

**APPENDIX A**  
**HAZOP SUMMARY AND WORKSHEETS**

## HAZOP SUMMARY

## Nodes

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- 1 Global 1 -- Nitrogen System
- 2 Retort/Gasifier
- 3 Coarse coal feed to retort
- 4 Fine coal feed to retort
- 5 Gasifier Booster Heater to Retort (Center)
- 6 Gasifier Booster Heater to Retort (Grid)
- 7 Inlet to Tar Quench Condenser
- 8 Tar Quench Condenser C-304
- 9 C-304 Bypass Line
- 10 Manual Tar Recirculation Line
- 11 Condenser C-304 to Tar Separator
- 12 Tar Quench Cooler Bypass
- 13 Quench Cooler to Condenser Nozzle
- 14 Tar Separator C-301
- 15 Suction to G-301 from C-301
- 16 Pump G-301 Tar Quench Pump
- 17 Pump Discharge to Tar Quench Cooler
- 18 Relief / Minimum Flow Path
- 19 Tar Quench Heat Exchanger E-301
- 20 C-301 to Relief Header
- 21 Product gas from C-301 to middle oil
- 22 Tar product to storage tank
- 23 Nat Gas Supply to Preheater
- 24 Recycle Gas from Preheater to Boosters
- 25 Air from Preheater to Boosters
- 26 Recycle Gas Inlet to Preheater
- 27 Air inlet to Preheater
- 28 Recycle gas inlet to Booster A
- 29 Air inlet to Booster A
- 30 Nat Gas inlet to Booster A
- 31 Booster Heater A
- 32 Recycle gas inlet to Booster B
- 33 Air inlet to Booster B
- 34 Nat Gas inlet to Booster B
- 35 Booster Heater B
- 36 Vent gases to Thermal oxidizer
- 37 Sour water to Thermal Oxidizer
- 38 Weigh Hopper for Coarse Coal attached tote bag unloader
- 39 Fill line from Weigh hopper to Lock hopper
- 40 Coarse coal lock hopper
- 41 Fill line from Lock hopper to Feed hopper
- 42 Coarse coal feed hopper
- 43 LT-0601,04,10,21,24 and 30
- 44 Rupture disc discharge lines
- 45 N2 feed to Hoppers
- 46 N2 Vent from Hoppers
- 47 Baghouse system
- 48 Coarse Char Surge Vessel C-703
- 49 Fill line from Coarse Char Surge Vessel to Blowcase
- 50 Coarse Char Blowcase C-704
- 51 Coarse char pneumatic conveyence to Storage Hopper D-702
- 52 Coarse char Storage Hopper D-702
- 53 Fill line from D-702 to Supersac
- 54 Char Storage Baghouse
- 55 Char Fines Surge Vessel C-701
- 56 Fill line from Char Fines Surge Vessel to Blowcase
- 57 Char Fines Blowcase C-702
- 58 Char Fines pneumatic conveyence to Storage Hopper D-701
- 59 Char Fines Storage Hopper D-701
- 60 Fill line from D-701 to Supersac
- 61 Weigh Hopper for Coal Fines and attached tote bag unloader
- 62 Fill line from Weigh Hopper to Lockhopper (fines)
- 63 Coal Fines Lockhopper
- 64 Fill Line from Lockhopper to Feed Vessel (Fines)
- 65 Coal Fines Feed Vessel
- 66 Flare
- 67 Bypass around T.O to K.O. pot
- 68 Emergency Shutdown
- 69 Tar Separator to middle oil separator (see node 21)
- 70 Middle oil separator
- 71 Middle oil separator to run tank
- 72 Run tank
- 73 Middle oil separator to the light oil separator
- 74 Recycle gas to return to the middle oil separator (HOLD)
- 75 Light oil separator
- 76 Light oil separator to run tank
- 77 Light oil separator sour water to incinerator
- 78 Low pressure depressurization line
- 79 High pressure depressurization line (DELETED FROM DESIGN)
- 80 Recycle gas to the T.O.
- 81 Recycle gas to preheater (See node 26)
- 82 Coarse char from retort to coarse char surge vessel
- 83 Fine char from cyclone to fine char surge vessel
- 84 Primary Cyclone
- 85 Secondary Cyclone
- 86 Glycol Cooling System

Company: IGT  
Facility: Roberts & Schafer  
Session: 1 02-13-95  
Node: 1 Global 1 -- Nitrogen System  
Parameter: Flow

Revision: 0 02-13-95 Dwg#: 9417-1006-C

Intention: Provide adequate flow to support all I/C and process operations

DEVIATION	CAUSES	CONSEQUENCES	SAFEGUARDS	RECOMMENDATIONS	REMARKS	BY	COMMENTS
No/less Flow	1) Plugging	1.1) Inadequate supply to specific or all users	C1.1) Downstream flow ind. FIT-0904 and FAL-0904(S) C1.2) Local PI's	Ensure control room pressure ind. and alarm on N2 vendor package		B	
	2) Regulator failure	2.1) same as above	C2.1) same as C1.*)				
	3) Excessive user	3.1) Same as above	C3.1) FIT-0902, FIT-0903 and Hi/LO(S) on FIT-0902,3 and 4. C3.2) FIT-0733 and Hi/LO(S) course char cooler				
	4) Valve left or fails closed	4.1) Same as above	C4.1) Oper. Proc.				
	5) Line break, flange leak, etc.	5.1) Same as above	C5.1) same as above				

Session: 1 02-13-95

Revision: 0 02-13-95 Dwg#: 9417-1006-C

Node: 1 Global 1 -- Nitrogen System

Parameter: Composition

Intention: Pure N2 in the lines at all times

DEVIATION	CAUSES	CONSEQUENCES	SAFEGUARDS	RECOMMENDATIONS	REMARKS	BY	COMMENTS
Other Than Composition	1) Failure to purge after outage or at start-up	1.1) Undesired combustion in the coal transfer lines, hoppers, and other blanketed storage vessels for liquids	C1.1) Operating procedures to include vent and purge	Ensure inclusion in op. proc.		I B	
			C1.2) Pressure indication at various critical locations				
	2) Loss of N2 source	2.1) same as 1.1	C2.1) Pressure and level instrumentation C2.2) Oper proc. to ensure sufficient N2 to support run	Verify low liq. level alarm is provided Verify the need for emerg. S/D on lost of N2.	B RS		
		2.2) loss of I/C		Review need for N2 back-up source		I B	

Company: IGT  
 Facility: Roberts & Schafer  
 Session: 1 02-13-95 Revision: 0 02-13-95 Dwg#: 9417-1006-C  
 Node: 1 Global 1 -- Nitrogen System  
 Parameter: Composition Intention: Pure N2 in the lines at all times

DEVIATION	CAUSES	CONSEQUENCES	SAFEGUARDS	RECOMMENDATIONS	REMARKS	BY	COMMENTS
		2.3) loss transport of material (coal and char)					

Session: 1 02-13-95 Revision: 0 02-13-95 Dwg#: 9417-1006-C  
 Node: 1 Global 1 -- Nitrogen System  
 Parameter: Level Intention: Contain the N2 as either liquid or gas as appropriate

DEVIATION	CAUSES	CONSEQUENCES	SAFEGUARDS	RECOMMENDATIONS	REMARKS	BY	COMMENTS

Session: 1 02-13-95 Revision: 0 02-13-95 Dwg#: 9417-1006-C  
 Node: 1 Global 1 -- Nitrogen System  
 Parameter: Safety Intention: To ensure operator and maintenance personnel safety

DEVIATION	CAUSES	CONSEQUENCES	SAFEGUARDS	RECOMMENDATIONS	REMARKS	BY	COMMENTS
No Safety	1) Inappropriate confined space entry	1.1) Personnel injury or death	c1.1.1) Confined space entry procedures	Review current procedures to ensure they are adequate for this facility		I	

HAZOP-PC 2.12  
Company: IGT  
Facility: Roberts & Schafer  
Session: 1 02-13-95  
Node: 2 Retort/Gasifier  
Parameter: Pressure

Worksheet

Revision: 0 02-13-95 Dwg#: 9417-1006-C  
Intention: Operate 35 psia

Primatech Inc.  
Node: 2  
Page: 1

DEVIATION	CAUSES	CONSEQUENCES	SAFEGUARDS	RECOMMENDATIONS	REMARKS	BY	COMMENTS
Higher Pressure	1) Blocked/restricted nozzle to cyclone			Add overpressure protection		RS	

DEVIATION	CAUSES	CONSEQUENCES	SAFEGUARDS	RECOMMENDATIONS	REMARKS	BY	COMMENTS
No/less Flow	1) Conveyor failure	1.1) Inadequate supply to retort	C1.1) speed indication SI-0641	Review need for alarm on SI-0641 ????		I B	
		1.2) Overheating of coal	c1.2.1) Oil temp limit 600F				
		1.3) Retort temp rise	c1.3.1) TE-0729B indicate initial rise and control				
		1.4) Product gas make reduced	c1.3.2) TE-0710/27 indicate rise				
		1.5) Bed level reduction					
1.6) Exit oil temp rise							
1.7) Plugging of line and conveyor							
	2) Driver failure	2.1) same as 1.*)	c2.1.1) Same as 1.*)				
	3) Pluggage or blockage in line	3.1) same as 1.*)	C3.1) Pressure ind. PI-0640 will rise  C3.2) If blockage upstream of N2 conn. then TE-0644 will indicate low				PI-06-40 will move to downstream of N2 connect. No impact
	4) Slow speed on conveyor	4.1) same as 1.*) a slower rate					
	5) Pluggage or blockage in conveyor	5.1) same as 1.*)	c5.1.1) Same as 1.2.*) thru 1.3.*)				
More Flow	1) Improper speed control setting	1.1) Imbalance in gasifier control point level and temp	C1.1) Oper training  C1.2) Specific calibration by coal type  C1.3) Temp decrease at TE-0710/27  C1.4) Level via pressure dP at PDIT-0703				

DEVIATION	CAUSES	CONSEQUENCES	SAFEGUARDS	RECOMMENDATIONS	REMARKS	BY	COMMENTS
Reverse Flow	1) Loss of N2	1.1) TI-0644 reads HI 1.2) Disrupt bed control	C1.1) N2 Control system see global node 1 C1.2) TI-0644 Hi	Add alarm(S) on hi		RS	
	2) Failure of pressure boundary(lock hopper, seals, etc.)	2.1) Same as 1.*) 2.2) Release of haz. material 2.3) Damage instrumentation due to hi temp 2.4) Damage to screw conveyor	C2.1) Maintenance and oper. procedures C2.2) same as C1.2	Review the need for auto S/D of line on Hi temp		I B	

DEVIATION	CAUSES	CONSEQUENCES	SAFEGUARDS	RECOMMENDATIONS	REMARKS	BY	COMMENTS
Higher Temperature	1) TV-0615 too open	1.1) Coal discharge temp high 1.2) Potential for pluggage 1.3) Higher temp in gasifier	c1.1) Temp limited too oil temp of 600F C1.1) oper proc. and calibr. c1.3) Gasifier controls				
	2) SE-0641 too slow	2.1) see Flow No/Less	c2.1) same as No/Less Flow				
Lower Temperature	1) TV-0615 too closed	1.1) Lower bed temp in gasifier 1.2) Coal discharge temp low	c1.1) Gasifier controls c1.2) Operating proc.				
	2) Failure of TE-	2.1) same as above	C2.1) deleted				

Company: IGT  
Facility: Roberts & Schafer  
Session: 1 02-13-95  
Node: 3 Coarse coal feed to retort  
Parameter: Temperature  
Revision: 0 02-13-95 Dwg#: 9417-1006-C  
Intention: Supply coal at 500F

DEVIATION	CAUSES	CONSEQUENCES	SAFEGUARDS	RECOMMENDATIONS	REMARKS	BY	COMMENTS
	0615		C2.2) same as c1.*)				
	3) SE-0641 too fast	3.1) see Flow-High 3.2) same as 1.*)	3.1) see Flow- High c3.2) same as c1.*)				
	4) Fouling of screw	4.1) same as 1.*)	c4.1) same as c1.*)				
	5) Loss of N2	5.1) same as 1.*)	c5.1) same as c1.*)				

Session: 1 02-13-95  
Node: 3 Coarse coal feed to retort  
Parameter: Composition  
Revision: 0 02-13-95 Dwg#: 9417-1006-C  
Intention: No contamination from heating oil

DEVIATION	CAUSES	CONSEQUENCES	SAFEGUARDS	RECOMMENDATIONS	REMARKS	BY	COMMENTS
Other Than Composition	1) Leakage from oil side to coal side	1.1) Pluggage/blockage 1.2) No impact in gasifier 1.3) Recycle gas/liq product composition change (no impact) 1.4) Increase liq product 1.5) False test result (No impact) 1.6) Damage to hot system due to low volume	c1.1) same as Flow-No/less C1.1) Low level at LIT-0801 and 06 and alarm(S) at L and LL. C1.2) LALL-0801&06 causes S/D c1.6.1) same as C1.1 and C1.2			RS	Review level control interlock with heater control and pump control



Intention: Provide flow at rate of xxx

DEVIATION	CAUSES	CONSEQUENCES	SAFEGUARDS	RECOMMENDATIONS	REMARKS	BY	COMMENTS
No/less Flow	1) Conveyor failure	1.1) Inadequate supply to retort	C1.1) speed indication SI-0642	Review need for alarm on SI-0642 ????		I B	
		1.2) Overheating of coal	c1.2.1) Oil temp limit 600F				
		1.3) Retort temp rise	c1.3.1) TE-0729B indicate initial rise and control				
		1.4) Product gas make reduced	c1.3.2) TE-0710/27 indicate rise				
		1.5) Bed level reduction					
1.6) Exit oil temp rise							
1.7) Plugging of line and conveyor							
	2) Driver failure	2.1) same as 1.*)	c2.1.1) Same as 1.*)				
	3) Pluggage or blockage in line	3.1) same as 1.*)	C3.1) Pressure ind. PI-0643 will rise  C3.2) If blockage upstream of N2 conn. then TE-0645 will indicate low				PI-06-40 will move to downstream of N2 connect. No impact
	4) Slow speed on conveyor	4.1) same as 1.*) a slower rate					
	5) Pluggage or blockage in conveyor	5.1) same as 1.*)	c5.1.1) Same as 1.2.*) thru 1.3.*)				
More Flow	1) Improper speed control setting	1.1) Imbalance in gasifier control point level and temp	C1.1) Oper training  C1.2) Specific calibration by coal type  C1.3) Temp decrease at TE-0710/27  C1.4) Level via pressure dP at PDIT-0703				

DEVIATION	CAUSES	CONSEQUENCES	SAFEGUARDS	RECOMMENDATIONS	REMARKS	BY	COMMENTS
Reverse Flow	1) Loss of N2	1.1) TI-0645 reads HI 1.2) Disrupt bed control	C1.1) N2 Control system see global node 1 C1.2) TI-0645 Hi	Add alarm(S) on hi		R	
	2) Failure of pressure boundary(lock hopper, seals, etc.)	2.1) Same as 1.*) 2.2) Release of haz. material 2.3) Damage instrumentation due to hi temp 2.4) Damage to screw conveyor	C2.1) Maintenance and oper. procedures C2.2) same as C1.2	Review the need for auto S/D of line on Hi temp		I B	

DEVIATION	CAUSES	CONSEQUENCES	SAFEGUARDS	RECOMMENDATIONS	REMARKS	BY	COMMENTS
Higher Temperature	1) TV-0635 too open	1.1) Coal discharge temp high	c1.1) Temp limited too oil temp of 600F				
		1.2) Potential for pluggage	C1.1) oper proc. and calibr. c1.3) Gasifier controls				
		1.3) Higher temp in gasifier					
	2) SE-0642 too slow	2.1) see Flow No/Less	c2.1) same as No/Less Flow				
Lower Temperature	1) TV-0635 too closed	1.1) Lower bed temp in gasifier	c1.1) Gasifier controls				
		1.2) Coal discharge temp low	c1.2) Operating proc.				
	2) Failure of TE-0635	2.1) same as above	C2.1) deleted				

Company: IGT  
Facility: Roberts & Schafer  
Session: 1 02-13-95  
Node: 4 Fine coal feed to retort  
Parameter: Temperature

Revision: 0 02-13-95 Dwg#: 9417-1006-C  
Intention: To supply fine coal at \*\*\*F

DEVIATION	CAUSES	CONSEQUENCES	SAFEGUARDS	RECOMMENDATIONS	REMARKS	BY	COMMENTS
	3) SE-0642 too fast	3.1) see Flow-High 3.2) same as 1.*)	C2.2) same as c1.*) 3.1) see Flow- High c3.2) same as c1.*)				
	4) Fouling of screw	4.1) same as 1.*)	c4.1) same as c1.*)				
	5) Loss of N2	5.1) same as 1.*)	c5.1) same as c1.*)				

Session: 1 02-13-95  
Node: 4 Fine coal feed to retort  
Parameter: Composition

Revision: 0 02-13-95 Dwg#: 9417-1006-C  
Intention: No contamination from heating oil

DEVIATION	CAUSES	CONSEQUENCES	SAFEGUARDS	RECOMMENDATIONS	REMARKS	BY	COMMENTS
Other Than Composition	1) Leakage from oil side to coal side	1.1) Pluggage/blockage 1.2) No impact in gasifier 1.3) Recycle gas/liq product composition change (no impact) 1.4) Increase liq product 1.5) False test result (No impact) 1.6) Damage to hot system due to low volume	c1.1) same as Flow-No/less Cl.1) Low level at LIT-0801 and 06 and alarm(S) at L and LL. Cl.2) LALL-0801&06 causes S/D c1.6.1) same as Cl.1 and Cl.2		Review level control interlock with heater control and pump control	RS	

Company: IGT

Node: 5

Facility: Roberts &amp; Schafer

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Session: 1 02-13-95

Revision: 0 02-13-95 Dwg#: 9417-1006-C

Node: 5 Gasifier Booster Heater to Retort (Center)

Parameter: Flow

Intention: Provide process heat input to gasifier to fluidize bed and maintain fluidization

DEVIATION	CAUSES	CONSEQUENCES	SAFEGUARDS	RECOMMENDATIONS	REMARKS	BY	COMMENTS
Less Flow	1) Restriction of air compressor flow	1.1) Booster heater temperature output low 1.2) Bed velocity fluidization reduced 1.3) Bed temp decreases 1.4) Recycle gas composition changes 1.5) Reduced cyclone performance, secondary cyclone duty increase, fines in heavy liq recovery 1.6) TV-0729C tries to maintain stoic. 1.7) Booster heater may respond	C1.1) Flow ind. at FIT-0736 and alarm (S)L c1.1) Low temp at TE-0729A and (S)L and LL c1.3.1) Low temp at TE-0710/27 and alarm (S) L and LL c1.4.1) At on-line GC (long response time) C2.2) Trouble alarm at compressor	Verify that vendor package has alarm          Review the control strategy for ind. of secondary booster needed and manual permissive (remove as needed TY-0729A, etc.)		RS	
	2) Restriction of recycle compressor flow	2.1) Booster heater discharge temp increases 2.2) same as 1.2) thru 1.5) 2.3 TV-0729B&C throttle back	C2.1) Flow ind. low at FE-0738 and alarm (S)L c2.1) Hi temp at TE-0729A and (S)H and HH C2.2) Trouble alarm at compressor	Verify vendor package has trouble alarm		RS	
	3) Restriction	3.1) Same as 1.*)	c2.2.1) Low temp at TE-				

DEVIATION	CAUSES	CONSEQUENCES	SAFEGUARDS	RECOMMENDATIONS	REMARKS	BY	COMMENTS
	of nat gas flow	3.2) Possibility for excess O2 resulting in lower booster temp, hi local temp. and product slate differences	0710/27 and alarm (S) L and LL c2.2.2) At on-line GC (long response time) c3.1.1) same as air compr c3.2.1) Product testing at end of run				
	4) Leakage or line breakage	4.1) Release of haz mat	c4.1.1) Approved fire protection program C.4.1) Oper. training	Review whether or not FS's provide adequate/recommended protection  Review burner management I/C program (w/Callidus)		B  C	
	5) Firing of Booster Heater B	4.2) release of VERY hot air 4.3) Personnel inj 4.4) Potential for fire/explosion 5.1) Changes balance of recycle gas flow		Review addition of control valves in the individual recycle feed lines and remove the control valve upstream of the fired heater		RS	
More Flow	1) Operator error or miscalib	1.1) Higher entrainment 1.2) Higher temp at TE-0710/27 due to hot fines 1.3) Higher duty					

DEVIATION	CAUSES	CONSEQUENCES	SAFEGUARDS	RECOMMENDATIONS	REMARKS	BY	COMMENTS
		on liq recovery 1.4) Offspec operation-no hazards					

DEVIATION	CAUSES	CONSEQUENCES	SAFEGUARDS	RECOMMENDATIONS	REMARKS	BY	COMMENTS
Higher Temperature	1) More Nat Gas and air flow  2) Excess air  3) Preheater too hot	1.1) Higher bed temp 1.2) Slightly higher bed velocity 1.3) Product slate differences 1.4) Char composition changes 1.5) Approaching materials limits 1.6) Booster heater may respond  2.1) same as 1.*) 2.2) excess O2 see Flow- Less item 3.2  3.1) Excess temp to gasifier 3.2) same as 1.*)	c1.1.1) TE-0710/27 read hi, alarm (S)H and HH c1.1.2) TE-0729A reads Hi and alarm (S)H and HH c1.5.1) 150F margin in gasifier and that less 100F in the coarse char cooler  c2.1.1) same as 1.1  c3.2.1) same as 1.1 c3.2.2) preheater design margin XXXX	Review the control strategy for ind. of secondary booster needed and manual permissive (remove as needed TY-0729A, etc.)  Review temp loop	Verify preheater design margin	RS C  B C	

DEVIATION	CAUSES	CONSEQUENCES	SAFEGUARDS	RECOMMENDATIONS	REMARKS	BY	COMMENTS
Lower Temperature	1) Preheater too cold  2) Low nat gas flow 3) Insufficient air	1.1) Lower bed temp 1.2) Slightly lower bed velocity 1.3) Product slate differences 1.4) Char composition changes 2.1) Same as 1.*) 3.1) same as 1.*)	c3.1.3) Temp control at preheater c1.1.1) TE-0710/27 read low, alarm (S)L and LL c1.1.2) TE-0729A reads low and alarm (S)L and LL c1.1.3) Temp control at preheater	including TS and alarm with Callidus  Review temp loop with Callidus		C	

DEVIATION	CAUSES	CONSEQUENCES	SAFEGUARDS	RECOMMENDATIONS	REMARKS	BY	COMMENTS
Less Flow	1) Restriction of air compressor flow	1.1) Booster heater temperature output low 1.2) Bed velocity fluidization reduced 1.3) Bed temp may decrease 1.4) Recycle gas composition changes 1.5) TV-0729E tries to maintain stoic.	C1.1) Flow ind. at FIT-0741 and alarm (S)L c1.1) Low temp at TE-0729B and (S)L and LL c1.3.1) Low temp at TE-0710/27 and alarm (S) L and LL c1.4.1) At on-line GC (long response time) C2.2) Trouble alarm at compressor				
	2) Restriction of recycle compressor flow	2.1) Booster heater discharge temp increases  2.2) same as 1.2) thru 1.4) 2.3) Reduced cyclone performance, secondary cyclone duty increase, fines in heavy liq recovery 2.3) TV-0729D&E throttle back 2.4) Blockage of grid	C2.1) Flow ind. low at FE-0743 and alarm (S)L c2.1) Hi temp at TE-0729B and (S)H and HH C2.2) Trouble alarm at compressor	Verify that vendor package has alarm  Move TE-0729B to secondary booster heater exit line. Review alarms and setpts. Also revise TIC-0729A logic to get bed input from TE-0710/27.  Verify vendor package has trouble alarm		RS C  RS	
	3) Restriction	3.1) Same as 1.*)	c2.2.1) Low temp at TE-				



DEVIATION	CAUSES	CONSEQUENCES	SAFEGUARDS	RECOMMENDATIONS	REMARKS	BY	COMMENTS
More Flow	of nat gas flow	3.2) Possibility for excess O2 resulting in lower booster temp., hi local temp. and prod. slate differences	0710/27 and alarm (S) L and LL c2.2.2) At on-line GC (long response time) c3.1.1) same as air compr c3.2.1) Product testing at end of run				
	4) Leakage or line breakage	4.1) Release of haz mat  4.2) release of VERY hot air 4.3) Personnel inj 4.4) Potential for fire/explosion	c4.1.1) Approved fire protection program C.4.1) Oper. training	Review whether or not PS's provide adequate/recommended protection  Review burner management I/C program (w/Callidus)		B  C	
	1) Operator error or miscalib	1.1) Higher entrainment 1.2) Higher temp at TE-0710/27 due to hot fines 1.3) Higher duty on liq recovery 1.4) Offspec operation-no hazards					

Company: IGT  
Facility: Roberts & Schafer  
Session: 1 02-13-95  
Node: 6 Gasifier Booster Heater to Retort (Grid)  
Parameter: Temperature  
Revision: 0 02-13-95 Dwg#: 9417-1006-C  
Intention: Provide flow at 1100F to 1500F

DEVIATION	CAUSES	CONSEQUENCES	SAFEGUARDS	RECOMMENDATIONS	REMARKS	BY	COMMENTS	
Higher Temperature	1) More Nat Gas and air flow	1.1) Higher bed temp	c1.1.1) TE-0710/27 read hi, alarm (S)H and HH					
		1.2) Slightly higher bed velocity	c1.1.2) TE-0729B reads Hi and alarm (S)H and HH					
		1.3) Product slate differences	c1.5.1) 150F margin in gasifier and that less 100F in the coarse char cooler					
		1.4) Approaching materials limits						
	2) Excess air	2.1) same as 1.*)	c2.1.1) same as 1.1					
		2.2) excess O2 see Flow 3.2						
3) Preheater too hot	3.1) Excess temp to gasifier	c3.2.1) same as 1.1			Verify preheater design margin	B		
		c3.2.2) preheater design margin XXXX		Review temp loop including TS and alarm with Callidus		C		
	3.2) same as 1.*)	c3.1.3) Temp control at preheater						
Lower Temperature	1) Pre heater too cold	1.1) Lower bed temp	c1.1.1) TE-0710/27 read low, alarm (S)L and LL					
		1.2) Slightly lower bed velocity	c1.1.2) TE-0729B reads low and alarm (S)L and LL					
		1.3) Product slate differences	c1.1.3) Temp control at preheater		Review temp loop with Callidus		C	
	2) Low nat gas flow	2.1) Same as 1.*)						
	3) Insufficient air	3.1) same as 1.*)						

DEVIATION	CAUSES	CONSEQUENCES	SAFEGUARDS	RECOMMENDATIONS	REMARKS	BY	COMMENTS
No/Less Flow	<p>1) Valve XV-1101 fails closed due loss of N2</p> <p>2) Valve XV-1101 fails closed (mechanical failure)</p> <p>3) Valve XV-1001 fails open (mechanical failure or operator error)</p> <p>4) XV-1001 fails open on loss of N2</p>	<p>1.1) No flow to C-304</p> <p>1.2) XV-1001 opens</p> <p>1.3) Flow diverted to relief system.</p> <p>1.4) Gasifier upset</p> <p>1.5) Stoppage of liq's recovery</p> <p>3.1) Flow to relief system</p> <p>3.2) Minimum liq's recovery</p> <p>3.3) Gasifier upset</p> <p>4.1) Same as 3.)*</p>	<p>C1.1) see global node 1</p> <p>c3.2.1) TE-1104 decreases slowly</p> <p>c3.2.2) PIT-1109 decreases</p> <p>c3.2.3) PIT-0709 decreases</p> <p>C4.1) see Global Node 1</p>	<p>Review need for XV-1101</p> <p>Review need for XV-1001 as part of SD session</p>	<p>To be reviewed at S/D philosophy session</p>	<p>B I</p>	

DEVIATION	CAUSES	CONSEQUENCES	SAFEGUARDS	RECOMMENDATIONS	REMARKS	BY	COMMENTS
Less Phase (less tar produced)	1) Less recirc. liquid flow  2) Higher recirc. liquid temp  3) Higher product gas temp	1.1) Less tar produced  1.2) Tars carried to middle oil recovery section  1.3) May upset/fouling middle recovery	C1.1) TE-1104 and (S)HH at 473F  C1.2) FIT-1121 lower  C1.3) PIT-1120A higher	Review increase HH setpt to say 500F. Watch for middle oil air cooler fouling  Review removal/relocation of PV20  Review removal of PIT-1120A loop completely		RS I B	

HAZOP-PC 2.12  
 Company: IGT  
 Facility: Roberts & Schafer  
 Session: 1 02-13-95  
 Parameter: Flow

Worksheet

Primatech Inc.  
 Node: 9  
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Revision: 0 02-14-95 Dwg#: 9417-1006-C e: 9 C-304 Bypass Line  
 Intention: No flow unless required by high pressure condition

DEVIATION	CAUSES	CONSEQUENCES	SAFEGUARDS	RECOMMENDATIONS	REMARKS	BY	COMMENTS
More Flow	1) PV-1103 open or leaking	1.1) Less flow to spray nozzle  1.2) May effect quench performance  1.3) May have higher temperature in tar separator	C1.1) PIT-1102 lower if valve full open	Review alternative methods for determining PV-1103 is open		B RS	
No Flow (when required to open)	1) PV-1103 fails to open mechanical or control loop failure	1.1) Pressure increases in piping system	c1.1.1) PSE-1119 ruptures  c1.1.2) Alarms at PIT-1102 (S)H and HH				

Company: IGT  
Facility: Roberts & Schafer  
Session: 1 02-13-95  
Node: 10 Manual Tar Recirculation Line  
Parameter: Flow

Revision: 0 02-14-95 Dwg#: 9417-1006-C

Intention: No flow under normal op's, recirc flow during S/D

DEVIATION	CAUSES	CONSEQUENCES	SAFEGUARDS	RECOMMENDATIONS	REMARKS	BY	COMMENTS
More Flow (during operation)	1) Manual valve open or leaking	1.1) Insufficient cooling 1.2) Reduced quench performance 1.3) Heavy liquids to middle liquids separation	c1.1.1) FIT-1121 lower c1.1.2) TIC-1104 higher C1.1) Operator training and procedures				
No Flow (during bypass mode)	1) Manual valve closed (mechanical failure or operator error)  2) Blockage	1.1) Fouling of tar quench cooler 1.2) Reduced heat transfer in cooler and pluggage  2.1) Same as 1.*)	c1.1.1) TIC-1104 lower C1.1) Operator training and procedures  c2.1.1) Same as c1.1.1) C2.1) Electric heat tracing				

Company: IGT

Node: 11

Facility: Roberts & Schafer

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Session: 1 02-13-95

Revision: 0 02-14-95 Dwg#: 9417-1006-C

Node: 11 Condenser C-304 to Tar Separator

Parameter: Flow

Intention: Provide flow from C-304 to C-301

DEVIATION	CAUSES	CONSEQUENCES	SAFEGUARDS	RECOMMENDATIONS	REMARKS	BY	COMMENTS
No/Less Flow	1) Blockage or plugging	1.1) Reduced flow to C-301 1.2) Reduced performance in C-304 1.3) C-301 operates more efficiently	C1.1) Large line size C1.2) Electric heat trace C1.3) Sloped line				

DEVIATION	CAUSES	CONSEQUENCES	SAFEGUARDS	RECOMMENDATIONS	REMARKS	BY	COMMENTS
Less Flow	1) TV-1104 doesn't open enough	1.1) Slight over-cooling of recirc fluid	c1.1.1) TIC-1104 slightly lower c1.1.2) Cooling loop will self-adjust	Change fail position of TV-1104 to FC		RS	
	2) Manual valve left closed	2.1) Same as 1.*)					
	3) Malfunction of TIC-1104 logic and devices	3.1) Same as 1.*)					
	4) Pluggage	4.1) Same as 1.*)					
	5) Loss of N2	5.1) Same as 1.*					
More Flow	1) TV-1104 doesn't close enough	1.1) Slight undercooling of recirc fluid	c1.1.1) Cooling loop will self-adjust c1.1.2) TIC-1104 slightly higher				
	2) Malfunction of TIC-1104 logic and devices	2.1) Same as 1.*)					



Company: IGT

Node: 13

Facility: Roberts & Schafer

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Session: 1 02-13-95

Revision: 0 02-14-95 Dwg#: 9417-1006-C

Node: 13 Quench Cooler to Condenser Nozzle

Parameter: Flow

Intention: Provide flow from Cooler to Condenser

DEVIATION	CAUSES	CONSEQUENCES	SAFEGUARDS	RECOMMENDATIONS	REMARKS	BY	COMMENTS
No/Less Flow	1) Pluggage and blockage in line or nozzle	1.1) Reduced performance of condenser 1.2) Higher temperature at TIC-1104 1.3) Higher pressure at PIT-1102, and later by PI-1103 1.4) Tars to the middle oils	C1.1) Electric heat trace c1.2.1) Temperature alarm at TIC-1104 (S)H and HH c.1.3.1) Pressure alarm at PIT-1102 (S)H and HH				

DEVIATION	CAUSES	CONSEQUENCES	SAFEGUARDS	RECOMMENDATIONS	REMARKS	BY	COMMENTS
Lower Level	1) Failure of LIC-1108 logic or devices  2) Low product input  3) System leak	1.1) Pump runs dry  1.2) Reduced or no spray  1.3) Poor condenser performance  1.4) Heavy oils to middle oils  1.5) Low flow to heavy product storage  2.1) Same as 1.*)  3.1) Same as 1.*)  3.2) Toxic and flammable product release to local area.	C1.1) Alarms at LIC-1108 (S)L and LL  c1.1.1) Low flow alarm at FIT-1121 (S)L and LL  c1.1.3) High temp alarm at TIC-1104 (S)H and HH  c1.5.1) LIT-1404 will not rise aspected  c2.1.1) Same as 1.*)  c3.1.1) Same as 1.*)  c3.2.1) Area slab drain drains to storage tank and pretreat prior to discharge  c3.2.2) Approved fire protection program  c3.2.3) Oper. training  c3.2.4) IEPA approved constr. plan  c3.2.5) NEPA approved siting	Review addition of independent LS for low level alarm		I B	
Higher Level	1) Failure of LIC-1108 logic or devices	1.1) Heavy oil to middle oil due to poor separation in C-301  1.2) Spill over to middle oil	C1.1) Alarms at LIC-1108 (S)H and HH	Review addition of independent LS for high level alarm		I B	

HAZOP-PC 2.12  
 Company: IGT  
 Facility: Roberts & Schafer  
 Session: 1 02-13-95  
 Node: 14 Tar Separator C-301  
 Parameter: Level

Worksheet

Primatech Inc.  
 Node: 14  
 Page: 2

Revision: 0 02-14-95 Dwg#: 9417-1006-C

Intention: To maintain level between ?? and ??

DEVIATION	CAUSES	CONSEQUENCES	SAFEGUARDS	RECOMMENDATIONS	REMARKS	BY	COMMENTS
	2) Line pluggage or LV-1108 closed	2.1) Same as 1.*)	c2.1.1) Same as C1.1) C2.1) No change in FQIT-1401. C2.2) Heat tracing to reduce probability of pluggage				

DEVIATION	CAUSES	CONSEQUENCES	SAFEGUARDS	RECOMMENDATIONS	REMARKS	BY	COMMENTS
No/Less Flow	1) Blockage or plugging  2) Valve left closed  3) Flush connections left open	1.1) See Level-Node 14  2.1) See Level-Node 14  3.1) See Level-Node 14	1.1) Electric heat trace to reduce probability of plugging				
No/Less Flow (pressure relief path)				Review moving block valve upstream of PSE tie-in		RS	

Company: IGT

Facility: Roberts & Schafer

Session: 1 02-13-95

Revision: 0 02-14-95 Dwg#: 9417-1006-C

Node: 16 Pump G-301 Tar Quench Pump

Parameter: Flow

Intention: Provide flow to Tar Quench Condenser and Cooler

DEVIATION	CAUSES	CONSEQUENCES	SAFEGUARDS	RECOMMENDATIONS	REMARKS	BY	COMMENTS
No/Less Flow	1) Mechanical failure of pump	1.1) See Level Node 14	c1.2.1) Low flow alarm at FIT-1121 (S)L and LL				
		1.2) Low flow at FIT-1121	c1.3.1) ES alarm at ES-1118				
		1.3) Breaker trip	c1.4.1) Low pressure alarm at FIT-1102 (S)L and LL				
		1.4) Low pressure at PIT-1102					
	2) Electrical failure	2.1) Same as 1.*) except 1.3)	c2.1) Same as 1.*)				
3) Operator error	3.1) Same as 2.1	c3.1) Same as 1.*) except c1.3.1)					
4) Vent left open	4.1) See Low Level- Node 14						
5) Seal failure/leakage	5.1) See Low Level- Node 14						

DEVIATION	CAUSES	CONSEQUENCES	SAFEGUARDS	RECOMMENDATIONS	REMARKS	BY	COMMENTS
No/Less Flow	1) Manual valve closed or not open enough	1.1) See Level -- Node 14					Note PV-1120 and associated logic will be removed
	2) Blockage or plugging	2.1) Same as 1.*)	c2.1.1) Heat trace to reduce probability of plugging				Note manual valves have been added to mainline up and down stream of tee to Tar Storage Tank
	3) Drain valve left open	3.1) Same as 1.*)	c3.1.1) Valve and cap				
	4) Leak or rupture	4.1) Same as 1.*)					
Reverse Flow	1) New upstream valve left close, leaving path for hot vapor to tar storage		1.1) Only possible during start-up. Rapid detection results in system shutdown		To be reviewed in S/D session		

DEVIATION	CAUSES	CONSEQUENCES	SAFEGUARDS	RECOMMENDATIONS	REMARKS	BY	COMMENTS
No/Less Flow (after rupture burst)	1) Blockage or plugging	1.1) System overpressure	1.1) Electric heat trace	Review piping design to minimize plugging potential		RS	
More Flow (after rupture disc bursts)	1) Undetected rupture disc burst	1.1) Similar to Low flow Node 17	cl.1.1) Reduced flow at FIT-1121 cl.1.2) Low pressure at PIT-1102	Review use of orifice plate flow meter in this service (considering plugging and erosion)  Review method for detecting rupture disc burst		RS  I B	

DEVIATION	CAUSES	CONSEQUENCES	SAFEGUARDS	RECOMMENDATIONS	REMARKS	BY	COMMENTS
More Flow	1) Tube leak or rupture	1.1) Glycol in recirc side  1.2) Low glycol level at gage LG-1113 (sight gage)  1.3) Contaminate tar system. Significant clean-up required		Review necessity for leak detection		I B	

Session: 1 02-13-95

Revision: 0 02-14-95 Dwg#: 9417-1006-C

Node: 19 Tar Quench Heat Exchanger E-301

Parameter: Temperature

Intention: Reduce inlet temperature from 450F to 415F (Approx.)

DEVIATION	CAUSES	CONSEQUENCES	SAFEGUARDS	RECOMMENDATIONS	REMARKS	BY	COMMENTS
Higher Temperature	1) Undercooling on secondary side	1.1) C-304 performance reduced (See Node XX)	C1.1) Glycol system temperature control  c1.1.1) TIC-1104 reads high and alarms (S)H and HH				
	2) Tube fouling	2.1) Same as 1.1) 2.2) High differential pressure across cooler 2.3) Pump motor runs hotter	C2.1) TIC-1104 reads high and alarms (S)H and HH  C2.2) Periodic maintenance				
Lower Temperature	1) Overcooling on secondary side	1.1) C-304 performance increased (See Node XX)  1.2) TV-1104 opens	C1.1) Glycol system temperature control  c1.2.1) TIC-1104 opens up TV-1104 and alarms at (S)L and LL	Review need for cooler local dP		I B	



HAZOP-PC 2.12  
 Company: IGT  
 Facility: Roberts & Schafer  
 Session: 1 02-13-95  
 Node: 20 C-301 to Relief Header  
 Parameter: Flow

Worksheet

Primatech Inc.  
 Node: 20  
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Revision: 0 02-14-95 Dwg#: 9417-1006-C

Intention: Provide relief path from C-301

DEVIATION	CAUSES	CONSEQUENCES	SAFEGUARDS	RECOMMENDATIONS	REMARKS	BY	COMMENTS
No/Less Flow (when relieving)	None						
More Flow (when not relieving)	1) Leaking or burst rupture disc	1.1) Unwanted release to relief system	C1.1) Double disc protection PSE-1105 and PSE-1107  C1.2) Peaking pressure gage PI-1106				

HAZOP-PC 2.12

Worksheet

Primatech Inc.

Company: IGT

Node: 21

Facility: Roberts & Schafer

Page: 1

Session: 1 02-13-95

Revision: 0 02-14-95 Dwg#: 9417-1006-C

Node: 21 Product gas from C-301 to middle oil

Parameter: Flow

Intention: Provide product flow from C-301 to middle oil

DEVIATION	CAUSES	CONSEQUENCES	SAFEGUARDS	RECOMMENDATIONS	REMARKS	BY	COMMENTS
No/Less Flow	None			Remove PV and PY-1109		RS	

DEVIATION	CAUSES	CONSEQUENCES	SAFEGUARDS	RECOMMENDATIONS	REMARKS	BY	COMMENTS
No/Less Flow	1) Plugging or blockage  2) Manual valve left closed  3) Failure of LV-1108	1.1) High level in tar separator  1.2) Low flow to tank D-503  1.3) Plugging due to low velocity  2.1) Same as 1.*)  3.1) Same as 1.*)	c1.1.1) High level and alarm at LIT-1108 (S)H and HH  c1.2.1) Low flow at FIT-1401  C2.1) Operator training and procedures  C3.1) LV-1108 is FO	Review line sizing and considering salting velocity		RS	
More Flow	1) Failure of LV-1108	1.1) Low level in C-301  1.2) Higher flow to tank D-503	c1.2.1) Hi flow at FIT-1401				

HAZOP-PC 2.12  
 Company: IGT  
 Facility: Roberts & Schafer  
 Session: 1 02-13-95  
 Node: 23 Nat Gas Supply to Preheater  
 Parameter: Pressure

Worksheet

Revision: 0 02-15-95 Dwg#: 9417-1006-C  
 Intention: Provide Nat Gas to preheater at 6" to 250psig

Primatech Inc.  
 Node: 23  
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DEVIATION	CAUSES	CONSEQUENCES	SAFEGUARDS	RECOMMENDATIONS	REMARKS	BY	COMMENTS
Higher Pressure	1) Any cause	1.1) Over pressure of regulator body	c1.2.1) High pressure switch (set at 15") downstream of reg.trips unit	Verify max nat gas supply pressure		B	
		1.2) Shutdown of preheater	c.1.2.2) Loss of flame at tip will be seen by scanner and unit is tripped.	Common shutdown alarm will be provided via PLC interface		C RS	
		1.3) Recycle gas and air temp drops	c1.3.1) Low temp alarm TIC-0729A/B (S)L and LL				
		1.4) Bed temp drops	c1.4.1) Low temp alarm TE-0710/27 (S)L and LL	Operating procedures to address reduced coal feed rate operations for this event		I	
Lower Pressure	1) Any cause	1.1) Shutdown of preheater	c1.1.1) Low pressure switch downstream of reg.trips unit				
		1.2) Recycle gas and air temp drops	c.1.1.2) Loss of flame at tip will be seen by scanner and unit is tripped.				
		1.3) Bed temp drops	c1.2.1) same as Higher pressure				
			c1.3.1) same as Higher pressure				

DEVIATION	CAUSES	CONSEQUENCES	SAFEGUARDS	RECOMMENDATIONS	REMARKS	BY	COMMENTS
Higher Temperature	1) Instrument error	1) Recycle gas to booster has higher temp	1.1) Booster heater controls response 2.1) Stack temp Hi shutdown	Determine maximum temp for materials Add indep. TESHH on recycle and air lines to shutdown heater Add TS(S)H alarm to existing TE Review stress analysis and support design for piping Review line sizing/materials		B C  C  RS  RS  B RS	
		2) Stack temp increases					
Lower Temperature	1) Instrument error	1) Recycle gas to booster has lower temp 2) Stack temp decreases	1.1) Booster controls respond	Operating procedures to address reduced operations mode		I	

Company: IGT  
Facility: Roberts & Schafer  
Session: 1 02-13-95  
Node: 25 Air from Preheater to Boosters  
Parameter: Temperature

Revision: 0 02-15-95 Dwg#: 9417-1006-C

Intention: Provide Air to Boosters at 1100F

DEVIATION	CAUSES	CONSEQUENCES	SAFEGUARDS	RECOMMENDATIONS	REMARKS	BY	COMMENTS
Higher Temperature	1) Instrument error	1) Air to booster has higher temp	1.1) Booster heater controls response 2.1) Stack temp Hi shutdown	Determine maximum temp for materials Add indep. TESH (1200F) on recycle and air lines to shutdown heater Add TS(S)H alarm to existing TE (1150F) Review stress analysis and support design for piping Review line sizing/materials		B C  C  RS RS  B RS	
		2) Stack temp increases					
Lower Temperature	1) Instrument error	1) Air to booster has lower temp	1.1) Booster controls respond	Operating procedures to address reduced operations mode		I	
		2) Stack temp decreases					

DEVIATION	CAUSES	CONSEQUENCES	SAFEGUARDS	RECOMMENDATIONS	REMARKS	BY	COMMENTS
No/Less Flow	1) Manual valve left closed	1.1) Low flow to preheater 1.2) Low flow at FE-0901, and FE-0738 and FE-0743	c1.2.1) Low flow alarms on FE-0901, -0738, and -0743 (S)L and LL c1.2.2) FE-0901 (S)LL results in shutdown	Review need for additional shutdown protection switch for feeds to boosters A&B.		I B	Note: FV-0901 has been removed
	2) Any other cause	2.1) Same as 1.*)					
More Flow	1) Tube rupture	1.1) Stack temp may increase 1.2) deleted 1.3) Higher flow at FE-0901 1.4) Lower flow at FE-0738 and FE-0743 1.5) Bed velocity flow decreases 1.6) Release to environment	c1.1.1) High stack temp alarm and S/D c1.3.1) High flow alarm at FE-0901 (S)H c1.4.1) Low flow alarm at FE-0738 and 0743 (S)L	Review need for flow balance and associated operating procedures. Also consider envir. impact.		I	
	2) Any other	1.1) Exit temp	c1.1.1) TE-0729A and B				

DEVIATION	CAUSES	CONSEQUENCES	SAFEGUARDS	RECOMMENDATIONS	REMARKS	BY	COMMENTS
	cause	decreases 1.2) Higher flow at FE-0901, -0738 and -0743 1.3) Bed velocity increases	alarm (S)H c1.2.1) High flow alarm on FE-0901, -0738, and 0743 (S)H				



DEVIATION	CAUSES	CONSEQUENCES	SAFEGUARDS	RECOMMENDATIONS	REMARKS	BY	COMMENTS
No/Less Flow	1) Air compressor failure	1.1) Low flow to preheater 1.2) Low flow at FE-09**, and FE-0736 and FE-0741	c1.2.1) Low flow alarms on FE-09**, -0736, and -0741 (S)L and LL c1.2.2) FE-09** (S)LL results in shutdown	Review need for additional shutdown protection switch for feeds to boosters A&B. Add start-up block valve in air line to allow for start-up N2		I B	Note: Butterfly valve has been removed
	2) Any other cause	2.1) Same as 1.)				I B	
More Flow	1) Tube rupture	1.1) Stack temp decrease 1.2) deleted 1.3) Higher flow at FE-09** 1.4) Lower flow at FE-0736 and FE-0741 1.5) Bed velocity flow decreases	c1.3.1) High flow alarm at FE-09** (S)H c1.4.1) Low flow alarm at FE-0736 and 0741 (S)L	Review need for flow balance and associated operating procedures.		I	
	2) Any other	1.1) Exit temp	c1.1.1) TE-0729A and B				

DEVIATION	CAUSES	CONSEQUENCES	SAFEGUARDS	RECOMMENDATIONS	REMARKS	BY	COMMENTS
	cause  3) Increase flow demand for loss of preheater	decreases  1.2) Higher flow at FE-09**, -0736 and -0741  1.3) Bed velocity increases  3.1) Unknown	alarm (S)H  c1.2.1) High flow alarm on FE-09**, -0736, and 0741 (S)H			I B	
				Review off-normal flow conditions and changed flow conditions			

DEVIATION	CAUSES	CONSEQUENCES	SAFEGUARDS	RECOMMENDATIONS	REMARKS	BY	COMMENTS
No/Less Flow	1) Valve failure FV-0738	1.1) Low flow at FIT-0738  1.2) High temperature in Booster A resulting in potential damage to vessel and refractory  1.3) Low bed velocity  1.4) High outlet temp from Booster A  1.5) High bed temp  1.6) Bed upset/ coal feed interruption	C1.1) Valve fails open  c1.1.2) Low flow alarm at FIT-0738 (S)L  c1.4.1) High temp alarm at TE-0729A (S)H and TSHH-07** resulting in S/D  c1.5.1) High temp alarms at TE-0710/27 (S)H and HH  C1.1) Booster A air and nat gas valves modulate down to as low as low fire	Review need for mechanical percent closed limit  TSHH07** and resulting S/D logic will be added  Review preheated recycle gas piping material spec.		I B C  C  B	Note: Control valve will be added to line
More Flow	1) Valve fails open mechanical or logic problem	1.1) Booster exit temperature goes down  1.2) Bed temp decreases slowly  1.3) High flow at FIT-0738	c1.1.1) Low temp alarm TE-0729A (S)L  c1.2.1) Low temp indication at TE-0710/27  c1.3.1) High flow alarm FIT-0738 (S)H	Review max. flow rate thru valve to assist in upset evaluation		C RS	

DEVIATION	CAUSES	CONSEQUENCES	SAFEGUARDS	RECOMMENDATIONS	REMARKS	BY	COMMENTS
Less Flow	1) Valve failure FV-0729B down to protective stop  2) Booster B inlet valve too open	1.1) Low flow at FIT-0736	c1.1.2) Low flow alarm at FIT-0736 (S)L and resulting S/D	TE-0729 (S)LL should be removed		RS	Note: Control valve will be added to linr
		1.2) Low temperature in Booster A	c1.4.1) Low temp alarm at TE-0729A (S)L and LL				
More Flow	1) Valve fails open mechanical or logic problem	1.3) Low bed velocity	c1.5.1) High temp alarms at TE-0710/27 (S)L and LL	Review how control logic will respond		C	
		1.4) Lower outlet temp from Booster A	C1.1) Booster A nat gas valve modulate down				
		1.5) Lower bed temp	C1.2) Auto S/D on loss of flame detector				
		1.6) Bed upset/ coal feed interruption	c1.4.1) Operator training and procedures				
		1.7) Nat gas will increase due to temp demand					
		2.1) Same as above	C2.1) Same as above				
			C2.2) High flow alarm at FIT-0741 (S) H and HH				
		1.1) Booster exit temperature goes up	c1.1.1) High temp alarm TE-0729A (S)H				
		1.2) Bed temp up slowly	c1.1.2) High temp alarm TSHH-07** and resulting S/D				
		1.3) High flow at FIT-0736	c1.2.1) High temp indication at TE-0710/27				
		1.4) Nat gas will back-off on temp rise	c1.3.1) High flow alarm FIT-0736 (S)H				

DEVIATION	CAUSES	CONSEQUENCES	SAFEGUARDS	RECOMMENDATIONS	REMARKS	BY	COMMENTS
Less Flow	1) Valve failure FV-0729C down to protective stop	1.1) Low flow at FIT-0737	c1.1.2) Low pressure alarm at PSL-07** and resulting S/D  c1.4.1) Low temp alarm at TE-07** (S)L and LL  c1.5.1) Low temp alarms at TE-0710/27 (S)L and LL	TE-07** (S)LL should be removed		RS	Note: Control valve will be added to line Note: The design and control philosophy is the same as the burner management system for the preheater.
		1.2) Low temperature in Booster A	C1.1) Booster A air valve modulate down				
		1.3) Low bed velocity	C1.2) Auto S/D on loss of flame detector				
		1.4) Lower outlet temp from Booster A	c1.4.1) Operator training and procedures				
		1.5) Lower bed temp					
		1.6) Bed upset/ coal feed interruption					
		1.7) Air will decrease following gas		Review how control logic will respond		C	
	2) Booster B inlet valve too open	2.1) Same as above	C2.1) Same as above 1.*) C2.2) High flow alarm at FIT-0742 (S) H and HH				
	3) Block valve fails closed	3.1) Same as 1.*)	C3.1) Same as above 1.*) except PSL doesn't close block valve				
	4) Regulator failure	3.1) Same as 1.*)	4.1) Same as above 1.*)				
More Flow	1) Valve fails open mechanical or logic problem	1.1) Booster exit temperature goes up	c1.1.1) High temp alarm TE-07** (S)H  c1.1.2) High temp alarm TSHH-07** and resulting				
		1.2) Bed temp					

Company: IGT

Facility: Roberts & Schafer

Session: 1 02-13-95

Revision: 0 02-15-95 Dwg#: 9417-1006-C

Node: 30 Nat Gas inlet to Booster A

Parameter: Flow

Intention: Provide nat gas at 81 #/hr

DEVIATION	CAUSES	CONSEQUENCES	SAFEGUARDS	RECOMMENDATIONS	REMARKS	BY	COMMENTS
	2) Regulator fails	up slowly 1.3) High flow at FIT-0737 1.4) Air will back-off on temp rise 2.1) Same as 1.*)	S/D c1.3.1) High pressure switch PSH-07** alarm and resulting S/D c1.3.2) Loss of flame tip seen by scanner and resulting S/D c1.2.1) High temp indication at TE-0710/27 c1.3.1) High flow alarm FIT-0737 (S)H C2.1) Same as 1.*0 C2.2) Flow control valve throttles back				

HAZOP-PC 2.12  
 Company: IGT  
 Facility: Roberts & Schafer  
 Session: 1 02-13-95  
 Node: 31 Booster Heater A  
 Parameter: Pressure

Worksheet

Primatech Inc.  
 Node: 31  
 Page: 1

Revision: 0 02-15-95 Dwg#: 9417-1006-C

Intention: Retain process materials at less than 35 psia

DEVIATION	CAUSES	CONSEQUENCES	SAFEGUARDS	RECOMMENDATIONS	REMARKS	BY	COMMENTS
Lower Pressure	1) Any leak	1.1) Release of hazardous materials 1.2) Lower bed temp 1.3) Bed upset	C1.1.1) Approved fire protection plan C1.1.2) Lower pressure in retort and PIT-0706 (S)L and (S)LL C1.1.3) Lower bed temp at TE-0710/27				

Session: 1 02-13-95  
 Node: 31 Booster Heater A  
 Parameter: Safety

Revision: 0 02-15-95 Dwg#: 9417-1006-C

Intention: Maintain integrity of refractory

DEVIATION	CAUSES	CONSEQUENCES	SAFEGUARDS	RECOMMENDATIONS	REMARKS	BY	COMMENTS
Less Safety	1) Partial loss of refractory			Review need for detecting refractory failure (eg. heat sensitive paint)		I	

DEVIATION	CAUSES	CONSEQUENCES	SAFEGUARDS	RECOMMENDATIONS	REMARKS	BY	COMMENTS
No/Less Flow	1) Valve failure FV-0743	1.1) Low flow at FIT-0743  1.2) High temperature in Booster B resulting in potential damage to vessel and refractory  1.3) Low bed velocity  1.4) High outlet temp from Booster B  1.5) High bed temp  1.6) Bed upset/ coal feed interruption	C1.1) Valve fails open  c1.1.2) Low flow alarm at FIT-0743 (S)L  c1.4.1) High temp alarm at TE-07** (S)H and TSHH-07** resulting in S/D  c1.5.1) High temp alarms at TE-0710/27 (S)H and HH  C1.1) Booster B air and nat gas valves modulate down to as low as low fire	Review need for mechanical percent closed limit  TSHH07** and resulting S/D logic will be added  Review preheated recycle gas piping material spec.		I B C  C  B	Note: Control valve will be added to line
More Flow	1) Valve fails open mechanical or logic problem	1.1) Booster exit temperature goes down  1.2) Bed temp decreases slowly  1.3) High flow at FIT-0743	c1.1.1) Low temp alarm TE-07** (S)L  c1.2.1) Low temp indication at TE-0710/27  c1.3.1) High flow alarm FIT-0743 (S)H	Review max. flow rate thru valve to assist in upset evaluation		C RS	



HAZOP-PC 2.12  
 Company: IGT  
 Facility: Roberts & Schafer  
 Session: 1 02-13-95  
 Node: 33 Air inlet to Booster B  
 Parameter: Flow

Worksheet

Primatech Inc.  
 Node: 33  
 Page: 1

Revision: 0 02-15-95 Dwg#: 9417-1006-C

Intention: Provide air at a rate of xxx #/hr

DEVIATION	CAUSES	CONSEQUENCES	SAFEGUARDS	RECOMMENDATIONS	REMARKS	BY	COMMENTS
Less Flow	1) Valve failure FV-0729D down to protective stop	1.1) Low flow at FIT-0741	c1.1.2) Low flow alarm at FIT-0741 (S)L and resulting S/D	TE-0729 (S)LL should be removed			Note: Control valve will be added to line
		1.2) Low temperature in Booster B	c1.4.1) Low temp alarm at TE-07** (S)L and LL				
1.3) Low bed velocity		c1.5.1) High temp alarms at TE-0710/27 (S)L and LL					
1.4) Lower outlet temp from Booster B		C1.1) Booster B nat gas valve modulate down					
1.5) Lower bed temp		C1.2) Auto S/D on loss of flame detector					
1.6) Bed upset/ coal feed interruption		c1.4.1) Operator training and procedures					
1.7) Nat gas will increase due to temp demand			Review how control logic will respond				
Less Flow	2) Booster A inlet valve too open	2.1) Same as above	C2.1) Same as above				
			C2.2) High flow alarm at FIT-0741 (S) H and HH				
More Flow	1) Valve fails open mechanical or logic problem	1.1) Booster exit temperature goes up	c1.1.1) High temp alarm TE-07** (S)H				
		1.2) Bed temp up slowly	c1.1.2) High temp alarm TSHH-07** and resulting S/D				
		1.3) High flow at FIT-0741	c1.2.1) High temp indication at TE-0710/27				
		1.4) Nat gas will back-off on temp rise	c1.3.1) High flow alarm FIT-0741 (S)H				

DEVIATION	CAUSES	CONSEQUENCES	SAFEGUARDS	RECOMMENDATIONS	REMARKS	BY	COMMENTS
Less Flow	1) Valve failure FV-0729E down to protective stop	1.1) Low flow at FIT-0742  1.2) Low temperature in Booster B  1.3) Low bed velocity  1.4) Lower outlet temp from Booster B  1.5) Lower bed temp  1.6) Bed upset/ coal feed interruption  1.7) Air will decrease following gas	c1.1.2) Low pressure alarm at PSL-07** and resulting S/D	TE-07** (S)LL should be removed		RS	Note: Control valve will be added to line Note: The design and control philosophy is the same as the burner management system for the preheater.
			c1.4.1) Low temp alarm at TE-07** (S)L and LL				
			c1.5.1) Low temp alarms at TE-0710/27 (S)L and LL				
			C1.1) Booster B air valve modulate down				
			C1.2) Auto S/D on loss of flame detector				
			c1.4.1) Operator training and procedures				
	2) Booster A inlet valve too open  3) Block valve fails closed  4) Regulator failure	2.1) Same as above  3.1) Same as 1.*)  3.1) Same as 1.*)	C2.1) Same as above 1.*)	Review how control logic will respond		C	
			C2.2) High flow alarm at FIT-0742 (S) H and HH				
			C3.1) Same as above 1.*) except PSL doesn't close block valve				
	4.1) Same as above 1.*)						
More Flow	1) Valve fails open mechanical or logic problem	1.1) Booster exit temperature goes up	c1.1.1) High temp alarm TE-07** (S)H				
		1.2) Bed temp	c1.1.2) High temp alarm TSHH-07** and resulting				

Company: IGT

Facility: Roberts & Schafer

Session: 1 02-13-95

Revision: 0 02-15-95 Dwg#: 9417-1006-C

Node: 34 Nat Gas inlet to Booster B

Parameter: Flow

Intention: Provide nat gas to Booster at a rate of \*\*\* #/hr

DEVIATION	CAUSES	CONSEQUENCES	SAFEGUARDS	RECOMMENDATIONS	REMARKS	BY	COMMENTS
	2) Regulator fails	up slowly 1.3) High flow at FIT-0742 1.4) Air will back-off on temp rise 2.1) Same as 1.*)	S/D c1.3.1) High pressure switch PSH-07** alarm and resulting S/D c1.3.2) Loss of flame tip seen by scanner and resulting S/D c1.2.1) High temp indication at TE-0710/27 c1.3.1) High flow alarm FIT-0742 (S)H C2.1) Same as 1.*0 C2.2) Flow control valve throttles back				

HAZOP-PC 2.12  
 Company: IGT  
 Facility: Roberts & Schafer  
 Session: 1 02-13-95  
 Node: 35 Booster Heater B  
 Parameter: Pressure

Worksheet

Primatech Inc.  
 Node: 35  
 Page: 1

Revision: 0 02-15-95 Dwg#: 9417-1006-C

Intention: Retain material at a pressure of 35 psia

DEVIATION	CAUSES	CONSEQUENCES	SAFEGUARDS	RECOMMENDATIONS	REMARKS	BY	COMMENTS
Lower Pressure	1) Any leak	1.1) Release of hazardous materials 1.2) Lower bed temp 1.3) Bed upset	C1.1.1) Approved fire protection plan C1.1.2) Lower pressure in retort and PIT-0706 (S)L and (S)LL C1.1.3) Lower bed temp at TE-0710/27				

Session: 1 02-13-95  
 Node: 35 Booster Heater B  
 Parameter: Safety

Revision: 0 02-15-95 Dwg#: 9417-1006-C

Intention: Maintain refractory integrity

DEVIATION	CAUSES	CONSEQUENCES	SAFEGUARDS	RECOMMENDATIONS	REMARKS	BY	COMMENTS
Less Safety	1) Partial loss of refractory			Review need for detecting refractory failure (eg. heat sensitive paint)		I	

Company: IGT  
Facility: Roberts & Schafer  
Session: 1 02-13-95  
Node: 36 Vent gases to Thermal oxidizer  
Parameter: Flow

Revision: 0 02-15-95 Dwg#: 9417-1006-C

Intention: Route vents to T/O at a rate of 959 #/hr

DEVIATION	CAUSES	CONSEQUENCES	SAFEGUARDS	RECOMMENDATIONS	REMARKS	BY	COMMENTS
No/Less Flow	1) FV-136 fails closed	1.1) Back-up of the vent system 1.2) T/O continues to run consuming additional fuel gas	C1.1) FV-135 interlocked to open				
	2) Upstream effects (eg. valve left closed, plugging, etc.)	2.1) Same as 1.* 2.2) Pressure will build-up in upstream sources	c2.2.1) Pressure indication at the upstream systems				
More Flow	1) Upstream sources exceed expected values	1.1) Increase temp in T/O	c1.1.1) Hi temp trip TE-122 (S)HH	Revise P&ID to reflect shutdown via TE-122 loop. Also indicate open flare diversion valve		C	
	2) Valve not closed during maintenance	2.1) Release hot gas to maintenance operators	c2.1.1) Blind at T/O	Review PFD stream 503 instant. flow		B	
	3) Valve fails to close on signal from TIC-108	3.1) Continued flow from upstream sources 3.2) Possible releases at above permit limits	c3.1.1) Low temp alarm at TIC-108 (S)L				

Session: 1 02-13-95

Revision: 0 02-15-95 Dwg#: 9417-1006-C

Node: 36 Vent gases to Thermal oxidizer

Parameter: Composition

Intention: Heating value not to exceed 4 MBtu/hr

DEVIATION	CAUSES	CONSEQUENCES	SAFEGUARDS	RECOMMENDATIONS	REMARKS	BY	COMMENTS
More Composition	1) Unknown	1.1) High temp in T/O and exhaust	c1.1.1) TE-122 (S)HH causes S/D	Review max heat value expected		I B	

DEVIATION	CAUSES	CONSEQUENCES	SAFEGUARDS	RECOMMENDATIONS	REMARKS	BY	COMMENTS
No/Less Flow	1) Valve fails shut	1.1) High temp at TE-122 and TE-108	c1.1.1) TE-122 (S)HH results in S/D				
		1.2) High level at LIC-1310	c1.2.1) High level alarm at LIC-1310 (S)H and HH				
		1.3) Water into the middle oil system					
	2) Manual valve left closed	2.1) Same as 1.*)					
	3) Plugging of tip	3.1) Same as 1.*)					
	4) Low level in light oil separator	4.1) Same as 1.1		Review need for LIC-1310 (S)L and LL and addition of city water quench  Revise design to address loss of sour quench water		I B RS	
More Flow	1) Upstream pressure source	1.1) Lower temp at TIC-108 and TE-122				C	

Company: IGT  
Facility: Roberts & Schafer  
Session: 1 02-13-95  
Node: 38 Weigh Hopper for Coarse Coal attached tote bag unloader  
Parameter: Composition  
Revision: 0 02-16-95 Dwg#: 9417-1006-C  
Intention: Moisture control

DEVIATION	CAUSES	CONSEQUENCES	SAFEGUARDS	RECOMMENDATIONS	REMARKS	BY	COMMENTS
Other Than Composition	1) Weather induced moisture	1.1) Difficult operation and freeze-up		Review need for weather protection	Temporary wind protection (such as a wall tarp) will be provided in the field (closed -- 3/15/95)	I B	

Session: 1 02-13-95  
Node: 38 Weigh Hopper for Coarse Coal attached tote bag unloader  
Parameter: Level  
Revision: 0 02-16-95 Dwg#: 9417-1006-C  
Intention: Hold and measure coarse coal load

DEVIATION	CAUSES	CONSEQUENCES	SAFEGUARDS	RECOMMENDATIONS	REMARKS	BY	COMMENTS
Higher Level	1) Overfill operator error	1.1) Overfill  1.2) Cleanout and maintain	C1.1) WT-0602	Review and recommend how and where to determine weight of coal for a given run	Coal feed will be determined by the decrease in weight in the weigh hopper and correlated by the feed screw rate. Additional isolation valves eliminate simultaneous fill and feed concerns. Interlock isolation valve to high weight in weigh hopper. Revise level loop to high level switch only, not continuous readout. (3/15/95)  Delete liner tensioner and liner impaler from Reimelt scope (3/15/95)	I B	

HAZOP-PC 2.12

Worksheet

Primatech Inc.

Company: IGT

Node: 38

Facility: Roberts & Schafer

Page: 2

Session: 1 02-13-95

Revision: 0 02-16-95 Dwg#: 9417-1006-C

Node: 38 Weigh Hopper for Coarse Coal attached tote bag unloader

Parameter: Level

Intention: Hold and measure coarse coal load

DEVIATION	CAUSES	CONSEQUENCES	SAFEGUARDS	RECOMMENDATIONS	REMARKS	BY	COMMENTS
	2) Failure to flow out due to sticking	2.1) Same as above		Operating and maintenance procedures will include inspection of the cone lining		I	



DEVIATION	CAUSES	CONSEQUENCES	SAFEGUARDS	RECOMMENDATIONS	REMARKS	BY	COMMENTS
Reverse Flow	1) Poor seal of block valve	1.1) Not able to equalize pressure  1.2) Not able to feed coal		Investigate design change to knife gate or other alternative isolation valve	Design to reflect use of 8" Macawber dome valves for coarse inlet and 6" for fine and all other coarse for isolation. (Valve supply no longer part of Reimelt scope) (3/15/95)	ALL	Cost info and stack height are to be considered
	2) Instrument loop failure	2.1) Same as 1.*)  2.2) Seal Valve could jam and fail	C2.1) Weight and level in weigh hopper does not decrease  C2.2) Valve position ind.	Reimelt will review and revise PLC program to include a trouble alarm on weight change rate	PLC program will be revised (3/15/95)	R	Note: Reimelt system is completely automated, P&ID will reflect this
No Flow (when required to flow)	1) Valve fails to open	1.1) No flow to lock hopper  1.2) No flow from the Weigh hopper	C.1.1) Valve position ind.  C.1.2) Weight and level in weigh hopper does not decrease				
	2) Instrument loop fails	2.1) Same as 1.*)					
	3) Plugging	3.1) Same as 1.*)					

DEVIATION	CAUSES	CONSEQUENCES	SAFEGUARDS	RECOMMENDATIONS	REMARKS	BY	COMMENTS
Higher Pressure	1) Failure of instrument loop	1.1) Overpressurization of vessel	C1.1.1) Rupture disc	Investigate pressure rating and pressure relieving on the N2 feed to Feed System	A downstream line PSV set at 50 psi will be supplied by Reimelt. (3/15/95)	B I R	
		1.2) Rupture first disc	C1.2.1) Peaking PI-0607				
Less Pressure	1) Instrument failure	1.1) Reverse flow		Investigate and recommend the addition of redundant pressure loops or other alternative	Severity of failure and probability of failure low, no immediate action required. Note: Spare nozzles are provided on the vessels to accommodate later modifications. (3/15/95)	R	PDI alternative to be considered
	2) N2 failure	1.2) System upset					
		2.1) Can't pressurize	C2.1.1) Delta Pressure control				
		2.2) Can't operate	C.2.1.2) PI-0608A				
	3) Leak or gasket failure	3.1) Same as 2.*)	C.3.1.1) Maintenance procedures				

Session: 1 02-13-95

Revision: 0 02-16-95 Dwg#: 9417-1006-C

Node: 40 Coarse coal lock hopper

Parameter: Level

Intention: To hold coarse coal (25 cuft gross)

DEVIATION	CAUSES	CONSEQUENCES	SAFEGUARDS	RECOMMENDATIONS	REMARKS	BY	COMMENTS
Higher Level	1) Instrument loop failure	1.1) Overfill	C1.1) Manual inspection of weigh change	Review weight change vs. time alarm and possible cut-off	Improved reliability by using Celtek probe. No safety issue. Sufficient information is	I B R RS	
			c1.2.1) See node 39				

DEVIATION	CAUSES	CONSEQUENCES	SAFEGUARDS	RECOMMENDATIONS	REMARKS	BY	COMMENTS
		1.2) Plugging of feed line			provided with the existing instrumentation. DCS will be used to generate alarm (3/15/95)		

DEVIATION	CAUSES	CONSEQUENCES	SAFEGUARDS	RECOMMENDATIONS	REMARKS	BY	COMMENTS
Reverse Flow	1) Poor seal of block valve	1.1) Heat-up of feed line, material and release of gas from coal	C1.1) Valve position indication and interlocks to PLC controls	Investigate design change to knife gate or other alternative isolation valve	Design to reflect use of 8" Macawber dome valves for coarse inlet and 6" for fine and all other coarse for isolation. (Valve supply no longer part of Reimelt scope) (3/15/95)	ALL	Cost info and stack height are to be considered  Note: Reimelt system is completely automated, P&ID will reflect this
		1.2) Inability to feed coal 1.3) System upset 1.4) Potential baghouse damage					
	2) Instrument loop failure	2.1) No consequence	C2.1) Lock hopper at same pressure	Reimelt will review and revise PLC program to include a trouble alarm on weight change rate	PLC program will be revised (3/15/95)	R	
No Flow (when required to flow)	1) Valve fails to open	1.1) No flow to feed hopper	C.1.1) Valve position ind.				
		1.2) No flow from the lock hopper	C.1.2) Level in lock hopper does not decrease				
		1.3) System shutdown operator initiated	C1.3) Level in feed hopper does not increase				
	2) Instrument loop fails	2.1) Same as 1.*)					
	3) Plugging	3.1) Same as 1.*)					

HAZOP-FC 2.12  
 Company: IGT  
 Facility: Roberts & Schafer  
 Session: 1 02-13-95  
 Node: 42 Coarse coal feed hopper  
 Parameter: Pressure

Worksheet

Revision: 0 02-16-95 Dwg#: 9417-1006-C  
 Intention: Maintain pressure at 35-40 psia

Primatech Inc.  
 Node: 42  
 Page: 1

DEVIATION	CAUSES	CONSEQUENCES	SAFEGUARDS	RECOMMENDATIONS	REMARKS	BY	COMMENTS
Higher Pressure	1) Failure of instrument loop	1.1) Overpressurization of vessel	C1.1.1) Rupture disc C1.2.1) Peaking PI-0613	Investigate pressure rating and pressure relieving on the N2 feed to Feed System	Add in N2 header downstream PSV set at 50 psi. PSV now in Reimelt scope (same valve as in node 40 (3/15/95)	B I R	
		1.2) Rupture first disc					
Less Pressure	2) Gasifier upset	1.1) Back pressure to feed hopper	C.2.1) Same as C1.*)	Review need for continuous bleed flow N2 to the feed hopper	Add a manual adjust rotometer and remove PV-08B (3/15/95)	I B R	
		1.2) Hot gases back-up line 1.3) Eventual plugging. Cleaning required.	C.2.2) Gasifier pressure indication				
Less Pressure	1) Instrument failure	1.1) Reverse flow		Include in the review of the lock hopper pressure protection issue the need to protect the feed hopper	Severity of failure and probability of failure low, no immediate action required. Note: Spare nozzles are provided on the vessels to accommodate later modifications. (3/15/95)	R	
		1.2) System upset					
		2) N2 failure	2.1) Can't pressurize 2.2) Can't operate 2.3) Unit upset				
	3) Leak or	3.1) Same as 2.*)	C.3.1.1) Maintenance				

DEVIATION	CAUSES	CONSEQUENCES	SAFEGUARDS	RECOMMENDATIONS	REMARKS	BY	COMMENTS
	gasket failure 4) Rupture leak or failure		procedures C4.1) Double disc protection				

DEVIATION	CAUSES	CONSEQUENCES	SAFEGUARDS	RECOMMENDATIONS	REMARKS	BY	COMMENTS
Higher Level	1) Instrument loop failure  2) Plugging	1.1) Overfill 1.2) Plugging of feed line 1.3) Valve may not close and thus indicate so.	C1.1) Manual inspection of level change at lock hopper  C2.1) LI-0610 and the PLC program control				
No/Lower Level	1) Instrument loop failure	1.1) Empty hopper 1.2) No feed to screws 1.3) System interruption	c1.1.1) TE-0615 may decrease c1.1.2) Gasifier temp increase at TE-0710/27 c1.1.3) Hot oil retron temp will rise				

Company: IGT

Facility: Roberts & Schafer

Session: 1 02-13-95

Revision: 0 02-16-95 Dwg#: 9417-1006-C

Node: 43 LT-0601,04,10,21,24 and 30

Parameter: Instrumentation

Intention: Common Level Transmitter for all Hoppers

DEVIATION	CAUSES	CONSEQUENCES	SAFEGUARDS	RECOMMENDATIONS	REMARKS	BY	COMMENTS
Other Than Instrumentation	1) Any malfunction  2) Trouble with limited depth	1.1) Loss of all level information	C1.1) Failure mode is total failure. Set to zero  C1.2) High reliability of LT	Review appropriateness of ultrasonic probes	Revise design to utilize Celtek probes (3/15/95)	I B R	

HAZOP-PC 2.12

Worksheet

Primatech Inc.

Company: IGT

Node: 44

Facility: Roberts & Schafer

Page: 1

Session: 1 02-13-95

Revision: 0 02-16-95 Dwg#: 9417-1006-C

Node: 44 Rupture disc discharge lines

Parameter: Flow

Intention: Provide safe routing of vessel discharge

DEVIATION	CAUSES	CONSEQUENCES	SAFEGUARDS	RECOMMENDATIONS	REMARKS	BY	COMMENTS
More Flow	1) Discs rupture	1.1) Damage to any downstream components		Review routing of rupture disc discharge lines to flare	Route to T.O. stack (3/15/95)	I B	



HAZOP-PC 2.12  
 Company: IGT  
 Facility: Roberts & Schafer  
 Session: 1 02-13-95  
 Node: 45 N2 feed to Hoppers  
 Parameter: Flow

Worksheet

Primatech Inc.  
 Node: 45  
 Page: 1

Revision: 0 02-16-95 Dwg#: 9417-1006-C

Intention: Provide purge and pressurization flow

DEVIATION	CAUSES	CONSEQUENCES	SAFEGUARDS	RECOMMENDATIONS	REMARKS	BY	COMMENTS
No/Less Flow	1) Interruption of N2 supply  2) Valve or regulator failure  3) Leak/rupture	1.1) Can't pressurize  1.2) Can't feed  1.3) Unit interruption  1.4) Potential for hot gas back-up at retort entrance	C1.1) Local ind. PI-0619 and PI-0636  C1.2) Coal feed system PIT's 0608A and 0608B read low  3.1.1) Gasifier feed line temp increases TE-0644 or 0645	Add PIT's low alarms (S)L		RS	
More Flow	1) Regulator fails	1) Higher pressure in hopper		Review need for line PSV	Add per node 42 (3/15/95)	I B	

HAZOP-PC 2.12  
 Company: IGT  
 Facility: Roberts & Schafer  
 Session: 1 02-13-95  
 Node: 46 N2 Vent from Hoppers  
 Parameter: Flow

Worksheet

Primatech Inc.  
 Node: 46  
 Page: 1

Revision: 0 02-16-95 Dwg#: 9417-1006-C

Intention: Provide adequate vent/equalization flow from hoppers

DEVIATION	CAUSES	CONSEQUENCES	SAFEGUARDS	RECOMMENDATIONS	REMARKS	BY	COMMENTS
No Flow (equalization mode)	1) Valve fails to open	1.1) System may oper poorly	C1.1) PIT-0608A C1.2) PLC interlock on sequence and alarm C1.3) Valve position ind.	All hopper N2 fill and vent valves FC		R	
No Flow (the vent mode)	1) Valve fails to open  2) Plugging	1.1) System interruption  2.1) Same as 1.*)	C1.1) Valve position ind. C1.2) PLC interlock on sequence and alarm C1.3) PIT-0608A	Review need for procedure to "blow" line clean after venting		I B	
More Flow thru vent valve in pressurize mode	1) Valve fails to closed	1.1) Can't pressurize	C1.1) Valve position ind. C1.2) Low pressure at PIT-0608A				
More Flow (vent mode)	1) Equalization valve leaks or fails to close	1.1) Can't hold pressure in feed hopper 1.2) Backflow from retort 1.3) System inop	C1.1) Valve position ind. C1.2) Low pressure at PI-0608B C1.3) High temp at TE-0615				

HAZOP-PC 2.12  
 Company: IGT  
 Facility: Roberts & Schafer  
 Session: 1 02-13-95  
 Node: 47 Baghouse system  
 Parameter: Flow

Worksheet

Primattech Inc.  
 Node: 47  
 Page: 1

Revision: 0 02-16-95 Dwg#: 9417-1006-C

Intention: Free flow from weigh hoppers to baghouse

DEVIATION	CAUSES	CONSEQUENCES	SAFEGUARDS	RECOMMENDATIONS	REMARKS	BY	COMMENTS
No/Less Flow (to the baghouse)	1) Blower failure	1.1) Dust at loading area 1.2) Settling in lines	c1.1.1) Operating procedures require respirator and eye prot. C1.1) Low reading on bag dP				
	2) High dP on bag	2.1) Same as 1.*)	C2.1) High dP at PDIT-0620 and alarm (S)H				
	3) Plugging in lines	3.1) Same as 1.1)	C2.2) Maintain bag with bag cleaning system (N2 pulse)				
No/Less Flow (baghouse to fines weigh hopper)	1) Plugging	1.1) Build-up of fines baghouse		Review design of recycle of fines and/or disposal	Design to reflect disposal of baghouse fines. Rotary valve located at top by baghouse. Discharge routed to grade for collection. No recycle. (3/15/95)	I B	
	2) Too low pressure in baghouse	1.2) High dP at PDIT-0620					

Session: 1 02-13-95  
 Node: 47 Baghouse system  
 Parameter: Composition

Revision: 0 02-16-95 Dwg#: 9417-1006-C

Intention: Discharge particle free air

DEVIATION	CAUSES	CONSEQUENCES	SAFEGUARDS	RECOMMENDATIONS	REMARKS	BY	COMMENTS
More Composition	1) Bag failure	1.1) Dust release to stack	1.1) low dP at PDIT-0620 1.2) Visual insp and maintenance procedures 1.3) Visual plume out of stack				

HAZOP-PC 2.12  
 Company: IGT  
 Facility: Roberts & Schafer  
 Session: 1 02-13-95  
 Node: 47 Baghouse system  
 Parameter: Safety

Worksheet

Primatech Inc.  
 Node: 47  
 Page: 2

Revision: 0 02-16-95 Dwg#: 9417-1006-C

Intention: Provide adequate safety

DEVIATION	CAUSES	CONSEQUENCES	SAFEGUARDS	RECOMMENDATIONS	REMARKS	BY	COMMENTS
Less Safety	1) explosion in baghouse	1.1) Damage to equipment	C1.1) Overpressure panel is supplied. (Note: NOT Explosion panel)	Review need for additional protection	Reimelt to provide explosion panel (3/15/95)	R	

Company: IGT  
 Facility: Roberts & Schafer  
 Session: 1 02-13-95  
 Node: 48 Coarse Char Surge Vessel C-703  
 Parameter: Pressure  
 Revision: 0 02-17-95 Dwg#: 9417-1006-C  
 Intention: Maintain pressure at 35 psia (nominal)

DEVIATION	CAUSES	CONSEQUENCES	SAFEGUARDS	RECOMMENDATIONS	REMARKS	BY	COMMENTS
Higher Pressure	1) block valve leak or left open		C1.1) N2 system has pressure regulation C1.2) Rupture disc protection				
Lower Pressure	1) leaks	1.1) Hot gas thru screw cooler  1.2) Local operator hazard  1.3) Environmental release 1.4) High temperature into vessel	C1.1) PIT-15** C1.2) TE-0740 C1.3) TE-0728 (S)H and HH alarms C1.4.1) Cooling by screw cooler	Provide software comparison of bed free-board pressure PIT-0701 and PIT-15** and possible alarm  Revise P&ID to move TE-0728 to char inlet line upstream of N2  Review TE-0740 (S)HH shutdown of screw	     Will add FS in cooling water return to ensure flow. FSL will stop masterial feed. (3/15/95)	I B RS  RS  I B RS	

Session: 1 02-13-95  
 Node: 48 Coarse Char Surge Vessel C-703  
 Parameter: Level  
 Revision: 0 02-17-95 Dwg#: 9417-1006-C  
 Intention: Retain up to 25 cuft gross of coarse char

DEVIATION	CAUSES	CONSEQUENCES	SAFEGUARDS	RECOMMENDATIONS	REMARKS	BY	OMMENTS
Higher Level	1) Failure to discharge any cause	1.1) Overfill vessel and backfill fill line	C1.1) LT-**	Revise logic to reflect alarm (S)HH trips screw  Review addition of back-up LS stop thru PLC	  Not a safety issue. Not required. Sufficient additional	RS  R	

Company: IGT

Node: 48

Facility: Roberts & Schafer

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Session: 1 02-13-95

Revision: 0 02-17-95 Dwg#: 9417-1006-C

Node: 48 Coarse Char Surge Vessel C-703

Parameter: Level

Intention: Retain up to 25 cuft gross of coarse char

DEVIATION	CAUSES	CONSEQUENCES	SAFEGUARDS	RECOMMENDATIONS	REMARKS	BY	COMMENTS
		1.2) Possibly jam char cooling screw			information available to assess plant condition. (3/15/95)		

Session: 1 02-13-95

Revision: 0 02-17-95 Dwg#: 9417-1006-C

Node: 48 Coarse Char Surge Vessel C-703

Parameter: Sampling

Intention: Potential sample point

DEVIATION	CAUSES	CONSEQUENCES	SAFEGUARDS	RECOMMENDATIONS	REMARKS	BY	COMMENTS
No Sampling	1) Sample point flanged off			When piping defined, review if sampling at this point is appropriate		I RS	

DEVIATION	CAUSES	CONSEQUENCES	SAFEGUARDS	RECOMMENDATIONS	REMARKS	BY	COMMENTS
No Flow (when required to flow)	1) Valve fails to open	1.1) Same as node 48 - high level 1.2) System shutdown operator initiated	C.1.1) Valve position ind. and cycle interrupt C.1.2) Level in surge vessel does not decrease C1.3) Level in blowcase does not increase C1.4) No or less weight increase at blowcase C1.5) Same as node 48 high level				
	2) Instrument loop fails	2.1) Same as 1.*)					
	3) Plugging	3.1) Same as 1.*)					
More Flow	1) Valve leaks or doesn't close	1.1) Same as node 48 low pressure 1.2) Unwanted overflow of blowcase	c1.1.1) Same as node 48 low pressure c1.2.1) High level blowcase WIT-15** c1.2.2) High level blowcase LIT-15** C.1.1) Valve position ind. and cycle interrupt				

Company: IGT  
Facility: Roberts & Schafer  
Session: 1 02-13-95  
Node: 50 Coarse Char Blowcase C-704  
Parameter: Pressure  
Revision: 0 02-17-95 Dwg#: 9417-1006-C  
Intention: Maintain between atmos. and 35 psia

DEVIATION	CAUSES	CONSEQUENCES	SAFEGUARDS	RECOMMENDATIONS	REMARKS	BY	COMMENTS
Lower Pressure (below equalized pressure)	1) No equalization line	1.1) Poor operation		Revise design to reflect equalization line	Reimelt will revise PFD design to reflect equalization line and elimination of secondary conveyance line (3/15/95)	R	
Lower Pressure (when repressurizing)	1) Leakage 2) N2 system failure 3) Control loop failure	1.1) Can't return to service	c1.1.1) PIT-15**	Review PLC program permissives for PIT-15** and alarming	Within Reimelt existing scope	R	
Higher Pressure	1) Overpressure by N2	1.1) Pressure surge back to retort	C1.1) N2 overpressurization protection				

Session: 1 02-13-95  
Node: 50 Coarse Char Blowcase C-704  
Parameter: Level  
Revision: 0 02-17-95 Dwg#: 9417-1006-C  
Intention: Contain coarse char up to a volume 19 cuft gross

DEVIATION	CAUSES	CONSEQUENCES	SAFEGUARDS	RECOMMENDATIONS	REMARKS	BY	COMMENTS
Higher Level	1) Failure to discharge any cause	1.1) Overfill vessel and backfill fill line and surge vessel	C1.1) LT-15** C1.2) WIT-15** c1.1.1) Operator training and procedures	Revise logic to reflect alarm (S)HH		RS	



DEVIATION	CAUSES	CONSEQUENCES	SAFEGUARDS	RECOMMENDATIONS	REMARKS	BY	COMMENTS
No Flow	1) Discharge valve fails to open  2) Plugging  3) N2 supply valves failure	1.1) Product not conveyed  2.1) Same as 1.1)  2.1) Same as 1.1)	c.1.1) Rate of discharge by weight PLC calc and alarm  c1.2) Valve ind.  c2.1.1) Same as c.1.1)  c.3.1.1) Same as c.1.1)  c.3.1.2) PIT-15**				
More Flow (in the isolation mode)	1) Valve leakage or failure	1.1) Inability to pressurize the blowcase		Investigate design to increase reliability (eg. double valving)        Investigate price of utilizing air for conveyence, followed by N2 purge of vessel	Revise design to reflect Macawber valve and a butterfly valve on blowcase discharge. Between surge vessel and blowcase utilize 1 Macawber valve (3/15/95)    Reimelt's very approx. consumption of 4000 cfh is well within the current N2 supply capacity. Project will proceed with N2 supply only, no air system. (3/15/95)	R I B      R	

Session: 1 02-13-95

Revision: 0 02-17-95 Dwg#: 9417-1006-C

Node: 51 Coarse char pneumatic conveyence to Storage Hopper D-702

Parameter: Pressure

Intention: Provide sufficient pressure to adequately convey char to storage vessel

DEVIATION	CAUSES	CONSEQUENCES	SAFEGUARDS	RECOMMENDATIONS	REMARKS	BY	COMMENTS

Company: IGT  
 Facility: Roberts & Schafer  
 Session: 1 02-13-95  
 Node: 52 Coarse char Storage Hopper D-702  
 Parameter: Pressure  
 Revision: 0 02-17-95 Dwg#: 9417-1006-C  
 Intention: Maintain vessel at near atmos

DEVIATION	CAUSES	CONSEQUENCES	SAFEGUARDS	RECOMMENDATIONS	REMARKS	BY	COMMENTS
Higher Pressure	1) During conveyence			Verify over/under pressure protection	Adequate protection already include in base design (3/15/95)	R	
Lower Pressure	1) During draining						

Session: 1 02-13-95  
 Node: 52 Coarse char Storage Hopper D-702  
 Parameter: Level  
 Revision: 0 02-17-95 Dwg#: 9417-1006-C  
 Intention: Maintain Char level acceptable

DEVIATION	CAUSES	CONSEQUENCES	SAFEGUARDS	RECOMMENDATIONS	REMARKS	BY	COMMENTS
Higher Level	1) Overfill		Cl.1) LIT-16**	Add (S)H alarm to PLC	Celtek probes will be provided RS will add to DCS logic (3/15/95)	R RS	

DEVIATION	CAUSES	CONSEQUENCES	SAFEGUARDS	RECOMMENDATIONS	REMARKS	BY	COMMENTS
No/Less Flow	1) Rotary valve failure  2) Plugging  3) Scale fails	1.1) No flow to sac  2.1) Same as 1.1) 2.2) Maintenance  3.1) Bag overflow and back-up 3.2) May damage rotary valve	c1.1.1) Visual insp. of bag fill  c1.1.2) No weight gain in fill measuring system  c.3.1.1) Visual insp. of operation				Note: rotary valve no longer VS

Session: 1 02-13-95

Revision: 0 02-17-95 Dwg#: 9417-1006-C

Node: 53 Fill line from D-702 to Supersac

Parameter: Temperature

Intention: Temperature not hazardous to operators

DEVIATION	CAUSES	CONSEQUENCES	SAFEGUARDS	RECOMMENDATIONS	REMARKS	BY	COMMENTS
Higher Temperature	1) Any cause	1.1) Personnel safety		Add thermal couple bin cone area and interlock to rotary valve	IGT will incorporate into operating procedures (3/15/95)	R I	

HAZOP-PC 2.12  
 Company: IGT  
 Facility: Roberts & Schafer  
 Session: 1 02-13-95  
 Node: 54 Char Storage Baghouse  
 Parameter: Flow

Worksheet

Primattech Inc.  
 Node: 54  
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Revision: 0 02-17-95 Dwg#: 9417-1006-C  
 Intention: Provide adequate flow to vent supported vessels and systems

DEVIATION	CAUSES	CONSEQUENCES	SAFEGUARDS	RECOMMENDATIONS	REMARKS	BY	COMMENTS
No/Less Flow (to the baghouse)	1) Blower failure	1.1) Possible settling in lines	C1.1) Low reading on bag dP	Review impact of air conveying on the thermal oxidizer Also reverse flow	No air conveying. Non-issue. (3/15/95)	I B	
		1.2) Reverse flow from Thermal oxidizer					
	2) High dP on bag	2.1) Same as 1.*)	C2.1) High dP at PDIT-16** and alarm (S)H				
	3) Plugging in lines	3.1) Same as 1.1)	C2.2) Maintain bag with bag cleaning system (N2 pulse)				
No/Less Flow (baghouse to dump bag)	1) Failure of rotary valve	1.1) Build-up of fines baghouse	cl.2.1) Alarm on high dP at PDIT-16**	Review design of disposal (assuming continuous operation when conveyence in operation)	Baghouse routed to disposal. Rotary valve located near baghouse. Collect at grade. (3/15/95)	I B R	
		1.2) High dP at PDIT-16**					

Session: 1 02-13-95 Revision: 0 02-17-95 Dwg#: 9417-1006-C  
 Node: 54 Char Storage Baghouse Intention: Maintain discharge particle free  
 Parameter: Composition

DEVIATION	CAUSES	CONSEQUENCES	SAFEGUARDS	RECOMMENDATIONS	REMARKS	BY	COMMENTS
More Composition	1) Bag failure	1.1) Dust release to thermal oxidizer	1.1) low dP at PDIT-16** 1.2) Visual insp and maintenance procedures 1.3) Caught by scrubber				

Company: IGT  
Facility: Roberts & Schafer  
Session: 1 02-13-95  
Node: 55 Char Fines Surge Vessel C-701  
Parameter: Pressure  
Revision: 0 02-17-95 Dwg#: 9417-1006-C  
Intention: Maintain pressure at 35 psia (nominal)

DEVIATION	CAUSES	CONSEQUENCES	SAFEGUARDS	RECOMMENDATIONS	REMARKS	BY	COMMENTS
Higher Pressure	1) block valve leak or left open		C1.1) N2 system has pressure regulation C1.2) Rupture disc protection				
Lower Pressure	1) leaks	1.1) Hot gas thru screw cooler  1.2) Local operator hazard  1.3) Environmental release  1.4) High temperature into vessel	C1.1) PIT-15** C1.2) TE-1003  C1.4.1) Cooling by screw cooler	Provide software comparison of bed free-board pressure PIT-0701 and PIT-15** and possible alarm  Review TE-1003 (S)HH shutdown of screw	Will add FS in cooling water return to ensure flow. FSL will stop masterial feed. (3/15/95)	I B RS  I B RS	

Session: 1 02-13-95  
Node: 55 Char Fines Surge Vessel C-701  
Parameter: Level  
Revision: 0 02-17-95 Dwg#: 9417-1006-C  
Intention: Retain up to 25 cuft gross of coarse char

DEVIATION	CAUSES	CONSEQUENCES	SAFEGUARDS	RECOMMENDATIONS	REMARKS	BY	COMMENTS
Higher Level	1) Failure to discharge any cause	1.1) Overfill vessel and backfill fill line	C1.1) LT-**	Revise logic to reflect alarm (S)HH trips screw  Review addition of back-up LS stop thru PLC		RS  R	
					Not a safety issue. Not required. Sufficient additional information available to assess plant condition. (3/15/95)		

HAZOP-PC 2.12

Worksheet

Primatech Inc.  
Node: 55  
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Company: IGT

Facility: Roberts & Schafer

Session: 1 02-13-95

Revision: 0 02-17-95 Dwg#: 9417-1006-C

Node: 55 Char Fines Surge Vessel C-701

Parameter: Level

Intention: Retain up to 25 cuft gross of coarse char

DEVIATION	CAUSES	CONSEQUENCES	SAFEGUARDS	RECOMMENDATIONS	REMARKS	BY	COMMENTS
		1.2) Possibly jam char cooling screw					

Session: 1 02-13-95

Revision: 0 02-17-95 Dwg#: 9417-1006-C

Node: 55 Char Fines Surge Vessel C-701

Parameter: Sampling

Intention: Potential sample point

DEVIATION	CAUSES	CONSEQUENCES	SAFEGUARDS	RECOMMENDATIONS	REMARKS	BY	COMMENTS
No Sampling	1) Sample point flanged off			When piping defined, review if sampling at this point is appropriate		I RS	

Company: IGT

Facility: Roberts & Schafer

Session: 1 02-13-95

Revision: 0 02-17-95 Dwg#: 9417-1006-C

Node: 56 Fill line from Char Fines Surge Vessel to Blowcase

Parameter: Flow

Intention: Transfer of char from surge vessel to blowcase

DEVIATION	CAUSES	CONSEQUENCES	SAFEGUARDS	RECOMMENDATIONS	REMARKS	BY	COMMENTS
No Flow (when required to flow)	1) Valve fails to open  2) Instrument loop fails 3) Plugging	1.1) Same as node 55 - high level  1.2) System shutdown operator initiated  2.1) Same as 1.*) 3.1) Same as 1.*)	C.1.1) Valve position ind. and cycle interrupt  C.1.2) Level in surge vessel does not decrease  C1.3) Level in blowcase does not increase  C1.4) No or less weight increase at blowcase  C1.5) Same as node 55 high level				
More Flow	1) Valve leaks or doesn't close	1.1) Same as node 48 low pressure  1.2) Unwanted overflow of blowcase	c1.1.1) Same as node 48 low pressure  c1.2.1) High level blowcase WIT-15** c1.2.2) High level blowcase LIT-15**  C.1.1) Valve position ind. and cycle interrupt				

Company: IGT  
Facility: Roberts & Schafer  
Session: 1 02-13-95  
Node: 57 Char Fines Blowcase C-702  
Parameter: Pressure  
Revision: 0 02-17-95 Dwg#: 9417-1006-C  
Intention: Maintain between atmos. and 35 psia

DEVIATION	CAUSES	CONSEQUENCES	SAFEGUARDS	RECOMMENDATIONS	REMARKS	BY	COMMENTS
Lower Pressure (below equalized pressure)	1) No equalization line	1.1) Poor operation		Revise design to reflect equalization line	Reimelt will revise PFD design to reflect equalization line and elimination of secondary conveyance line (3/15/95)	R	
Lower Pressure (when repressurizing)	1) Leakage 2) N2 system failure 3) Control loop failure	1.1) Can't return to service	c1.1.1) PIT-15**	Review PLC program permissives for PIT-15** and alarming	Within Reimelt existing scope	R	
Higher Pressure	1) Overpressure by N2	1.1) Pressure surge back to retort	C1.1) N2 overpressurization protection				

Session: 1 02-13-95  
Parameter: Level  
Revision: 0 02-17-95 Dwg#: 9417-1006-C e: 57 Char Fines Blowcase C-702  
Intention: Contain coarse char up to a volume 19 cuft gross

DEVIATION	CAUSES	CONSEQUENCES	SAFEGUARDS	RECOMMENDATIONS	REMARKS	BY	COMMENTS
Higher Level	1) Failure to discharge any cause	1.1) Overfill vessel and backfill fill line and surge vessel	C1.1) LT-15** C1.2) WIT-15** c1.1.1) Operator training and procedures	Revise logic to reflect alarm (S)HH		RS	



Company: IGT  
Facility: Roberts & Schafer  
Session: 1 02-13-95  
Node: 58 Char Fines pneumatic conveyence to Storage Hopper D-701  
Parameter: Flow

Revision: 0 02-17-95 Dwg#: 9417-1006-C  
Intention: Convey char to storage vessel

DEVIATION	CAUSES	CONSEQUENCES	SAFEGUARDS	RECOMMENDATIONS	REMARKS	BY	COMMENTS
No Flow	1) Discharge valve fails to open  2) Plugging  3) N2 supply valves failure	1.1) Product not conveyed  2.1) Same as 1.1)  2.1) Same as 1.1)	c.1.1) Rate of discharge by weight PLC calc and alarm  c1.2) Valve ind.  c2.1.1) Same as c.1.1)  c.3.1.1) Same as c.1.1)  c.3.1.2) PIT-15**				
More Flow (in the isolation mode)	1) Valve leakage or failure	1.1) Inability to pressurize the blowcase		Investigate design to increase reliability (eg. double valving)  Investigate price of utilizing air for conveyence, followed by N2 purge of vessel	Revise design to reflect Macawber valve and a butterfly valve on blowcase discharge. Between surge vessel and blowcase utilize 1 Macawber valve (3/15/95)  Reimelt's very approx. consumption of 4000 cfh is well within the current N2 supply capacity. Project will proceed with N2 supply only, no air system. (3/15/95)	R I B	

Session: 1 02-13-95  
Node: 58 Char Fines pneumatic conveyence to Storage Hopper D-701  
Parameter: Pressure

Revision: 0 02-17-95 Dwg#: 9417-1006-C  
Intention: Provide sufficient pressure to adequately convey char to storage vessel

DEVIATION	CAUSES	CONSEQUENCES	SAFEGUARDS	RECOMMENDATIONS	REMARKS	BY	COMMENTS

HAZOP-PC 2.12

Worksheet

Primatch Inc.

Company: IGT

Node: 59

Facility: Roberts & Schafer

Page: 1

Session: 1 02-13-95

Revision: 0 02-17-95 Dwg#: 9417-1006-C

Node: 59 Char Fines Storage Hopper D-701

Parameter: Pressure

Intention: Maintain vessel at near atmos

DEVIATION	CAUSES	CONSEQUENCES	SAFEGUARDS	RECOMMENDATIONS	REMARKS	BY	COMMENTS
Higher Pressure	1) During conveyence			Verify over/under pressure protection	Adequate protection already include in base design (3/15/95)	R	
Lower Pressure	1) During draining						

Session: 1 02-13-95

Revision: 0 02-17-95 Dwg#: 9417-1006-C

Node: 59 Char Fines Storage Hopper D-701

Parameter: Level

Intention: Maintain Char level acceptable

DEVIATION	CAUSES	CONSEQUENCES	SAFEGUARDS	RECOMMENDATIONS	REMARKS	BY	COMMENTS
Higher Level	1) Overfill		C1.1) LIT-16**	Add (S)H alarm to PLC	Celtek probes will be provided RS will add to DCS logic (3/15/95)	R RS	

DEVIATION	CAUSES	CONSEQUENCES	SAFEGUARDS	RECOMMENDATIONS	REMARKS	BY	COMMENTS
No/Less Flow	1) Rotary valve failure  2) Plugging  3) Scale falls	1.1) No flow to sac  2.1) Same as 1.1) 2.2) Maintenance  3.1) Bag overfill and back-up 3.2) May damage rotary valve	c1.1.1) Visual insp. of bag fill  c1.1.2) No weight gain in fill measuring system  c.3.1.1) Visual insp. of operation				Note: rotary valve no longer VS

Session: 1 02-13-95

Revision: 0 02-17-95 Dwg#: 9417-1006-C

Node: 60 Fill line from D-701 to Supersac

Parameter: Temperature

Intention: Temperature not hazardous to operators

DEVIATION	CAUSES	CONSEQUENCES	SAFEGUARDS	RECOMMENDATIONS	REMARKS	BY	COMMENTS
Higher Temperature	1) Any cause	1.1) Personnel safety		Add thermal couple bin cone area and interlock to rotary valve	IGT will incorporate into operating procedures (3/15/95)	R	

HAZOP-PC 2.12  
 Company: IGT  
 Facility: Roberts & Schafer  
 Session: 1 02-13-95  
 Node: 61 Weigh Hopper for Coal Fines and attached tote bag unloader  
 Parameter: Composition

Worksheet

Primatech Inc.  
 Node: 61  
 Page: 1

Revision: 0 02-16-95 Dwg#: 9417-1006-C  
 Intention: Moisture control

DEVIATION	CAUSES	CONSEQUENCES	SAFEGUARDS	RECOMMENDATIONS	REMARKS	BY	COMMENTS
Other Than Composition	1) Weather induced moisture	1.1) Difficult operation and freeze-up		Review need for weather protection	Provide roof and field installation of side wall tarp	I B	

Session: 1 02-13-95 Revision: 0 02-16-95 Dwg#: 9417-1006-C  
 Node: 61 Weigh Hopper for Coal Fines and attached tote bag unloader  
 Parameter: Level Intention: Hold and measure coarse coal load

DEVIATION	CAUSES	CONSEQUENCES	SAFEGUARDS	RECOMMENDATIONS	REMARKS	BY	COMMENTS
Higher Level	1) Overfill operator error  2) Failure to flow out due to sticking	1.1) Overfill  1.2) Cleanout and maintain  2.1) Same as above	Cl.1) WT-0622	Review and recommend how and where to determine weight of coal for a given run  Operating and maintenance procedures will include inspection of the cone lining	Coal feed will be determined by the decrease in weight in the weigh hopper and correlated by the feed screw rate. Additional isolation valves eliminate simultaneous fill and feed concerns. Interlock isolation valve to high weight in weigh hopper. Revise level loop to high level switch only, not continuous readout. (3/15/95)  Delete liner tensioner and liner impaler from Reimelt scope (3/15/95)	I B          I	

Company: IGT  
Facility: Roberts & Schafer  
Session: 1 02-13-95  
Node: 62 Fill line from Weigh Hopper to Lockhopper (fines)  
Parameter: Flow

Revision: 0 02-16-95 Dwg#: 9417-1006-C

Intention: Flow control and isolation of transfer from weigh hopper to lock hopper

DEVIATION	CAUSES	CONSEQUENCES	SAFEGUARDS	RECOMMENDATIONS	REMARKS	BY	COMMENTS
Reverse Flow	1) Poor seal of block valve	1.1) Not able to equalize pressure  1.2) Not able to feed coal		Investigate design change to knife gate or other alternative isolation valve	Design to reflect use of 8" Macawber dome valves for coarse inlet and 6" for fine and all other coarse for isolation. (Valve supply no longer part of Reimelt scope) (3/15/95)	ALL	Cost info and stack height are to be considered  Note: Reimelt system is completely automated, P&ID will reflect this
	2) Instrument loop failure	2.1) Same as 1.*  2.2) Seal Valve could jam and fail	C2.1) Weight and level in weigh hopper does not decrease  C2.2) Valve position ind.	Reimelt will review and revise PLC program to include a trouble alarm on weight change rate	PLC program will be revised (3/15/95)	R	
No Flow (when required to flow)	1) Valve fails to open	1.1) No flow to lock hopper 1.2) No flow from the Weigh hopper	C.1.1) Valve position ind. C.1.2) Weight and level in weigh hopper does not decrease				
	2) Instrument loop fails	2.1) Same as 1.*)					
	3) Plugging	3.1) Same as 1.*)					

HAZOP-PC 2.12  
 Company: IGT  
 Facility: Roberts & Schafer  
 Session: 1 02-13-95  
 Node: 63 Coal Fines Lockhopper  
 Parameter: Pressure

Worksheet

Primatech Inc.  
 Node: 63  
 Page: 1

Revision: 0 02-16-95 Dwg#: 9417-1006-C  
 Intention: Operate between atmos. and 40 psia

DEVIATION	CAUSES	CONSEQUENCES	SAFEGUARDS	RECOMMENDATIONS	REMARKS	BY	COMMENTS
Higher Pressure	1) Failure of instrument loop	1.1) Overpressurization of vessel	C1.1.1) Rupture disc	Investigate pressure rating and pressure relieving on the N2 feed to Feed System	A downstream line PSV set at 50 psi will be supplied by Reimelt. (3/15/95)	B I	
		1.2) Rupture first disc	C1.2.1) Peaking PI-0627				
Less Pressure	1) Instrument failure	1.1) Reverse flow		Investigate and recommend the addition of redundant pressure loops or other alternative	Severity of failure and probability of failure low, no immediate action required. Note: Spare nozzles are provided on the vessels to accommodate later modifications. (3/15/95)	R	PDI alternative to br considered
		1.2) System upset					
	2) N2 failure	2.1) Can't pressurize	C2.1.1) Delta Pressure control				
		2.2) Can't operate	C.2.1.2) PI-0628A				
	3) Leak or gasket failure	3.1) Same as 2.*)	C.3.1.1) Maintenance procedures				

Session: 1 02-13-95  
 Node: 63 Coal Fines Lockhopper  
 Parameter: Level

Revision: 0 02-16-95 Dwg#: 9417-1006-C  
 Intention: To hold coarse coal (25 cuft gross)

DEVIATION	CAUSES	CONSEQUENCES	SAFEGUARDS	RECOMMENDATIONS	REMARKS	BY	COMMENTS
Higher Level	1) Instrument loop failure	1.1) Overfill	C1.1) Manual inspection of weigh change C1.2.1) See node 62	Review weigh change vs. time alarm and possible cut-off	Improved reliability by using Celtek probe. No safety issue. Sufficient information is provided with	I B R RS	

HAZOP-PC 2.12  
 Company: IGT  
 Facility: Roberts & Schafer  
 Session: 1 02-13-95  
 Node: 63 Coal Fines Lockhopper  
 Parameter: Level

Worksheet

Revision: 0 02-16-95 Dwg#: 9417-1006-C  
 Intention: To hold coarse coal (25 cuft gross)

Primatech Inc.  
 Node: 63  
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DEVIATION	CAUSES	CONSEQUENCES	SAFEGUARDS	RECOMMENDATIONS	REMARKS	BY	COMMENTS
		1.2) Plugging of feed line			the existing instrumentation. DCS will be used to generate alarm (3/15/95)		

DEVIATION	CAUSES	CONSEQUENCES	SAFEGUARDS	RECOMMENDATIONS	REMARKS	BY	COMMENTS
Reverse Flow	1) Poor seal of block valve	1.1) Heat-up of feed line, material and release of gas from coal	C1.1) Valve position indication and interlocks to PLC controls	Investigate design change to knife gate or other alternative isolation valve	Design to reflect use of 8" Macawber dome valves for coarse inlet and 6" for fine and all other coarse for isolation. (Valve supply no longer part of Reimelt scope) (3/15/95)	ALL	Cost info and stack height are to be considered  Note: Reimelt system is completely automated, P&ID will reflect this
		1.2) Inability to feed coal 1.3) System upset 1.4) Potential baghouse damage					
	2) Instrument loop failure	2.1) No consequence	C2.1) Lock hopper at same pressure	Reimelt will review and revise PLC program to include a trouble alarm on weight change rate	PLC program will be revised (3/15/95)	R	
No Flow (when required to flow)	1) Valve fails to open	1.1) No flow to feed hopper	C.1.1) Valve position ind.				
		1.2) No flow from the lock hopper	C.1.2) Level in lock hopper does not decrease				
		1.3) System shutdown operator initiated	C1.3) Level in feed hopper does not increase				
	2) Instrument loop fails	2.1) Same as 1.*)					
	3) Plugging	3.1) Same as 1.*)					



HAZOP-PC 2.12  
 Company: IGT  
 Facility: Roberts & Schafer  
 Session: 1 02-13-95  
 Node: 65 Coal Fines Feed Vessel  
 Parameter: Pressure

Worksheet

Revision: 0 02-16-95 Dwg#: 9417-1006-C  
 Intention: Maintain pressure at 35-40 psia

Primatech Inc.  
 Node: 65  
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DEVIATION	CAUSES	CONSEQUENCES	SAFEGUARDS	RECOMMENDATIONS	REMARKS	BY	COMMENTS
Higher Pressure	1) Failure of instrument loop	1.1) Overpressurization of vessel  1.2) Rupture first disc	C1.1.1) Rupture disc C1.2.1) Peaking PI-0633	Investigate pressure rating and pressure relieving on the N2 feed to Feed System	Add in N2 header downstream PSV set at 50 psi. PSV now in Reimelt scope (same valve as in node 40 (3/15/95)	B I	
	2) Gasifier upset	1.1) Back pressure to feed hopper  1.2) Hot gases back-up line  1.3) Eventual plugging. Cleaning required.	C.2.1) Same as C1.*) C.2.2) Gasifier pressure indication	Review need for continuous bleed flow N2 to the feed hopper	Add a manual adjust rotometer and remove PV-08B (3/15/95)	I B R	
Less Pressure	1) Instrument failure	1.1) Reverse flow  1.2) System upset		Include in the review of the lock hopper pressure protection issue the need to protect the feed hopper	Severity of failure and probability of failure low, no immediate action required. Note: Spare nozzles are provided on the vessels to accommodate later modifications. (3/15/95)	R	
	2) N2 failure	2.1) Can't pressurize 2.2) Can't operate 2.3) Unit upset	C.2.1.1) PI-0628B C.2.1.2) Gasifier instrumentation				
	3) Leak or	3.1) Same as 2.*)	C.3.1.1) Maintenance				

HAZOP-PC 2.12  
 Company: IGT  
 Facility: Roberts & Schafer  
 Session: 1 02-13-95  
 Node: 65 Coal Fines Feed Vessel  
 Parameter: Pressure

Worksheet

Primatech Inc.  
 Node: 65  
 Page: 2

Revision: 0 02-16-95 Dwg#: 9417-1006-C

Intention: Maintain pressure at 35-40 psia

DEVIATION	CAUSES	CONSEQUENCES	SAFEGUARDS	RECOMMENDATIONS	REMARKS	BY	COMMENTS
	gasket failure 4) Rupture leak or failure		procedures C4.1) Double disc protection				

Session: 1 02-13-95  
 Node: 65 Coal Fines Feed Vessel  
 Parameter: Level

Revision: 0 02-16-95 Dwg#: 9417-1006-C

Intention: To hold 45 cuft gross

DEVIATION	CAUSES	CONSEQUENCES	SAFEGUARDS	RECOMMENDATIONS	REMARKS	BY	COMMENTS
Higher Level	1) Instrument loop failure  2) Plugging	1.1) Overfill 1.2) Plugging of feed line 1.3) Valve may not close and thus indicate so.	C1.1) Manual inspection of level change at lock hopper  C2.1) LI-0630 and the PLC program control				
No/Lower Level	1) Instrument loop failure	1.1) Empty hopper 1.2) No feed to screws 1.3) System interruption	c1.1.1) TE-0635 may decrease c1.1.2) Gasifier temp increase at TE-0710/27 c1.1.3) Hot oil retron temp will rise				

HAZOP-PC 2.12  
 Company: IGT  
 Facility: Roberts & Schafer  
 Session: 2 03-14-95  
 Node: 66 Flare  
 Parameter: Flow

Worksheet

Primatech Inc.  
 Node: 66  
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Revision: 0 03-14-95 Dwg#: 9417-1006-C

Intention: Provide adequate flow for the various relief conditions

DEVIATION	CAUSES	CONSEQUENCES	SAFEGUARDS	RECOMMENDATIONS	REMARKS	BY	COMMENTS
No/Less Flow (main flow)	1) Plugging	1.1) Back-up of relief header	C1.1) Knock-out drum protects discharge line				
	2) Valve fails closed	1.2) Same as 1.1	C1.2) Same as C1.1)				
(pilot gas)	1) Any cause	1.1) Loss of pilot 1.2) Non-ignited atmospheric release	C1.1.1) Low temp alarms TSL445 and 444				
More Flow	1) Any cause			Flare loads will be confirmed as part of the relief study		B	
Reverse Flow	1) Back flow from atmospheric conditions	1.1) Oxygen in relief system	C1.1) Check valve in line	Callidus to provide recommendation on flare design and replacement of check valve with molecule seal		C	

Session: 2 03-14-95  
 Node: 66 Flare  
 Parameter: Temperature

Revision: 0 03-14-95 Dwg#: 9417-1006-C

Intention: Dual pilots always on

DEVIATION	CAUSES	CONSEQUENCES	SAFEGUARDS	RECOMMENDATIONS	REMARKS	BY	COMMENTS
Lower Temperature	1) Loss of either pilot (any cause)	1.1) None	C1.1) Dual pilots C1.2) Thermal couple on each pilot TE444A and 445 A.	Callidus will revise PLC to try to re-ignite pilot and alarm if unsuccessful		C	
	2) Loss of both pilots	2.1) Loss of flare combustion	C2.1) Low temp alarms TSL-444 and 445 C2.2) Cut-off gas to pilots				

HAZOP-PC 2.12  
 Company: IGT  
 Facility: Roberts & Schafer  
 Session: 2 03-14-95  
 Node: 66 Flare  
 Parameter: Composition

Worksheet

Revision: 0 03-14-95 Dwg#: 9417-1006-C

Primatech Inc.  
 Node: 66  
 Page: 2

Intention: Typical flare flow is combustible

DEVIATION	CAUSES	CONSEQUENCES	SAFEGUARDS	RECOMMENDATIONS	REMARKS	BY	COMMENTS
Other Than Composition	1) Pure N2 release  2) H2S and N2  3) Hot Syntherm vapors	1.1) None  2.1) Release to atmosphere  3.1) Release to atmosphere	C2.1) Intermittant and unlikely. Release is elevated.  c3.1.1) Non-toxic  c3.1.2) K.O. pot protects against large liquid releases	MSDS required		B	

Company: IGT  
 Facility: Roberts & Schafer  
 Session: 2 03-14-95  
 Node: 67 Bypass around T.O to K.O. pot  
 Parameter: Flow  
 Revision: 0 03-14-95 Dwg#: 9417-1006-C  
 Intention: Flow to flare in the bypass mode

DEVIATION	CAUSES	CONSEQUENCES	SAFEGUARDS	RECOMMENDATIONS	REMARKS	BY	COMMENTS
More Flow (not bypass mode)	1) FV-135 fails open	1.1) Flared release  1.2) Reduced load on the T.O.	c1.1) Limit switch on valve is monitored by the PLC	DCS will pick-up information and display as appropriate		RS	
No/Less Flow (bypass mode)	1) FV-135 fails in closed position when FV- 136 closes	1.1) Back-up vent system	c1.1.1) Relieve via rupture discs  c1.1.2) Release to flare	Review re-routing bypass to scrubber instead of flare  Review routing of char baghouse vent to T.O.  Review capacity of T.O. for the max flow condition		B I  B I  C	



Company: IGT  
Facility: Roberts & Schafer  
Session: 2 03-14-95  
Node: 69 Tar Separator to middle oil separator (see node 21)  
Parameter: Flow

Revision: 0 03-16-95 Dwg#: 9417-1006-C

Intention: Provide flow path from Tar Separator to Middle Oil Separator

DEVIATION	CAUSES	CONSEQUENCES	SAFEGUARDS	RECOMMENDATIONS	REMARKS	BY	COMMENTS
No/Less Flow	1) Manual valve left closed  2) XV-01A valve open  3) Plugging in air cooler  4) Flush valves left open  5) Air cooler tube leak or rupture	1.1) Unit upset  1.2) Pressure in retort increases  2.1) Release to flare  2.2) Pressure in system decreases  2.3) Unit upset  3.1) Same as 1.*)  4.1) Release to environment  5.1) Release to environment  5.2) Potential fire	c1.2.1) PIT-1109 reads high  c1.2.2) PIT-1109 PAH and (HH) alarms  c1.2.3) Low pressure at PIT-1208  c1.2.4) Low pressure alarm at PAL and (LL)  c2.1.1) Low pressure at PIT-1208, PIT-1202 and PIT-1109  c2.1.2) Low pressure alarms PAL and (LL) -1109 -1202 and -1208  c3.1.1) Same as c1.*.)  c4.1.1) Operator training and procedures  c4.1.2) Odor detection  c5.1.1) Located outside of primary structure  c5.1.2) Possible odor detection  c5.1.3) PIT-1208 reads lower than normal  c5.1.4) Relatively low heating value.	Add blind flange to flush connections		RS	

Company: IGT  
 Facility: Roberts & Schafer  
 Session: 2 03-14-95  
 Node: 69 Tar Separator to middle oil separator (see node 21)  
 Parameter: Temperature  
 Revision: 0 03-16-95 Dwg#: 9417-1006-C  
 Intention: Cool gas down to 170F

DEVIATION	CAUSES	CONSEQUENCES	SAFEGUARDS	RECOMMENDATIONS	REMARKS	BY	COMMENTS
Higher Temperature	1) Fan failure	1.1) Discharge temperature rises 1.2) Less condensation of middle oil 1.3) Middle oil carry-over to light oil	c1.1.1) TAH-1206 (H) and (HH) alarms on the cooler skid c1.1.2) Local run lights				
	2) Tube fouling	2.1) Discharge temperature above normal 2.2) Higher upstream pressure (gradual) 2.3) Less condensation of middle oil 2.4) Middle oil carry-over to light oil	c2.1.1) Same as c1.1.1) c2.1.2) Flush connections are provided	Add additional downstream TE (TIT-1216) off of cooler skid		RS	
	3) Damper failure	3.1) Similar to 1.*)	c3.1.1) Same as c1.1.1)				
	4) Instrument loop	4.1) Similar to 1.*)	c4.1.1) Same as c1.1.1)				
Lower Temperature	1) Loop calibration error	1.1) No significant consequences					
	2) Louver failure						



HAZOP-PC 2.12  
 Company: IGT  
 Facility: Roberts & Schafer  
 Session: 2 03-14-95  
 Node: 70 Middle oil separator  
 Parameter: Temperature

Worksheet

Primatech Inc.  
 Node: 70  
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Revision: 0 03-16-95 Dwg#: 9417-1006-C  
 Intention: Maintain temperature above 40F

DEVIATION	CAUSES	CONSEQUENCES	SAFEGUARDS	RECOMMENDATIONS	REMARKS	BY	COMMENTS
Lower Temperature	1) Failure of heat trace	1.1) No significant consequence, only affects start-up freeze protection					

Session: 2 03-14-95  
 Node: 70 Middle oil separator  
 Parameter: Pressure

Revision: 0 03-16-95 Dwg#: 9417-1006-C  
 Intention: Maintain the pressure in the vessel between 23 and 27 psia

DEVIATION	CAUSES	CONSEQUENCES	SAFEGUARDS	RECOMMENDATIONS	REMARKS	BY	COMMENTS
Higher Pressure	1) Valve doesn't open enough  2) Instrument loop calibr. error  3) ESD valve closed  4) Blocked nozzle  5) Fire	4.1) Overpressurize vessel  5.1) Overpressurize vessel	c4.1.1) PSE-1209 sized for worst case between blocked nozzle or fire  c5.1.1) Same as c4.1.1)				All issues covering pressure control other than PSE are on hold until compressor selection is completed

Session: 2 03-14-95  
 Node: 70 Middle oil separator  
 Parameter: Level

Revision: 0 03-16-95 Dwg#: 9417-1006-C  
 Intention: Maintain liquid level between 12" and 24"

DEVIATION	CAUSES	CONSEQUENCES	SAFEGUARDS	RECOMMENDATIONS	REMARKS	BY	COMMENTS
No/Less Level	1) Level transmitter failure	1.1) Pump runs dry  1.2) Pump gas to run tank	c1.1.1) LG-1210  c1.1.2) Loop failure alarm	Add back-up low level switch on C-302 pump cut-off and alarm (LSH-1217)		RS	

HAZOP-PC 2.12  
 Company: IGT  
 Facility: Roberts & Schafer  
 Session: 2 03-14-95  
 Node: 70 Middle oil separator  
 Parameter: Level

Worksheet

Revision: 0 03-16-95 Dwg#: 9417-1006-C  
 Intention: Maintain liquid level between 12" and 24"

Primatech Inc.  
 Node: 70  
 Page: 2

DEVIATION	CAUSES	CONSEQUENCES	SAFEGUARDS	RECOMMENDATIONS	REMARKS	BY	COMMENTS
Higher Level	2) Loop calibration error	2.1) Pump runs dry 1.2) Pump gas to run tank	c2.1.1) LG-1210				
	3) Root valve left open		c3.1.1) Double protection via valve and cap				
	1) Nozzle plugged	1.1) No flow of middle oil to run tank 1.2) Overfill separator and may damage compressor	c1.1.1) High level at LIT-1211 and alarm H(S) c1.1.2) No or low full at FIT-1407 and alarm S(L) c1.1.3) LG-1210 c1.1.4) High level alarm and compressor trip LSH-1214 S(H) and S(HH)				
	2) Loop calibration error	2.1) Same as 1.*)	c2.1.1) No or low full at FIT-1407 and alarm S(L) c2.1.2) LG-1210 c2.1.3) High level alarm and compressor trip LSH-1214 S(H) and S(HH)				

Company: IGT  
Facility: Roberts & Schafer  
Session: 2 03-14-95  
Node: 71 Middle oil separator to  
Parameter: Flow

Revision: 0 03-16-95 Dwg#: 9417-1006-C  
Intention: Flow path from separator to run tank

DEVIATION	CAUSES	CONSEQUENCES	SAFEGUARDS	RECOMMENDATIONS	REMARKS	BY	COMMENTS
No/Less Flow	1) Manual valve closed	1.1) Same as Node 70 Level High	c1.1.1) Same as Node 70 Level High c1.1.2) Low pressure at PI-1212				
	2) Pump failure	2.1) Same as 1.1	c2.1.1) Same as c1.1.1) c2.1.2) Pump motor status UA-1213				
	3) Control valve failure	3.1) Same as 1.1)	c3.1.1) Same as c1.1.1) c3.1.2) High pressure at PI-1212	Delete LV/LY-1211 and revise logic to pump control		RS	
Other Than Flow	4) Plugging	4.1) Same as 1.1)	c4.1.1) Same as c1.1.1)	Develop operating scenarios		I	

Session: 2 03-14-95  
Node: 71 Middle oil separator to  
Parameter: Pressure

Revision: 0 03-16-95 Dwg#: 9417-1006-C  
Intention: Maintain pressure below design pressure for associated piping and equipment

DEVIATION	CAUSES	CONSEQUENCES	SAFEGUARDS	RECOMMENDATIONS	REMARKS	BY	COMMENTS
Higher Pressure	1) Dead head pump	1.1) Overpressurize system	C1.1) Internal relief on pump				

HAZOP-FC 2.12  
 Company: IGT  
 Facility: Roberts & Schafer  
 Session: 2 03-14-95  
 Node: 72 Run tank  
 Parameter: Temperature

Worksheet

Primatech Inc.  
 Node: 72  
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Revision: 0 03-17-95 Dwg#: 9417-1006-C

Intention: Maintain temperature above 40F

DEVIATION	CAUSES	CONSEQUENCES	SAFEGUARDS	RECOMMENDATIONS	REMARKS	BY	COMMENTS
Lower Temperature	1) Failure of heat trace	1.1) Set-up of fluid	c1.1.1) TIT-1412 low temp alarms (S)L and (S)LL				

Session: 2 03-14-95  
 Node: 72 Run tank  
 Parameter: Pressure

Revision: 0 03-17-95 Dwg#: 9417-1006-C

Intention: Maintain the pressure between 0 and 1-2 psi

DEVIATION	CAUSES	CONSEQUENCES	SAFEGUARDS	RECOMMENDATIONS	REMARKS	BY	COMMENTS
Higher Pressure	1) PRV 1421 failure	1.1) Overpressurize vessel	c1.1.1) PSE 1409 set at 10 psig c1.1.2) PCV -1422 shuts off c1.1.3) PI-1410				
	2) PCV 1422 failure	2.1) Same as 1.1)	c2.1.1) PSE 1409 set at 10 psig c2.1.2) PRV -1421 opens c2.1.3) PI-1410				
Lower Pressure	1) PCV 1422 fails	1.1) Draw vacuum in vessel 1.2) Pump cavitation	c1.1.1) PI-1410 c1.1.2) Low level alarms LIT-1408 (S)L and (S)LL	Add vacuum breaker		RS	

Session: 2 03-14-95  
 Node: 72 Run tank  
 Parameter: Level

Revision: 0 03-16-95 Dwg#: 9417-1006-C

Intention: Maintain level below 80% capacity

DEVIATION	CAUSES	CONSEQUENCES	SAFEGUARDS	RECOMMENDATIONS	REMARKS	BY	COMMENTS
Higher Level	1) Plugged discharge	1.1) Increased level in the tank 1.2) Overfill tank 1.3) Relieve thru rupture disc to K.O. pot and flare	c1.1.1) Hi level alarm LIT-1408 (S)H and (S)HH c1.1.2) Operator training and procedures				
	2) Instrument loop failure	2.1) Same as 1.*)	c2.1.1) Loop failure alarm				

HAZOP-PC 2.12  
 Company: IGT  
 Facility: Roberts & Schafer  
 Session: 2 03-14-95  
 Node: 72 Run tank  
 Parameter: Level

Worksheet

Primatech Inc.  
 Node: 72  
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Revision: 0 03-16-95 Dwg#: 9417-1006-C

Intention: Maintain level below 80% capacity

DEVIATION	CAUSES	CONSEQUENCES	SAFEGUARDS	RECOMMENDATIONS	REMARKS	BY	COMMENTS
No/Less Level	3) Loop calibration error	3.1) Same as 1.*)	c2.1.2) Operator training and procedures c3.1.1) Operator training and procedures				
	1) Operator error	1.1) Pump runs dry 1.2) Blow N2 to tanker	c1.1.1) Low level alarm LIT-1408 (S)L and (S)LL c1.1.2) Operator training and procedures				
	2) Loop calibr. error	2.1) Same as 1.*)	c2.1.1) Operator training and procedures				
	3) Loop failure	3.1) Same as 1.*)	c3.1.1) Operator training and procedures c3.1.2) Loop failure alarm				

Company: IGT  
Facility: Roberts & Schafer  
Session: 2 03-14-95  
Node: 73 Middle oil separator to the light oil separator  
Parameter: Flow

Revision: 0 03-16-95 Dwg#: 9417-1006-C

Intention: Flow path for recycle gas from middle oil separator to light oil separator

Intention: Flow path for recycle gas from middle oil separator to light oil separator

DEVIATION	CAUSES	CONSEQUENCES	SAFEGUARDS	RECOMMENDATIONS	REMARKS	BY	COMMENTS
No/Less Flow	1) Manual valve closed	1.1) Dead head compressor	c1.1.1) Operator training and procedures	Review of set pressure to be performed with compressor selection and considering preheater coils		RS	
		1.2) Unit upset	c1.1.2) High pressure at PIT-1301				
		1.3) High pressure in C-302	c1.1.3) High pressure alarms at PIT-1301 (S)H and (S)HH.				
1.4) Low pressure in C-303	c1.1.4) High pressure at PIT1208						
1.5) High pressure upstream of manual valve	c1.1.5) High pressure alarms PIT-1208 (S)H and (S)HH						
1.6) No change in level in C-303	c1.1.6) PSV-1205 set ** psig design for compressor dead head flow						
1.7) Reduced temperature at cooling water side discharge							
	2) Plugging in cooler	2.1) Same as 1.*)	c2.1.1) Same as c1.1.*)				
	3) Compressor failure	3.1) Unit upset	c3.1.1) Compressor trip alarm UA-1207				
		3.2) Low pressure in C-303	c3.1.2) High pressure alarm PIT-1208 (S)H and (S)HH				
		3.3) Higher pressure in C-302	3.1.3) Low pressure alarm in PIT-1301 (S)L and (S)LL				
Other Than Flow	1) Tube failure	1.1) Water in the light oil	c1.1.1) Reduce flow indication on cooling water return line	Add flow indication and totalizing logic on sour water to T.O. line. Remove solenoid LV-		RS	

Company: IGT  
Facility: Roberts & Schafer  
Session: 2 03-14-95  
Node: 73 Middle oil separator to the light oil separator  
Parameter: Flow

Revision: 0 03-16-95 Dwg#: 9417-1006-C

Intention: Flow path for recycle gas from middle oil separator to light oil separator

DEVIATION	CAUSES	CONSEQUENCES	SAFEGUARDS	RECOMMENDATIONS	REMARKS	BY	COMMENTS
		1.2) Increase water at C-303 boot 1.3) Contaminated product at run tank		1310A (not required, already supplied on Callidus skid)  Review Callidus control logic to ensure that Callidus logic does not back-up sour water discharge		I B	

Session: 2 03-14-95

Revision: 0 03-16-95 Dwg#: 9417-1006-C

Node: 73 Middle oil separator to the light oil separator

Parameter: Temperature

Intention: Reduce temperature from 300F to 100F

DEVIATION	CAUSES	CONSEQUENCES	SAFEGUARDS	RECOMMENDATIONS	REMARKS	BY	COMMENTS
Higher Temperature	1) Loss of cooling water	1.1) High temperature in C-303 1.2) Less product 1.3) Higher load on T.O. 1.4) Higher heating valve of recycle gas 1.5) Increased potential for carbon deposition in preheater F-202 1.6) Less load on water boot	C1.1) FIT-1303 low flow c1.1.1) TIT-1306 high temp alarms (S)H and (S)HH	Add low flow alarms		RS	

DEVIATION	CAUSES	CONSEQUENCES	SAFEGUARDS	RECOMMENDATIONS	REMARKS	BY	COMMENTS
		1.7) Less load on run tank					
	2) Fouling	2.1) Same as 1.*)	c2.1.1) TIT-1306 high temp alarms (S)H and (S)HH				
Lower Temperature	1) Overcooling due to any reason	No significant consequence					



Revision: 0 03-17-95 Dwg#: 9417-1006-C

Intention: Maintain pressure below vessel 75 (??) psig

DEVIATION	CAUSES	CONSEQUENCES	SAFEGUARDS	RECOMMENDATIONS	REMARKS	BY	COMMENTS
Higher Pressure	1) Any cause	1.1) Overpressurize vessel	c1.1.1) PSV-1309 set at 75 (??) psig and design capacity for fire or blocked outlet	Review pressure protection of the light oil quench cooler (gas side)			

Revision: 0 03-16-95 Dwg#: 9417-1006-C

Intention: Maintain light oil level at between \*\*\* and \*\*\* and the water level in the boot below \*\*\*

DEVIATION	CAUSES	CONSEQUENCES	SAFEGUARDS	RECOMMENDATIONS	REMARKS	BY	COMMENTS
No/Less Level (oil)	1) Instrument loop failure	1.1) Recycle gas to the run tank  1.2) Recycle gas then flows thru the run tank to the T.O.	c1.1.1) Gear pump has minimum flow thru  c1.1) Failure of instrument loop fails to the shut-off condition	Add low level LS (same as middle oil) with pump control and remove control valve		RS	
(water)	2) Instrument loop calibr. error	2.1) Same as 1.*)	c2.1.1) Operator training and procedures				
	1) Instrument loop failure	1.1) Oil to the sour water line to the T.O.  1.2) Higher temp potential in T.O.	c1.1) Failure of instrument loop fails to the shut-off condition  c1.2.1) High temperature alarm in T.O.	Add low water level switch protection		RS	
	2) Instrument loop calibr. error		c2.1.1) Operator training and procedures				
Higher Level (oil)	1) Instrument loop failure	1.1) Carry oil over with the recycle gas to the preheater  1.2) May carbon up the preheater	c1.1.1) Production rate low  c1.1.2) Instrument failure alarm				
	2) Instrument loop calibr.	2.1) Same as 1.*)	c2.1.1) Low production rate				

HAZOP-PC 2.12  
 Company: IGT  
 Facility: Roberts & Schafer  
 Session: 2 03-14-95  
 Node: 75 Light oil separator  
 Parameter: Level

Worksheet

Primatech Inc.  
 Node: 75  
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Revision: 0 03-16-95 Dwg#: 9417-1006-C

Intention: Maintain light oil level at between \*\* and \*\* and the water level in the boot below \*\*

DEVIATION	CAUSES	CONSEQUENCES	SAFEGUARDS	RECOMMENDATIONS	REMARKS	BY	COMMENTS
(water)	error 1) Instrument loop failure  2) Instrument loop calibr. error	1.1) High water level in C-303 boot  1.2) Water into the run tank  2.1) Same as 1.*)	c1.1.1) Low production rate  c2.1.1) Low production rate				

Company: IGT  
 Facility: Roberts & Schafer  
 Session: 2 03-14-95  
 Node: 76 Light oil separator to run tank  
 Parameter: Flow  
 Revision: 0 03-16-95  
 Dwg#: 9417-1006-C  
 Intention: Flow path from separator to run tank

DEVIATION	CAUSES	CONSEQUENCES	SAFEGUARDS	RECOMMENDATIONS	REMARKS	BY	COMMENTS
No/Less Flow	1) Manual valve closed	1.1) Same as Node 75 Level High	c1.1.1) Same as Node 75 Level High c1.1.2) Low flow at FIT-1407	Delete manual valve downstream of FIT		RS	
	2) Pump failure	2.1) Same as 1.1	c2.1.1) Same as c1.1.1) c2.1.2) Pump motor status UA-1311				
	3) Control valve failure	3.1) Same as 1.1)	c3.1.1) Same as c1.1.1)	Delete LV/LY-1308 and revise logic to pump control		RS	
	4) Plugging	4.1) Same as 1.1)	c4.1.1) Same as c1.1.1)				
	5) Drain open	5.1) Release to environment	c5.1.1) Operator training and procedures c5.1.2) Double protection block valve and cap				
Reverse Flow			Check valve and positive displacement pump				

Session: 2 03-14-95  
 Node: 76 Light oil separator to run tank  
 Parameter: Pressure  
 Revision: 0 03-16-95  
 Dwg#: 9417-1006-C  
 Intention: Maintain pressure below design pressure for associated piping and equipment

DEVIATION	CAUSES	CONSEQUENCES	SAFEGUARDS	RECOMMENDATIONS	REMARKS	BY	COMMENTS
Higher Pressure	1) Dead head pump	1.1) Overpressurize system	C1.1) Internal relief on pump				

DEVIATION	CAUSES	CONSEQUENCES	SAFEGUARDS	RECOMMENDATIONS	REMARKS	BY	COMMENTS
No/Less Flow	1) Manual valve closed	1.1) Same as High level (water) in node 75	c1.1.1) Same as High level (water) in node 75				
		1.2) Low flow to T.O.	c.1.2.1) Fresh water make-up to T.O. (in Callidus design)				
	2) Plugging	2.1) Same as 1.*)	c2.1.1) Same as c1.*.*)				
Reverse Flow	3) Control valve failure	3.1) Same as 1.*)	c3.1.1) Same as c1.*.*)				
		1) Check valve failure	C1.1) C-303 operating pressure higher than T.O.				
			C1.2) High level alarm in C-303 boot LIT-1310 (S)H and (S)HH				

HAZOP-PC 2.12

Worksheet

Primatech Inc.

Company: IGT

Node: 78

Facility: Roberts & Schafer

Page: 1

Session: 2 03-14-95

Revision: 0 03-16-95

Dwg#: 9417-1006-C

Node: 78 Low pressure depressurization line

Parameter: Flow

Intention: ESD line

DEVIATION	CAUSES	CONSEQUENCES	SAFEGUARDS	RECOMMENDATIONS	REMARKS	BY	COMMENTS
More Flow	1) Valve fails open, any reason	1.1) Unit upset 1.2) Relieve to flare	C1.1) Unit shutdown as designed c1.2.1) Flare capacity designed for this event				

Company: IGT  
Facility: Roberts & Schafer  
Session: 2 03-14-95

Revision: 0 03-17-95 Dwg#: 9417-1006-C

Node: 80 Recycle gas to the T.O.  
Parameter: Flow

Intention: Provide flow path from light oil separator to T.O. during operation to bleed-off production

DEVIATION	CAUSES	CONSEQUENCES	SAFEGUARDS	RECOMMENDATIONS	REMARKS	BY	COMMENTS
No/Less Flow	1) Manual valve closed	1.1) Higher pressure in C-303	c1.1.1) PSV 1309 lifts to flare c1.1.2) PI-1307 c.1.1.3) PIT-1301 high pressure alarm (S)H	Add flow measurement and indication		RS	
	2) Control valve failure	2.1) Same as 1.1)	c2.1.1) Same as c1.1.*) c2.1.2) PIT-1305 high pressure alarm (S)H and (S)HH				
More Flow	1) Control valve fails open	1.1) Insufficient recycle gas 1.2) Bed disturbance	c1.1.1) Low flow alarm FIT-0901 (S)L				

Session: 2 03-14-95  
Parameter: Pressure

Revision: 0 03-17-95 Dwg#: 9417-1006-C e: 80 Recycle gas to the T.O.  
Intention: Control pressure in process loop

DEVIATION	CAUSES	CONSEQUENCES	SAFEGUARDS	RECOMMENDATIONS	REMARKS	BY	COMMENTS
Higher Pressure				To be reviewed as part of the overall pressure regulation/compressor control study		B I	

HAZOP-PC 2.12

Worksheet

Primatech Inc.  
Node: 81  
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Company: IGT

Facility: Roberts & Schafer

Session: 2 03-14-95

Revision: 0 03-17-95 Dwg#: 9417-1006-C

Node: 81 Recycle gas to preheater (See node 26)

Parameter: Flow

Intention: Provide flow path from light oil separator to preheater

DEVIATION	CAUSES	CONSEQUENCES	SAFEGUARDS	RECOMMENDATIONS	REMARKS	BY	COMMENTS
No/Less Flow	1) Manual or check valve closed	See node 26	See node 26				

HAZOP-FC 2.12  
 Company: IGT  
 Facility: Roberts & Schafer  
 Session: 2 03-14-95  
 Node: 82 Coarse char from retort  
 Parameter: Flow

Worksheet

Primatech Inc.  
 Node: 82  
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Revision: 0 03-17-95 Dwg#: 9417-1006-C  
 Intention: Provide flow from retort to surge vessel at approx. 900 lbs/hr

DEVIATION	CAUSES	CONSEQUENCES	SAFEGUARDS	RECOMMENDATIONS	REMARKS	BY	COMMENTS
No/Less Flow	1) Plugging	1.1) Char build-up in bed 1.2) Unit upset 1.3) Low level in surge vessel 1.4) Lower temperature in flow lines 2.1) Same as 1.*)	c1.1.1) PDI-0703/02 high alarms (S)H and (S)HH c1.1.2) TE-0728/40 high temp alarms (S)L and (S)LL c2.1.1) Same as c1.*.)				
	2) Driver failure	2.1) Same as 1.*)	c2.1.1) Driver status alarm UA-0746 c2.1.2) Same as c1.1.*.)				
More Flow	1) Miscalibration of discharge rate	1.1) Bed goes to minimum draw-off point 1.2) No significant impact	c1.1.1) PDI-0703/02 low indication				
Other Than Flow	1) Cooling water leak into char side	1.1) Steam generation 1.2) Downstream condensation 1.3) Interrupt solids product flow 1.4) Run interruption	c1.1.1) Low flow switch FSL-0752 and alarm (S)L				



DEVIATION	CAUSES	CONSEQUENCES	SAFEGUARDS	RECOMMENDATIONS	REMARKS	BY	COMMENTS
Higher Temperature	1) Insufficient cooling	1.1) Hot char at surge vessel  1.2) Personnel hazard	C1.1) Low flow on cooling water return line. Stops screw and alarms (S)H and (S)HH	Insure that over-pressurization protection on cooling water side  Add no-touch screens in appropriate locations (such as C-703)		RS  RS	

HAZOP-PC 2.12  
 Company: IGT  
 Facility: Roberts & Schafer  
 Session: 2 03-14-95  
 Node: 83 Fine char from cyclone to fine char surge vessel  
 Parameter: Flow

Worksheet

Primatech Inc.  
 Node: 83  
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Revision: 0 03-17-95 Dwg#: 9417-1006-C  
 Intention: Provide flow from cyclone to surge vessel at approx. 900 lbs/hr

DEVIATION	CAUSES	CONSEQUENCES	SAFEGUARDS	RECOMMENDATIONS	REMARKS	BY	COMMENTS
No/Less Flow	1) Plugging	1.1) Char to liquid recovery 1.2) Low level in surge vessel 1.3) Plugging in quench condenser and pump 1.4) Lower temperature in flow lines	c1.1.1) TE-1003 high temp alarm (S)L and (S)LL c1.1.2) No/less change in the fines surge vessel LIT-15** c1.1.3) Eventually lower than expected fines discharge rate WE-15**				
	2) Driver failure	2.1) Same as 1.*	c2.1.1) Driver status alarm UA-1004 c2.1.2) Same as c1.1.*				
More Flow	1) Miscalibration of discharge rate	1.1) No significant impact					
Other Than Flow	1) Cooling water leak into char side	1.1) Steam generation 1.2) Downstream condensation 1.3) Interrupt solids product flow 1.4) Run interruption	c1.1.1) Low flow switch FSL-1005 and alarm (S)L				

Session: 2 03-14-95 Revision: 0 03-17-95 Dwg#: 9417-1006-C  
 Node: 83 Fine char from cyclone to fine char surge vessel  
 Parameter: Temperature Intention: Discharge coarse char at 140F

DEVIATION	CAUSES	CONSEQUENCES	SAFEGUARDS	RECOMMENDATIONS	REMARKS	BY	COMMENTS
Higher Temperature	1) Insufficient cooling	1.1) Hot char at surge vessel	C1.1) Low flow on cooling water return line. Stops screw and alarms (S)H and (S)HH	Insure that over-pressurization protection on cooling water side		RS	

HAZOP-FC 2.12

Worksheet

Primatech Inc.

Company: IGT

Node: 83

Facility: Roberts & Schafer

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Session: 2 03-14-95

Revision: 0 03-17-95 Dwg#: 9417-1006-C

Node: 83 Fine char from cyclone to fine char surge vessel

Parameter: Temperature

Intention: Discharge coarse char at 140F

DEVIATION	CAUSES	CONSEQUENCES	SAFEGUARDS	RECOMMENDATIONS	REMARKS	BY	COMMENTS
		1.2) Personnel hazard		Add no-touch screens in appropriate locations (such as C-701)		RS	

DEVIATION	CAUSES	CONSEQUENCES	SAFEGUARDS	RECOMMENDATIONS	REMARKS	BY	COMMENTS
No/Less Flow (inlet)	1) Plugging	1.1) Unit upset 1.2) Reverse flow in return dip leg 1.3) Dip leg plugging	c1.1.1) PIT-0709 low pressure alarm (S)L and (S)LL c1.1.2) PDIT-0705 alarms low (S)L and (S)LL				
(gas outlet)	1) Plugging	1.1) Unit upset	c1.1.1) PIT-0709 low pressure alarm (S)L and (S)LL c1.1.2) PIT-0706 high pressure alarm (S)H and (S)HH				
(solids return)	1) Plugging	1.1) Increase solids carry over to secondary cyclone 1.2) Overwhelm secondary cyclone yielding carry over to the liquids recovery					

HAZOP-PC 2.12  
 Company: IGR  
 Facility: Roberts & Schafer  
 Session: 2 03-14-95  
 Node: 85 Secondary Cyclone  
 Parameter: Flow

Worksheet

Primatech Inc.  
 Node: 85  
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Revision: 0 03-17-95 Dwg#: 9417-1006-C

Intention: Provide flow path from primary cyclone to liquids recovery and solids to char fines collection

DEVIATION	CAUSES	CONSEQUENCES	SAFEGUARDS	RECOMMENDATIONS	REMARKS	BY	COMMENTS
No/Less Flow (inlet)	1) Plugging	1.1) See node 84 outlet	c.1.1.1) See node 84 outlet				
(gas outlet)	1) Plugging	1.1) Stop gas flow from gasifier, unit upset  1.2) Send gas to char fines collection	c1.1.1) See node 84 outlet	Review relief study, ESD philosophy, mechanical design limits of equipment and the compressor pressure control		B RS	
(solids outlet)	1) Plugging	1.1) Same as No/less Flow node 83	c1.1.1) Same as No/less Flow node 83				

HAZOP-PC 2.12  
 Company: IGT  
 Facility: Roberts & Schafer  
 Session: 2 03-14-95  
 Node: 86 Glycol Cooling System  
 Parameter: Flow

Worksheet

Primatech Inc.  
 Node: 86  
 Page: 1

Revision: 0 03-17-95 Dwg#: 9417-1006-C  
 Intention: Closed loop cooling of the tar quench cooler

DEVIATION	CAUSES	CONSEQUENCES	SAFEGUARDS	RECOMMENDATIONS	REMARKS	BY	COMMENTS
No/Less Flow	1) Leak or break	1.1) Potential environmental release	c1.1.1) Contaminated drain collection system provides environmental release protection				