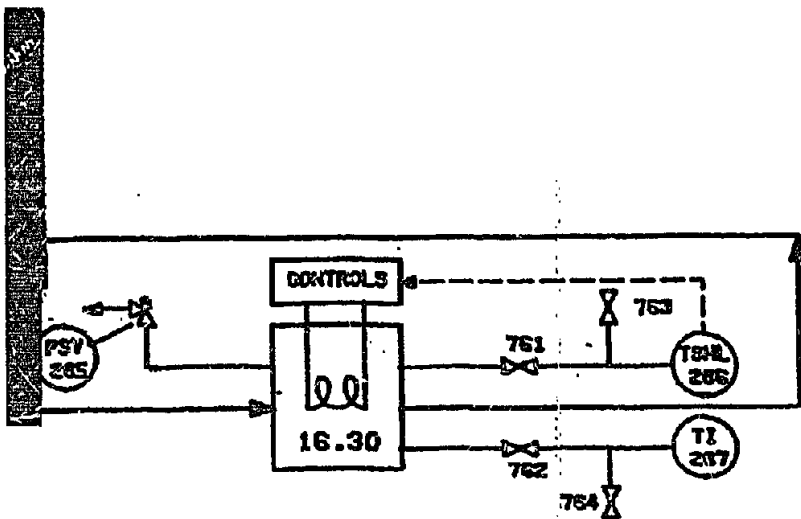
16.40
PRODUCT VAPORIZER



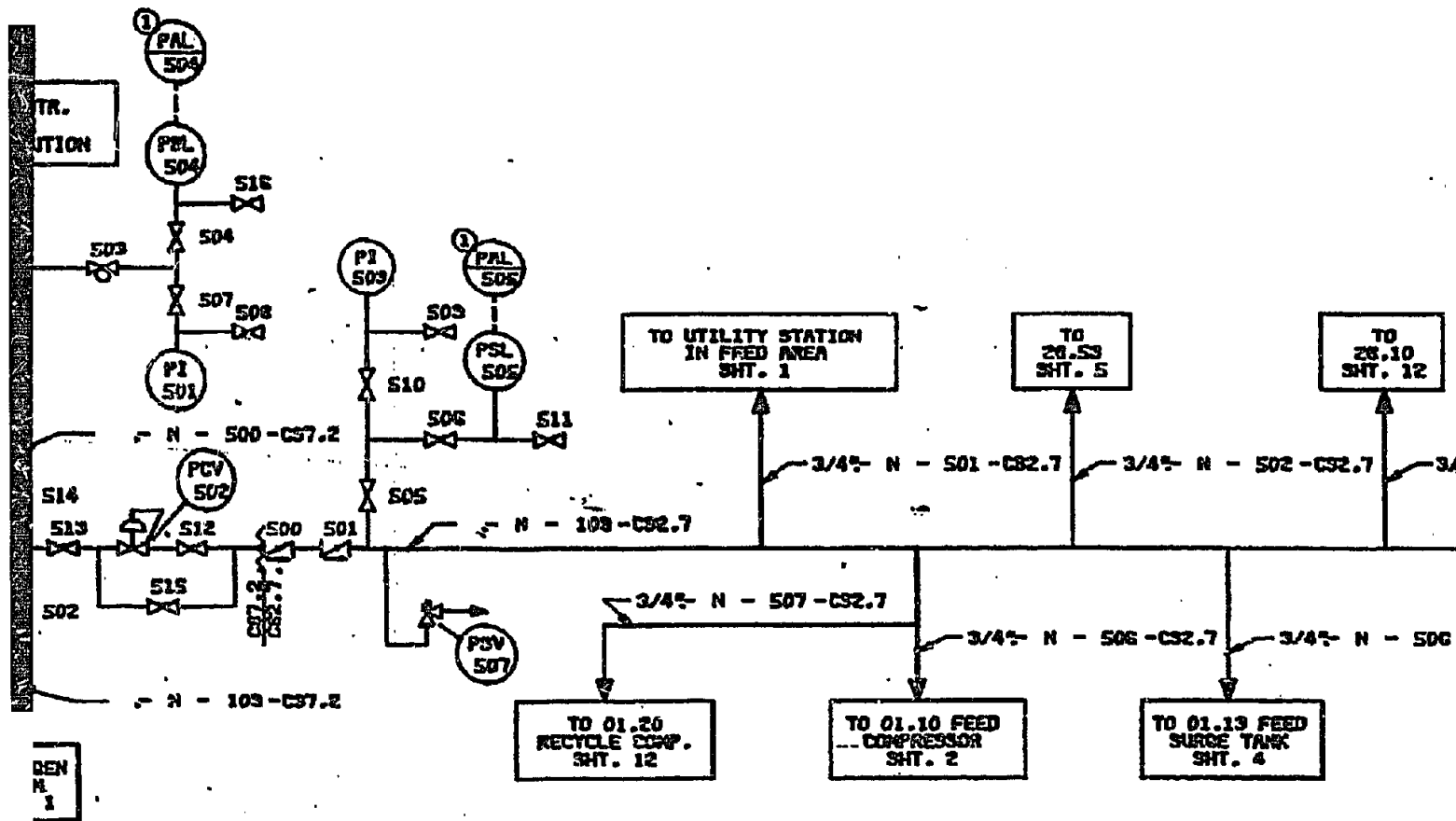
16.30
PRESSURE BUILD-UP
VAPORIZER

SHEET 17
 P20300

SHEET 18



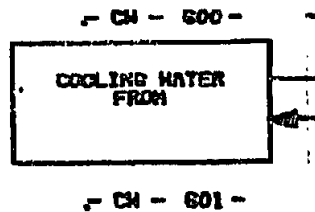
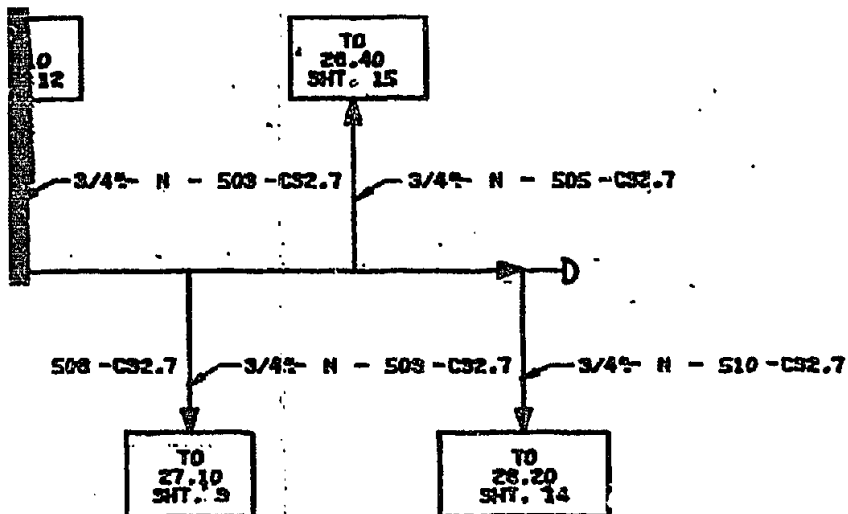
NITROGEN PURGE AND INSTR. AIR SYSTEM



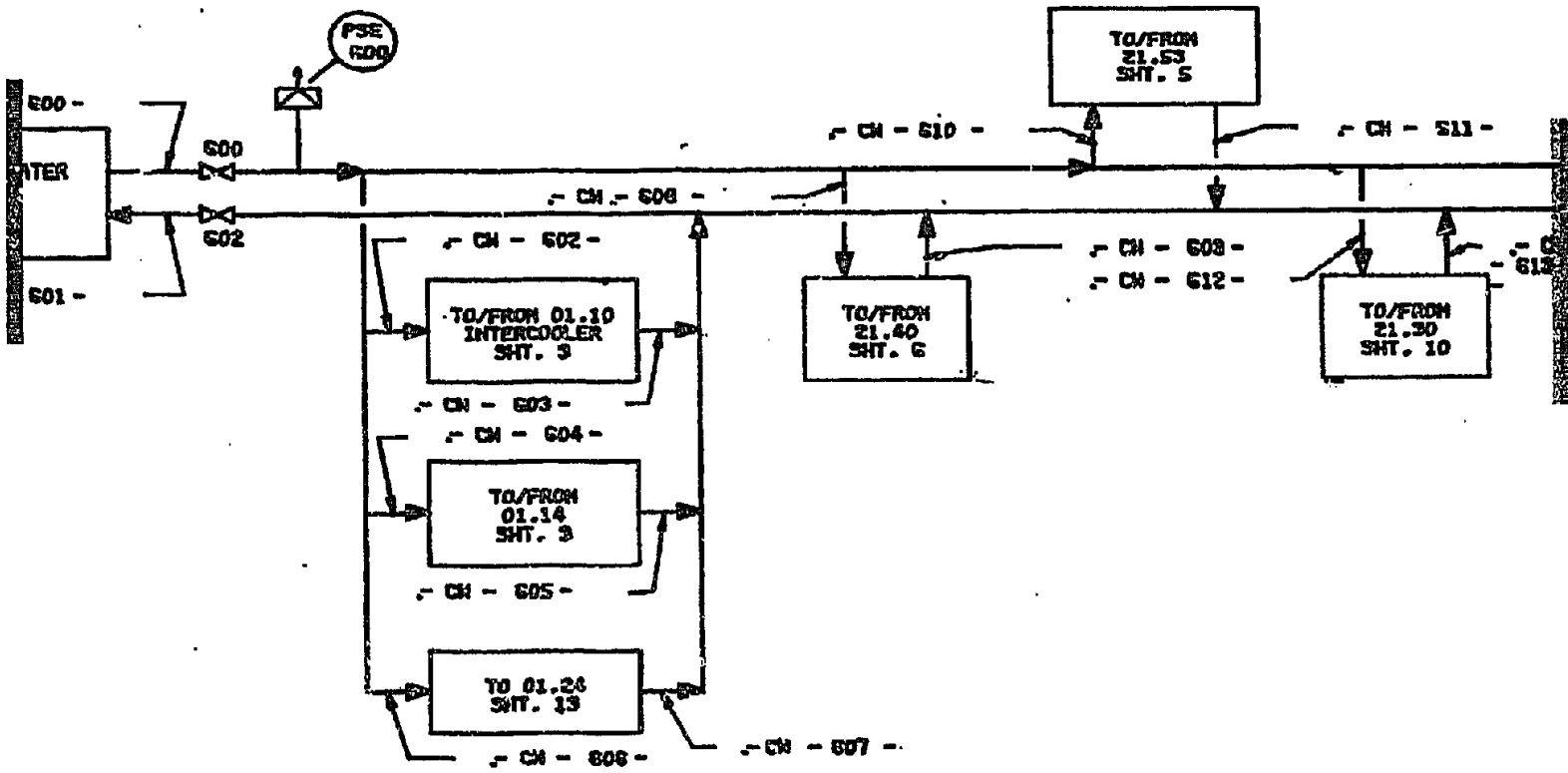
SHEET 18

FE27301

SHEET 19



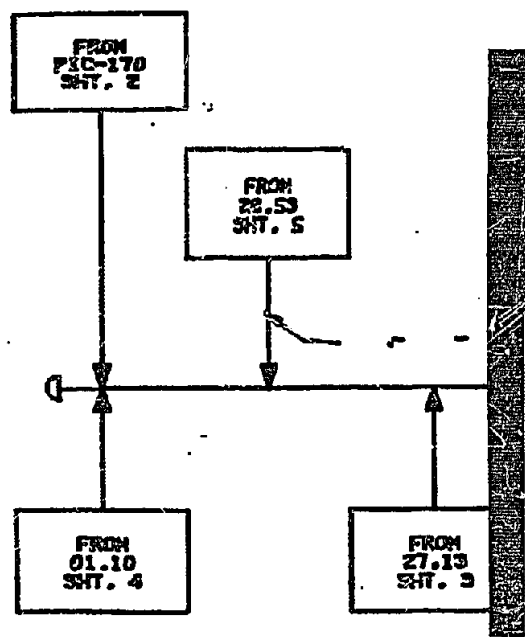
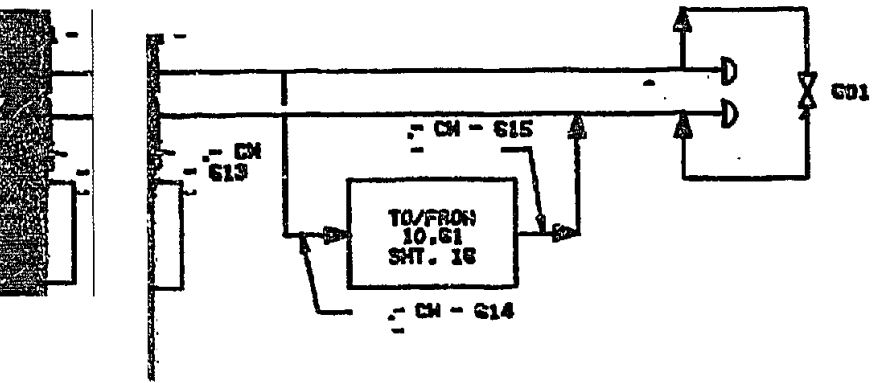
COOLING WATER SYSTEM



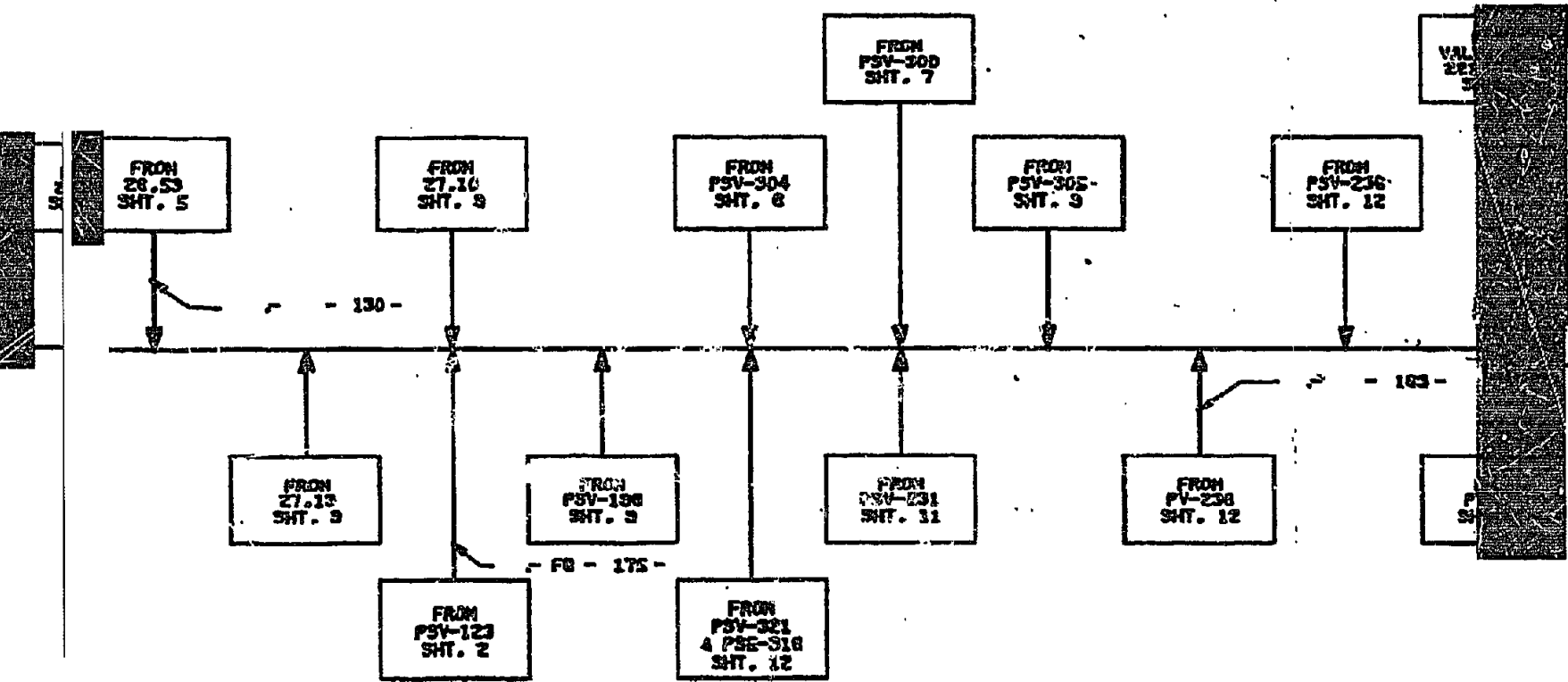
SHEET 19 -

PROJ 02

SHEET 20



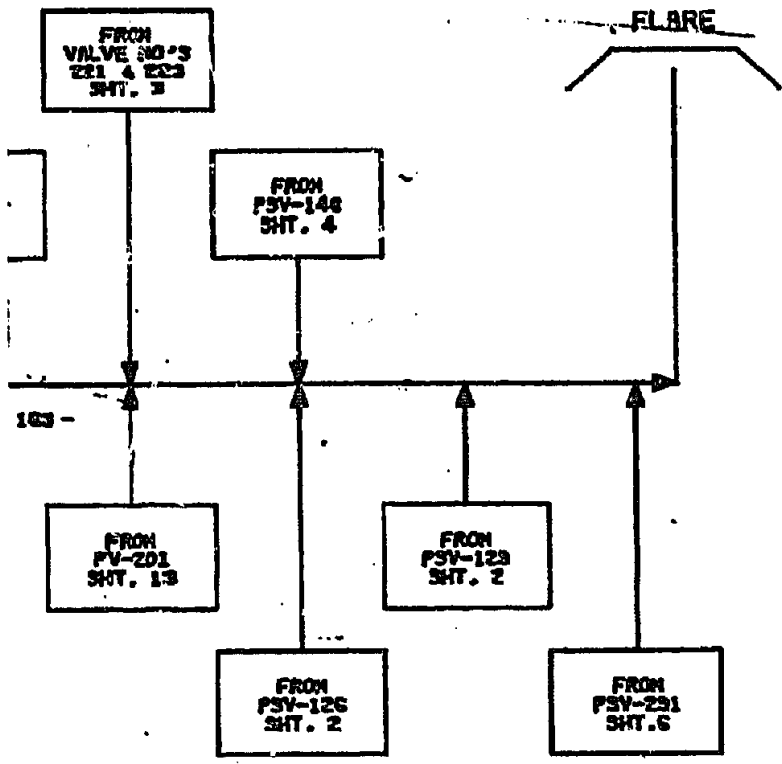
FLARE SYSTEM



END

LIC

U.



NOTE: DUE TO E

REVISION			
NO.	FCN'S	DATE	MA
P1		10MAR82	JK
DA		13APR82	27

2
 SET 20
 720303

ENGINEERING FLOWSHEET

87-7-1533

LIQUID PHASE METHANOL

FOR PRELIMINARY

**U.S. DEPT. OF ENERGY
(D.O.E.)**

LAPORTE, TEXAS

NOTE: DUE TO EXTENSIVE CHANGES THRU-OUT FIS, REV. 0A IS NOT CIRCLED



REVISIONS					APPROVED					
NO.	FCN'S	DATE	MADE	CHK'D	PROCESS	START-UP	OPER.	CHF. ENG.	PROJECT	SAFETY
P1		10MAR82	JK/CE	DRC/DB						
0A		13APR82	SN/JK CB	DRC						

EXHIBIT 2.3.1-3

Design Cases for Liquid-Fluidized Bed:
Operating Conditions for LaPorte LPMeOH PDU

Case No.	Space Velocity 1/hr kg	Press. psig	Temp. °C	Catalyst Bed. Ht. ft	Catalyst Loading kg/l	% CO Conv. (Single pass)	% CH ₃ OH Select. (Single pass)	% CO ₂ Select. (Single pass)	% C ₂ H ₅ OH Select. (Single pass)	Reactor Feed lb-mol/hr	Liq./Vapor Linear Velocity ft/sec	Fresh Feed lb-mol/hr	Recycle Flow lb-mol/hr	Purge Flow lb-mol/hr	MeOH Product Rate SI/D
FB-4930.8	4,000	900	230	7	-	25	98	2	0	247	0.16/0.26	53	194	1	6.5
FL-3750.8	2,500	700	250	7	-	20	98	2	0	155	0.16/0.22	30	125	10	2.6
FK-2750.6	2,000	700	250	7	-	10	83	12	5	124	0.16/0.18	46	78	20	3.3
FK-1570.3	1,000	500	270	7	-	7	83	12	5	61	0.16/0.13	41	20	36	0.5

20 April 1982

EXHIBIT 2.3.1-4

Design Cases for Liquid-Entrained Mode:

Operating Conditions for LaPorte LPMeOH PDU

Case No.	Space Velocity 1/hr kg	Press. psig	Temp. °C	Catalyst Bed. Ht. ft	Catalyst Loading kg/l	%CO Conv. (Single pass)	%CO ₂ Cmb. (Single pass)	%CH ₃ OH Select.	%C ₂ H ₅ OH Select.	%CO ₂ Select.	Reactor Feed lb-Mol/hr	Liq./Vapor Linear Velocity ft/sec	Fresh Feed lb-Mol/hr	Recycle Flow lb-Mol/hr	Purge Flow lb-Mol/hr	MeOH Product Rate ST/D
EB-4954.8	10,000	900	250	-	0.4	30	3	98	2	0	350	0.20/0.40	77	273	0.5	9.7
EL-6752.7	6,000	700	250	-	0.2	24	2	98	2	0	107	0.16/0.15	27	80	10	2.3
EK-4752.7	4,000	700	250	-	0.2	12	0	83	12	5	72	0.16/0.10	22	50	10	1.6
EK-2571.0	2,000	500	270	-	0.1	7	0	83	12	5	18	0.16/0.04	18	0	17	0.2

20 April 1982

EXHIBIT 2.3.1-5

Point-by-point Heat and Mass Balances

STREAM SUMMARY

STREAM NUMBER	1	3	5	8	10	15	18
MOLES - BELOW	44	41.4	41.4	41.4	41.4	44	44
TEMPERATURE PSIA	150.00	370.00	385.00	350.00	350.00	340.00	315.00
TEMPERATURE DEG, F	-163.52	332.47	120.00	377.73	172.82	335.00	285.37
DEN POINT DEG, F						103.75	256.77
ENTHALPY BTU/HR	-1002607.00	-917740.50	-995593.75	-90052.44	-8917937.00	-8506615.00	-8500615.08
VAP. DENSITY LB/CUFT	0.280188	0.484719	0.653734	1.156292	2.151783	1.681300	1.311841
AVE. MOL WT	11.269170	11.269170	11.269170	11.269170	15.603806	15.603806	17.998810
FLOW RATES MOLES/HR							
HYDROGEN	34.000000	34.000000	34.000000	34.000000	122.299988	122.299988	88.684891
CARBON MONOXIDE	15.790000	15.790000	15.790000	15.790000	60.989990	60.989990	45.519417
CARBON DIOXIDE	1.560000	1.560000	1.560000	1.560000	29.399994	29.399994	20.517990
METHANE	0.183000	0.183000	0.183000	0.183000	29.182998	29.182998	29.182998
NITROGEN	1.700000E-02	1.700000E-02	1.700000E-02	1.700000E-02	8.000000E-02	8.000000E-02	7.116998
WATER	0.0	0.0	0.0	0.0	1.700000	1.700000	1.132375
METHANOL	0.0	0.0	0.0	0.0	1.700000	1.700000	1.723800
ETHANOL	0.0	0.0	0.0	0.0	1.100000E-02	1.100000E-02	0.161375
HITCO 40 OIL	0.0	0.0	0.0	0.0	0.0	0.0	0.0
TOTAL FLOW	51.489990	51.489990	51.489990	51.489990	245.980927	245.980927	213.267818
LB/HR	580.249268	580.249268	580.249268	580.249268	3838.238770	3838.238770	3838.206787
ACTUAL CFM	34.515503	19.951385	14.793214	8.363649	29.729126	36.048309	48.763611

STREAMS ARE ALL VAPOR

13

STREAM SUMMARY
VERSION 82.011-A

AIR PRODUCTS & CHEMICALS, INC -- CYCLE SYNTHESIS
LPMEDH FLUIDIZED/BALANCED MAX PRODN: FB-4930

BONHELL
87-7-1533

18JAN.82 PAGE 12
14:30:36

STREAM SUMMARY

T	STREAM NUMBER	75	76	77	78	80	83	84	86	89
0	NOTES - BELOW									
T	PRESSURE PSIA	910.00	900.00	900.00	885.00	885.00	910.00	885.00	945.00	
A	TEMPERATURE DEG.F	445.99	289.09	289.09	110.50	253.24	253.40	253.40	446.98	
L	BUBBLE PT	445.99	289.09	289.09						
	ENTHALPY BTU/HR	-4270976.00	-14636.59	-58546.35	-18563.94	-77390.25	-77372.59	-77372.59	-42492928.00	
	LIQ. DENSITY, LB/CUFT	35.621307	39.297028	39.297089	42.309258	39.922760	39.519159	39.519159	35.596100	
	AVE. MOL WT	204.750865	201.157776	201.157700	194.867208	199.711136	199.711136	199.711136	204.751099	
	FLOW RATES MOLES/HR									
	HYDROGEN	25.687149	6.97505E-03	2.79002E-02	7.60282E-03	3.55038E-02	3.55030E-02	3.55030E-02	25.722661	
	CARBON MONOXIDE	9.073135	2.59079E-03	1.03632E-02	3.18949E-03	1.35266E-02	1.35266E-02	1.35266E-02	9.066667	
	CARBON DIOXIDE	7.011108	3.15333E-03	1.26133E-02	9.22483E-03	2.18380E-02	2.18380E-02	2.18380E-02	7.932948	
	METHANE	8.812714	2.12539E-03	8.50157E-03	3.06183E-03	1.15434E-02	1.15434E-02	1.15434E-02	6.824297	
	NITROGEN	0.892246	2.24536E-04	8.98142E-04	2.22271E-04	1.12041E-03	1.12041E-03	1.12041E-03	0.893367	
	WATER	0.0	2.53446E-10	1.03382E-09	2.76017E-10	1.28983E-09	1.28983E-09	1.28983E-09	1.28983E-09	
	METHANOL	8.203552	3.82507E-03	1.53303E-02	1.79742E-03	1.70977E-02	1.70977E-02	1.70977E-02	8.220658	
	ETHANOL	0.242162	1.22295E-04	4.91702E-04	5.37048E-05	5.45406E-04	5.45406E-04	5.45406E-04	0.242162	
	MITCO 40 OIL	239.534291	7.02553E-02	0.281021	7.72383E-02	0.358259	0.358259	0.358259	239.912537	
	TOTAL FLOW	297.479004	0.889972	0.357089	0.102410	0.459499	0.459499	0.459499	297.938977	
	LB/HR	60911.460938	17.957779	71.831192	19.355944	91.767136	91.767136	91.767136	61003.226563	
			LIQ	LIQ	LIQ	LIQ	LIQ	LIQ	LIQ	

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STREAM SUMMARY
VERSION 82.011-A

AIR PRODUCTS & CHEMICALS, INC -- CYCLE SYNTHESIS
LPMEDH FLUIDIZED/BALANCED MAX PRODN: FB-4930

BONHELL
87-7-1533

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14:30:36

STREAM SUMMARY

T	STREAM NUMBER	90	95
0	NOTES - BELOW		
T	PRESSURE PSIA	82.4	82.4
A	TEMPERATURE DEG.F	945.00	935.00
L	BUBBLE PT	945.00	935.00
	ENTHALPY BTU/HR	446.98	435.53
	LIQ. DENSITY, LB/CUFT	-42491392.00	-42997088.00
	AVE. MOL WT	35.595413	35.882294
	FLOW RATES MOLES/HR	204.752594	204.752594
	HYDROGEN	25.742432	25.742432
	CARBON MONOXIDE	9.089486	9.089486
	CARBON DIOXIDE	7.013533	7.013533
	METHANE	6.825317	6.825317
	NITROGEN	0.893609	0.893609
	WATER	1.37693E-09	1.37693E-09
	METHANOL	8.207340	8.207340
	ETHANOL	0.248345	0.248345
	MITCO 40 OIL	239.926743	239.926743
	TOTAL FLOW	297.948975	297.948975
	LB/HR	61005.824219	61005.824219
		LIQ	LIQ

NOTES

1. STREAM SPECIFIED AS ALL VAPOR
2. STREAM SPECIFIED AS ALL LIQUID
3. STREAM SPECIFIED AS LIQUID
4. STREAM SPECIFIED AS LIQUID PHASES NOT CONSIDERED. *RESULTS MAY BE IN ERROR.

CYCLE SYNTHESIS RUN TIME 1 48.77 CPU SECONDS

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STREAM SUMMARY
VERSION 82.011-A

AIR PRODUCTS & CHEMICALS, INC -- CYCLE SYNTHESIS
LPMEDH FLUIDIZED/LURGI: FL-3750

T.R.TSAD
87-7-1533

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13:35:05

STREAM SUMMARY

STREAM NUMBER	1	3	5	8	10	14	15	18
NOTES - BELOW								
PRESSURE PSIA	81.4	81.4	81.4	81.4	81.4	81.4	81.4	81.4
TEMPERATURE DEG.F	150.00	370.00	335.00	750.00	750.00	740.00	740.00	715.00
DEW POINT	180.00	326.13	120.00	326.56	165.61	395.00	307.00	617.21
ENTHALPY BTU/HR	-717935.00	-668495.00	-713853.13	-668406.06	-5162945.00	-4880366.00	-4880366.00	191.60
VAP. DENSITY, LB/CUFT	0.30386	0.591136	0.665971	1.083788	1.665792	1.393227	1.393227	1.091349
AVE. MOL WT	12.470467	12.470467	12.470467	12.470467	15.071447	15.071447	15.071447	16.469866
FLOW RATES								
HYDROGEN	18.19997	18.19997	18.19997	18.19997	77.121994	77.121994	77.121994	63.627666
CARBON MONOXIDE	8.65899	8.65899	8.65899	8.65899	38.288986	38.288986	38.288986	32.00631
CARBON DIOXIDE	1.51000	1.51000	1.51000	1.51000	15.68999	15.68999	15.68999	15.180199
METHANE	1.91000	1.91000	1.91000	1.91000	21.50999	21.50999	21.50999	21.50999
NITROGEN	0.11000	0.11000	0.11000	0.11000	1.50999	1.50999	1.50999	1.50999
WATER	0.0	0.0	0.0	0.0	4.20000E-02	4.20000E-02	4.20000E-02	0.22466
METHANOL	0.0	0.0	0.0	0.0	1.32000	1.32000	1.32000	7.787521
ETHANOL	0.0	0.0	0.0	0.0	8.50000E-03	8.50000E-03	8.50000E-03	8.08662E-02
MTCD 40 OIL	0.0	0.0	0.0	0.0	6.10000E-05	6.10000E-05	6.10000E-05	6.10000E-05
TOTAL FLOW	30.108963	30.108963	30.108963	30.108963	155.291458	155.291458	155.291458	142.106964
LB/HR	375.472656	375.472656	375.472656	375.472656	2340.466797	2340.466797	2340.466797	2340.454102
ACTUAL CFM	20.161575	11.564336	9.396616	5.774079	23.416962	32.690170	32.690170	38.955502

STREAMS ARE ALL VAPOR

STREAM SUMMARY

STREAM NUMBER	50	54	55	57	60	62	65
NOTES - BELOW							
PSIA	685.00	685.00	685.00	750.00	685.00	70.00	20.00
TEMPERATURE DEG.F	189.98	189.98	189.98	129.76	189.98	189.26	189.26
DEW POINT DEG.F							
BUBBLE PT DEG.F							
ENTHALPY BTU/HR							
LIQ. DENSITY, LB/CUFT	-358442.19	-4514830.00	-4533183.00	-6494540.00	-758303.94	-22203.65	-732399.88
VAP. DENSITY, LB/CUFT	0.0	0.0	0.0	0.0	49.171310	0.0	49.669852
AVE. MOL WT	1.756322	1.756322	1.756178	1.852674	0.0	0.194757	0.0
FLOW RATES MOLES/HR	15.698313	15.698315	15.697038	15.697038	31.333771	31.444412	31.330307
HYDROGEN	4.676510	58.930359	58.921997	58.921997	2.242005-02	2.222995-02	1.900795-04
CARBON MONOXIDE	2.352649	29.633255	29.629990	29.629990	2.107495-02	2.076395-02	3.118785-04
CARBON DIOXIDE	1.188875	13.957064	13.959999	13.959999	0.106690	9.263995-02	1.405095-02
METHANE	1.580015	19.901382	19.899994	19.899994	2.998275-02	2.972775-02	3.558585-04
NITROGEN	0.111035	1.400000	1.400000	1.400000	8.100195-04	7.998995-04	1.013385-05
WATER	3.313145-03	4.200005-02	4.200005-02	4.200005-02	0.629122	1.709315-03	0.627712
METHANOL	0.705056	1.352254	1.350000	1.350000	6.331405	5.317925-02	6.820223
ETHANOL	6.725425-04	8.471145-03	8.500005-03	8.500005-03	7.377231-02	3.275965-04	7.144475-02
MITCO 40 OIL	4.659795-06	6.121255-05	6.100005-05	6.100005-05	1.227045-02	2.115095-06	1.226835-02
TOTAL FLOW MOL/HR	9.940230	125.204132	125.182495	125.182495	7.225545	0.218778	7.006766
LB/HR	156.044830	1965.493652	1964.994141	1964.994141	226.403564	6.879342	219.524139
ACTUAL CFM	1.480792	18.651596	18.648468	17.677094	0.0	1.094601	0.0
	VAP	VAP	VAP	VAP	L1Q	VAP	L1Q

STREAM SUMMARY
VERSION 82.011-A

AIR PRODUCTS & CHEMICALS, INC --- CYCLE SYNTHESIS
LPNEON FLUIDIZED/LURGI: FL-3750

I.R. ISAAC
87-7-1533

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STREAM SUMMARY

T	STREAM NUMBER	75	76	77	78	80	83	84	89
0	NOTES - BELOW								
1	PRESSURE PSIA	719.00	700.00	700.00	685.00	62.4	62.4	64	85
2	TEMPERATURE DEG.F	481.96	235.19	235.19	109.98	685.00	710.00	745.00	745.00
3	BUBBLE PT	481.96	235.19	235.19	109.98	244.68	244.74	682.68	682.68
4	ENTHALPY BTU/HR	-3580064.00	-20921.84	-8337.31	-23807.32	-107534.63	-107510.19	-35857904.00	-35857904.00
5	LIQ. DENSITY, LB/CUFT	35.893881	40.517090	40.517090	49.171110	41.107925	41.106659	38.674457	38.674457
6	LIQ. DENSITY, LB/CUFT	0.0	0.0	0.0	43.605042	0.0	0.0	0.0	0.0
7	AVE. MOL WT	216.936737	214.947617	214.947586	210.014771	213.943176	213.943176	216.929489	216.929489
8	FLOW RATES								
9	HYDROGEN	16.585297	7.195386-03	2.87812E-02	6.85064E-03	3.56318E-02	3.56318E-02	16.520926	16.520926
10	CARBON MONOXIDE	6.341644	2.86773E-03	1.14709E-02	2.99718E-03	1.44881E-02	1.44881E-02	6.356112	6.356112
11	CARBON DIOXIDE	3.526520	2.87958E-03	1.15183E-02	6.91237E-03	1.84307E-02	1.84307E-02	3.544950	3.544950
12	METHANE	4.940521	2.49824E-03	9.92965E-03	3.96608E-03	1.3070E-02	1.3070E-02	4.953578	4.953578
13	NITROGEN	0.596059	2.31603E-04	9.26410E-04	1.97252E-04	1.12366E-03	1.12366E-03	0.597182	0.597182
14	WATER	0.0	5.11224E-11	2.04490E-10	5.33963E-11	2.57866E-10	2.57866E-10	2.57866E-10	2.57866E-10
15	METHANOL	3.373138	2.62218E-03	1.04887E-02	1.77319E-03	1.22619E-02	1.22619E-02	3.385440	3.385440
16	ETHANOL	9.91564E-02	8.82677E-05	3.41071E-04	4.99228E-05	3.90993E-04	3.90993E-04	9.95473E-02	9.95473E-02
17	MIXCO 40 JIL	215.290146	0.112551	0.410203	0.101836	0.512038	0.512038	215.802170	215.802170
18	TOTAL FLOW	250.752319	0.120950	0.483722	0.123580	0.607403	0.607403	251.359711	251.359711
19	LB/HR	54397.386719	25.993713	103.974915	25.974701	129.949646	129.949646	54527.352831	54527.352831
20		LIQ	LIQ	LIQ	LIQ	LIQ	LIQ	LIQ	LIQ

STREAM SUMMARY
VERSION 82.011-A

AIR PRODUCTS & CHEMICALS, INC --- CYCLE SYNTHESIS
LPNEON FLUIDIZED/LURGI: FL-3750

I.R. ISAAC
87-7-1533

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STREAM SUMMARY

T	STREAM NUMBER	90	95	95	95	95	95	95	95
0	NOTES - BELOW								
1	PRESSURE PSIA	82.4	84	84	735.00	735.00	735.00	735.00	735.00
2	TEMPERATURE DEG.F	745.00	745.00	745.00	478.16	478.16	478.16	478.16	478.16
3	BUBBLE PT	745.00	745.00	745.00	478.16	478.16	478.16	478.16	478.16
4	ENTHALPY BTU/HR	-35859136.00	-36064400.00	-36064400.00	-36064400.00	-36064400.00	-36064400.00	-36064400.00	-36064400.00
5	LIQ. DENSITY, LB/CUFT	35.673785	35.596376	35.596376	35.596376	35.596376	35.596376	35.596376	35.596376
6	LIQ. DENSITY, LB/CUFT	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
7	AVE. MOL WT	216.930008	216.930008	216.930008	216.930008	216.930008	216.930008	216.930008	216.930008
8	FLOW RATES								
9	HYDROGEN	16.624664	16.624664	16.624664	16.624664	16.624664	16.624664	16.624664	16.624664
10	CARBON MONOXIDE	6.356624	6.356624	6.356624	6.356624	6.356624	6.356624	6.356624	6.356624
11	CARBON DIOXIDE	3.547398	3.547398	3.547398	3.547398	3.547398	3.547398	3.547398	3.547398
12	METHANE	4.955025	4.955025	4.955025	4.955025	4.955025	4.955025	4.955025	4.955025
13	NITROGEN	0.597591	0.597591	0.597591	0.597591	0.597591	0.597591	0.597591	0.597591
14	WATER	2.64869E-10	2.64869E-10	2.64869E-10	2.64869E-10	2.64869E-10	2.64869E-10	2.64869E-10	2.64869E-10
15	METHANOL	3.377596	3.377596	3.377596	3.377596	3.377596	3.377596	3.377596	3.377596
16	ETHANOL	9.95973E-02	9.95973E-02	9.95973E-02	9.95973E-02	9.95973E-02	9.95973E-02	9.95973E-02	9.95973E-02
17	MIXCO 40 OIL	215.814484	215.814484	215.814484	215.814484	215.814484	215.814484	215.814484	215.814484
18	TOTAL FLOW	251.372940	251.372940	251.372940	251.372940	251.372940	251.372940	251.372940	251.372940
19	LB/HR	54530.332031	54530.332031	54530.332031	54530.332031	54530.332031	54530.332031	54530.332031	54530.332031
20		LIQ	LIQ	LIQ	LIQ	LIQ	LIQ	LIQ	LIQ

NOTES

1. STREAM SPECIFIED AS ALL VAPOR
2. STREAM SPECIFIED AS ALL LIQUID
3. STREAM SPECIFIED AS LIQUID
4. CAUTION: TWO LIQUID PHASES NOT CONSIDERED. RESULTS MAY BE IN ERROR.

CYCLE SYNTHESIS RUN TIME : 27.71 CPU SECONDS

AIR PRODUCTS & CHEMICALS, INC -- CYCLE SYNTHESIS
LFMEGR FLUIDIZED/KT GAS: FK-2750

STREAM SUMMARY
VERSION 82.011-A

STREAM SUMMARY

	1	3	5	8	10	15	85	18
T	81.4	81.4	81.4	81.4	81.4	81.4	81.4	81.4
O	160.00	170.00	335.00	750.00	750.00	740.00	715.00	715.00
T	100.00	335.22	120.00	335.01	205.17	402.00	863.18	863.18
A						102.65	213.97	213.97
L								
	-1090524.00	-1013961.19	-1086395.00	-1013960.75	-3919410.00	-3730897.80	-3730897.00	-3730897.00
	0.370634	0.838305	0.798542	1.378420	1.915168	1.453766	1.071272	1.071272
	14.898660	14.898660	14.898660	14.898660	18.584152	18.584152	21.700775	21.700775
	23.477997	23.477997	23.477997	23.477997	47.093994	47.093994	29.586212	29.586212
	22.709991	22.709991	22.709991	22.709991	74.479856	74.479856	64.969127	64.969127
	0.104560	0.104560	0.104560	0.104560	2.389560	2.389560	2.894155	2.894155
	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.126280	0.126280	0.126280	0.126280	0.622280	0.622280	0.622280	0.622280
	0.0	0.0	0.0	0.0	2.65000E-03	2.65000E-03	0.106221	0.106221
	0.0	0.0	0.0	0.0	0.792000	0.792000	8.581861	8.581861
	0.0	0.0	0.0	0.0	3.40000E-02	3.40000E-02	0.642166	0.642166
	0.0	0.0	0.0	0.0	4.00000E-05	4.00000E-05	4.00000E-05	4.00000E-05
	46.418808	46.418808	46.418808	46.418808	125.414229	125.414229	107.402059	107.402059
	691.577881	691.577881	691.577881	691.577881	2330.720703	2330.720703	2330.708008	2330.708008
	31.097229	18.052017	14.501365	9.014642	28.277908	26.720474	36.560757	36.560757
	TOTAL FLOW							
	MOLES/HR							
	LB/HR							
	ACTUAL CFM							

STREAMS ARE ALL VAPOR

STREAM SUMMARY

STREAM NUMBER	20	25	30	32	35	38	45
NOTES - BELOW							
PRESSURE PSIA	715.00	710.00	700.00	700.00	690.00	690.00	685.00
TEMPERATURE DEG. F	482.00	481.99	300.40	300.40	110.00	100.00	111.00
DEW POINT DEG. F		481.99		300.40			
ENTHALPY BTU/HR	-40066560.00	-4125196.00	-4304907.00	-4228292.00	-5520251.00	-85764.81	-3646817.00
AVE. MOL WT	158.836838	22.543457	22.543457	21.726912	21.692380	18.819989	20.751114
FLOW RATES MOLES/HR							
HYDROGEN	61.689316	29.617172	29.617172	29.598190	29.601975	0.0	29.577698
CARBON MONOXIDE	81.575775	65.001281	65.001281	64.975113	64.980763	0.0	64.885666
CARBON DIOXIDE	3.777861	2.893759	2.893759	2.893380	2.893797	0.0	2.895729
METHANE	0.0	0.0	0.0	0.0	0.0	0.0	0.0
NITROGEN	0.964322	0.622295	0.622295	0.622425	0.622587	0.8	0.621776
WATER	0.106221	0.106221	0.106221	0.106221	0.106221	0.0	3.50370E-02
METHANOL	13.375243	8.583569	8.583569	8.571045	8.573549	0.0	0.992185
ETHANOL	1.680047	0.629762	0.629762	0.626860	0.627540	0.0	4.27914E-02
MITCO 40 OIL	215.770205	0.400970	0.400970	1.63629E-02	9.32842E-02	0.0	5.00636E-05
TOTAL FLOW LB/HR	358.939697	107.859680	107.859680	107.409546	107.499557	0.700000	99.008881
	57012.843750	2431.530029	2431.530029	2333.892578	2353.620598	12.613992	2054.544434

LIQUID	20	25	30	32	35	38	45
ENTHALPY BTU/HR	-35933328.00	0.0	-76655.06	0.0	-882112.69	-85768.81	0.0
LIQ. DENSITY LB/CUFT	35.634705	0.0	40.271378	0.0	0.0	61.967270	0.0
AVE. MOL WT	217.098236	0.0	216.758682	0.0	35.137390	18.019989	0.0
FLOW RATES MOLES/HR							
HYDROGEN	12.220123	0.0	1.90802E-02	0.0	2.72869E-02	0.0	0.0
CARBON MONOXIDE	16.737791	0.0	2.83057E-02	0.0	0.120097	0.0	0.0
CARBON DIOXIDE	0.890105	0.0	2.46237E-03	0.0	4.28258E-02	0.0	0.0
METHANE	0.0	0.0	0.0	0.0	0.0	0.0	0.0
NITROGEN	0.344284	0.0	5.13016E-04	0.0	9.55664E-04	0.0	0.0
WATER	0.0	0.0	4.25167E-11	0.0	0.100997	0.700000	0.0
METHANOL	4.827169	0.0	1.25523E-02	0.0	7.531105	0.0	0.0
ETHANOL	1.055299	0.0	2.91941E-03	0.0	0.584268	0.0	0.0
MITCO 40 OIL	215.374146	0.0	0.386658	0.0	9.32842E-02	0.0	0.0
TOTAL LIQ. LB/HR	251.448792	0.0	8.450531	0.0	8.502769	0.700000	0.0
	54559.085938	0.0	97.656494	0.0	298.764893	12.613992	0.0

LIQUID	20	25	30	32	35	38	45
ENTHALPY BTU/HR	0.0	0.0	0.0	0.0	-875358.25	0.0	0.0
LIQ. DENSITY LB/CUFT	0.0	0.0	0.0	0.0	47.795700	0.0	0.0
AVE. MOL WT	0.0	0.0	0.0	0.0	34.386841	0.0	0.0
FLOW RATES MOLES/HR							
HYDROGEN	0.0	0.0	0.0	0.0	2.58702E-02	0.0	0.0
CARBON MONOXIDE	0.0	0.0	0.0	0.0	0.117777	0.0	0.0
CARBON DIOXIDE	0.0	0.0	0.0	0.0	4.23272E-02	0.0	0.0
METHANE	0.0	0.0	0.0	0.0	0.0	0.0	0.0
NITROGEN	0.0	0.0	0.0	0.0	9.21017E-04	0.0	0.0
WATER	0.0	0.0	0.0	0.0	0.100997	0.0	0.0
METHANOL	0.0	0.0	0.0	0.0	7.530669	0.0	0.0
ETHANOL	0.0	0.0	0.0	0.0	0.584268	0.0	0.0
MITCO 40 OIL	0.0	0.0	0.0	0.0	6.33769E-02	0.0	0.0

STREAM SUMMARY

	50	54	55	57	60	62	65
T							
O							
F							
A							
L							
STREAM NUMBER	#4	#4	#1	#1,4		#4	#4
MOLES - BELOW	685.00	685.00	685.00	750.00	685.00	108.96	20.00
PRESSURE PSIA	111.00	111.00	111.00	132.13	111.00	108.96	108.96
TEMPERATURE DEG,F							
DEW POINT DEG,F							
BUBBLE PT DEG,F							
ENTHALPY BTU/HR	-736400.61	-2910415.00	-2916312.00	-2866450.00	-950767.88	-13649.44	-937117.88
LIQ DENSITY, LB/CUFT	0.0	0.0	0.0	0.0	49.157944	8.0	49.557159
LIQ DENSITY, LB/CUFT	0.0	0.0	0.0	0.0	49.157944	8.0	0.0
VAP DENSITY, LB/CUFT	2.304755	2.304755	2.304525	2.424841	0.0	8.095037	0.0
AVE MOL WT	20.751129	20.751114	20.749802	20.749802	32.097534	28.829468	32.167007
FLOW RATES							
MOLES/HR							
HYDROGEN	5.973616	23.608072	23.615997	21.615997	2.07488E-02	2.05670E-02	1.81817E-04
CARBON MONOXIDE	13.102345	51.783310	51.789989	51.789989	8.92987E-02	8.78515E-02	1.84315E-03
CARBON DIOXIDE	0.576657	2.279072	2.285000	2.285000	3.68308E-02	3.08597E-02	6.77103E-03
METHANE	0.0	0.0	0.0	0.0	0.0	0.0	0.0
NITROGEN	0.12555	0.496221	0.496000	0.496000	7.24909E-04	7.12430E-04	1.24788E-05
WATER	6.67114E-03	2.63658E-02	2.65000E-03	2.65000E-03	0.773184	1.75075E-03	8.771433
METHANOL	0.200352	0.791834	0.792000	0.792000	7.580351	4.68016E-02	7.533649
ETHANOL	8.64085E-03	3.41505E-02	3.40000E-02	3.40000E-02	0.584433	2.84483E-03	0.582408
ITCO 40 OIL	1.01093E-05	3.99542E-05	4.00000E-05	4.00000E-05	1.70170E-02	2.04794E-06	1.70150E-02
TOTAL FLOW	19.992928	79.014022	78.995621	78.995621	9.102602	0.189490	8.913112
LB/HR	414.873535	1639.620410	1639.143311	1639.143311	292.170898	5.462889	286.708003
ACTUAL CFM	3.000121	11.857155	11.854526	11.854526	0.0	0.957997	0.0
	VAP	VAP	VAP	VAP	LIQ	VAP	LIQ

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STREAM SUMMARY
VERSION 82.011-A

AIR PRODUCTS & CHEMICALS, INC -- CYCLE SYNTHESIS
LPMEGH FLUIDIZED/KT GAS: FK-2750

T.R. TSAD
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STREAM SUMMARY

	75	76	77	78	80	83	84	89
T	84	84	700.00	685.00	62.4	710.00	745.00	
NOTES - BELOW								
PRESSURE PSIA	710.00	700.00	700.00	685.00	62.4	710.00	745.00	
TEMPERATURE DEG.F	481.99	300.40	300.40	111.00	265.80	265.86	482.86	
BUBBLE PT	481.99	300.40						
ENTHALPY BTU/HR	-3592136.00	-15321.54	-61286.13	-17209.13	-78495.25	-78476.94	-35950400.00	
LIQ. DENSITY LB/CUFT	35.657761	40.282776	40.282776	49.157944	41.073166	41.071793	35.654506	
LIQ2 DENSITY LB/CUFT	0.0	0.0	0.0	44.420074	0.0	0.0	0.0	
AVE. MOL WT	217.386124	216.906281	216.906265	219.465149	217.408966	217.408966	217.386154	
FLOW RATES								
HYDROGEN	12.07214	3.79392E-03	1.51757E-02	3.51491E-03	1.86906E-02	1.86906E-02	12.090834	
CARBON MONOXIDE	16.572495	5.63329E-03	2.25332E-02	5.77578E-03	2.83090E-02	2.83090E-02	16.600810	
CARBON DIOXIDE	0.882122	4.90130E-04	1.96052E-03	1.23642E-03	3.19694E-03	3.19694E-03	0.885319	
METHANE	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
NITROGEN	0.341397	1.02087E-04	4.08348E-04	8.63717E-05	4.94720E-04	4.94720E-04	0.341891	
WATER	0.0	4.39855E-12	3.45942E-11	1.45482E-11	4.81823E-11	4.81823E-11	0.0	
ETHANOL	4.791679	2.56470E-03	1.00148E-02	1.01235E-03	1.10310E-02	1.10310E-02	4.802710	
METHANOL	1.038284	5.88516E-04	2.32266E-03	1.95491E-04	2.51800E-03	2.51800E-03	1.952802	
WITCO 40 OIL	215.369934	7.69213E-02	0.307686	7.62171E-02	0.3583903	0.3583903	215.753830	
TOTAL FLOW	251.080017	0.090026	0.360104	0.088039	0.448143	0.448143	251.528152	
LB/HR	54581.308594	19.527191	76.108841	19.321411	97.430267	97.430267	54678.734373	
	LIQ	LIQ	LIQ	LIQ2	LIQ	LIQ	LIQ	

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STREAM SUMMARY
VERSION 82.011-A

AIR PRODUCTS & CHEMICALS, INC -- CYCLE SYNTHESIS
LPMEGH FLUIDIZED/KT GAS: FK-2750

T.R. TSAD
87-7-1513

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STREAM SUMMARY

	90	95
T	84	84
NOTES - BELOW		
PRESSURE PSIA	745.00	735.00
TEMPERATURE DEG.F	482.86	473.67
ENTHALPY BTU/HR	-35950592.00	-36335666.00
LIQ. DENSITY LB/CUFT	35.633942	35.871840
AVE. MOL WT	217.391464	217.391464
FLOW RATES		
HYDROGEN	12.103110	12.103110
CARBON MONOXIDE	16.606598	16.606598
CARBON DIOXIDE	0.883726	0.883726
METHANE	0.0	0.0
NITROGEN	0.342112	0.342112
WATER	4.67067E-11	4.67067E-11
ETHANOL	4.793387	4.793387
METHANOL	1.037881	1.037881
WITCO 40 OIL	215.770874	215.770874
TOTAL FLOW	251.537643	251.537643
LB/HR	54682.132813	54682.132813
	LIQ	LIQ

NOTES

1. STREAM SPECIFIED AS ALL VAPOR
2. STREAM SPECIFIED AS ALL LIQUID
3. CAUTION: TWO LIQUID PHASES NOT CONSIDERED. *RESULTS MAY BE IN ERROR.

CYCLE SYNTHESIS RUN TIME : 41.56 CPU SECONDS

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STREAM SUMMARY

T	STREAM NUMBER	1	3	5	8	10	15	18
0	MOLES - BELOW	150.00	207.00	282.00	550.00	550.00	540.00	515.00
1	PRESSURE PSIA	100.00	261.91	120.00	293.27	241.01	503.00	717.84
2	TEMPERATURE DEG.F							136.80
3	DEW POINT DEG.F							-1808823.00
4	ENTHALPY BTU/HR	-1269828.00	-1222889.00	-1264395.00	-121707.00	-1928855.00	-1808823.00	0.797885
5	VAP. DENSITY, LB/CUFT	0.448639	0.663482	0.813572	1.208411	1.339336	0.953338	19.873077
6	AVE. MOL WT	18.050034	18.050034	18.050034	18.050034	18.544342	18.544342	19.873077
7	FLOW RATES							
8	HYDROGEN	16.309998	16.309998	16.309998	16.309998	23.479996	23.479996	19.4533690
9	CARBON MONOXIDE	24.269989	24.269989	24.269989	24.269989	37.134979	37.134979	34.913666
10	CARBON DIOXIDE	0.720000	0.720000	0.720000	0.720000	1.219999	1.219999	1.358768
11	METHANE	0.0	0.0	0.0	0.0	0.0	0.0	0.0
12	NITROGEN	0.110000	0.110000	0.110000	0.110000	0.174000	0.174000	0.174000
13	WATER	0.0	0.0	0.0	0.0	1.00000E-02	1.00000E-02	1.75429E-02
14	METHANOL	0.0	0.0	0.0	0.0	0.260000	0.260000	2.068905
15	ETHANOL	0.0	0.0	0.0	0.0	1.30000E-02	1.30000E-02	6.159312
16	MITCO 40 OIL	0.0	0.0	0.0	0.0	1.00000E-05	1.00000E-05	1.00000E-05
17	TOTAL FLOW	41.609958	41.609958	41.609958	41.609958	62.291916	62.291916	58.126866
18	LB/HR	747.450928	747.450928	747.450928	747.450928	1155.162354	1155.162354	1155.159180
19	ACTUAL CFM	27.705627	18.777108	15.312116	10.309004	14.411409	20.195073	24.129573

STREAMS ARE ALL VAPOR

STREAM SUMMARY

	20	25	30	32	35	38	45
T	84	84	84	84	84	82.4	85
0	515.00	510.00	500.00	500.00	490.00	590.00	585.00
1	518.00	517.98	517.72	518.25	510.00	110.00	110.00
A							
L							
ENTHALPY	-35746944.00	-1962833.00	-3080665.00	-1968732.00	-2122871.00	-20922.10	-1965371.00
AVE. MOL WT	187.550339	21.813324	21.813324	19.938492	20.316162	18.019589	19.522125
FLOW RATES							
HYDROGEN	27.920456	19.470413	19.470413	19.453796	19.457188	0.0	19.450465
CARBON MONOXIDE	46.215240	34.938644	34.938644	34.915421	34.920059	0.0	34.903486
CARBON DIOXIDE	1.558758	1.360917	1.360917	1.359201	1.359544	0.0	1.354386
METHANE	0.0	0.0	0.0	0.0	0.0	0.0	0.0
NITROGEN	0.295842	0.174411	0.174411	0.174191	0.174235	0.0	0.174146
WATER	1.75429E-02	1.75429E-02	1.75429E-02	1.75429E-02	1.75429E-02	0.171000	2.77779E-02
METHANOL	3.472294	2.055002	2.055002	2.050994	2.051723	0.0	0.693439
ETHANOL	0.460698	0.161746	0.161746	0.160766	0.160952	0.0	3.60832E-02
WIICD 40 OIL	215.859401	0.494321	0.494321	1.62234E-02	0.111632	0.0	3.52781E-05
TOTAL FLOW	296.104980	58.672958	58.672958	58.148026	58.233086	0.171000	56.639709
LB/HR	55534.585938	1279.852051	1279.852051	1259.368789	1183.477295	3.081417	1105.727295

ENTHALPY	-33792976.00	0.0	-91928.00	0.0	-174779.75	-20922.10	0.0
LIQ. DENSITY	35.380753	0.0	40.702026	0.0	0.0	61.833420	0.0
AVE. MOL WT	228.255081	0.0	229.519316	0.0	48.309799	18.019589	0.0
FLOW RATES							
HYDROGEN	8.573242	0.0	1.65796E-02	0.0	6.96459E-03	0.0	0.0
CARBON MONOXIDE	11.415451	0.0	2.31420E-02	0.0	1.96986E-02	0.0	0.0
CARBON DIOXIDE	0.503619	0.0	1.71567E-03	0.0	5.62776E-03	0.0	0.0
METHANE	0.0	0.0	0.0	0.0	0.0	0.0	0.0
NITROGEN	0.122646	0.0	2.19619E-04	0.0	9.80236E-05	0.0	0.0
WATER	0.0	0.0	3.37815E-12	0.0	1.42416E-02	0.171000	0.0
METHANOL	1.435139	0.0	4.09994E-03	0.0	1.266425	0.0	0.0
ETHANOL	0.320716	0.0	9.80770E-04	0.0	0.154142	0.0	0.0
WIICD 40 OIL	215.352432	0.0	0.478277	0.0	0.111608	0.0	0.0
TOTAL LIQ.	237.723038	0.0	0.525055	0.0	1.579014	0.171000	0.0
LB/HR	54261.468281	0.0	120.510339	0.0	76.281630	3.081417	0.0

ENTHALPY	0.0	0.0	0.0	0.0	-152359.75	0.0	0.0
LIQ. DENSITY	0.0	0.0	0.0	0.0	47.673260	0.0	0.0
AVE. MOL WT	0.0	0.0	0.0	0.0	34.742783	0.0	0.0
FLOW RATES							
HYDROGEN	0.0	0.0	0.0	0.0	3.66451E-03	0.0	0.0
CARBON MONOXIDE	0.0	0.0	0.0	0.0	1.46780E-02	0.0	0.0
CARBON DIOXIDE	0.0	0.0	0.0	0.0	4.63761E-03	0.0	0.0
METHANE	0.0	0.0	0.0	0.0	0.0	0.0	0.0
NITROGEN	0.0	0.0	0.0	0.0	5.99723E-05	0.0	0.0
WATER	0.0	0.0	0.0	0.0	1.62416E-02	0.0	0.0
METHANOL	0.0	0.0	0.0	0.0	1.295226	0.0	0.0
ETHANOL	0.0	0.0	0.0	0.0	0.123691	0.0	0.0
WIICD 40 OIL	0.0	0.0	0.0	0.0	1.16668E-02	0.0	0.0

STREAM SUMMARY

STREAM NUMBER	30	54	55	57	60	62	65
MOLES BELOW	84	81.4	81.4	81.4	84	84	84
TEMPERATURE DEG, F	485.00	485.00	485.00	550.08	485.00	20.00	20.00
DEW POINT DEG, F	110.00	110.00	110.00	139.40	110.00	108.96	108.96
BUBBLE PT DEG, F							
ENTHALPY BTU/HR	-1228278.00	-717092.50	-717505.50	-717148.94	-174599.25	-1567.97	108.96
LIQ. DENSITY, LB/CUFT	0.0	0.0	0.0	0.0	49.478851	0.0	49.745851
LIQI DENSITY, LB/CUFT	0.0	0.0	0.0	0.0	49.478851	0.0	0.0
VAP. DENSITY, LB/CUFT	19.522125	19.522141	19.524643	19.524643	0.0	0.0	0.0
Avg. Mol Wt					32.009460	27.942444	32.065633
FLOW RATES							
HYDROGEN	12.280747	7.169736	7.169999	7.169999	2.95176E-03	2.91074E-03	4.1013E-05
CARBON MONOXIDE	22.037537	12.865942	12.865900	12.865900	1.09961E-02	1.06459E-02	3.50177E-04
CARBON DIOXIDE	0.855089	0.499217	0.500000	0.500000	4.13852E-03	3.07978E-03	1.05874E-03
METHANE	0.0	0.0	0.0	0.0	0.0	0.0	0.0
NITROGEN	0.109953	6.41827E-02	6.40000E-02	6.40000E-02	4.68483E-05	4.56001E-05	1.26817E-06
WATER	1.75386E-02	1.02394E-02	1.00000E-02	1.00000E-02	0.160765	2.36211E-04	8.160529
METHANOL	0.432627	0.2355812	0.230000	0.230000	1.357037	5.85722E-03	1.351599
ETHANOL	2.27824E-02	1.33088E-02	1.30000E-02	1.30000E-02	0.124606	2.86077E-04	0.124320
WITCD 40 OIL	2.10113E-05	1.22668E-05	1.00000E-05	1.00000E-05	2.47072E-03	2.35849E-07	2.47099E-03
TOTAL FLOW	35.761459	20.88220	20.881958	20.881958	1.663030	0.922862	1.664538
LB/HR	698.139648	407.567402	407.712646	407.712646	53.232681	0.533225	52.599426
ACTUAL CFM	7.556958	4.411887	4.412535	4.412535	0.0	0.114612	0.0
	VAP	VAP	VAP	VAP	LIQI	VAP	LIQ

STREAM SUMMARY

STREAM NUMBER	75	76	77	78	80	83	89
NOTES - BELOW							
TEMPERATURE DEG.F	510.00	500.00	500.00	485.00	445.00	510.00	545.00
BUBBLE PT	517.98	518.25	518.25	110.00	275.76	275.77	518.68
ENTHALPY BTU/HR	-33784086.00	-18370.95	-73483.81	-24479.11	-97962.88	-97939.88	-33832368.00
LIQ. DENSITY, LB/CUFT	35.481764	40.886447	40.886447	45.268511	41.865131	41.864917	35.882339
Avg. MOL WT	228.506376	229.490585	229.490601	227.786824	229.090897	229.090897	228.507706
FLOW RATES							
HYDROGEN	8.450043	3.32186E-03	1.32850E-02	3.65796E-03	1.69430E-02	1.69430E-02	8.466986
CARBON MONOXIDE	11.276596	4.64232E-03	1.85693E-02	5.56990E-03	2.41392E-02	2.41392E-02	11.300735
CARBON DIOXIDE	0.497841	3.43085E-04	1.37202E-03	1.09361E-03	2.47063E-03	2.47063E-03	0.500311
METHANE	0.0	0.0	0.0	0.0	0.0	0.0	0.0
NITROGEN	0.121431	4.40003E-05	1.76001E-04	4.22449E-05	2.18244E-04	2.18244E-04	0.121649
WATER	0.0	6.74925E-13	2.69970E-12	1.09081E-11	1.36078E-11	1.36078E-11	1.36078E-11
METHANOL	1.422292	8.19554E-04	3.27826E-03	1.22659E-03	4.50485E-03	4.50485E-03	1.422796
ETHANOL	0.318452	1.96031E-04	7.66091E-04	2.72688E-04	1.05658E-03	1.05658E-03	0.320809
MIXCO 40 OIL	215.345078	9.56196E-02	0.382479	0.110338	0.491817	0.491817	215.833684
TOTAL FLOW	237.432022	0.104926	0.419993	0.121206	0.541149	0.541149	237.973160
LB/HR	54254.730469	24.093246	96.373032	27.599243	123.972275	123.972275	54378.699219
		LIQ	LIQ	LIQ	LIQ	LIQ	LIQ

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STREAM SUMMARY

STREAM NUMBER	90	95
NOTES - BELOW		
TEMPERATURE DEG.F	545.00	535.00
BUBBLE PT	518.68	516.14
ENTHALPY BTU/HR	-33833072.00	-33930128.00
LIQ. DENSITY, LB/CUFT	35.382294	35.453808
Avg. MOL WT	228.505798	228.505798
FLOW RATES		
HYDROGEN	8.466772	8.466772
CARBON MONOXIDE	11.301579	11.301579
CARBON DIOXIDE	0.499991	0.499991
METHANE	0.0	0.0
NITROGEN	0.121842	0.121842
WATER	1.29744E-11	1.29744E-11
METHANOL	1.427389	1.427389
ETHANOL	0.321386	0.321386
MIXCO 40 OIL	215.839401	215.839401
TOTAL FLOW	237.978333	237.978333
LB/HR	54379.425781	54379.425781
	LIQ	LIQ

NOTES

1. STREAM SPECIFIED AS ALL VAPOR
2. STREAM SPECIFIED AS ALL LIQUID
4. CAUTION: TWO LIQUID PHASES NOT CONSIDERED. *RESULTS MAY BE IN ERROR.

CYCLE SYNTHESIS RUN TIME : 27.37 CPU SECONDS

STREAM SUMMARY

	1	3	5	8	10	14	15	16
T	81.4	81.4	81.4	81.4	81.4	81.4	81.4	81.4
D	150.00	370.00	365.00	950.00	950.00	940.00	940.00	915.00
A	100.00	333.30	120.00	378.78	378.78	370.00	370.00	743.64
L						183.41	183.41	229.80
ENTHALPY BTU/HR	-1418418.00	-1291209.00	-1407896.00	-1265368.00	-11579949.00	-11037388.00	-11037388.00	-11037388.00
WAP. DENSITY, LB/CUF	0.275142	0.675541	0.641910	1.134044	2.062237	1.549935	1.549935	1.714838
WAVE. MOL WT	11.068531	11.068531	11.068531	11.068531	15.035516	15.035516	15.035516	17.521133
FLOW RATES MOLES/HR								
HYDROGEN	51.189987	51.189987	51.189987	51.189987	174.389984	174.389984	174.389984	123.630366
CARBON MONOXIDE	24.059998	24.059998	24.059998	24.059998	86.469997	86.469997	86.469997	62.642807
CARBON DIOXIDE	1.650000	1.650000	1.650000	1.650000	58.948991	58.948991	58.948991	33.898575
METHANE	0.220000	0.220000	0.220000	0.220000	48.548982	48.548982	48.548982	48.548982
NITROGEN	2.00000E-02	2.00000E-02	2.00000E-02	2.00000E-02	3.549999	3.549999	3.549999	3.549999
WATER	0.0	0.0	0.0	0.0	0.110000	0.110000	0.110000	1.911713
METHANOL	0.0	0.0	0.0	0.0	2.359999	2.359999	2.359999	26.740882
ETHANOL	0.0	0.0	0.0	0.0	1.50000E-02	1.50000E-02	1.50000E-02	0.267304
WTCO 40 OIL	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
TOTAL FLOW MOL/HR	77.139954	77.139954	77.139954	77.139954	350.393311	350.393311	350.393311	300.682373
LB/HR	853.825928	853.825928	853.825928	853.825928	5268.343750	5268.343750	5268.343750	5268.292969
ACTUAL CFM	51.716555	29.924744	22.166884	12.548399	42.577805	56.651093	56.651093	72.276978

STREAMS ARE ALL VAPOR

STREAM SUMMARY

STREAM NUMBER	20	25	30	32	35	38	45
NOTES BELOW	84	84	84	84	84	84	84
PRESSURE PSIA	915.00	919.00	900.00	900.00	890.00	890.00	885.00
TEMPERATURE DEG.F	482.01	482.00	300.24	300.24	110.00	100.00	110.83
DEW POINT DEG.F							
ENTHALPY BTU/HR	-57568480.00	-11911480.00	-12454051.00	-12241809.00	-13190355.00	-306296.06	-10370231.00
AVE. MOL WT	116.829631	16.203125	16.203125	17.552795	17.683228	18.019989	16.156082
FLOW RATES							
HYDROGEN	153.268631	123.709167	123.709167	123.625105	123.642075	0.0	123.521851
CARBON MONOXIDE	72.812653	62.675201	62.675201	62.644886	62.650172	0.0	62.556703
CARBON DIOXIDE	40.166946	33.946793	33.946793	33.925585	33.922136	0.0	33.377136
METHANE	57.575378	48.579971	48.579971	48.530171	48.528122	0.0	48.336102
NITROGEN	4.673783	3.545218	3.545218	3.542253	3.542845	0.0	3.528052
WATER	1.411713	1.411712	1.411712	1.411712	1.411712	0.0	1.412035
METHANOL	36.220856	26.788528	26.788528	26.741608	26.745077	0.0	2.913450
ETHANOL	0.541141	0.270494	0.270494	0.269052	0.269348	0.0	1.50010E-02
MITCO 40 OIL	269.934326	0.880471	0.880471	3.83675E-02	0.206728	0.0	1.19881E-04
TOTAL FLOW	636.604980	501.806885	501.806885	500.738281	500.751904	2.500000	273.930176
	73865.125800	5493.828125	5493.828125	5278.796575	5321.600781	45.049973	4425.636719

LIQUID	20	25	30	32	35	38	45
ENTHALPY	-45676592.00	0.0	-173043.06	0.0	-2824587.00	-306296.06	0.0
LIQ. DENSITY, LB/CUFT	34.604614	0.0	39.031647	0.0	0.0	61.963270	0.0
AVE. MOL WT	203.872894	0.0	201.276703	0.0	35.117864	18.019989	0.0
FLOW RATES							
HYDROGEN	29.880783	0.0	0.0	0.0	0.136697	0.0	0.0
CARBON MONOXIDE	10.226974	0.0	0.0	0.0	0.120080	0.0	0.0
CARBON DIOXIDE	6.268677	0.0	0.0	0.0	0.607118	0.0	0.0
METHANE	9.070129	0.0	0.0	0.0	0.185307	0.0	0.0
NITROGEN	1.133205	0.0	0.0	0.0	5.60666E-03	0.0	0.0
WATER	1.907355206	0.0	0.0	0.0	1.364987	2.500000	0.0
METHANOL	3.498306	0.0	0.0	0.0	24.189545	0.0	0.0
ETHANOL	0.271997	0.0	0.0	0.0	0.254859	0.0	0.0
MITCO 40 OIL	269.060791	0.0	0.0	0.0	0.206677	0.0	0.0
TOTAL LIQ.	335.414795	0.0	1.088603	0.0	27.070867	2.500000	0.0
	68381.937500	0.0	215.064793	0.0	896.527832	45.049973	0.0

LIQUID	20	25	30	32	35	38	45
ENTHALPY	0.0	0.0	0.0	0.0	-2795946.00	0.0	0.0
LIQ. DENSITY, LB/CUFT	0.0	0.0	0.0	0.0	48.510966	0.0	0.0
AVE. MOL WT	0.0	0.0	0.0	0.0	32.156845	0.0	0.0
FLOW RATES							
HYDROGEN	0.0	0.0	0.0	0.0	0.123276	0.0	0.0
CARBON MONOXIDE	0.0	0.0	0.0	0.0	0.214592	0.0	0.0
CARBON DIOXIDE	0.0	0.0	0.0	0.0	0.593583	0.0	0.0
METHANE	0.0	0.0	0.0	0.0	0.178981	0.0	0.0
NITROGEN	0.0	0.0	0.0	0.0	5.18124E-03	0.0	0.0
WATER	0.0	0.0	0.0	0.0	1.364987	0.0	0.0
METHANOL	0.0	0.0	0.0	0.0	24.186050	0.0	0.0
ETHANOL	0.0	0.0	0.0	0.0	0.254747	0.0	0.0
MITCO 40 OIL	0.0	0.0	0.0	0.0	8.55607E-02	0.0	0.0

STREAM SUMMARY

STREAM NUMBER	50	54	55	57	60	62	65
MOLES BELOW	84	84	81.6	81.6	84	84	84
PRESSURE PSIA	885.00	885.00	885.00	950.00	885.00	20.00	20.00
TEMPERATURE DEG.F	110.83	110.83	110.00	125.33	110.83	104.19	104.19
DEW POINT							
BUBBLE PT DEG.F							
ENTHALPY BTU/HR	-17271.32	-10352956.00	-10346293.00	-10314581.00	-3081865.00	-107778.44	-2974083.00
LIQ. DENSITY, LB/CUFT	0.0	0.0	0.0	0.0	59.658737	0.0	50.225095
LIQ. DENSITY, LB/CUFT	0.0	0.0	0.0	0.0	59.658737	0.0	0.0
VAP. DENSITY, LB/CUFT	2.334481	2.334481	2.338123	2.436488	0.0	0.106008	0.0
VAP. DENSITY, LB/CUFT	16.156082	16.156097	16.155380	16.155380	30.522278	31.808578	30.675159
FLOW RATES MOLES/HR							
HYDROGEN	0.205722	123.316086	123.190997	123.190997	0.101866	8.93629E-22	2.48349E-03
CARBON MONOXIDE	5.5286E-02	53.323733	53.323733	53.323733	8.52125E-02	8.52125E-02	2.5366E-03
CARBON DIOXIDE	5.89253E-03	48.317474	48.320996	48.320996	0.149395	0.1493904	5.34201E-02
NITROGEN	1.86591E-04	0.118468	0.118000	0.118000	4.13647E-03	6.98209E-02	1.13952E-01
WATER	4.01953E-03	2.409430	2.389999	2.389999	24.333287	1.19501E-02	24.108598
METHANOL	2.49837E-05	1.69760E-02	1.50000E-02	1.50000E-02	0.254218	1.40724E-03	0.252819
MITCO 40 OIL	1.99658E-07	1.19681E-04	1.0000E-02	1.0000E-02	2.19663E-02	9.94952E-06	2.19564E-02
TOTAL FLOW	0.456223	273.473633	273.253418	273.253418	29.279297	1.035372	28.2643912
LB/HR	7.37071	4418.265625	4414.511719	4414.511719	891.670654	32.933701	860.737569
ACTUAL CFM	0.052623	31.543488	31.467590	30.197205	0.0	5.179864	0.0
	VAP	VAP	VAP	VAP	LIQ	VAP	LIQ

T	STREAM NUMBER	75	76	77	78	88	83	89
0	NOTES - BELOW	#4	#4	900.00	885.00	42.4	#4	#4
1	PRESSURE PSIA	910.00	900.00	900.00	885.00	885.00	910.00	945.00
2	TEMPERATURE DEG.F	482.00	300.24	300.24	119.83	262.39	262.56	482.62
3	BUBBLE PT DEG.F	482.00	340.24					
4	ENTHALPY BTU/HR	-45656726.00	-34661.07	-44493.20	-44493.20	-182897.44	-182897.44	-95775490.00
5	LIQ. DENSITY LB/CUFT	34.631424	39.031250	39.031250	49.302536	39.714432	39.710602	39.514668
6	VAPOR DENSITY LB/CUFT	0.8	0.0	0.0	0.0	0.0	0.0	0.0
7	LIQ. MOL WT	204.216827	201.271973	201.271988	195.716249	200.842068	200.842068	204.263150
8	FLOW RATES MOLES/HR	29.559864	1.67699E-02	6.70797E-02	7.83582E-02	8.56379E-02	3.59379E-02	29.654897
9	HYDROGEN	10.137451	6.10297E-03	2.44119E-02	7.54444E-03	3.19564E-02	3.19564E-02	10.169407
10	CARBON MONOXIDE	6.220154	6.15865E-03	2.46346E-02	1.86518E-02	4.32864E-02	4.32864E-02	6.283440
11	CARBON DIOXIDE	8.995407	5.96015E-03	2.38405E-02	8.70287E-03	3.25435E-02	3.25435E-02	9.827950
12	METHANE	1.128565	5.93153E-04	2.37261E-03	5.87934E-04	2.96055E-03	2.96055E-03	1.131525
13	NITROGEN	9.53074E-07	4.84961E-10	1.95984E-09	5.64691E-10	2.50453E-09	2.50453E-09	9.56178E-07
14	WATER	9.452327	9.38258E-03	3.75303E-02	4.24897E-03	4.17793E-02	4.17793E-02	9.474106
15	METHANOL	0.270647	2.88398E-04	1.15356E-03	1.21773E-04	1.27533E-03	1.27533E-03	0.271822
16	ETHANOL	269.053711	0.168421	0.673682	0.184702	0.658384	0.658384	269.911855
17	WITCO 40 OIL							
18	TOTAL FLOW LB/HR	335.797607	0.213676	0.854706	0.242918	1.097623	1.097623	335.895020
19		68371.250000	43.007050	172.028275	47.542450	219.570740	219.570740	68590.812500
20			LIQ	LIQ	LIQ2	LIQ	LIQ	LIQ

T	STREAM NUMBER	90	95
0	NOTES - BELOW	#4	#4
1	PRESSURE PSIA	745.00	735.00
2	TEMPERATURE DEG.F	482.00	487.92
3	BUBBLE PT DEG.F	482.00	487.92
4	ENTHALPY BTU/HR	-45781856.00	-46531104.00
5	LIQ. DENSITY LB/CUFT	34.615616	34.995331
6	VAPOR DENSITY LB/CUFT	0.8	0.0
7	LIQ. MOL WT	204.204407	204.204407
8	FLOW RATES MOLES/HR	29.638245	29.638245
9	HYDROGEN	10.169850	10.169850
10	CARBON MONOXIDE	6.268373	6.268373
11	CARBON DIOXIDE	9.028349	9.028349
12	METHANE	1.129785	1.129785
13	NITROGEN	2.52267E-09	2.52267E-09
14	WATER	9.479876	9.479876
15	METHANOL	0.273837	0.273837
16	ETHANOL	269.934326	269.934326
17	WITCO 40 OIL		
18	TOTAL FLOW LB/HR	335.922607	335.922607
19		68596.875000	68596.875000
20		LIQ	LIQ

NOTES
1. STREAM SPECIFIED AS ALL VAPOR
2. STREAM SPECIFIED AS ALL LIQUID
3. CAUTION: TWO LIQUID PHASES NOT CONSIDERED. *RESULTS MAY BE IN ERROR.
4. CAUTION: TWO LIQUID PHASES NOT CONSIDERED. *RESULTS MAY BE IN ERROR.

CYCLE SYNTHESIS RUN TIME : 34.43 CPU SECONDS

STREAM SUMMARY
VERSION 82.021-A

AIR PRODUCTS & CHEMICALS, INC -- CYCLE SYNTHESIS
LPMEDH ENTRAINED/LURGI: EL-6752

T.R.TSAO
87-7-1533

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STREAM SUMMARY

STREAM NUMBER	1	3	5	8	10	15	18
NOTES - BELOW	41.4	41.4	41.4	41.4	41.4	41.4	41.4
PRESSURE PSIA	150.00	370.00	135.00	750.00	750.00	740.00	715.00
TEMPERATURE DEG.F	100.00	325.29	120.00	325.78	178.46	395.00	672.93
DEW POINT DEG.F						105.42	201.53
ENTHALPY BTU/HR	-671626.75	-628617.13	-667916.13	-628565.56	-3602679.00	-3414931.00	-3414931.00
VAP. DENSITY, LB/CUFT	0.315538	0.650684	0.977133	1.102342	1.631617	1.195558	0.974852
Avg. Mol Wt	12.675305	12.675305	12.675305	12.675305	15.075493	15.075493	16.857285
FLOW RATES MOLES/HR	16.319992	16.319992	16.319992	16.319992	53.919983	53.919983	62.227661
HYDROGEN	7.856000	7.856000	7.856000	7.856000	26.755981	26.755981	21.256221
CARBON MONOXIDE	1.469999	1.469999	1.469999	1.469999	10.879999	10.879999	10.862398
CARBON DIOXIDE	1.660000	1.660000	1.660000	1.660000	15.030000	15.030000	15.030000
METHANE	0.120000	0.120000	0.120000	0.120000	1.070000	1.070000	1.070000
NITROGEN	0.0	0.0	0.0	0.0	2.700000E-02	2.700000E-02	0.306139
WATER	0.0	0.0	0.0	0.0	0.865000	0.865000	6.479280
METHANOL	0.0	0.0	0.0	0.0	5.300000E-03	5.300000E-03	6.68387E-02
ETHANOL	0.0	0.0	0.0	0.0	4.000000E-05	4.000000E-05	4.000000E-05
MITCO 40 OIL	0.0	0.0	0.0	0.0	0.0	0.0	0.0
TOTAL FLOW MOL/HR	27.425949	27.425949	27.425949	27.425949	108.553223	108.553223	97.078517
LD/HR	347.632080	347.632080	347.632080	347.632080	1638.493164	1638.493164	1456.680469
ACTUAL CFM	18.361852	10.521221	8.556461	5.253101	16.667433	22.651746	27.364009

STREAMS ARE ALL VAPOR

STREAM SUMMARY
VERSION 82.021-A

AIR PRODUCTS & CHEMICALS, INC -- CYCLE SYNTHESIS
LPMEOH ENTRAINED/LURGI: EL-6752

I.R.TSAD
87-7-1533

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STREAM SUMMARY

STREAM NUMBER	50	54	55	57	60	62	65
NOTES BELOW							
PRESSURE PSIA	685.00	685.00	685.00	750.00	685.00	20.00	20.00
TEMPERATURE DEG.F	109.97	109.97	109.98	129.70	109.97	103.97	103.97
DEW POINT DEG.F							
BUBBLE PT DEG.F							
ENTHALPY BTU/HR	-369171.56	-2990183.04	-2988203.00	-2978134.00	-657066.96	-19880.19	-637086.25
LIQ. DENSITY, LB/CUFT	0.0	0.0	0.0	0.0	49.176234	0.0	49.684326
LIQ. DENSITY, LB/CUFT	0.0	0.0	0.0	0.0	49.176234	0.0	0.0
VAP. DENSITY, LB/CUFT	1.779609	1.779609	1.779241	1.877176	0.0	0.105447	0.0
AVE. MOL WT	15.890013	15.890018	15.886910	15.886910	31.328415	31.630569	31.318756
FLOW RATES MOLES/HR							
HYDROGEN	4.592957	37.609116	37.599991	37.599991	1.93458E-02	1.91109E-02	2.34812E-04
CARBON MONOXIDE	2.309000	16.907089	16.899994	16.899994	1.81498E-02	1.78179E-02	3.31931E-04
CARBON DIOXIDE	1.150602	9.421634	9.410000	9.410000	9.69459E-02	8.40843E-02	1.28617E-02
METHANE	1.412837	13.372022	13.370000	13.370000	2.71801E-02	2.63200E-02	8.68054E-04
NITROGEN	0.116302	0.952332	0.950000	0.950000	7.44156E-04	7.32701E-04	1.19533E-05
WATER	3.29735E-03	2.70000E-02	2.70000E-02	2.70000E-02	0.545841	1.49211E-03	8.544337
METHANOL	0.105112	0.866194	0.865000	0.865000	5.714433	4.51456E-02	5.469337
ETHANOL	6.43547E-04	5.26364E-03	5.30000E-03	5.30000E-03	5.87804E-02	2.76148E-02	5.95143E-02
WITCO 40 DIL	4.71924E-06	3.86432E-05	4.00000E-05	4.00000E-05	1.04928E-02	1.80631E-06	1.06010E-02
TOTAL FLOW	9.910791	81.153839	81.127274	81.127274	6.292862	0.194987	6.097835
LB/HR	157.482590	1289.535889	1288.861572	1288.861572	197.146811	6.167543	190.997478
ACTUAL CFM	1.474880	12.076961	12.073144	12.073144	0.0	0.975023	0.0
	VAP	VAP	VAP	VAP	LIQ	VAP	LIQ

STREAM SUMMARY
VERSION 82.021-A

AIR PRODUCTS & CHEMICALS, INC -- CYCLE SYNTHESIS
LPMCOII ENTRAINED/LURGI: EL-6752

I.R.1540
87-7-1533

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STREAM SUMMARY

STREAM NUMBER	75	76	77	78	80	83	89
INDICES BELOW	84	84	84	84	82.4	82.4	84
LIQ. DENSITY, LB/CUFT	710.00	700.80	700.00	685.00	710.00	710.00	745.08
AVE. MOL WT	481.99	283.27	283.27	109.97	251.45	251.47	482.87
TEMPERATURE DEG.F	481.99	283.27	283.27	109.97	251.45	251.47	482.87
BUBBLE PT	481.99	283.27	283.27	109.97	251.45	251.47	482.87
ENTHALPY BTU/HR	-35900672.00	-143355.02	-57420.10	-164668.38	-73888.44	-73871.56	-35924848.00
AVE. MOL WT	216.826004	214.075897	214.075821	206.989105	212.621964	212.621964	216.818954
FLOW RATES MOLES/HR							
HYDROGEN	14.074356	4.911866E-03	1.966758E-02	5.03041E-03	2.467795E-02	2.467795E-02	16.099030
CARBON MONOXIDE	6.138626	1.94557E-03	7.78226E-03	2.18790E-03	1.97017E-03	1.97017E-03	6.148596
CARBON DIOXIDE	3.614662	2.0012E-03	8.02947E-03	5.31036E-03	1.33308E-02	1.33308E-02	3.623893
METHANE	5.032829	1.77556E-03	7.10223E-03	2.35227E-03	9.45450E-03	9.45450E-03	5.046283
NITROGEN	0.613418	1.68160E-04	6.72441E-04	1.52748E-04	8.26886E-04	8.26886E-04	0.614243
WATER	0.0	3.81985E-11	1.52794E-10	4.72748E-11	2.00669E-10	2.00669E-10	0.012545
METHANOL	4.130284	2.17576E-03	8.70391E-03	1.34928E-03	1.00522E-02	1.00522E-02	2.00669E-10
ETHANOL	0.117740	6.79054E-05	2.71621E-04	3.66592E-05	3.08281E-04	3.08281E-04	4.140336
MITCO 40 OIL	215.455429	7.05653E-02	0.282261	6.99044E-02	0.352166	0.352166	215.607587
TOTAL FLOW	251.183228	0.083615	0.334461	0.086324	0.420785	0.420785	251.604804
	54463.054688	17.899994	71.599976	17.868179	89.468155	89.468155	54552.513625
ENTHALPY BTU/HR	-35900672.00	-143355.02	-57420.10	-164668.38	-73888.44	-73871.56	-35924848.00
LIQ. DENSITY, LB/CUFT	710.00	700.80	700.00	685.00	710.00	710.00	745.08
AVE. MOL WT	481.99	283.27	283.27	109.97	251.45	251.47	482.87
TEMPERATURE DEG.F	481.99	283.27	283.27	109.97	251.45	251.47	482.87
BUBBLE PT	481.99	283.27	283.27	109.97	251.45	251.47	482.87
ENTHALPY BTU/HR	-35900672.00	-143355.02	-57420.10	-164668.38	-73888.44	-73871.56	-35924848.00
AVE. MOL WT	216.826004	214.075897	214.075821	206.989105	212.621964	212.621964	216.818954
FLOW RATES MOLES/HR							
HYDROGEN	16.074356	4.911866E-03	1.966758E-02	5.03041E-03	2.467795E-02	2.467795E-02	16.099030
CARBON MONOXIDE	9.138626	1.94557E-03	7.78226E-03	2.18790E-03	1.97017E-03	1.97017E-03	6.148596
CARBON DIOXIDE	5.032829	2.0012E-03	8.02947E-03	5.31036E-03	1.33308E-02	1.33308E-02	3.623893
METHANE	5.032829	1.77556E-03	7.10223E-03	2.35227E-03	9.45450E-03	9.45450E-03	5.046283
NITROGEN	0.613418	1.68160E-04	6.72441E-04	1.52748E-04	8.26886E-04	8.26886E-04	0.614243
WATER	0.0	3.81985E-11	1.52794E-10	4.72748E-11	2.00669E-10	2.00669E-10	0.012545
METHANOL	4.130284	2.17576E-03	8.70391E-03	1.34928E-03	1.00522E-02	1.00522E-02	2.00669E-10
ETHANOL	0.117740	6.79054E-05	2.71621E-04	3.66592E-05	3.08281E-04	3.08281E-04	4.140336
MITCO 40 OIL	215.455429	7.05653E-02	0.282261	6.99044E-02	0.352166	0.352166	215.607587
TOTAL LIQ.	251.183228	0.083615	0.334461	0.086324	0.420785	0.420785	251.604804
	54463.054688	17.899994	71.599976	17.868179	89.468155	89.468155	54552.513625
ENTHALPY BTU/HR	-35900672.00	-143355.02	-57420.10	-164668.38	-73888.44	-73871.56	-35924848.00
LIQ. DENSITY, LB/CUFT	710.00	700.80	700.00	685.00	710.00	710.00	745.08
AVE. MOL WT	481.99	283.27	283.27	109.97	251.45	251.47	482.87
TEMPERATURE DEG.F	481.99	283.27	283.27	109.97	251.45	251.47	482.87
BUBBLE PT	481.99	283.27	283.27	109.97	251.45	251.47	482.87
ENTHALPY BTU/HR	-35900672.00	-143355.02	-57420.10	-164668.38	-73888.44	-73871.56	-35924848.00
AVE. MOL WT	216.826004	214.075897	214.075821	206.989105	212.621964	212.621964	216.818954
FLOW RATES MOLES/HR							
HYDROGEN	16.074356	4.911866E-03	1.966758E-02	5.03041E-03	2.467795E-02	2.467795E-02	16.099030
CARBON MONOXIDE	9.138626	1.94557E-03	7.78226E-03	2.18790E-03	1.97017E-03	1.97017E-03	6.148596
CARBON DIOXIDE	5.032829	2.0012E-03	8.02947E-03	5.31036E-03	1.33308E-02	1.33308E-02	3.623893
METHANE	5.032829	1.77556E-03	7.10223E-03	2.35227E-03	9.45450E-03	9.45450E-03	5.046283
NITROGEN	0.613418	1.68160E-04	6.72441E-04	1.52748E-04	8.26886E-04	8.26886E-04	0.614243
WATER	0.0	3.81985E-11	1.52794E-10	4.72748E-11	2.00669E-10	2.00669E-10	0.012545
METHANOL	4.130284	2.17576E-03	8.70391E-03	1.34928E-03	1.00522E-02	1.00522E-02	2.00669E-10
ETHANOL	0.117740	6.79054E-05	2.71621E-04	3.66592E-05	3.08281E-04	3.08281E-04	4.140336
MITCO 40 OIL	215.455429	7.05653E-02	0.282261	6.99044E-02	0.352166	0.352166	215.607587
TOTAL LIQ.	251.183228	0.083615	0.334461	0.086324	0.420785	0.420785	251.604804
	54463.054688	17.899994	71.599976	17.868179	89.468155	89.468155	54552.513625
ENTHALPY BTU/HR	-35900672.00	-143355.02	-57420.10	-164668.38	-73888.44	-73871.56	-35924848.00
LIQ. DENSITY, LB/CUFT	710.00	700.80	700.00	685.00	710.00	710.00	745.08
AVE. MOL WT	481.99	283.27	283.27	109.97	251.45	251.47	482.87
TEMPERATURE DEG.F	481.99	283.27	283.27	109.97	251.45	251.47	482.87
BUBBLE PT	481.99	283.27	283.27	109.97	251.45	251.47	482.87
ENTHALPY BTU/HR	-35900672.00	-143355.02	-57420.10	-164668.38	-73888.44	-73871.56	-35924848.00
AVE. MOL WT	216.826004	214.075897	214.075821	206.989105	212.621964	212.621964	216.818954
FLOW RATES MOLES/HR							
HYDROGEN	16.074356	4.911866E-03	1.966758E-02	5.03041E-03	2.467795E-02	2.467795E-02	16.099030
CARBON MONOXIDE	9.138626	1.94557E-03	7.78226E-03	2.18790E-03	1.97017E-03	1.97017E-03	6.148596
CARBON DIOXIDE	5.032829	2.0012E-03	8.02947E-03	5.31036E-03	1.33308E-02	1.33308E-02	3.623893
METHANE	5.032829	1.77556E-03	7.10223E-03	2.35227E-03	9.45450E-03	9.45450E-03	5.046283
NITROGEN	0.613418	1.68160E-04	6.72441E-04	1.52748E-04	8.26886E-04	8.26886E-04	0.614243
WATER	0.0	3.81985E-11	1.52794E-10	4.72748E-11	2.00669E-10	2.00669E-10	0.012545
METHANOL	4.130284	2.17576E-03	8.70391E-03	1.34928E-03	1.00522E-02	1.00522E-02	2.00669E-10
ETHANOL	0.117740	6.79054E-05	2.71621E-04	3.66592E-05	3.08281E-04	3.08281E-04	4.140336
MITCO 40 OIL	215.455429	7.05653E-02	0.282261	6.99044E-02	0.352166	0.352166	215.607587
TOTAL LIQ.	251.183228	0.083615	0.334461	0.086324	0.420785	0.420785	251.604804
	54463.054688	17.899994	71.599976	17.868179	89.468155	89.468155	54552.513625
ENTHALPY BTU/HR	-35900672.00	-143355.02	-57420.10	-164668.38	-73888.44	-73871.56	-35924848.00
LIQ. DENSITY, LB/CUFT	710.00	700.80	700.00	685.00	710.00	710.00	745.08
AVE. MOL WT	481.99	283.27	283.27	109.97	251.45	251.47	482.87
TEMPERATURE DEG.F	481.99	283.27	283.27	109.97	251.45	251.47	482.87
BUBBLE PT	481.99	283.27	283.27	109.97	251.45	251.47	482.87
ENTHALPY BTU/HR	-35900672.00	-143355.02	-57420.10	-164668.38	-73888.44	-73871.56	-35924848.00
AVE. MOL WT	216.826004	214.075897	214.075821	206.989105	212.621964	212.621964	216.818954
FLOW RATES MOLES/HR							
HYDROGEN	16.074356	4.911866E-03	1.966758E-02	5.03041E-03	2.467795E-02	2.467795E-02	16.099030
CARBON MONOXIDE	9.138626	1.94557E-03	7.78226E-03	2.18790E-03	1.97017E-03	1.97017E-03	6.148596
CARBON DIOXIDE	5.032829	2.0012E-03	8.02947E-03	5.31036E-03	1.33308E-02	1.33308E-02	3.623893
METHANE	5.032829	1.77556E-03	7.10223E-03	2.35227E-03	9.45450E-03	9.45450E-03	5.046283
NITROGEN	0.613418	1.68160E-04	6.72441E-04	1.52748E-04	8.26886E-04	8.26886E-04	0.614243
WATER	0.0	3.81985E-11	1.52794E-10	4.72748E-11	2.00669E-10	2.00669E-10	0.012545
METHANOL	4.130284	2.17576E-03	8.70391E-03	1.34928E-03	1.00522E-02	1.00522E-02	2.00669E-10
ETHANOL	0.117740	6.79054E-05	2.71621E-04	3.66592E-05	3.08281E-04	3.08281E-04	4.140336
MITCO 40 OIL	215.455429	7.05653E-02	0.282261	6.99044E-02	0.352166	0.352166	215.607587
TOTAL LIQ.	251.183228	0.083615	0.334461	0.086324	0.420785	0.420785	251.604804
	54463.054688	17.899994	71.599976	17.868179	89.468155	89.468155	54552.513625
ENTHALPY BTU/HR	-35900672.00	-143355.02	-57420.10	-164668.38	-73888.44	-73871.56	-35924848.00
LIQ. DENSITY, LB/CUFT	710.00	700.80	700.00	685.00	710.00	710.00	745.08
AVE. MOL WT	481.99	283.27	283.27	109.97	251.45	251.47	482.87
TEMPERATURE DEG.F	481.99	283.27	283.27	109.97	251.45	251.47	482.87
BUBBLE PT	481.99	283.27	283.27	109.97	251.45	251.47	482.87
ENTHALPY BTU/HR	-35900672.00	-143355.02	-57420.10	-164668.38	-73888.44	-73871.56	-35924848.00
AVE. MOL WT	216.826004	214.075897	21				

STREAM SUMMARY

	90	95
T O L		
STREAM NUMBER	42,4	44
NOTES - BELOW	745.00	735.00
PRESSURE PSIA	682.88	478.12
TEMPERATURE DEG.F	-35927536.00	-36121312.00
ENTHALPY BTU/HR	35.502228	35.628586
LIQ. DENSITY, LB/CUFT	216.822250	216.822250
AVE. MOL WT		
FLOW RATES MOLES/HR		
HYDROGEN	16.092834	16.092834
CARBON MONOXIDE	6.196657	6.146857
CARBON DIOXIDE	3.634781	3.634781
METHANE	5.048519	5.048519
NITROGEN	0.613624	0.613624
WATER	1.83656E-10	1.83656E-10
METHANOL	4.141909	4.141909
ETHANOL	0.116913	0.116913
MITCO 40 OIL	215.818024	215.818024
TOTAL FLOW	251.613235	251.613235
LB/HR	54555.347656	54555.347656
	LIQ	LIQ

NOTES

1. STREAM SPECIFIED AS ALL VAPOR
2. STREAM SPECIFIED AS ALL LIQUID
3. CAUTION! TWO LIQUID PHASES NOT CONSIDERED. RESULTS MAY BE IN ERROR.

CYCLE SYNTHESIS RUN TIME : 34.15 CPU SECONDS

STREAM SUMMARY

T D A L	STREAM NUMBER	1	5	5	8	10	15	18
	MOLES BELOW	81.4	81.4	81.4	81.4	81.4	84	89
	PRESSURE PSIA	150.00	150.00	150.00	150.00	150.00	150.00	150.00
	TEMPERATURE DEG.F	100.00	335.30	335.09	335.09	192.89	402.00	745.79
	DEW POINT DEG.F						103.60	203.41
	ENTHALPY BTU/K	-528254.25	-490745.94	-528249.63	-490750.88	-2284232.00	-2173362.00	-2173362.00
	VAP. DENSITY, LB/CUFT	0.368087	0.634932	0.789311	1.269641	1.956014	1.756134	1.107812
	AVE. MOL WT	14.796109	14.796109	14.796109	14.796109	18.613785	18.613785	21.158818
	FLOW RATES MOLES/HR							
	HYDROGEN	11.577000	11.577000	11.577000	11.577000	27.276993	27.276993	18.792923
	CARBON MONOXIDE	11.061999	11.061999	11.061999	11.061999	43.311996	43.311996	38.665501
	CARBON DIOXIDE	3.37000E-02	3.37000E-02	3.37000E-02	3.37000E-02	1.387699	1.387699	1.644003
	METHANE	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	NITROGEN	6.04000E-02	6.04000E-02	6.04000E-02	6.04000E-02	0.363400	0.363400	0.363400
	WATER	0.0	0.0	0.0	0.0	1.64000E-02	1.64000E-02	6.06805E-02
	METHANOL	0.0	0.0	0.0	0.0	0.487000	0.487000	4.256008
	ETHANOL	0.0	0.0	0.0	0.0	2.10000E-02	2.10000E-02	0.321585
	MITCO 40 OIL	0.0	0.0	0.0	0.0	2.40000E-05	2.40000E-05	2.40000E-05
	TOTAL FLOW	22.733078	22.733078	22.733078	22.733078	72.864456	72.864456	66.126069
	LB/HR	336.361084	336.361084	336.361084	336.361084	1356.283203	1356.283203	1356.276367
	ACTUAL CFM	15.230133	8.841858	7.102422	4.415436	11.556527	15.523796	20.404724

STREAMS ARE ALL VAPOR

STREAM SUMMARY
VERSION 82.021-A

AIR PRODUCTS & CHEMICALS, INC -- CYCLE SYNTHESIS
LPMEOH ENTRAINED/KT GAS: EK-4752

I.R. ISAD
87-7-1533

21JAN.82 PAGE 9
19:41:04

STREAM SUMMARY

STREAM NUMBER	20	25	30	32	35	38	45
INLET	715.00	710.00	700.00	700.00	690.00	62.4	685.00
TEMPERATURE DEG.F	482.00	481.99	290.23	291.22	110.80	100.00	109.95
DEW POINT				291.22			
ENTHALPY BTU/HR	-38225824.00	-2383043.00	-2473911.00	-2427595.59	-2587243.00	-60433.89	-2158758.00
AVERAGE MOL WT	177.558426	21.982254	21.982254	21.169586	21.332672	18.019989	28.354401
FLOW RATES MOLES/HR							
HYDROGEN	31.678818	18.609006	18.609006	18.796600	18.799872	0.0	18.786853
CARBON MONOXIDE	55.319504	38.694556	38.694556	38.681132	38.684801	0.0	38.658895
CARBON DIOXIDE	2.591321	1.646322	1.646322	1.644637	1.645134	0.0	1.627323
METHANE	0.0	0.0	0.0	0.0	0.0	0.0	0.0
NITROGEN	0.698560	0.362807	0.362807	0.362502	0.362583	0.0	0.362178
WATER	6.06805E-02	6.06805E-02	6.06805E-02	6.06805E-02	6.06805E-02	0.0	1.92394E-02
METHANOL	8.26767E-03	4.26613E-03	4.26613E-03	4.253491	4.254811	0.0	8.56473E-03
ETHANOL	1.56563E-03	0.306689	0.306689	0.305156	0.305463	0.0	2.45309E-02
WITCO 40 OIL	215.817841	0.238090	0.238090	7.57836E-03	5.32806E-02	0.0	2.87411E-05
TOTAL LIQ.	315.679736	64.380142	64.380142	64.111938	64.145373	0.0	68.043915
LB/HR	56016.082031	1415.220459	1415.220459	1357.223115	1368.822998	5.946595	1222.157715

ENTHALPY BTU/HR	-35874368.00	0.0	-45761.24	0.0	-427209.63	-60433.89	0.0
LIQ. DENSITY, LB/CUFT	35.587677	0.0	40.488052	0.0	0.0	61.967270	0.0
AVERAGE MOL WT	217.157181	0.0	217.343353	0.0	35.526917	18.019989	0.0
FLOW RATES MOLES/HR							
HYDROGEN	13.021103	0.0	1.18777E-02	0.0	1.40549E-02	0.0	0.0
CARBON MONOXIDE	16.793289	0.0	1.66783E-02	0.0	5.68054E-02	0.0	0.0
CARBON DIOXIDE	0.852882	0.0	1.43813E-03	0.0	1.94414E-02	0.0	0.0
METHANE	0.0	0.0	0.0	0.0	0.0	0.0	0.0
NITROGEN	0.338450	0.0	2.94003E-04	0.0	4.47310E-04	0.0	0.0
WATER	0.0	0.0	2.4377E-11	0.0	5.70113E-02	0.0	0.0
METHANOL	4.015853	0.0	6.42161E-03	0.0	3.62672E-02	0.0	0.0
ETHANOL	0.862344	0.0	1.47700E-03	0.0	0.280707	0.0	0.0
WITCO 40 OIL	215.584778	0.0	0.228537	0.0	5.32821E-02	0.0	0.0
TOTAL LIQ.	251.468704	0.0	0.268724	0.0	4.108442	0.336000	0.0
LB/HR	54608.234375	0.0	57.970581	0.0	145.960281	5.946595	0.0

ENTHALPY BTU/HR	0.0	0.0	0.0	0.0	-421759.94	0.0	0.0
LIQ. DENSITY, LB/CUFT	0.0	0.0	0.0	0.0	47.850601	0.0	0.0
AVERAGE MOL WT	0.0	0.0	0.0	0.0	34.272034	0.0	0.0
FLOW RATES MOLES/HR							
HYDROGEN	0.0	0.0	0.0	0.0	1.26617E-02	0.0	0.0
CARBON MONOXIDE	0.0	0.0	0.0	0.0	5.49612E-02	0.0	0.0
CARBON DIOXIDE	0.0	0.0	0.0	0.0	1.90014E-02	0.0	0.0
METHANE	0.0	0.0	0.0	0.0	0.0	0.0	0.0
NITROGEN	0.0	0.0	0.0	0.0	4.20391E-04	0.0	0.0
WATER	0.0	0.0	0.0	0.0	5.70113E-02	0.0	0.0
METHANOL	0.0	0.0	0.0	0.0	3.626370	0.0	0.0
ETHANOL	0.0	0.0	0.0	0.0	0.280645	0.0	0.0
WITCO 40 OIL	0.0	0.0	0.0	0.0	2.91377E-02	0.0	0.0

L I Q U I D 2										
TOTAL LIQ.	MOL/HR	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	LB/HR	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
ENTHALPY	BTU/HR	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
LIQ. DENSITY	LB/CUFT	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
AVE. MOL WT		0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
FLOW RATES	MOLES/HR	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
HYDROGEN		0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
CARBON MONOXIDE		0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
CARBON DIOXIDE		0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
METHANE		0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
NITROGEN		0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
WATER		0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
METHANOL		0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
ETHANOL		0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
MITCO 40 OIL		0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
TOTAL LIQ.	MOL/HR	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	LB/HR	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
V A P O R										
ENTHALPY	BTU/HR	-2351447.00	-2563045.00	-2428147.00	-2427595.00	-2165856.00	-2165856.00	-2158738.00	-2158738.00	-2158738.00
VAP. DENSITY	LB/CUFT	1.525253	1.514030	1.819180	1.816683	22.78258	22.78258	27.233008	27.233008	27.233008
AVE. MOL WT		21.993683	21.982254	21.169495	21.169586	20.381674	20.381674	20.354401	20.354401	20.354401
FLOW RATES	MOLES/HR	18.657715	18.809006	18.797119	18.796600	18.785004	18.785004	18.786453	18.786453	18.786453
HYDROGEN		38.526215	38.678456	38.681778	38.681152	38.527792	38.527792	38.638853	38.638853	38.638853
CARBON MONOXIDE		1.638438	1.646322	1.644884	1.644837	1.625691	1.625691	1.627523	1.627523	1.627523
CARBON DIOXIDE		0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
METHANE		0.360110	0.362807	0.362513	0.362502	0.362115	0.362115	0.362178	0.362178	0.362178
NITROGEN		6.06805E-02	6.06805E-02	6.06805E-02	6.06805E-02	6.06805E-02	6.06805E-02	6.06805E-02	6.06805E-02	6.06805E-02
WATER		4.231823	4.260136	4.253716	4.253481	4.25087	4.25087	4.25087	4.25087	4.25087
METHANOL		0.303286	0.306689	0.305212	0.305142	0.305142	0.305142	0.305142	0.305142	0.305142
ETHANOL		0.233050	0.236070	0.23518E-03	0.23518E-03	0.23518E-03	0.23518E-03	0.23518E-03	0.23518E-03	0.23518E-03
MITCO 40 OIL		0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
TOTAL VAPOR	MOL/HR	64.011276	64.580342	64.113419	64.111988	60.057083	60.057083	60.057083	60.057083	60.057083
	LB/HR	1407.843506	1415.220459	1357.248535	1357.223185	1222.863837	1222.863837	1222.17715	1222.17715	1222.17715
ACTUAL CFM		15.383712	15.578962	12.434621	12.451478	8.938054	8.938054	9.006951	9.006951	9.006951

STREAM SUMMARY
VERSION 82.021-A

AIR PRODUCTS & CHEMICALS, IHC --- CYCLE SYNTHESIS
LPMEOH ENTRAINED/KY GAS= EK-4752

T.R.TSAP
87-7-1533

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15:41:04

STREAM SUMMARY

T O A L	50	54	55	57	60	62	65
STREAM NUMBER	84	64	81.4	84	60	64	84
NOTES - BELOW							
PRESSURE PSIA	685.00	685.00	685.00	750.00	685.00	20.00	20.00
TEMPERATURE DEG.F	109.95	109.95	109.95	131.07	109.95	108.15	108.15
DEW POINT DEG.F							
BUBBLE PT DEG.F							
ENTHALPY BTU/HR	-358010.06	-1800727.00	-1801002.00	-1793682.50	-459482.00	-6323.04	-453158.56
LIQ. DENSITY, LB/CUFT	0.0	0.0	0.0	0.0	49.200256	0.0	49.588294
LIQ. DENSITY, LB/CUFT	0.0	0.0	0.0	0.0	49.200256	0.0	0.0
VAP. DENSITY, LB/CUFT	2.263008	2.263008	2.261893	2.379866	0.0	0.0	0.0
AVE. MOL WT	20.354401	20.354401	20.345016	20.345016	32.384901	28.536682	32.162933
FLOW RATES MOLES/HR							
HYDROGEN	3.115586	15.670462	15.780000	15.700000	1.04359E-02	1.03416E-02	9.44845E-05
CARBON MONOXIDE	6.407961	32.230911	32.250000	32.250000	4.23403E-02	4.14396E-02	9.08697E-01
CARBON DIOXIDE	0.269912	1.357611	1.353999	1.353999	1.69134E-02	1.37133E-02	3.19992E-03
METHANE	0.0	0.0	0.0	0.0	0.0	0.0	0.0
NITROGEN	6.00645E-02	0.302114	0.303000	0.303000	3.35529E-04	3.29581E-04	5.94789E-06
WATER	3.19070E-03	1.60487E-02	1.46000E-02	1.46000E-02	0.371491	7.28424E-04	0.370643
METHANOL	9.97338E-02	0.687762	0.687000	0.687000	3.669479	2.16585E-02	3.647820
ETHANOL	4.13460E-03	2.07363E-02	2.10000E-02	2.10000E-02	0.284014	9.31420E-04	0.279485
MITCO 40 OIL	4.76649E-06	2.59746E-05	2.40000E-05	2.40000E-05	8.13739E-01	9.23663E-07	8.13647E-03
TOTAL FLOW MOL/HR	9.957820	50.026075	50.131372	50.131372	4.399499	0.289215	6.310284
LB/HR	202.685455	1019.471924	1019.923384	1019.923384	141.177277	2.256704	138.631363
ACTUAL CFM	1.492744	7.502234	7.515265	7.515265	0.0	0.450481	0.0
	VAP	VAP	VAP	VAP	LIQ	VAP	LIQ

STREAM SUMMARY

STREAM NUMBER	75	76	77	78	80	83	89
NOTES - BELOW							
LIQ. DENSITY, LB/CUFT	710.00	700.00	700.00	685.00	665.00	710.00	765.00
AVE. MOL WT	481.99	291.22	291.22	105.95	258.09	258.14	485.00
FLOW RATES MOLES/HR	-35862768.00	-9158.22	-36632.90	-10163.68	-46816.58	-46805.73	-35859872.00
ETHANOL	217.446823	216.245728	216.245697	219.599338	216.862030	216.862030	217.446182
METHANOL	12.869812	2.48079E-03	9.9215E-03	2.17204E-03	1.20952E-02	1.20952E-02	12.881907
WATER	16.621048	3.45957E-03	1.38333E-02	3.37232E-03	1.72106E-02	1.72106E-02	16.636245
NITROGEN	0.844998	2.96890E-04	1.18756E-03	6.96947E-04	1.88451E-03	1.88451E-03	0.846883
CARBON MONOXIDE	0.0	0.0	0.0	0.0	0.0	0.0	0.0
CARBON DIOXIDE	0.0	0.0	0.0	0.0	0.0	0.0	0.0
METHANE	0.335753	6.10961E-05	2.44385E-04	4.92040E-05	2.93588E-04	2.93588E-04	0.336046
HYDROGEN	2.23517E-08	5.28117E-12	2.1127E-11	8.50404E-12	2.96367E-11	2.96367E-11	2.23514E-08
METHANOL	3.987540	1.33072E-03	5.32380E-03	5.95510E-04	5.91930E-03	5.91930E-03	3.994559
ETHANOL	0.858941	3.06576E-04	1.22830E-03	1.13745E-04	1.34005E-03	1.34005E-03	0.860281
MITCD 40 OIL	215.581741	4.57023E-02	0.182809	4.51145E-02	0.227924	0.227924	215.809662
TOTAL FLOW	251.099838	0.053638	0.214553	0.052114	0.266667	0.266667	251.366501
LIQ. DENSITY, LB/HR	54600.859375	11.599019	46.396072	11.433830	57.829895	57.829895	54658.683594

STREAM NUMBER	75	76	77	78	80	83	89
NOTES - BELOW							
LIQ. DENSITY, LB/CUFT	-35862768.00	-9158.22	-36632.90	-10163.68	-46816.57	-46804.44	-35859856.00
AVE. MOL WT	35.411115	40.375137	40.375137	49.206256	41.147368	41.147368	35.584213
FLOW RATES MOLES/HR	27.466823	216.245682	216.245636	219.399338	216.862030	216.866734	217.446213
ETHANOL	12.869812	2.48079E-03	9.9215E-03	2.17204E-03	1.20952E-02	1.20952E-02	12.881907
METHANOL	16.621048	3.45957E-03	1.38333E-02	3.37232E-03	1.72106E-02	1.72106E-02	16.636245
CARBON DIOXIDE	0.844998	2.96890E-04	1.18756E-03	6.96947E-04	1.88451E-03	1.88451E-03	0.846883
METHANE	0.0	0.0	0.0	0.0	0.0	0.0	0.0
NITROGEN	0.335753	6.10961E-05	2.44385E-04	4.92040E-05	2.93588E-04	2.93588E-04	0.336046
HYDROGEN	2.23517E-08	5.28117E-12	2.1127E-11	8.50404E-12	2.96367E-11	2.96367E-11	2.23514E-08
METHANOL	3.987540	1.33072E-03	5.32380E-03	5.95510E-04	5.91930E-03	5.91930E-03	3.994559
ETHANOL	0.858941	3.06576E-04	1.22830E-03	1.13745E-04	1.34005E-03	1.34005E-03	0.860281
MITCD 40 OIL	215.581741	4.57023E-02	0.182809	4.51145E-02	0.227924	0.227924	215.809662
TOTAL LIQ.	251.099838	0.053638	0.214553	0.052114	0.266667	0.266667	251.366501
LIQ. DENSITY, LB/HR	54600.859375	11.599019	46.396072	11.433830	57.829895	57.829895	54658.683594

STREAM NUMBER	75	76	77	78	80	83	89
NOTES - BELOW							
LIQ. DENSITY, LB/CUFT	0.0	0.0	0.0	-10163.68	0.0	0.0	0.0
AVE. MOL WT	0.0	0.0	0.0	49.206256	0.0	0.0	0.0
FLOW RATES MOLES/HR	0.0	0.0	0.0	219.399338	0.0	0.0	0.0
ETHANOL	0.0	0.0	0.0	2.17204E-03	0.0	0.0	0.0
METHANOL	0.0	0.0	0.0	3.37232E-03	0.0	0.0	0.0
CARBON DIOXIDE	0.0	0.0	0.0	6.96947E-04	0.0	0.0	0.0
METHANE	0.0	0.0	0.0	0.0	0.0	0.0	0.0
NITROGEN	0.0	0.0	0.0	4.92040E-05	0.0	0.0	0.0
HYDROGEN	0.0	0.0	0.0	8.50404E-12	0.0	0.0	0.0
METHANOL	0.0	0.0	0.0	5.95510E-04	0.0	0.0	0.0
ETHANOL	0.0	0.0	0.0	1.13745E-04	0.0	0.0	0.0
MITCD 40 OIL	0.0	0.0	0.0	4.51145E-02	0.0	0.0	0.0

AIR PRODUCTS & CHEMICALS, INC -- CYCLE SYNTHESIS
LPMEOH ENTRAINED/KT GAS: EK-4752

STREAM SUMMARY

STREAM SUMMARY
VERSION 82.021-A

	90	95
T STREAM NUMBER	82.4	86
D NOTES -- BELOW	735.00	478.25
T PRESSURE PSIA	483.00	-36052464.00
A TEMPERATURE DEG.F	-35859408.00	35.711826
L ENTHALPY BTU/HR	55.584747	217.459839
L LIQ. DENSITY, LB/CUFT	217.459839	12.885908
L AVE. MOL WT	12.885908	16.634003
L FLOW RATES MOLES/HR	16.634003	0.847319
L HYDROGEN	0.0	0.0
L CARBON MONOXIDE	0.0	0.335160
L CARBON DIOXIDE	0.0	2.77482E-11
L METHANE	0.0	3.91168
L NITROGEN	2.77482E-11	0.844095
L WATER	3.91168	215.817825
L METHANOL	0.844095	251.355881
L ETHANOL	0.844095	54659.808594
L WTCO 40 OIL	215.817825	
L TOTAL FLOW	251.355881	54659.808594
L MOL/HR	251.355881	54659.808594
L LB/HR	54659.808594	54659.808594
	LIQ	LIQ

- NOTES
1. STREAM SPECIFIED AS ALL VAPOR
 2. STREAM SPECIFIED AS ALL LIQUID
 3. STREAM SPECIFIED AS ALL LIQUID
 4. CAUTION: TWO LIQUID PHASES NOT CONSIDERED. RESULTS MAY BE IN ERROR.

CYCLE SYNTHESIS RUN TIME : 31.74 CPU SECONDS

STREAM SUMMARY
VERSION 82-011-A

AIR PRODUCTS & CHEMICALS, INC. -- CYCLE SYNTHESIS
LPMECH ENTRAINED/A-T MIN PRODH: EK-2371

V. H. EISENHAN
87-7-1533

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12:44:29

STREAM SUMMARY

STREAM NUMBER	1	3	5	10	15	18	20
LIQ. DENSITY, LB/CUFT	0.0	0.0	0.0	0.0	0.0	0.0	0.0
AVE. MOL WT	0.0	0.0	0.0	0.0	0.0	0.0	0.0
FLOW RATES	0.0	0.0	0.0	0.0	0.0	0.0	0.0
HYDROGEN	6.830000	6.830000	6.830000	6.830000	6.830000	5.432695	13.730750
CARBON MONOXIDE	10.790000	10.790000	10.790000	10.790000	10.790000	10.036699	21.610446
CARBON DIOXIDE	0.350000	0.350000	0.350000	0.350000	0.350000	0.387765	0.886584
METHANE	0.0	0.0	0.0	0.0	0.0	0.0	0.0
NITROGEN	1.50000E-02	1.50000E-02	1.50000E-02	1.50000E-02	1.50000E-02	1.50000E-02	5.29285E-02
WATER	0.0	0.0	0.0	0.0	0.0	0.0	7.55270E-03
METHANOL	0.0	0.0	0.0	0.0	0.0	0.0	2.180582
ETHANOL	0.0	0.0	0.0	0.0	0.0	0.0	0.350521
MITCO 40 OIL	0.0	0.0	0.0	0.0	0.0	0.0	215.849014
TOTAL FLOW	17.984985	17.984985	17.984985	17.984985	17.984985	16.549911	254.468323
	331.820313	331.820313	331.820313	331.820313	331.820313	331.818848	54716.281250

LIQ. DENSITY, LB/CUFT	1	3	5	10	15	18	20
AVE. MOL WT	0.0	0.0	0.0	0.0	0.0	0.0	0.0
FLOW RATES	0.0	0.0	0.0	0.0	0.0	0.0	0.0
HYDROGEN	0.0	0.0	0.0	0.0	0.0	0.0	0.0
CARBON MONOXIDE	0.0	0.0	0.0	0.0	0.0	0.0	0.0
CARBON DIOXIDE	0.0	0.0	0.0	0.0	0.0	0.0	0.0
METHANE	0.0	0.0	0.0	0.0	0.0	0.0	0.0
NITROGEN	0.0	0.0	0.0	0.0	0.0	0.0	0.0
WATER	0.0	0.0	0.0	0.0	0.0	0.0	0.0
METHANOL	0.0	0.0	0.0	0.0	0.0	0.0	0.0
ETHANOL	0.0	0.0	0.0	0.0	0.0	0.0	0.0
MITCO 40 OIL	0.0	0.0	0.0	0.0	0.0	0.0	0.0
TOTAL LIQ.	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	0.0	0.0	0.0

ENTHALPY	1	3	5	10	15	18	20
LIQ. DENSITY, LB/CUFT	0.0	0.0	0.0	0.0	0.0	0.0	0.0
AVE. MOL WT	0.0	0.0	0.0	0.0	0.0	0.0	0.0
FLOW RATES	0.0	0.0	0.0	0.0	0.0	0.0	0.0
HYDROGEN	0.0	0.0	0.0	0.0	0.0	0.0	0.0
CARBON MONOXIDE	0.0	0.0	0.0	0.0	0.0	0.0	0.0
CARBON DIOXIDE	0.0	0.0	0.0	0.0	0.0	0.0	0.0
METHANE	0.0	0.0	0.0	0.0	0.0	0.0	0.0
NITROGEN	0.0	0.0	0.0	0.0	0.0	0.0	0.0
WATER	0.0	0.0	0.0	0.0	0.0	0.0	0.0
METHANOL	0.0	0.0	0.0	0.0	0.0	0.0	0.0
ETHANOL	0.0	0.0	0.0	0.0	0.0	0.0	0.0
MITCO 40 OIL	0.0	0.0	0.0	0.0	0.0	0.0	0.0
TOTAL LIQ.	0.0	0.0	0.0	0.0	0.0	0.0	0.0
	0.0	0.0	0.0	0.0	0.0	0.0	0.0

ENTHALPY	1	3	5	10	15	18	20
LIQ. DENSITY, LB/CUFT	0.0	0.0	0.0	0.0	0.0	0.0	0.0
AVE. MOL WT	0.0	0.0	0.0	0.0	0.0	0.0	0.0
FLOW RATES	0.0	0.0	0.0	0.0	0.0	0.0	0.0
HYDROGEN	6.830000	6.830000	6.830000	6.830000	6.830000	5.432695	13.730750
CARBON MONOXIDE	10.790000	10.790000	10.790000	10.790000	10.790000	10.036699	21.610446
CARBON DIOXIDE	0.350000	0.350000	0.350000	0.350000	0.350000	0.387765	0.886584
METHANE	0.0	0.0	0.0	0.0	0.0	0.0	0.0
NITROGEN	1.50000E-02	1.50000E-02	1.50000E-02	1.50000E-02	1.50000E-02	1.50000E-02	5.29285E-02
WATER	0.0	0.0	0.0	0.0	0.0	0.0	7.55270E-03
METHANOL	0.0	0.0	0.0	0.0	0.0	0.0	2.180582
ETHANOL	0.0	0.0	0.0	0.0	0.0	0.0	0.350521
MITCO 40 OIL	0.0	0.0	0.0	0.0	0.0	0.0	215.849014
TOTAL LIQ.	17.984985	17.984985	17.984985	17.984985	17.984985	16.549911	254.468323
	331.820313	331.820313	331.820313	331.820313	331.820313	331.818848	54716.281250

ENTHALPY	1	3	5	10	15	18	20
LIQ. DENSITY, LB/CUFT	0.0	0.0	0.0	0.0	0.0	0.0	0.0
AVE. MOL WT	0.0	0.0	0.0	0.0	0.0	0.0	0.0
FLOW RATES	0.0	0.0	0.0	0.0	0.0	0.0	0.0
HYDROGEN	6.830000	6.830000	6.830000	6.830000	6.830000	5.432695	13.730750
CARBON MONOXIDE	10.790000	10.790000	10.790000	10.790000	10.790000	10.036699	21.610446
CARBON DIOXIDE	0.350000	0.350000	0.350000	0.350000	0.350000	0.387765	0.886584
METHANE	0.0	0.0	0.0	0.0	0.0	0.0	0.0
NITROGEN	1.50000E-02	1.50000E-02	1.50000E-02	1.50000E-02	1.50000E-02	1.50000E-02	5.29285E-02
WATER	0.0	0.0	0.0	0.0	0.0	0.0	7.55270E-03
METHANOL	0.0	0.0	0.0	0.0	0.0	0.0	2.180582
ETHANOL	0.0	0.0	0.0	0.0	0.0	0.0	0.350521
MITCO 40 OIL	0.0	0.0	0.0	0.0	0.0	0.0	215.849014
TOTAL LIQ.	17.984985	17.984985	17.984985	17.984985	17.984985	16.549911	254.468323
	331.820313	331.820313	331.820313	331.820313	331.820313	331.818848	54716.281250

ENTHALPY	1	3	5	10	15	18	20
LIQ. DENSITY, LB/CUFT	0.0	0.0	0.0	0.0	0.0	0.0	0.0
AVE. MOL WT	0.0	0.0	0.0	0.0	0.0	0.0	0.0
FLOW RATES	0.0	0.0	0.0	0.0	0.0	0.0	0.0
HYDROGEN	6.830000	6.830000	6.830000	6.830000	6.830000	5.432695	13.730750
CARBON MONOXIDE	10.790000	10.790000	10.790000	10.790000	10.790000	10.036699	21.610446
CARBON DIOXIDE	0.350000	0.350000	0.350000	0.350000	0.350000	0.387765	0.886584
METHANE	0.0	0.0	0.0	0.0	0.0	0.0	0.0
NITROGEN	1.50000E-02	1.50000E-02	1.50000E-02	1.50000E-02	1.50000E-02	1.50000E-02	5.29285E-02
WATER	0.0	0.0	0.0	0.0	0.0	0.0	7.55270E-03
METHANOL	0.0	0.0	0.0	0.0	0.0	0.0	2.180582
ETHANOL	0.0	0.0	0.0	0.0	0.0	0.0	0.350521
MITCO 40 OIL	0.0	0.0	0.0	0.0	0.0	0.0	215.849014
TOTAL LIQ.	17.984985	17.984985	17.984985	17.984985	17.984985	16.549911	254.468323
	331.820313	331.820313	331.820313	331.820313	331.820313	331.818848	54716.281250

ENTHALPY	1	3	5	10	15	18	20
LIQ. DENSITY, LB/CUFT	0.0	0.0	0.0	0.0	0.0	0.0	0.0
AVE. MOL WT	0.0	0.0	0.0	0.0	0.0	0.0	0.0
FLOW RATES	0.0	0.0	0.0	0.0	0.0	0.0	0.0
HYDROGEN	6.830000	6.830000	6.830000	6.830000	6.830000	5.432695	13.730750
CARBON MONOXIDE	10.790000	10.790000	10.790000	10.790000	10.790000	10.036699	21.610446
CARBON DIOXIDE	0.350000	0.350000	0.350000	0.350000	0.350000	0.387765	0.886584
METHANE	0.0	0.0	0.0	0.0	0.0	0.0	0.0
NITROGEN	1.50000E-02	1.50000E-02	1.50000E-02	1.50000E-02	1.50000E-02	1.50000E-02	5.29285E-02
WATER	0.0	0.0	0.0	0.0	0.0	0.0	7.55270E-03
METHANOL	0.0	0.0	0.0	0.0	0.0	0.0	2.180582
ETHANOL	0.0	0.0	0.0	0.0	0.0	0.0	0.350521
MITCO 40 OIL	0.0	0.0	0.0	0.0	0.0	0.0	215.849014
TOTAL LIQ.	17.984985	17.984985	17.984985	17.984985	17.984985	16.549911	254.468323
	331.820313	331.820313	331.820313	331.820313	331.820313	331.818848	54716.281250

T	STREAM NUMBER	64	65	75	76	77	78	80
0	NOTES - BELOW							
1	TEMPERATURE PSIA	20.00	120.95	510.00	500.00	500.00	485.00	82.4
2	TEMPERATURE DEG.F	110.95	110.95	517.98	380.62	360.62	111.44	685.00
3	TEMPERATURE DEG.F	110.95	110.95	517.98	380.62	360.62	111.44	381.30
4	ENTHALPY BTU/HR	-420.59	-59716.89	-33853696.00	-4811.83	-19247.33	-8231.73	-27879.85
5	LIQ. DENSITY, LB/CUFT	0.0	58.337173	35.416061	0.0	39.656020	50.132236	41.079178
6	LIQ. DENSITY, LB/CUFT	0.0	0.0	0.0	0.0	0.0	45.308197	0.0
7	VAP. DENSITY, LB/CUFT	0.0	0.0	0.0	0.0	0.0	0.0	0.0
8	AVE. MOL WT	27.950607	30.825104	228.587967	229.532414	229.552490	228.546821	229.288132
9	FLOW RATES MOLES/HR							
10	HYDROGEN	7.85976E-04	1.17184E-05	8.292952	9.03152E-04	3.61261E-03	1.17247E-03	4.78597E-03
11	CARBON MONOXIDE	2.75960E-03	8.87543E-05	11.370148	1.28414E-03	5.13656E-03	1.83617E-03	6.97271E-03
12	CARBON DIOXIDE	8.72240E-04	3.26645E-04	0.498584	8.26423E-05	3.30569E-04	3.56114E-04	6.46683E-04
13	METHANE	0.0	0.0	0.0	0.0	0.0	0.0	0.0
14	NITROGEN	3.72299E-06	1.04352E-07	3.75555E-02	3.85393E-06	1.54157E-05	4.28025E-06	1.95940E-05
15	WATER	1.01322E-04	8.80014E-02	0.0	2.16963E-13	0.67844E-13	5.20623E-12	4.37431E-12
16	METHANOL	1.45187E-03	0.432843	1.565284	2.37132E-04	8.68730E-04	3.59652E-04	1.52339E-03
17	ETHANOL	6.98284E-05	3.45612E-02	0.306313	4.30478E-05	1.80391E-04	7.83792E-05	2.56571E-04
18	MITCO 40 OIL	6.78559E-08	2.91367E-04	215.707886	2.595968E-02	0.180387	3.66362E-02	0.140823
19	TOTAL FLOW	0.006849	0.561524	237.756713	0.028553	0.114131	0.040668	0.154799
20	LB/HR	0.168953	17.309836	54368.777344	6.549754	26.199005	9.294561	35.493561
21	ACTUAL CFM	0.0	0.0	0.0	0.0	0.0	0.0	0.0

T	STREAM NUMBER	83	89	90	95
0	NOTES - BELOW				
1	TEMPERATURE PSIA	82.4	82.4	82.4	84
2	TEMPERATURE DEG.F	510.00	545.00	545.00	535.00
3	TEMPERATURE DEG.F	301.33	519.05	519.34	517.32
4	ENTHALPY BTU/HR	-27872.39	-33831440.00	-33831440.00	-33903296.00
5	LIQ. DENSITY, LB/CUFT	41.078465	35.386124	35.386124	35.434810
6	LIQ. DENSITY, LB/CUFT	229.288132	228.588425	228.584518	228.584518
7	VAP. DENSITY, LB/CUFT	0.0	0.0	0.0	0.0
8	AVE. MOL WT	27.950607	30.825104	228.587967	229.532414
9	FLOW RATES MOLES/HR				
10	HYDROGEN	4.78507E-03	8.237736	8.298075	8.298075
11	CARBON MONOXIDE	6.97271E-03	11.377120	11.375752	11.375752
12	CARBON DIOXIDE	6.86683E-04	0.499270	0.498818	0.498818
13	METHANE	0.0	0.0	0.0	0.0
14	NITROGEN	1.96960E-05	3.75782E-02	3.79203E-02	3.79203E-02
15	WATER	6.07413E-12	6.07613E-12	6.49384E-12	6.49384E-12
16	METHANOL	1.25319E-03	1.546537	1.553643	1.553643
17	ETHANOL	2.58571E-04	0.306572	0.305203	0.305203
18	MITCO 40 OIL	0.140823	215.848694	215.849014	215.849014
19	TOTAL FLOW	0.154799	237.913498	237.918411	237.918411
20	LB/HR	35.493561	54384.289531	54384.464844	54384.464844

NOTES

1. STREAM SPECIFIED AS ALL VAPOR
2. STREAM SPECIFIED AS ALL LIQUID
3. STREAM SPECIFIED AS LIQUID AND VAPOR
4. CAUTION: TWO LIQUID PHASES NOT CONSIDERED. *RESULTS MAY BE IN ERROR.

CYCLE SYNTHESIS RUN TIME : 29.41 CPU SECONDS



PAGE 1 of 2
 DATE 1/29/82
 REVISED _____

EXHIBIT 2.3.1-6

CENTRIFUGAL PUMP SPECIFICATION SHEET

CUSTOMER	APCI	
VENDOR	By Elec. Mech.	UNIT LP MeOH PDU PROJECT NO. 87-7-1533
GENERAL INFORMATION		
1. ITEM NO.	Slurry Circulation Pump	
2. NO. REQUIRED	10.50 A & B	
3. TYPE	Two (2) - one on stream & one spare	
4. DUTY (CONTINUOUS, INTERMITTENT)	Continuous	
5. SERVICE	To circulate hot oil and hot oil-catalyst slurry	
PROCESS INFORMATION		
6.	Liquid Fluidized Mode	Liquid Entrained Mode
7. FLUID	*Hydrocarbon Fluid & Dissolved Syngas+CH ₃ OH	Hydrocarbon Fluid-Catalyst
8. CORROSIVE COMPOUNDS		Slurry & Dissolved Syngas & CH ₃ O
9. SOLIDS	None	Metal oxides powder: ~50%
10. TEMPERATURE, OPERATING, °F	430~530	430~530
11. TEMPERATURE, MAXIMUM, °F	550	550
12. VAPOR PRESSURE, OPERATING @530°F, psia	5 sat'd w/H ₂	5
13. SPECIFIC GRAVITY, OPERATING @480°F	0.63	0.89
14. SPECIFIC GRAVITY, @ 60°F	0.8	1.15
15. VISCOSITY, OPERATING @480°F CPS	0.7	1.0 Max. Slurry Conditions
16. VISCOSITY, @ 60°F CPS	6	9
17. NORMAL FLOW - GPM	200	200
18. MAXIMUM FLOW GPM	250	250
19. Minimum Flow GPM	150	150
20. Solid Concentration Wt.%	0	33 Max. (8% by vol. @ 100°F 6% by vol. @ 480°F)
HYDRAULIC INFORMATION		
21. NPSH REQUIRED	By Elec. Mech.	By Elec. Mech.
22. NPSH AVAILABLE		
23. SUCTION PRESSURE PSI	495/695/895	495/695/895
24. DISCHARGE PRESSURE PSI	545/745/945	545/745/945
25. HEAD REQUIRED PSI	50 = 185 ft. @ 480°F	50 = 130 ft. @ 480°F
26. HEAD AVAILABLE PSI		
27. Avail. Condensed Oil for Seal Flush, GPM @280°F, Min/Max	0.1/1	0.1/0.7
28.		
CONSTRUCTION		
29. MATERIAL OF CONSTRUCTION		
30. CONNECTIONS (INCLUDE FIG. RATING)	3-1/2" in/3-1/2" cut or by vendor	
31. PACKING AND/OR SEALS	Seal flush requirement should be minimized to less than 0.1 GPM	
32. IMPELLER TYPE	if possible. The use of water as supplement seal flush should	
33. STUFFING BOX	only be considered as the last alternative when other means to	
34. SMOOTHING GLAND	provide adequate seal flush fail. Vendor should specify the	
35. MANUFACTURERS MODEL NO.	desired quality of seal flush, allowable solid loading,	
36.	particle size, etc.	
DRIVER		
37. TYPE	Electric Motor	
38. CURRENT CHARACTERISTICS		
39. MOTOR CLASS		
40. RPM & HORSEPOWER RATING		
41. BHP @ REQUIRED CAPACITY		
42. MANUFACTURE & MODEL NO.		
43.	*See attached Table 1	
44.		

SPECIFIED BY T. R. Tsao 1/29/82

SPECIFICATION SHEET

For Slurry Circulation Pump 10.50 A&E

29 January 82

EXHIBIT 2.3.1-6

RELEASED FOR PROJECT

Table 1

PROPERTIES OF MITCO #40 OIL

1. Composition - (72% paraffinic, 28% naphthentic)

<u>Component</u>	<u>%</u>
C14	5
C14-C15	15
C16-C17	20
C18-C19	25
C20-C21	20
>C21	15
Sulfur	1 ppm

2. Viscosity,

Kinematic = 4.2 cSt @100°F
Saybolt = 40-43 SUS @100°F

3. Vapor Pressure < 0.002 mm Hg @100°F

4. Specific Gravity = 0.810 @ 60°F
Density = 0.810 g/cc @100°F

5. Initial Boiling Point = 471°F @ 1 atm.

6. Solubility in Methanol:

7.2 wt. % oil @ 0 wt. % H₂O in methanol and 120°F
2.9 wt. % oil @ 0 wt. % H₂O in methanol and 70°F
2.1 wt. % oil @ 5 wt. % H₂O in methanol and 120°F
(Insoluble in Water)

7. M.W. = 268.5 lb./lb. mole

8. ASTM Pour Point = -35°F, maximum

9. Surface Tension = 32 dynes/cm. @ ~ 68°F
= 13 dynes/cm. @ ~ 464°F

10. ASTM Cloud Point = +40°F, Maximum

11. Saybolt Color = +30

12. Odor or Taste → None

13. U.V. Absorbance → Passes FDA Requirements

14. USP Acid Test → Passes



COMPRESSOR SPECIFICATION SHEET
EXHIBIT 2.3.1-7A

PAGE 1/2
DATE 29 January 1982
REVISED _____

CUSTOMER	APCI		
VENDOR	By Elec. Mech.		
UNIT	LP MeOH PDU	PROJECT NO.	87-7-1533
GENERAL INFORMATION			
1. ITEM NO.	Feed Compressor		
2. NO. REQUIRED	01.10		
3. TYPE	one (1)		
4. DUTY	Reciprocating Compressor expected		
5. SERVICE	Continuous		
6. FLUID	Compress Dry Synthesis Gas (H ₂ , CO, CO ₂ , N ₂ , CH ₄)		
PROCESS INFORMATION			
7. COMPOSITION - MOL%	Synthesis Gas		
8. AVERAGE MOLECULAR WEIGHT	(see page 2/2)		
9. CORROSIVE COMPOUNDS	(see page 2/2)		
10. RELATIVE HUMIDITY	7% (7x10 ⁻⁴ LB H ₂ O/lb of Gas, D.P. = 27°F)		
11. SUCTION TEMPERATURE °F.	100 Norm., 125 Max.		
12. SUCTION PRESSURE - PSIA	150	150	150
13. DISCHARGE PRESSURE - PSIA*	550*	750**	950***
14. DISCHARGE TEMPERATURE °F.			
15. NORMAL SUCTION FLOW RATE			
A. A.C.F.M.	(see page 2/2)		
B. POUNDS/HOUR			
16. STANDARD CUBIC FEET/MINUTE			
17. COOLING WATER SUPPLY °F.	90 Nor., 105 Max. @ 43 psig†		
18. COOLING WATER RETURN °F.	120 Nor., 105 Max. @ 10 psig†		
19. CP/CV			
CONSTRUCTION			
20. TYPE OF COMPRESSOR			
21. MATERIAL OF CONSTRUCTION			
22. SUCTION CONNECTIONS	2-1/2" or by vendor		
23. DISCHARGE CONNECTIONS	2-1/2" or by vendor/interstage relief valve inlet flange		
24. TYPE OF LUBRICATION	2-1/2" with 450 psig design press		
25. COMPRESSOR SPEED			
26. AFTERCOOLER REQUIRED	Intercooler & recycle cooler design for 100% recycle		
27. CODE STAMP FOR AFTERCOOLER	Yes, ASME Sec. VIII		
28. AFTERCOOLER SURFACE FT ²	Intercooler by compressor vendor; recycle cooler by proce		
29. WATER REQUIRED GPM	By vendor **Cooling water is a premium		
30. Utility	Minimize cooling water requirement		
ACCESSORIES			
31. FILTER			
32. CLEARANCE POCKETS			
33. UNLOADERS			
34.			
35.			
36.			
DRIVER			
37. TYPE	Electric Motor		
38. POWER CHARACTERISTICS			
39.			
40.	+Vendor to specify the inlet condition of recycle cooler		
41. MOTOR CLASS	*Design/Elec. Mech. should confirm that the max. discharge		
42. MOTOR TYPE	pressure, 950 psig = 935 psig is attainable when the		
43. POWER FACTOR	relief valves of the compressor is set at 1000 psig,		
44. M. G. SET	the design pressure of the PDU.		
45.	*For cases operating at 500 psig		
46. STARTER	**For cases operating at 700 psig		
47. TYPE	***For cases operating at 900 psig		
48. ENCLOSURE	†Project should confirm temp. and pressure of		
49.	cooling water in writing.		

EXHIBIT 2.3.1-7A

LPMOH PDU; FEED COMPRESSOR, 01.10

87-7-1533

	For Lurgi-type Reactor Feed, Mol %	For KT-type Reactor Feed, Mol %	For Balanced Fresh Feed, Mol %	N ₂ Mol %
H ₂	50 ~ 63	38 ~ 51	65 ~ 67	
CO	25 ~ 29	49 ~ 60	30 ~ 33	
CO ₂	4 ~ 10	0 ~ 2	0 ~ 3	
N ₂	0 ~ 15	0 ~ 1	0 ~ 1	99.99
CH ₄	0 ~ 15	trace	trace	
O ₂	trace	trace	trace	trace

	Lightest Mol %	Heaviest Mol %	Lightest Mol %	Heaviest Mol %	Lightest Mol %	Heaviest Mol %	
H ₂	63	50	51	38	67	67	-
CO	29	25	49	60	33	29	-
CO ₂	4	10	-	2	-	3	-
N ₂	4	15	-	-	-	1	99.99
CH ₄	-	-	-	-	-	-	-
O ₂	-	-	-	-	-	-	Trace
Total	100	100	100	100	100	100	100
M.W.	12.3	16.6	14.7	18.5	10.6	11.1	28

Suction Flow Rate	Min	Nor	Max	Min	Nor	Max	Min	Nor	Max	Nor	Max
1b-mol/hr	18	60	100	18	40	55	18	50	80	20	30
A.C.F.M.	12	40	67	12	27	37	12	34	54	13	20
1b/hr	220	870	1660	265	660	1020	190	540	890	560	840
SCFM @ 1 atm. 70°F ‡	116	387	644	116	258	354	116	322	516	129	193

‡386.68 SCF/1b-mol

T. R. Tsao
1/29/82



COMPRESSOR SPECIFICATION SHEET

PAGE 1/2
DATE 29 January 1982
REVISED

EXHIBIT 2.3.1-7B

CUSTOMER APCI
VENDOR By Elec. Mech. UNIT LP MeOH PDU PROJECT NO. 87-7-1533

GENERAL INFORMATION
Recycle Compressor

- 1. ITEM NO. 01.20
2. NO. REQUIRED one (1)
3. TYPE Reciprocating Compressor Expected
4. DUTY Continuous
5. SERVICE Compress Recycle Gas

PROCESS INFORMATION

- 6. FLUID Unconverted Synthesis Gas or Nitrogen
7. COMPOSITION - MOL% (see page 2/2)
8. AVERAGE MOLECULAR WEIGHT (see page 2/2)
9. CORROSIVE COMPOUNDS H2O, CO2, CH3OH, C2H5OH & Higher Alcohols
10. RELATIVE HUMIDITY 100% Saturated w/H2O & CH3OH
11. SUCTION TEMPERATURE °F. 110 Norm., 125 Max.
12. SUCTION PRESSURE - PSIA 485* 685** 885***
13. DISCHARGE PRESSURE - PSIA* 550 750 950
14. DISCHARGE TEMPERATURE °F.
15. NORMAL SUCTION FLOW RATE
A. A.C.F.M.
B. POUNDS/HOUR (see page 2/2)
16. STANDARD CUBIC FEET/MINUTE
17. COOLING WATER SUPPLY °F. 90 Nor., 105 Max. @ 43 psig ‡
18. COOLING WATER RETURN °F. 120 Nor., 105 Max. @ 10 psig ‡
19. CP/CV

CONSTRUCTION

- 20. TYPE OF COMPRESSOR
21. MATERIAL OF CONSTRUCTION
22. SUCTION CONNECTIONS 2-1/2" or by vendor
23. DISCHARGE CONNECTIONS 2-1/2" or by vendor
24. TYPE OF LUBRICATION
25. COMPRESSOR SPEED
26. AFTERCOOLER REQUIRED Only required for the compressor recycle stream. Design
27. CODE STAMP FOR AFTERCOOLER Yes. ASME Sec. VIII 100% Recycle
28. AFTERCOOLER SURFACE FT² By Process. vendor to specify inlet condition of recycle
29. WATER REQUIRED GPM By vendor. **Cooling water is a premium cooler
30. Utility Minimize cooling water requirement

ACCESSORIES

- 31. FILTER
32. CLEARANCE POCKETS
33. UNLOADERS
34.
35.
36.

DRIVER

- 37. TYPE Electric Motor
38. POWER CHARACTERISTICS
39.
40.
41. MOTOR CLASS
42. MOTOR TYP. *Design/Elec. Mech. should confirm that the max.
43. POWER FACTOR discharge pressure, 950 psia = 935 psig, is attainable
44. M. G. SET when the relief valves of the compressor is set at
45. 1000 psig, the design pressure of the PDU.

STARTER *For cases operating at 500 psig

- 46. TYPE **For cases operating at 700 psig
47. ENCLOSURE ***For cases operating at 900 psig
48. ‡Project should confirm temp. and pressure of cooling water in writing.

	For Lurgi-type Reactor Feed, Mol %	For KT-type Reactor Feed, Mol %	For Balanced Fresh Feed, Mol %	N ₂ Mol %
H ₂	45 ~ 63	25 ~ 51	40 ~ 50	
CO	22 ~ 29	60 ~ 70	20 ~ 25	
CO ₂	10 ~ 15	1 ~ 3	10 ~ 20	
N ₂	15 ~ 18	0 ~ 2	10 ~ 20	99.99
CH ₄	15 ~ 18	trace	10 ~ 20	
CH ₃ OH	1 ~ 2	1 ~ 2	1 ~ 2	
C ₂ H ₅ OH	(0 ~ 1200 ppmv)	(0 ~ 1200 ppmv)	(0 ~ 1200 ppmv)	
H ₂ O	(200 ~ 1000 ppmv)	(200 ~ 1000 ppmv)	(200 ~ 1000 ppmv)	
O ₂	trace	trace	trace	trace
Witco #40 Oil	trace	trace	trace	trace

	Lightest Mol %	Heaviest Mol %	Lightest Mol %	Heaviest Mol %	Lightest Mol %	Heaviest Mol %	N ₂ Mol %
H ₂	63	45	51	25	67	40	-
CO	29	22	49	70	33	20	-
CO ₂	4	15	-	3	-	19	-
N ₂	4	16	-	-	-	19	99.99
CH ₄	-	-	-	-	-	-	-
CH ₃ OH	-	2	-	2	-	2	-
C ₂ H ₅ OH	-	1200 ppmv	-	1200 ppmv	-	1200 ppmv	-
H ₂ O	-	1000 ppmv	-	1000 ppmv	-	1000 ppmv	-
O ₂	-	-	-	-	-	-	trace
Total	100	100	100	100	100	100	100
M.W.	12.3	18.8	14.7	22.1	10.6	20.7	28

Suction Flow Rate	Min	Nor	Max	Min	Nor	Max	Min	Nor	Max	Nor	Max
lb.mol/hr	50	150	300	50	100	250	50	150	300	150	330
A.C.F.M.	*	*	*	*	*	*	*	*	*	*	*
lb/hr	615	2333	5640	735	1840	5525	530	2348	6210	4200	9240
SCFM @ 1 atm. 70°F #	322	967	1933	322	644	1611	322	967	1933	967	2127

*A.C.F.M. = $\frac{(\text{Suction Flow, Lb-Mol/Hr})}{60} \times \frac{(10.73)(460 + \text{Suction T, } ^\circ\text{F})}{(\text{Suction Press, psia})}$

‡386.68 SCF/lb-mol

T. R. Tsao
1/29/82



VENDOR:

EXHIBIT 2.3.1-8

HEAT EXCHANGER SPECIFICATION SHEET

1	Customer		APCI/DOE LPMeOH PDU		Job No.	27-7-1533		
2	Address		LaPorte, TX		Reference No.			
3	Plant Location		LaPorte, TX		Proposal No.			
4	Service of Unit		Slurry Heat Exchanger		Date	3/22/82 Rev. 0		
5	Size		Type (Hor./Vert) Vertical		Item No.	21.20		
6	Surf/Unit (Gross/Eff.)		58 ft ² *		Sq Ft: Shells/Unit	1		
7	Surf/Shell (Gross/EF.)		53*		Sq Ft			
8	PERFORMANCE OF ONE UNIT							
9	Fluid Allocation		Shell Side		Tube Side			
10	Fluid Name		Utility Oil		Oil/Catalyst Slurry			
11	Fluid Quantity, Total		Lb/Mr 60220		75390			
12	Vapor (In./Out)		0		0			
13	Liquid		60220		75390			
14	Steam		-		-			
15	Water		-		-			
16	Noncondensable		-		-			
17	Temperature (In./Out)		°F 554.0		551.3			
18	Density		Lb/Ft ³ 39		47			
19	Viscosity, Liquid		Cp 0.65		0.80			
20	Molecular Weight, Vapor		-		-			
21	Molecular Weight, Liquid		250		-			
22	Specific Heat		Btu/Lb °F 0.77		0.65			
23	Thermal Conductivity		Btu Ft/Hr Sq Ft °F 0.048		0.050			
24	Volume pct. solids		zero		1.5 (6.0 max.)			
25	Inlet Pressure (min/max.)		Psig 40/100		450/950			
26	Velocity minimum (note 3)		Ft/S 3		5 (10 max.)			
27	Pressure Drop, Allow. Calc.		Psi 5		5			
28	Fouling Resistance (Min.)		Hr. Ft ² °F/BTU 0.002		0.003			
29	Heat Exchanged		123,340 (see note 1)		Btu/Hr: MTD (Corrected) °F			
30	Transfer Rate, Service		Clean 88*		Btu/Hr Sq Ft °F			
31	CONSTRUCTION OF ONE SHELL							
32	Design-Test Pressure		Shell Side 140 /		Tube Side 1000 /			
33	Design Temperature		°F 600		600			
34	No. Passes per Shell		1		1 max.			
35	Corrosion Allowance		In. by design		by design			
36	Connections		In 4"*		4"*			
37	Size & Rating		Out 4"*		4"*			
38	Rating		Intermediate -		-			
39	Tube No.		42* OD 3/4" Thk (Min/Avg) 0.166" In.		Length 7* Ft: Pitch 15/16" (30) 60 90 45			
40	Tube Type		14 BWG (design to verify)*		Material C. Steel			
41	Shell		C. Steel Nom 10*		In. Shell Cover (Integ.) (Remov.)			
42	Channel or Bonnet		Conical (see note 4)		Channel Cover			
43	Tubesheet-Stationary				Tubesheet-Floating			
44	Floating Head Cover				Impingement Protection			
45	Baffles-Cross		Type by vendor		% Cut (Diam/Area) Sealing: c/c Inlet In.			
46	Baffles-Long				Seal Type			
47	Supports-Tube		U-Bend		Type			
48	Bypass Seal Arrangement				Tube-Tubesheet Joint			
49	Expansion Joint				Type			
50	1/2" Inlet Nozzle		Bundle Entrance		Bundle Exit			
51	Gaskets-Shell Side				Tube Side			
52	-Floating Head							
53	Code Requirements				TEMA Class			
54	Weight/Shell		Filled with Water		Bundle Lb			
55	Remarks							
56	SEE REMARKS PAGE 3							
57								
58								
59								
60								
61								

**HEAT EXCHANGER SPECIFICATION SHEET
ADDITIONAL INFORMATION REQUIRED BY AIR PRODUCTS & CHEMICALS, INC.**

ADDITIONAL PROCESS DATA										
9.1	Service of Unit	Condenser	Cooler	OR	Heater	Reboiler	Vaporizer			
7.1	Number of Units Required	ONE (1)								
		Shell Side				Tube Side				
		IN		OUT	IN		OUT			
17.1	Temperature/Bubble Point	°F	> 600°F				Saturated Liquid			
18.1	Density, V/L	Lbs./Cu. Ft.								
19.1	Viscosity, V/L	Cp								
20.1	Molecular Weight, V/L	Lbs./Mole								
22.1	Specific Heat, V/L	Btu/Lb. °F								
23.1	Thermal Conductivity, V/L	Btu Ft./Hr. Sq. Ft. °F								
25.1	Highest Operating Pressure, psia		100				950			
26.1	Velocity, In/Out	Ft./Sec.	3.1*				5.7*			
30.1	Heat Transfer Coeff. Clean	Btu/Hr. Sq. Ft. °F	150*				220*			
30.2	Transfer Rate Fouled	Btu/Hr. Sq. Ft. °F	Nominal				60*			
30.3	Transfer Rate Clean	Btu/Hr. Sq. Ft. °F	Nominal				88*			
30.4	Transfer Rate Service	Btu/Hr. Sq. Ft. °F	(includes 40% Process Safety Factor)				43*			
ADDITIONAL MECHANICAL DATA										
39.1	Additional Connections	Vents: Number	Size & Rating							
39.2		Drains: Number	Size & Rating							
39.3		Rupture Discs: Number	Size & Rating							
40.1	Finned or Extended Surface: Type						Area Ratio A _o /A _i			
40.2	Surface or Bundle Mfr.	Model & Description								
40.3	Fin Count	FPI	Fin Thick	In	Fin Mat'l.	Coating				
40.4	Bundle Length	In	Height	In	Depth	In	Face Area	Ft. ²		
40.5	Seal Type & Arrangement (Describe)									
44.1	Tube Sheet:									
44.2	Stationary	Material	Thickness	In.	Corrosion Allowance	In.				
	Floating	Material	Thickness	In.	Corrosion Allowance	In.				
	Baffle Thickness	In.	Method of Fastening (Describe)							
	Baffle Spacer Mat'l.	Size	Tie Rod Mat'l.	Size						
	Diametrical Clearances:									
	Bundle to Shell	In.	Baffle to Shell	In.	Tube to Baffle Hole	In.				
	Demister, Perforated Plate or Condensate Removal Device Type & Description:									
	Lifting Lugs									
	Paint									
	Cleaning Requirements									
	Shipping Requirements									
	Exchanger Drawing Number									
	Detail Method & Rating Heat Transfer Coefficient									
	Detail Method of Calculating MTD									
	Remarks									
	SEE REMARKS PAGE 3									

L. W. Bonnell 3/22/82
T. R. Tsao 3/22/82

L. W. Bonnell
19 March 1982

EXHIBIT 2.3.1-8

21.20 Slurry Heat Exchanger Remarks

87-7-1533

1. APCI Design Case: EK-2571 with 150 MBTU/hr. heat leak. 40 percent process duty safety factor has been applied.
2. Shell and Tube flowrate design ranges (gpm)

	Min.	Normal	Max.
Shell (oil)	100	200	210
Tube (slurry)	200	200	260

3. Minimum tubeside velocities must be maintained between 5 and 10 ft/sec for above flow range.
4. Due to slurry service and erosion concerns, one tube pass strongly recommended, with vertical upflow of slurry in normal operation. Inlet (front) head should be cone-shaped, to eliminate dead spaces where solids can gather.
5. Data marked with an asterisk ("*") on pp. 1 & 2 are given for estimate purposes only, and do not constrain the vendor's design.
6. See p. 4 for sketch of 21.20 and utility oil system. 21.20 will function as both heater and cooler. Design Eng. and the vendor to ensure that exchanger is designed to handle large shell-to-tube temperature differences.
7. Catalyst particle size (typical): 60 microns

UTILITY OIL SYSTEM

EXHIBIT 2.3.1-8

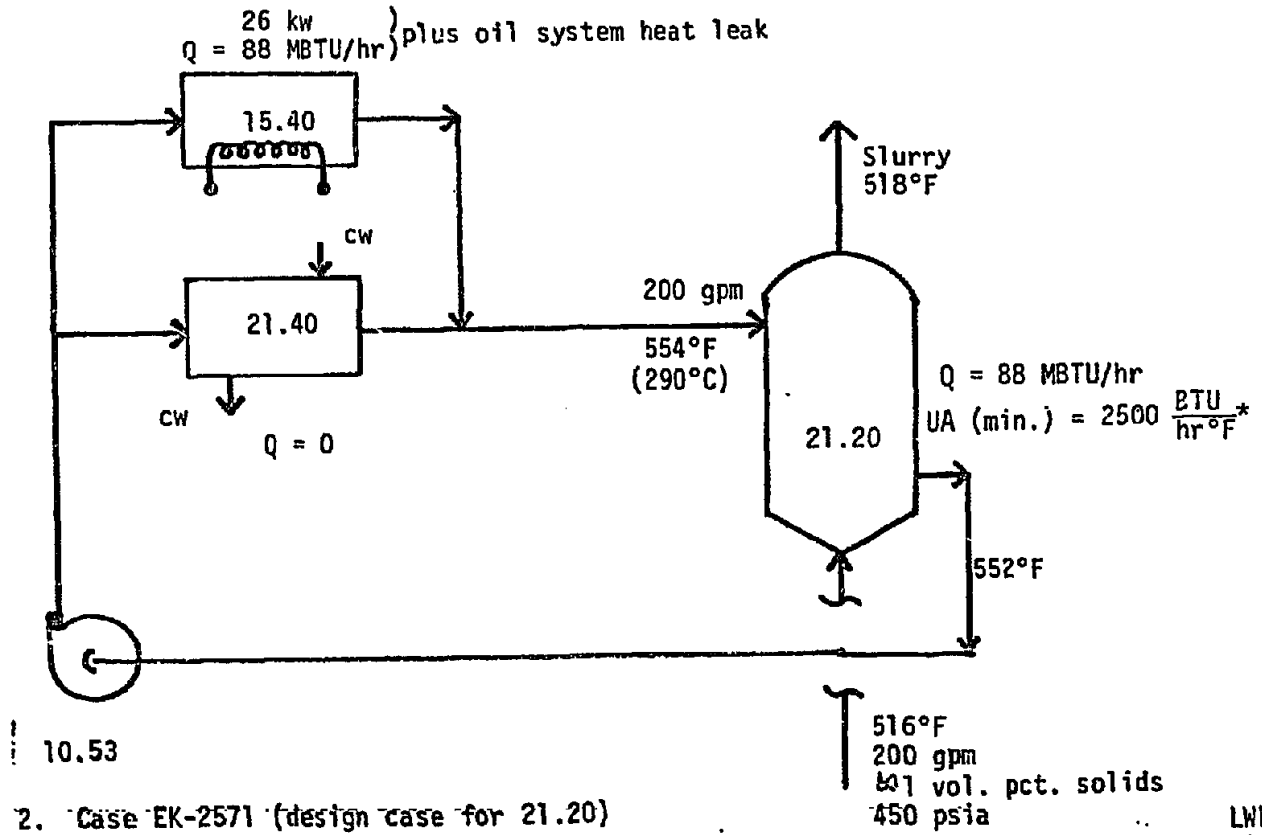
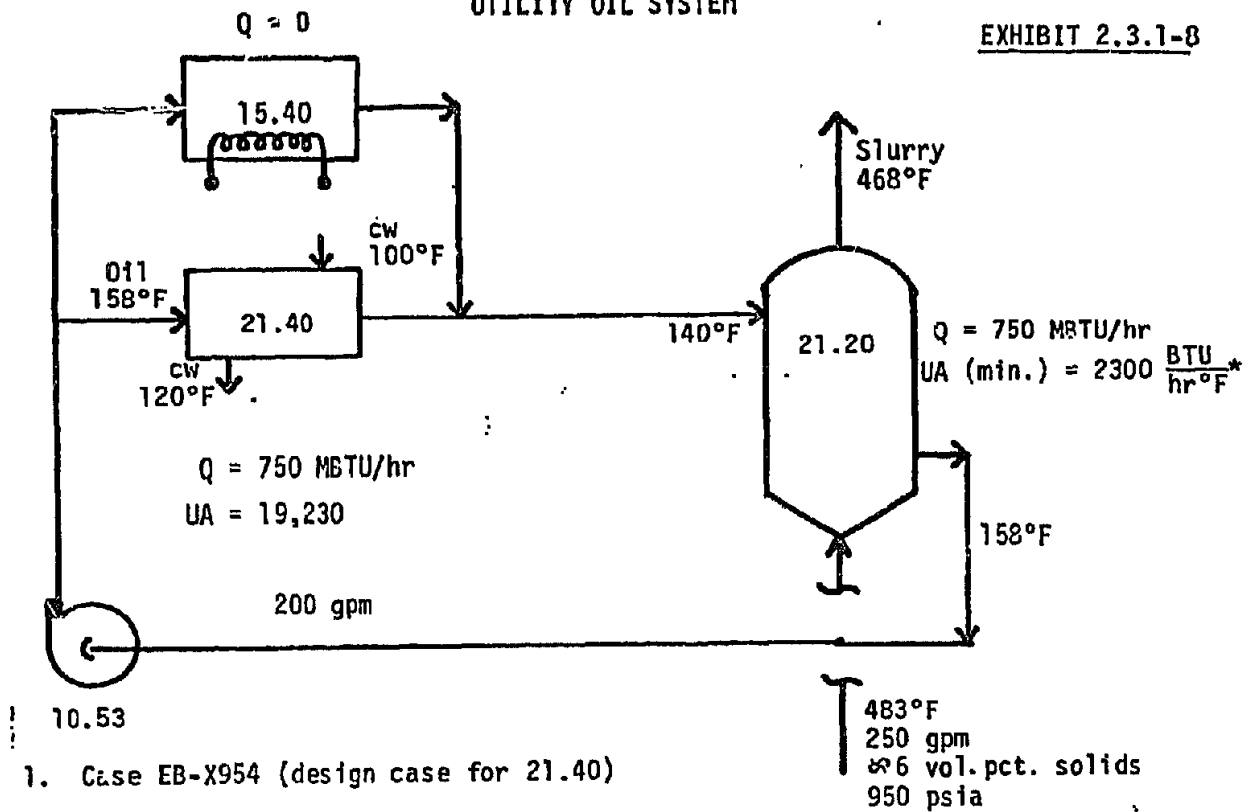
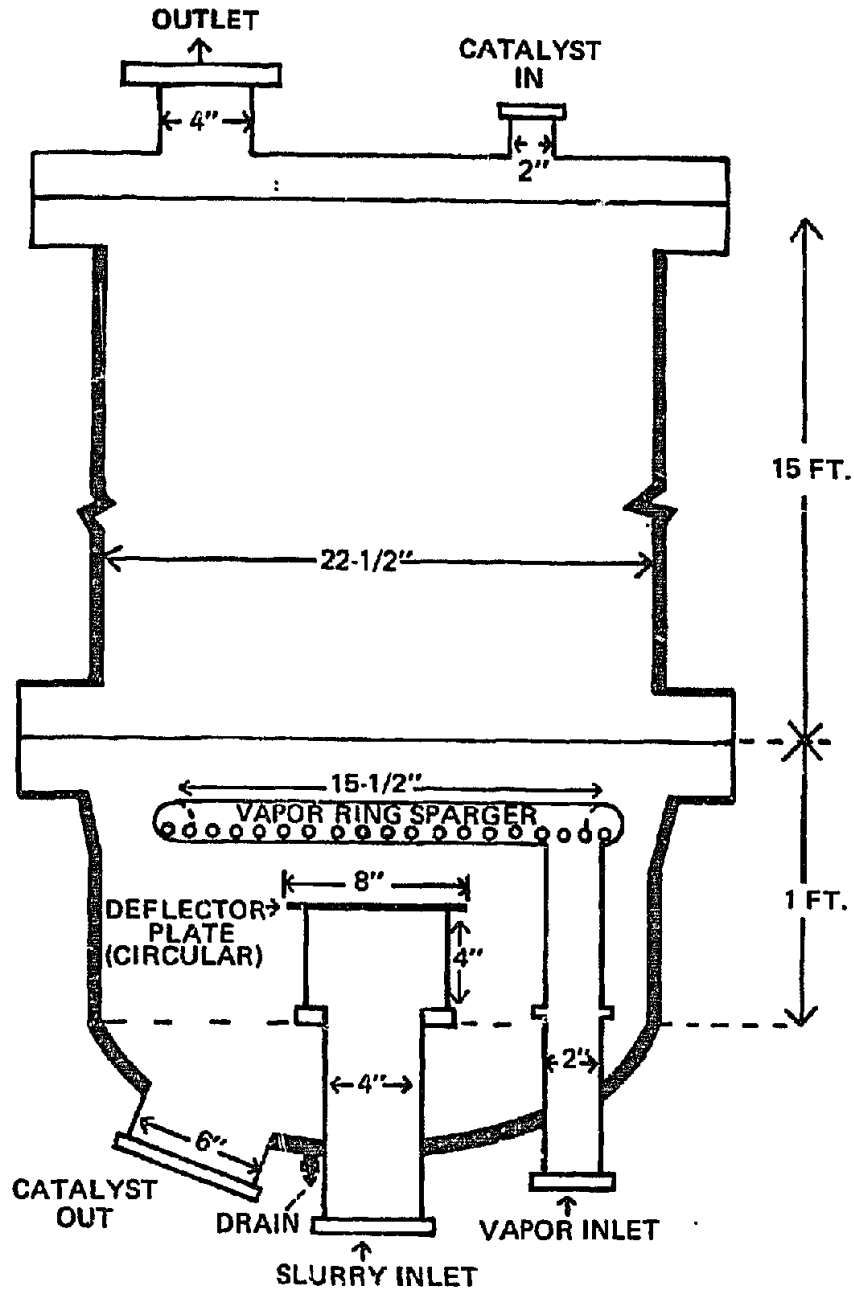


EXHIBIT 2.3.1-9A

**27.10 LPM_eOH REACTOR
(LIQUID-ENTRAINED OPERATING MODE)**



LWB
12 MAR. 82

EXHIBIT 2.3.1-9B

LaPorte LPMeOH Reactor Operating Parameters

	<u>Case EB-X954</u>	<u>Case FB-4930</u>
	(Max. Production, Liquid-Entrained)	(Max. Production Liquid Fluidized)
Superficial Vapor Velocity, ft/sec	0.39	0.26
Superficial Liquid Velocity, ft/sec	0.21	0.17
Space Velocity, acfh/ft ³ *	93.6	62.4
Space Velocity, scfh/ft ³	3270	2300
Space Velocity, Std. liters/hr-kg cat oxide	9770	3975
Catalyst Loading, lb	909	1387
Catalyst Particle Size, inches	0.0024	0.107
Catalyst Particle Size, microns	60	2718

*ft³ refers to reactor free volume.

EXHIBIT 2.3.2-1Engineering Specification Activity for Process Equipment/LaPorte LPMeOH PDU

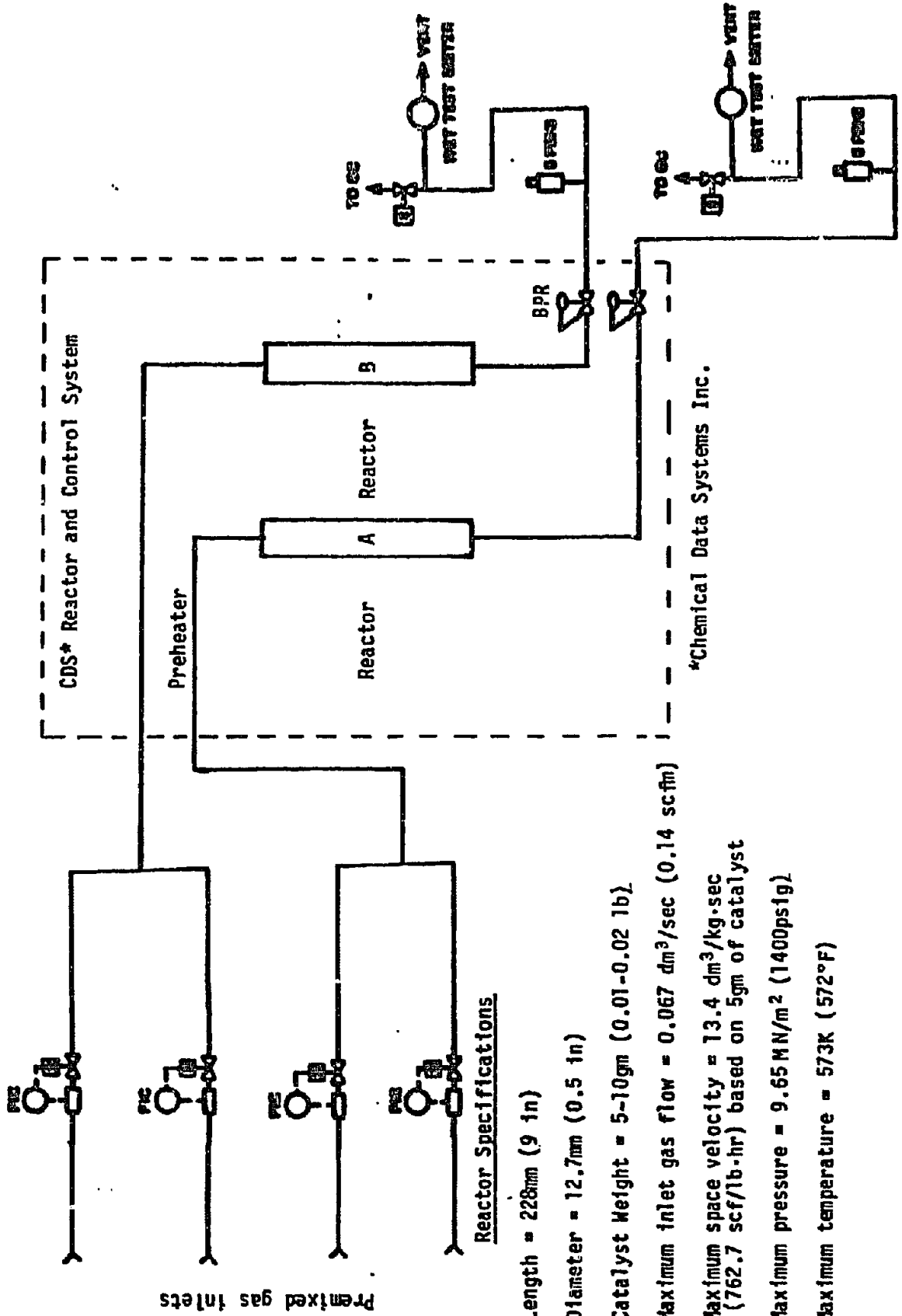
<u>Equipment Item</u>	<u>Process Specification</u>	<u>Mechanical Specification</u>	<u>Quotations Received</u>	<u>Existing Equipment</u>
01.10/01.20 Feed/Recycle Compressor	X (Note 1)		X	
01.13 Feed Surge Tank	X	X		
01.14 Feed Compressor Recycle Cooler	X	X		
01.24 Recycle Compressor Recycle Cooler	X	X		
02.50 Sulfur Trim Bed	X	X		
02.51 Sulfur Trim Bed Afterfilter	X	X		
02.81 Catalyst Reduction Vessel				
02.83 Reduction Gas Heater	X			X
02.91 A&B Water Pumps	X	X		
02.92 Water Feed Tank	X			X
10.50 A&B Slurry Circulation Pumps	X	X	X	
10.52 A&B Condensed Oil Pumps	X			X
10.53 A&B Hot Oil Pumps	X			X
10.54 Process Oil Make-up Pump	X			X
15.40 Oil Heater	X			X
21.10 Feed/Product Exchanger	X	X		
21.20 Slurry Heat Exchanger	X	X		
21.30 Product Gas Cooler	X			X
21.40 Oil Cooler	X	X		
21.53 Hop Seal Flush Cooler	X	X		
22.10 Three-phase Separator	X	X		X (Note 2)
22.11 Methanol Degasser	X			X
22.12 Demister	X			X
22.50 A&B Side Stream Filters	X			X
22.51 A&B Condensed Oil Filters	X			X
27.10 Reactor	(Note 3)			X
27.13 Primary V/L Separator	X	X		
27.14 Intermediate V/L Separator	X			X
28.10 Product Storage Tank	X	X		
28.20 Process Oil Storage Tank	X			X
28.30 Slurry Preparation Tank	(Note 4)			
28.40 Maintenance Dump Tank	X			
28.53 Oil Expansion Tank	X	X		
Total Items = 33	Total = 30	Total = 16	Total = 2	Total = 15

- NOTES: (1) Two process specifications issued, counted here as one for multiservice machine.
- (2) Existing vessel D-101 considered marginally acceptable for use on LaPorte LPMeOH PDU. Evaluation of modification costs versus new equipment fabrication must be made.
- (3) Process specification covering LaPorte LPMeOH reactor based on existing LPM vessel R-101, delayed pending determination of internals.
- (4) Slurry Preparation Tank required for liquid-entrained modifications only. Process specifications scheduled for 25 June 1982.

APCI Lab Gas Phase Reactor

EXHIBIT 7.1.3-1

20 April 1982



Reactor Specifications

- Length = 228mm (9 in)
- Diameter = 12.7mm (0.5 in)
- Catalyst Weight = 5-10gm (0.01-0.02 lb)
- Maximum inlet gas flow = 0.067 dm³/sec (0.14 scfm)
- Maximum space velocity = 13.4 dm³/kg·sec (762.7 scf/lb·hr) based on 5gm of catalyst
- Maximum pressure = 9.65 MN/m² (1400psig)
- Maximum temperature = 573K (572°F)

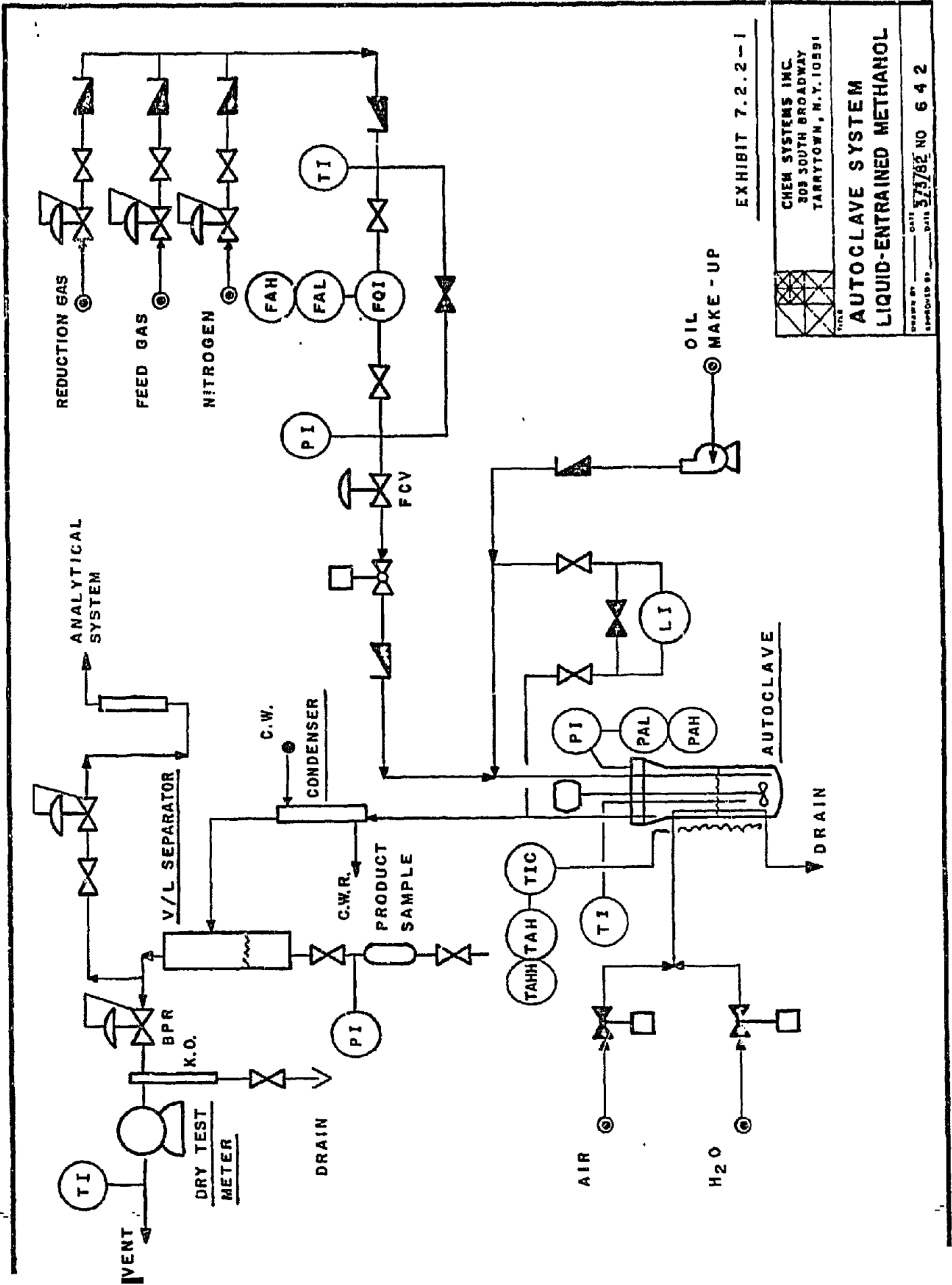


EXHIBIT 7.2.2-1

CHEM SYSTEMS INC. 308 SOUTH BROADWAY TARRYTOWN, N.Y. 10591	
AUTOCLAVE SYSTEM LIQUID-ENTRAINED METHANOL	
DRAWN BY: _____ CHECKED BY: _____	DATE: 5/5/62 NO 642

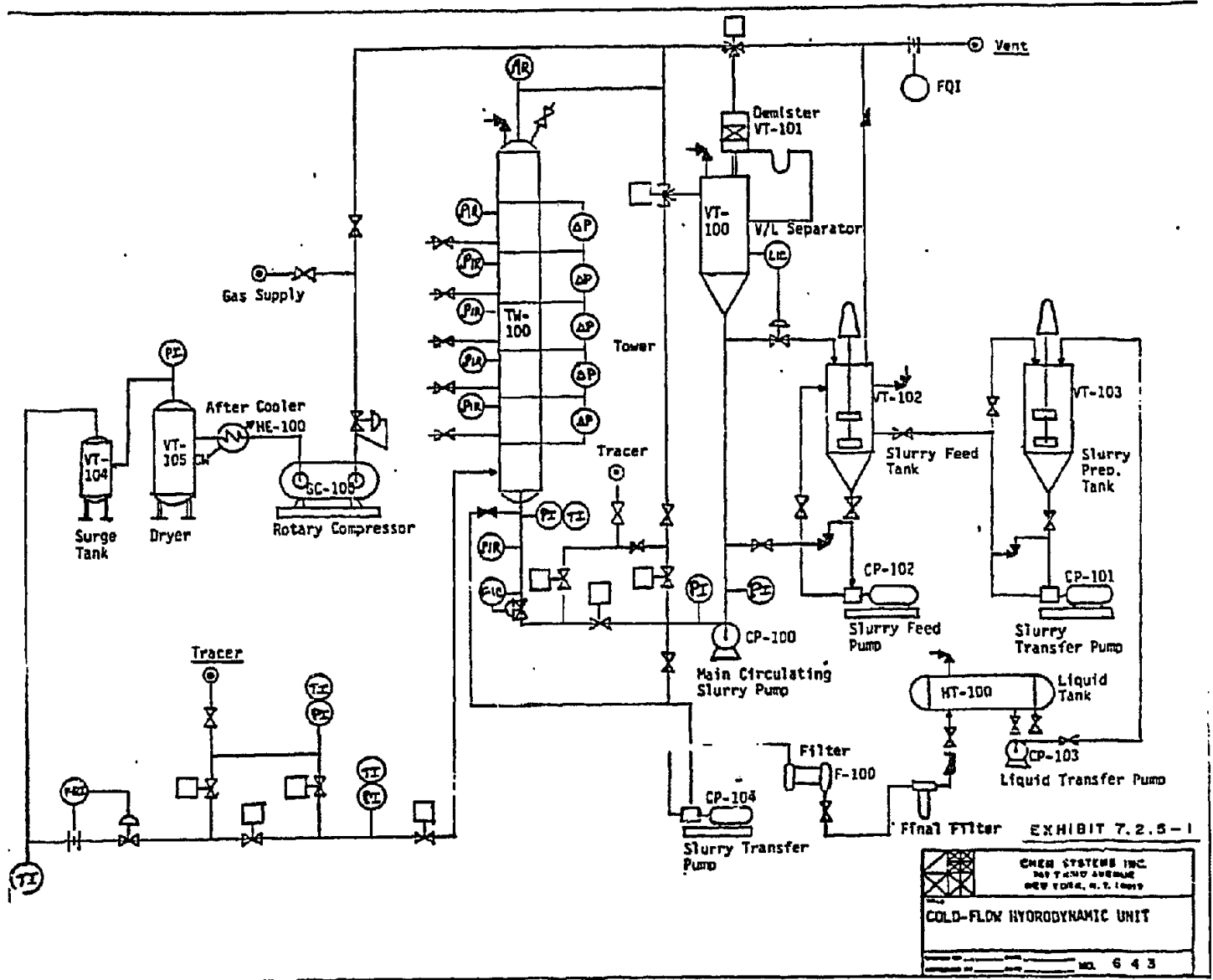
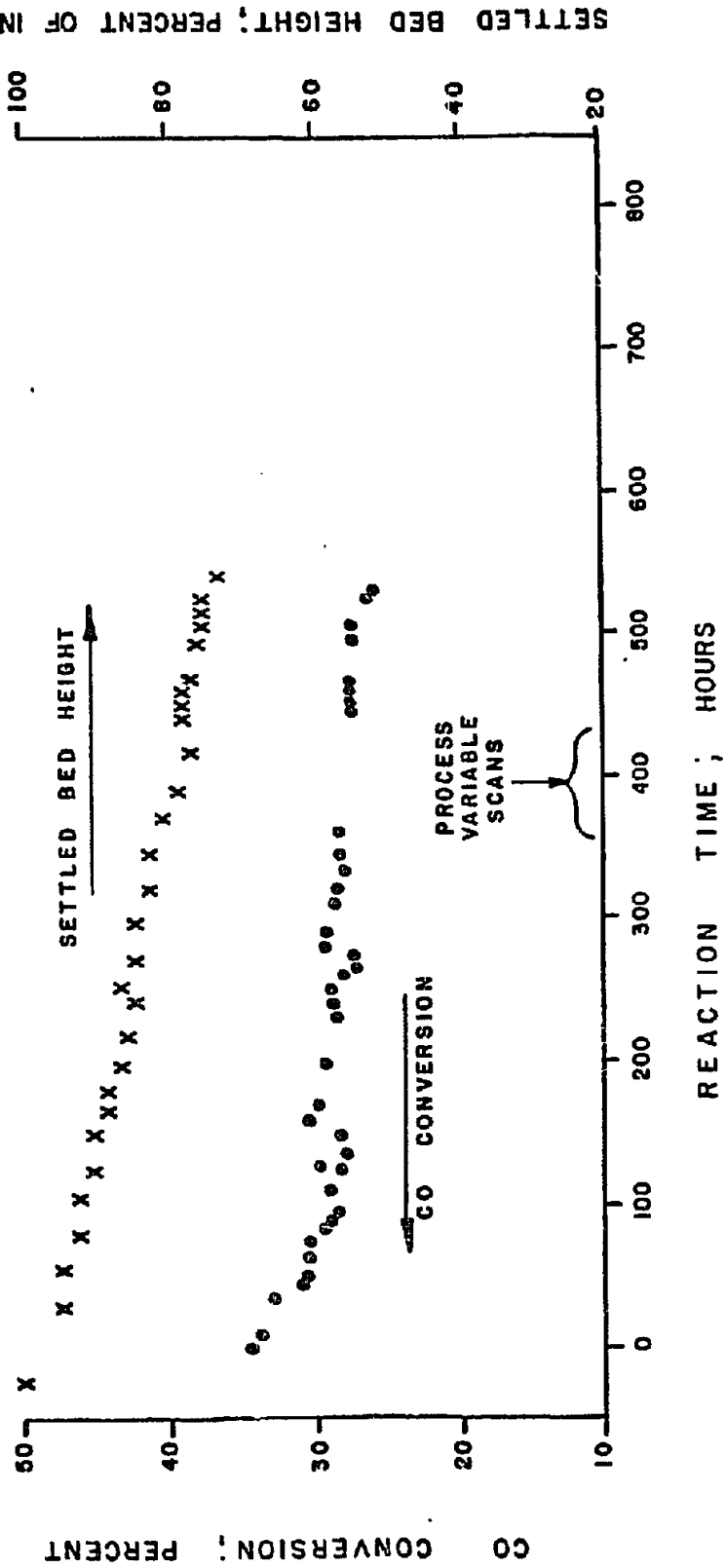


EXHIBIT 7.2.8-1

CATALYST ACTIVITY AND ATTRITION
IN CSI LIQUID-FLUIDIZED LAB PDU
WITH CATALYST R71/OF12 - O2

2/1 H₂/CO FEED GAS
250 °C, 7000 KPa
3000 L/HR. - Kg CAT



CHEM SYSTEMS INC.
PROJECT NO. 546
DATE

EXHIBIT 7.2.8-2CSI LIQUID-FLUIDIZED PDU RUN CHRONOLOGY

Page 1 of 2

WITH CATALYST R71/OF12-02

<u>Date</u>	<u>Time</u>	<u>Cumulative Reaction Time (Hours)</u>	<u>Milestone</u>
2/16/82	0900	0	4.4 Kg oxidized catalyst (R71/OF12-02) loaded into reactor. 2% H ₂ /N ₂ reduction gas in; catalyst heating to 180°C.
	1600	0	
2/17/82	--	0	Reduction continuing
2/18/82		0	Two Al ₂ O ₃ -filled guard chambers put on-line.
2/19/82	0300	0	First sight of H ₂ break through; a total of 45.0 gmol H ₂ has passed over catalyst at this point.
	0400	0	Begin heating catalyst @ 10°C per hour to 240°C.
	1100	0	Catalyst at 240°C.
	1200	0	Catalyst cooling to 200°C.
	1300	0	Oil circulating on reactor by-pass; heating to 200°C; pressurizing system to 3500 kPa with nitrogen.
	1630	0	Reactor filled w/Witco 40 oil.
	1830	0	Oil flow started through reactor; filters placed in-service.
2/20/82	0600	0	Oil through reactor @ 15 liters/min.
	1000	0	Fluidization tests at various oil flow rates at 7000 kPa and 250°C.
	1630	0	Gas flow started through reactor.
	1745	0	Fluidization tests @ 15 liters/min oil and various gas flows started at 7000 kPa and 250°C.
	2100	0	Gas fluidization tests complete and establishment of run conditions.
2/21/82	0800	11	At steady-state conditions of 3000 VHSV, 7000 kPa, 250°C; draining 2L methanol product each hour; fluidized bed height taken every 4 hrs, and settled bed height taken every 24 hrs.
2/22/82	1800	45	Change filter.
2/23/82	1400	65	Change filter.
2/26/82	0230	125	Change filter.
2/28/82	0230	173	Change filter.
3/2/82	1400	233	Change filter.
3/5/82	0100	292	Change filter.
3/8/82	0500	368	Change filter.

EXHIBIT 7.2.8-2 (Continued)CSI LIQUID-FLUIDIZED PDU RUN CHRONOLOGY

Page 2 of 2

WITH CATALYST R71/OF12-02

<u>Date</u>	<u>Time</u>	<u>Cumulative Reaction Time (Hours)</u>	<u>Milestone</u>
3/8/82	1315	376	Switch oil pumps due to excessive leaking.
	1330	376	Begin process variables scan.
	1400	377	7000 kPa, 250°C, 2000 VHSV, 2/1 H ₂ /CO feed gas.
	1900	382	7000 kPa, 230°C, 2000 VHSV, 2/1 H ₂ /CO feed gas.
3/9/82	0100	388	7000 kPa, 270°C, 2000 VHSV, 2/1 H ₂ /CO feed gas.
	0700	394	7000 kPa, 270°C, 4000 VHSV, 2/1 H ₂ /CO feed gas.
	1300	399	Change filter.
	1400	400	7000 kPa, 250°C, 4000 VHSV, 2/1 H ₂ /CO feed gas.
	1800	404	7000 kPa, 230°C, 4000 VHSV, 2/1 H ₂ /CO feed gas.
3/10/82	0100	411	3500 kPa, 230°C, 4000 VHSV, 2/1 H ₂ /CO feed gas.
	0600	416	3500 kPa, 250°C, 4000 VHSV, 2/1 H ₂ /CO feed gas.
	1100	421	3500 kPa, 270°C, 4000 VHSV, 2/1 H ₂ /CO feed gas.
	1700	427	3500 kPa, 270°C, 2000 VHSV, 2/1 H ₂ /CO feed gas.
	2200	432	3500 kPa, 230°C, 2000 VHSV, 2/1 H ₂ /CO feed gas.
3/11/82	0600	440	3500 kPa, 250°C, 1000 VHSV, 2/1 H ₂ /CO feed gas.
	1400	448	Change filter.
	1500	449	3500 kPa, 250°C, 3000 VHSV, 2/1 H ₂ /CO feed gas.
	2000	454	Back to original conditions of 7000 kPa, 250°C, 3000 VHSV, 2/1 H ₂ /CO feed gas.
3/12/82	1130	469	Start low CO ₂ -content 2/1 H ₂ /CO feed gas @ 7000 kPa, 250°C, 3000 VHSV.
	1800	476	7000 kPa, 270°C, 3000 VHSV, low CO ₂ 2/1 H ₂ /CO feed gas.
3/13/82	0200	484	7000 kPa, 270°C, 4000 VHSV, low CO ₂ 2/1 H ₂ /CO feed gas.
	0800	490	Change filter.
	1200	494	7000 kPa, 250°C, 4000 VHSV, low CO ₂ 2/1 H ₂ /CO feed gas.
	1800	500	Back to original with 2/1 H ₂ /CO feed gas at 7000 kPa, 250°C, 3000 VHSV.
3/14/82	0500	511	Change filter.
3/15/82	1000	540	2/1 H ₂ /CO feed off, K/T gas on-line.
	1100	541	Start K/T run; 7000 kPa, 250°C, 3000 VHSV.
	1700	547	End K/T run.
	1800	548	Shutdown; feed gas switched to N ₂ ; all heats off; circulating through oil cooler on reactor bypass; depressurize system and seal flush over 2 hr period; pump off when oil at 200°F; cooling water left on overnight.

CHEM SYSTEMS INC.

EXHIBIT 7.2.8-3CSI LIQUID-FLUIDIZEDPDU VARIABLE SCANS: PRELIMINARY RESULTS

<u>H₂/CO Feed Gas</u>	<u>P, kPa</u>	<u>Temp., °C</u>	<u>VHSV* L/Hr·Kg</u>	<u>Conversion, %</u>		
				<u>CO</u>	<u>H₂</u>	<u>CO₂</u>
2/1	7000	250	2000	33.1	34.6	3.3
2/1	7000	230	2000	31.1	33.6	6.1
2/1	7000	270	2000	29.8	30.0	1.5
2/1	7000	270	4000	23.8	24.2	4.5
2/1	7000	250	4000	24.1	24.6	5.3
2/1	7000	230	4000	20.3	21.4	6.8
2/1	3500	230	4000	9.4	10.3	1.9
2/1	3500	250	4000	10.2	10.5	1.7
2/1	3500	270	4000	8.7	9.7	2.3
2/1	3500	270	2000	12.8	13.2	2.3
2/1	3500	230	2000	17.3	21.5	5.2
2/1	3500	250	1000	17.4	18.2	0.7
2/1	3500	250	3000	11.9	13.2	3.0

*Based on weight of oxidized catalyst (R71/OF12-02) charged at start of run